

ECE 455 CAPSTONE DESIGN IN ELECTRICAL AND COMPUTER
ENGINEERING
PROJECT REPORT

**LOW-FREQUENCY ELECTROMAGNETIC
EMITTING AUTONOMOUS BOAT FOR
OFFSHORE PLANE WRECKAGE RECOVERY**

May 9, 2025

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1. Introduction

This project was developed to support the University of Wisconsin Missing in Action Recovery and Identification Project (UW MIA RIP), a program focused on locating and recovering U.S. service members who went missing during past wars. Many of these service members were lost when aircraft crashed in shallow coastal waters, especially in regions like Southeast Asia. Recovering their remains is difficult because traditional search methods are expensive and not always effective in those environments. Our team set out to design a low-cost, self-powered system that could help identify locations of underwater wreckage and assist with future recovery efforts.

The goal was to build an autonomous surface vehicle (ASV) that could generate a magnetic signal detectable by underwater equipment. The ASV works in tandem with an underwater autonomous vehicle (AUV), which has a 3-axis magnetometer on board to detect the magnetic field generated by the ASV. This magnetic signal provides a spatial reference point underwater, allowing the AUV to perform fine-grained magnetic mapping and search patterns beneath the ASV. By maintaining communication over a shared mission plan or synchronized search grid, the ASV and AUV work cooperatively to identify magnetic anomalies that may indicate buried aircraft debris or other metallic wreckage.

While our ASV does not directly transmit control commands to the AUV, both platforms are designed to follow coordinated search paths based on GPS and mission parameters pre-planned by operators. This coordinated approach reduces surface search time and improves underwater mapping efficiency.

We were challenged to build an ASV that could be built on a budget of \$500, uses accessible materials, fits in a suitcase, and could operate independently in the field.

To meet these goals, we constructed the boat using affordable components like PVC pipes for flotation, foam for stability, and a combination of wooden and polycarbonate boards for mounting electronics. A solar panel powers the system by charging two batteries, which then provide energy to the onboard electronics. These electronics include a flight controller for navigation, a Raspberry Pi for control, and a signal generator and amplifier to drive a coil that emits the magnetic field.

The boat is designed to follow GPS waypoints on its own, while also allowing manual control if needed. Electronics are enclosed in a waterproof box to keep them safe during outdoor testing. We used prebuilt circuit boards where possible to reduce development time and focus on integrating everything into a working prototype.

This report describes the design process, how the system works, and what we learned throughout the semester. We also discuss the challenges we faced and how future teams can continue building on this foundation to improve the technology and support the mission of recovering those who served.

2. Bill of Materials

Item	Price/unit	Quantity	Total Price
18AWG wire	\$0.00	702 ft	\$0.00
PVC Pipe 1"	\$0.00	1	\$0.00
PVC Pipe 4"	\$0.00	2	\$0.00
PVC cement	\$0.00	1	\$0.00
PVC caps (2 pack)	\$14.99	2	\$29.98
Underwater Motor	\$67.52	1	\$67.52
Servo	\$13.99	1	\$13.99
SpeedyBee	\$65.00	1	\$65.00
Amplifier	\$9.00	1	\$9.00
Transmitter / Reciever	\$50.00	1	\$50.00
100W Solar Panel	\$70.00	1	\$70.00
Battery	\$22.00	2	\$44.00
MPPT Charger	\$42.00	1	\$42.00
Acrylic	\$40.00	0	\$0.00
Electronic Box	\$31.00	1	\$31.00
Filament Roll	\$20.00	1	\$20.00
PolyCarbonate	\$0.00	1	\$0.00
Signal Generator	\$7.99	1	\$7.99
GPS	\$18.00	1	\$18.00
EPS Foam	\$0.00	1	\$0.00
1/4" inch bolt	\$0.00	14	\$0.00
1/4" nut	\$0.00	20	\$0.00
Washer	\$0.10	20	\$2.00
1/2" Fiber glass composite rods	\$0.00	4	\$0.00
HDF wood	\$3.75	1	\$3.75
M3 Screw	\$0.35	2	\$0.70
Long bolt	\$0.00	4	\$0.00
L7805CV	\$0.00	2	\$0.00
Capacitors	\$0.00	12	\$0.00
WM8672-ND	\$1.36	1	\$1.36
732-10955-ND	\$0.36	2	\$0.72
296-43663-1-ND	\$0.90	2	\$1.80
445-174398-1-ND	\$0.32	2	\$0.64
Total Price of ASV			\$479.45

The bill of materials includes what is actually used on the ASV. This doesn't include the cost of a few purchased items that were never used, such as an acrylic base. It also does not include the costs of materials that were given to us for free, such as the PVC pipe. An Excel sheet of the BOM can be found in the repository, including links to all purchased items. The total cost of the ASV is \$479.45, which is under the \$500 budget.

3. Circuit Schematics

The circuits we designed focused on power distribution. Specifically, how were we going to bring the 12V battery supply down to a usable voltage while still supplying enough current for our load? To solve this issue, we designed a voltage regulator using an L7805CV and a DC-DC buck converter using a TPS563200. The voltage regulator provides a stable 5V to devices like the servo and the Raspberry Pi. The buck converter allows us to select a desired output voltage and will supply up to 3A of current to the load.

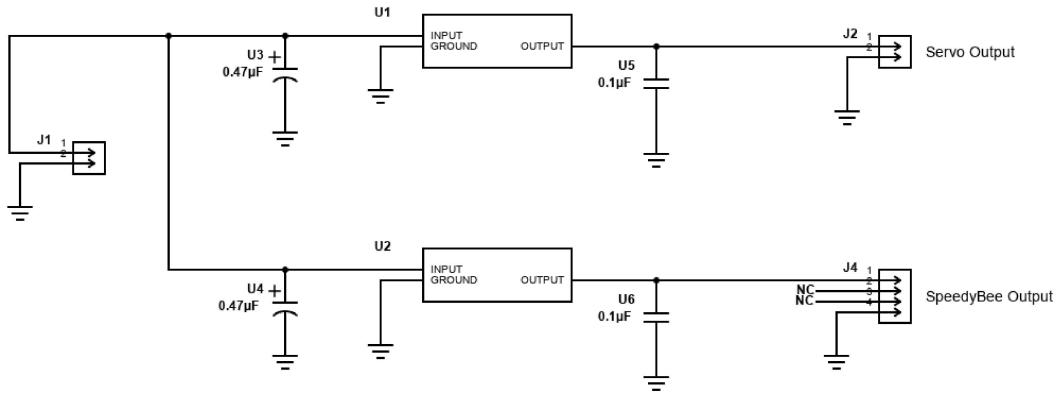


Figure 1: 12V-5V Voltage Regulator

Fig. 1 shows the schematic for the voltage regulator used to power both the servo motor and the Raspberry Pi. This circuit is centered around the L7805CV linear voltage regulator, which steps the 12V battery down to a stable 5V output and is capable of supplying up to 1.5A of current. The input and output capacitors are selected based on the recommendations provided in the datasheet to ensure optimal performance in DC applications.

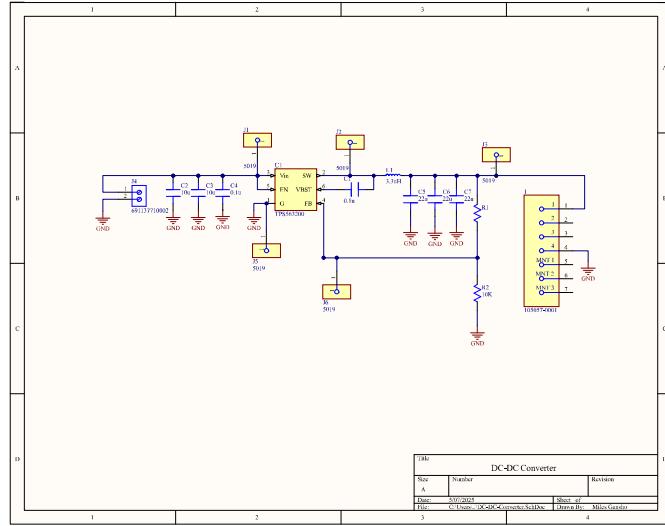


Figure 2: DC-DC converter

Fig. 2 is the second of our two designed circuits. This circuit also allows us to bring 12V down to a voltage we can use. However, the TPS563200 has a feedback on pin 4, which allows us to select a desired output voltage with the voltage divider constructed with R1 and R2. The output capacitors and inductors are selected based on datasheet recommendations for 5-7.5V outputs, and R1 is selected using the equation $V_{out} = 0.765 \times \left(1 + \frac{R_1}{R_2}\right)$. This chip also gives us an output current max of 3A, which is much higher than the voltage regulator, so better for larger loads.

4. Physical Design

4.1. Frame and Flotation

The ASV's frame is built from two 4" PVC pipes, each 30" long, mounted in parallel to provide flotation and structural support. A block of closed-cell EPS foam is secured between the pipes to improve buoyancy and overall water stability, as well as introducing some rigidity to the system. Closed-cell foam was required for underwater use, as open-cell foam would absorb water and lose buoyancy. The foam was cut to fit the frame and held in place with eight (1/4") bolts, along with 8 nuts and washers to distribute the load on the foam.

To calculate the buoyancy required by the ASV, we first calculated the ASV's mass to be approximately 14.4 kg. With a 25% safety factor, our target buoyancy is 18 kg. Buoyancy in kilograms is calculated by Buoyancy = Weight of water displaced \times Volume of submerged object. For our geometry, the two PVC pipes displace 15.64 L and the EPS foam displaces 19.66 L, for a total volume of 35.3 L. With a saltwater density of

1.025 kg/liter, the total buoyancy of the ASV is $1.025 \times 35.3 = 36.2$ kg, well above our 18 kg requirement.

4.2. Platform Structure

A 24" wide platform sits atop the PVC pipes, consisting of two 1/8" MDF wooden struts for rigidity and a polycarbonate sheet for mounting structural components. Polycarbonate was chosen for its strength and durability, but it is very flexible; the MDF and EPS foam serve to stiffen the base while the polycarbonate provides a strong, flat mounting surface.

A waterproof enclosure is mounted at the center of the platform to protect onboard systems. Above it, a 100 W solar panel is held in place by four pairs of custom 3D-printed brackets. The brackets attach to the panel's corners and interface with 10" long, (1/2") fiberglass composite rods seated in mating mounts. These brackets allow for easy removal of the solar panel for ease of transportation. The brackets proved strong enough to hold the panel, but future iterations could add captive set-screws to lock the rods in place rather than relying solely on friction and weight. An assembly view is shown in Figure 3.

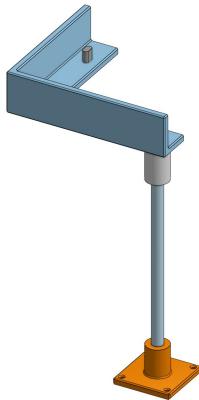


Figure 3: Solar panel assembly view.

4.3. Motor Mounting and Flange Design

The motor is mounted at the stern using a custom 3D-printed flange. The flange fits a 1" PVC shaft that connects the motor to the servo and keeps the shaft vertical during operation. To keep the motor in place, two 3D printed bushing were designed to fit the PVC shaft, which hold the motor at a constant depth. The bushing rotate above the flange, but the coefficient of friction between the two is low enough to allow the motor to rotate freely. This design choice ensures that the motor remains securely in place during operation,

even in rough water conditions. The choice of a friction based bushing and flange system was chosen over a bearing system to reduce cost and complexity, as well as to allow for easy replacement of parts if needed. In Figure 4, an assembly view of the flange can be seen, where the servo sits in a recess to protect it from the elements. The servo's axis is aligned to the PVC pipe so both rotate together.

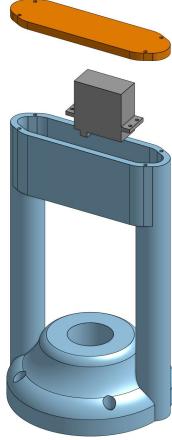


Figure 4: Flange assembly view.

Material choice for 3D printed parts was given careful consideration to ensure the ASV is lightweight, low cost, but also resistant to wear. The 3D printed flange is made from ASA, a material known for its excellent UV resistance and mechanical properties. All other parts were made from PETG, which is a strong and durable material that maintains its structure underwater, making it suitable for the ASV's environment. The use of these materials ensures that the ASV can withstand the rigors of outdoor use while remaining lightweight and cost-effective. Structural parts were printed using 5 perimeters and 25% gyroid infill, which provided a good balance of strength and weight, while also keeping costs relatively low. The entire project used under 750g of PETG, and around 250g of ASA, which can be purchased for around \$15. Further iterations could likely halve this number. Refer to the appendix for all isometric views of 3D printed parts.

5. Electrical

5.1. Power Distribution

The ASV is powered by two 12.8V 8Ah LiFePO₄ batteries connected in parallel. A 100W solar panel mounted above the electronics enclosure outputs power to an MPPT controller, which continuously regulates the voltage and current to maximize the power output from the solar panel. The charge controller adjusts the variable DC that comes in from the solar

panel to a constant voltage and current that is suitable for charging the batteries. The MPPT controller outputs the current through Anderson Powerpole connectors, which are tied into the circuit via a 12p junction terminal block, which distributes power to the rest of the system. The use of Anderson connectors allows for easy connection and disconnection of the solar panel. The batteries are connected with F2 spade connectors, also allowing for easy connection and disconnection.

Power is distributed through two voltage regulators that step the 12.8V battery voltage down to 5V. One converter supplies the SpeedyBee F405 V4 flight controller and GPS, and the other is dedicated to the servo motor. All components are placed inside a waterproof enclosure without mounting hardware. Initially, the voltage regulator was a buck converter on a PCB, but was replaced with a voltage regulator on a protoboard. The buck converter was not able to handle the current draw of the Speedybee, which caused it to overheat and fail.

5.2. Voltage Converter

The PCB design of the buck converter was based primarily on the datasheet recommendations for the TPS563200, targeting an output voltage range of 5–7.5V. See Figure 2 capacitors C5, C6, and C7 should all add up to have around $66 \mu\text{F}$ of output capacitance. the inductor is $3.3 \mu\text{H}$ and is the recommendation for the output voltage 5-7.5V. This DC-DC converter can provide 3A of current and has an input voltage range of 4.5V to 17V. Future design should include a copper pour between the inductor and output capacitors for heat dissipation, and if more current is needed, consider upgrading to a different chip. However, in our oscilloscope testing, we found that the servo never pulled more than around 0.75A when being held.

The Voltage Regulator (See Figure 1) provided us a quick and easy solution to the PCB board failures we were having with the DC-DC converters, the L7805CV regulator allowed us to bring 12v down to 5V but didn't allow us to increase or decrease the output voltage with a feedback pin. However, the servo was able to operate with a 5V power and the SpeedyBee was able to power on with 5V as well. The max output current we could output with this chip was internally limited to 1.5A, and if held at max output current for too long, you could deal with some overheating. To fix this, a heat sink could be added, but since we are using the voltage regulator to power our servo, we have never had an issue with overheating.

All electrical connections are made using soldered wires. Power and signal lines are routed manually inside the enclosure. Signal and high-current paths are physically separated to minimize noise. Fuses are installed on the battery output lines to protect critical components from short circuits.

The electrical system is simple, modular, and designed for ease of repair and future upgrades. Components can be swapped or rewired without requiring full system disassembly.

5.3. Signal Generator and Amplifier Boards

To generate a magnetic field, a 40 Hz sine wave is created by a prebuilt signal generator and passed through a power amplifier. The amplified signal drives a large copper coil wrapped around the ASV's structure, producing a low-frequency magnetic field detectable by submerged sensors. A high magnetic moment is required to ensure the field can penetrate water and be detected by the sensors. Refer to section 6 for a more detailed discussion of the effective range calculations, but the magnetic moment m of a coil is given by:

$$m = N \times I \times A \quad (1)$$

where:

- N is the number of turns in the coil,
- I is the peak current through the coil,
- A is the area of the loop.

Our goal for a magnetic moment was a value of 50 Am^2 , which would give a range of around 27m underwater. To achieve this, we used a coil with 78 turns, an area of 0.46 m^2 , and a peak current of 1.6 A . The coil was made from 18 AWG copper wire, and had a calculated magnetic moment of 59 Am^2 .

An issue we ran into when trying to provide ample power to our coil was the method for producing our sine wave. Initially, we wanted to create a sine wave with a modified PWM pin on the Raspberry Pi. However, the output ended up being incredibly noisy and, even after filtering, wasn't super clean. After that solution didn't work, we tried the audio jack, which didn't work for similar reasons, and finally, we tried a DAC, but the noise level was at the same amplitude we wanted to produce our sine wave at. With little time left, we found the best solution was to purchase a signal generator board and then send the low-frequency sine wave through a power amplifier that could bump up the sine wave to a larger amplitude. This allowed for out-of-the-box options we knew would work and at a cheap cost. However, since this was a last-minute solution, we never fully tested the capabilities of the Signal generator in conjunction with the power amplifier, but this is a brief overview of what we would expect the working solution to look like.

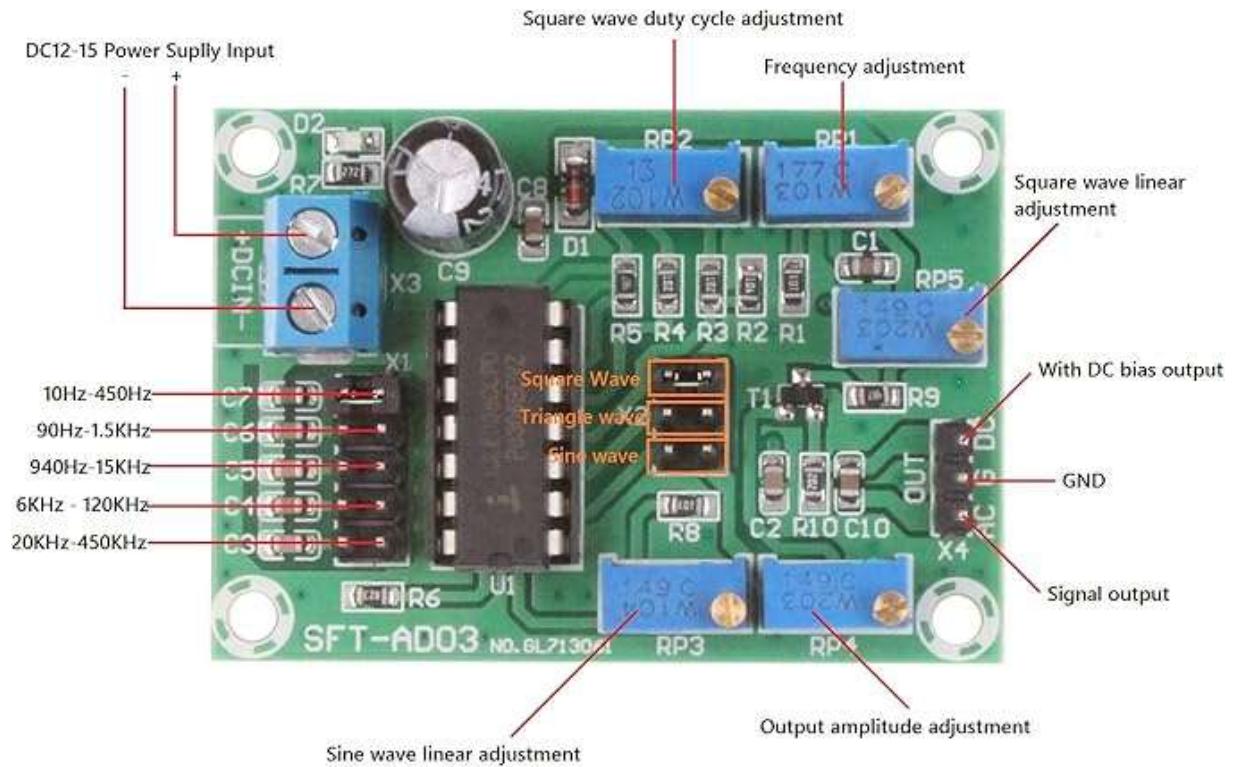


Figure 5: Signal Generator Overview

Fig. 5 gives us a nice overview of what the signal generator PCB can do. The main chip used in this board is the ICL8038, which can take in 10 - 30V and can output a sine wave, a square wave, or a triangle wave. For our purposes, we will strictly be outputting a sine wave. With the potentiometers located at the bottom right of the board and the top right of the board, we can control the frequency and amplitude. We can go as low as 10Hz, which is perfect for the low frequency that we need. Due to the limited time frame when we never fully got to test the working condition of this board; however, these normally work straight out of the box, and we can expect a positive output since we are within the working parameters of the ICL8038.

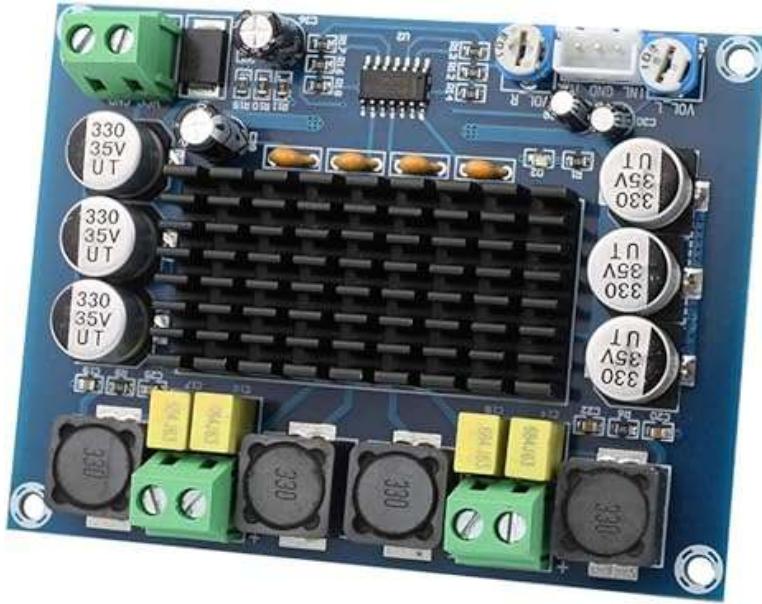


Figure 6: Power Amplifier

Fig. 6 shows the Power Amplifier board we bought and used to amplify a low-frequency sine wave to get our desired current amplitude. Looking at the top of the board, we can see an input channel and a power channel for 12V DC. The main chip in this board is the TPA3116D2, and it gives us 120W of power on each of the output channels. In our testing, we found that a 200 mV sine wave was able to get up to 9V with a (4Ω) load, giving us around 1.5A of current.

5.4. Flight Controller and GPS

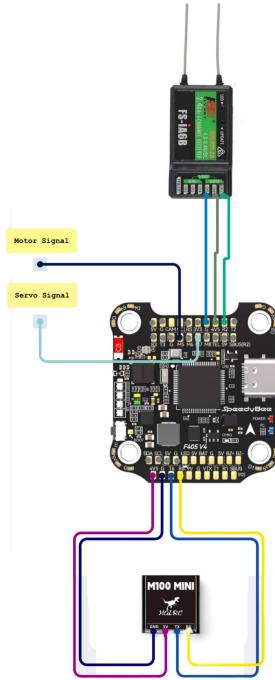


Figure 7: Schematic of the SpeedyBee F405 V4 flight controller and its connections.

The SpeedyBee F405 V4 flight controller runs iNav firmware and handles both GPS waypoint navigation and motor control. It outputs PWM signals to the brushed DC motor and rudder servo and receives location data from a GPS module. The GPS is soldered directly to UART6 on the flight controller: TX from the GPS is connected to RX6, and RX from the GPS is connected to TX6. A FlySky FS-iA6B receiver is soldered directly to the RX2 pad on the flight controller for SBUS communication, enabling manual RC override when needed.

6. Coding

In this section, we will include the programming aspects of our design. All code is available in the GitHub repository at <https://github.com/grgao/boat/tree/main>.

6.1. Electromagnetic Coil Modeling and Range Calculations

A critical component of the ASV's system is the electromagnetic coil, which generates a low-frequency magnetic field for underwater detection and tracking. To optimize the coil design and predict its performance, a Python-based simulation was developed. This code calculates the electrical properties of a rectangular coil and simulates the resulting magnetic moment, which is then used to calculate an effective range.

The script first defines the coil geometry and material parameters, such as the number of turns, loop dimensions, wire size, and frequency. The inductance of the rectangular loop is calculated with a standard formula that accounts for the loop's physical dimensions and number of turns. The resistance is determined from the total wire length and resistivity, while the impedance is computed at the operating frequency. The magnetic moment, which sets the strength of the magnetic field, is also calculated as $m = NIA$.

Once the magnetic moment of the coil is determined, the effective range is estimated using a model provided by Professor Strachen. We must first make some assumptions about the model. We model the coil as a magnetic dipole, and we assume that the underwater AUV has a field strength threshold of 0.2 nT, which is a reasonable value that the AUV teams were aiming for. The effective range is then calculated using the formula:

$$r = \left(\frac{\mu_0 m}{2\pi B_r} e^{-\alpha r} \right)^{1/3} \quad (2)$$

$$\alpha_s = \sqrt{\pi \cdot f \cdot \mu \cdot \sigma_W} \quad (3)$$

where:

- μ_0 is the permeability of free space,
- m is the magnetic moment of the coil,
- B_r is the field strength threshold,
- α is the attenuation coefficient given by the skin effect,
- f is the frequency of the signal,
- μ is the permeability of the medium,
- σ_W is the conductivity of water, 4 S m^{-1} .

The effective range of different magnetic moments can be seen by Figure 8. With our magnetic moment of 59, we have an effective range of around 30 meters. The reason for a skin depth coefficient is due to the skin effect, which is a phenomenon where the current density decreases closer to the wires surface. This results in the magnetic field decaying exponentially with distance.

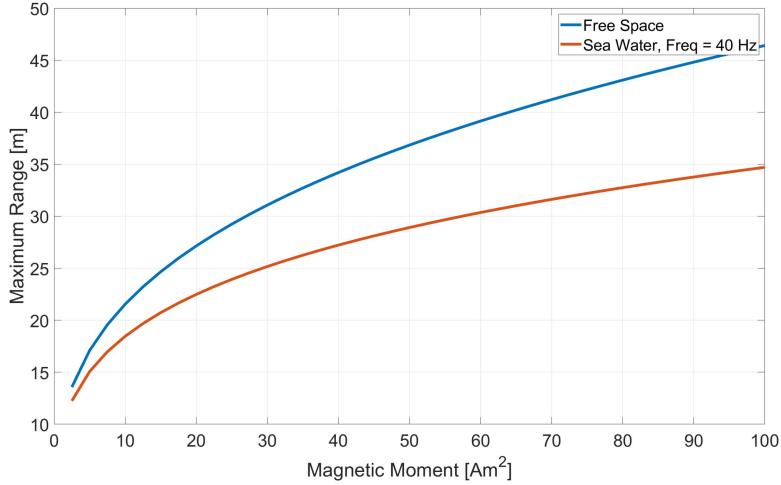


Figure 8: Effective range of the coil in water.

6.2. iNav Configuration

The SpeedyBee F405 V4 flight controller was flashed with iNav 7 firmware to enable GPS-based return-to-home (RTH) functionality and manual control. iNav 7 was selected because of its improved support for surface vehicles, enhanced GPS navigation features, and full compatibility with the SpeedyBee F405 V4 without requiring custom firmware builds.

Mixer Modifications

By default, iNav's boat mixer uses differential thrust with two motors for steering. Since our ASV uses a single brushed DC motor for propulsion and a rudder servo for steering, this default configuration was unsuitable.

To support our hardware, we modified the mixer setup in `mixer.c` to map throttle directly to Motor 0 and yaw to Servo 0. Pitch and roll mixing were disabled, as they are unnecessary for surface operation. This allowed the boat to steer using the rudder while maintaining forward propulsion with the single motor.

Firmware Configuration Changes

Several key settings were configured using the iNav Configurator and CLI to support manual control and GPS-assisted return-to-home:

- **Ports:**
 - UART6 configured for GPS (UBlox protocol)

- UART2 configured for SBUS receiver (FlySky FS-iA6B)
- **Failsafe:** Configured to trigger Return-to-Home (RTH) on signal loss.
- **Flight Modes:** Enabled MANUAL, ANGLE, and RTH. AUTO mode was left disabled.
- **Arming:** Manual arming allowed when GPS lock is acquired.
- **PID Tuning:** Pitch and roll control disabled; yaw PID tuned for surface steering only.

Example CLI commands used:

```
mixer load boat
set gps_provider = UBLX
set gps_auto_config = ON
set gps_auto_baud = ON
set serialrx_provider = SBUS
set failsafe_procedure = RTH
set nav_rth_allow_landing = OFF
save
```

Source Code Adjustments

The full iNav firmware was not rewritten, but minor modifications were made to the mixer definitions in `mixer.c` to support single-motor with rudder control. No other firmware files were changed. iNav's official repository was used as the base.

Reproduction Instructions

To reproduce this firmware setup:

1. Clone the official iNav firmware repository:

```
git clone https://github.com/iNavFlight/inav.git
cd inav
```

2. Modify `src/main/mixer/mixer.c` to implement a single-motor and rudder mixer by:

- **Disable pitch and roll mixing** by setting these inputs to zero in the `mixTable()` function:

```
input[ROLL] = 0;
input[PITCH] = 0;
```

- **Map throttle to Motor 0 only** by replacing the motor loop with:

```
for (int i = 0; i < motorCount; i++) {
    if (i == 0) {
        motor[i] = mixerThrottleCommand;
    } else {
        motor[i] = motorZeroCommand;
    }
}
```

- **Map yaw to Servo 0** by ensuring yaw control is configured in the servo mixer or output settings, instead of applying yaw to the motor mixer.
3. Build the firmware following iNav's official build instructions.
 4. Flash the compiled firmware to the SpeedyBee F405 V4.
 5. Apply the CLI configuration listed above.
 6. Test GPS lock, receiver input, motor output, rudder control, and Return-to-Home functionality before deployment.

7. Operating Instructions

Follow these steps to safely operate the Autonomous Surface Vehicle (ASV):

1. Power On:

- Ensure the batteries are charged. The solar panel provides slow passive charging and should not be relied on for full charge.
- Inside the electronics enclosure, connect the battery wires. Each lead is clearly labeled for polarity—connect positive to positive and negative to negative.
- Verify that LEDs on the flight controller (SpeedyBee F405 V4) illuminate, indicating power to the system.

2. System Initialization:

- Wait a few seconds for the flight controller to initialize.
- Confirm GPS lock. The GPS module's LED (typically solid or blinking depending on model) indicates satellite connection.

3. Manual Control (Optional):

- Turn on the FlySky transmitter. Ensure the receiver on the ASV is powered and paired.

- When connected, you can use the transmitter to manually control throttle and rudder. This is useful for testing or override.
- Manual control is not required for autonomous operation but is available at any time.

4. Autonomous Mission Launch:

- Use iNav Configurator to upload or verify the waypoint mission.
- Use iNav Configurator to verify basic telemetry such as GPS status, battery voltage, and input channel readings.
- Confirm that all connections are secure and components are functioning.
- Arm the vehicle using the transmitter or iNav interface. The motor should begin spinning, and the boat can now be manually operated or left to drift as designed.

5. Magnetic Field Activation:

- The signal generator automatically powers on with the system and begins outputting a 40 Hz sine wave.
- The output is amplified and fed to the coil. If needed, use a clamp meter to verify that current is flowing.

6. Monitoring:

- Observe the ASV visually or via iNav telemetry if connected.
- Monitor GPS LED status and waypoint progress to confirm correct operation.

7. Return to Home and Shutdown:

- Use the transmitter or iNav to switch to “Return to Home” mode. The ASV will autonomously return to its starting location.
- Once the vehicle has returned and stopped moving, disarm it using iNav or the transmitter.
- Disconnect the battery by separating the labeled leads.
- Verify that all indicator LEDs are off and reseal the electronics enclosure to maintain waterproofing.

Before each deployment, double-check polarity labels, confirm dry connections, and verify GPS and flight controller status.

8. Troubleshooting and Testing

During our project, we encountered various challenges that required creative problem-solving to keep things moving. Whether it was soldering mistakes, power-related issues, or flaws in the physical design, no prototype is perfect on the first try. This section outlines the key problems we faced during development, how we addressed them, and what tests we performed on the prototypes. This section will also discuss things we couldn't get working exactly how we wanted and what steps should be taken to fix them.

8.1. PCB and Power

When designing the PCB, we considered several chip options but ultimately settled on the TPS563200. This chip was selected using the WEBENCH Power Designer. This software allows you to pick an input voltage, desired output voltage, and current, and then generate possible chips and schematics. This allowed us to generate some simulation files like the one seen in Fig. 9. This shows a simulated start-up using this chip. R1 is selected so that V_{out} is 5V, and as you can see from the simulation, that is exactly what we got.

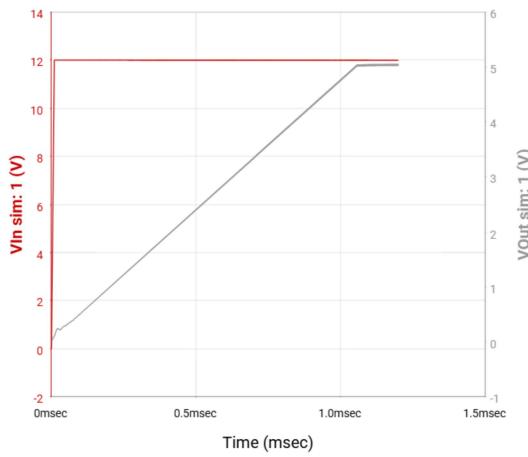


Figure 9: Simulated Start up for the TPS563200

The DC-DC converter PCB was one of the many problems we had to overcome. The main issue was that the PCB successfully worked at larger loads($20\ \Omega$), which drew around 0.25 amps. However, when we decreased the load to $3.5\ \Omega$, drawing around 1.5A, the chip would burn out. After looking at potential issues ranging from lack of inrush current protection, voltage spikes, etc., the actual issue turned out to be the lack of a V_{out} copper pour between the inductor and output capacitors. The copper pour allows for good heat dissipation within the circuit, and since we didn't have any, the chip would overheat at low loads. We tried a couple of quick fixes like soldering more connections between the output

capacitors and the inductor or increasing output capacitance. These solutions would hold the voltage for a little longer, up to around one minute, but ultimately, they would burn up. So we switched to a voltage regulator, which, although it has a lower output current, was still sufficient to operate the servo and power the SpeedyBee. A long-term fix for using a DC-DC converter would be to redesign the PCB with a V_{out} pour to allow for better heat dissipation.

8.2. Motor Operation and Grounding

The main motor used for propulsion was one of the first challenges we had to overcome when dealing with the construction of our ASV. We purchased our motor with an ESC already included, which allowed us to control the motor with just power and a PWM signal wire. However, when trying to power our motor, we had trouble with the initial start. The way to fix this issue was to make sure everything had a common ground. Soldering the Raspberry Pi, SpeedyBee, and battery grounds together ensures no ground is floating, and we can get a clean signal to our motor from the SpeedyBee. In the future, a custom PCB with a shared ground rail would be the most effective way to ensure all grounds are the same, and save the most amount of space instead of soldering all the grounds together.

8.3. Physical Construction and Design

Physical construction came with many unforeseen challenges, especially since the majority of our group specialized in electrical design and coding. One of the main issues we ran into was selecting what kind of material to make the base of our ASV with. The original plan was to make the base of the ASV out of acrylic. This would provide a lightweight base and allow us to laser cut or drill through it so we could attach things like the motor flange and our coil. However, when constructing our ASV, the acrylic sheet snapped under the tension of our coil while we were trying to drill the 1" hole for the motor connection. This made us switch to polycarbonate, which is slightly more flexible but is easier to drill through and cut. We also added MDF wood to give the base of the ASV a little more strength. In the future, teams should try and look to replace the MDF wood with something a little more secure and lightweight. Also, if future groups decide to go back to acrylic, the base case to cut through it is to laser cut all the holes for better precision.

9. Future Work

There is a considerable amount of work that can be done to improve the ASV, as this was a prototype. During our design phase, we were limited by time and budget constraints, but future teams can build on our work to create a more robust and effective systems, especially if they can learn from our mistakes. The following sections will discuss some of

the most important areas for improvement, including physical design, electronics, software, and testing.

9.1. Physical Design

Several improvements to our prototype's mechanical structure should be considered for future ASV iterations:

- **Optimized Part Geometry for Weight & Strength:** Our 3D-printed components were designed under tight time constraints and saw only a few iterations. If budget allows, future teams should perform wear tests on the 3D printed parts to see where they fail, and then redesign to optimize for weight and strength. There were a few prints where it was clear that the part was acceptable, but could use an easy redesign to improve the functionality. For example, the flange was one piece, but if it was split into two pieces, it would be easier to print and assemble.
- **Bracket Offset & Mounting Security:** The solar panel (27.5" wide) extended beyond platform, so we introduced an offset in the brackets to accommodate this. However, the offset distance was not large enough, and we didn't plan for the coil when designing the brackets, so the as a result only one of four bolts could engage, leading to instability. This could be solved by redesigning the bracket geometry or increasing the offset distance to ensure all fasteners seat properly. Additionally, the panel support rods currently rely on friction and panel weight to stay in their mounts. Introduce captive set-screws or spring-loaded clips in each bracket to mechanically lock the rods in place, preventing slippage under harsh conditions
- **Platform Material Stiffness:** Our polycarbonate sheet platform flexed under load. A stiffer base, such as treated wood, aluminum, or even a thicker sheet of polycarbonate would reduce deflection, improve stability, and better support mounted components.
- **Waterproofing at Fastener Joints:** To preserve disassembly ease, we avoided epoxy and ran bolts through PVC fixtures, which allowed water ingress. Future designs should apply marine epoxy or silicone sealant at critical joints, or employ O-ring-sealed fastener assemblies, to balance rigidity, waterproofing, and maintainability. The mounting holes may have to be redesigned to accommodate this, as the current design doesn't allow for easy disassembly after the epoxy is applied. If the ASV is to fit in a suitcase, then the easy assembly and disassembly of the ASV is a critical component of the next design phase.

9.2. Electronics

Several lessons from our prototype's wiring and power distribution should guide future iterations:

- **Modular Motor Connections:** Our motors were hard-wired via fully soldered leads, making removal and replacement cumbersome. Future designs should employ waterproof, keyed connectors inside the electrical box to allow rapid motor swap-outs for maintenance or upgrades without desoldering. We used some Anderson Powerpole connectors for the MPPT connections, but they were a bit cumbersome to use, as well as not waterproof.
- **Overcurrent & Reverse Polarity Safeguards:** We lacked fusing or electronic breakers on our high-current rails. Future designs should include appropriately rated fuses on each major branch (motor, batteries, electronics) to isolate faults and protect wiring and components. Additionally, during our demo, the battery pack was accidentally connected backwards, risking damage to electronics and breaking our ESC. Future designs should incorporate reverse-polarity protection—using a diode or MOSFET-based blocker to automatically guard against destructive reverse connections and prevent user error.
- **Power Distribution Board (PDB):** Our prototype relied on wiring into a terminal junction block, which increased bulk cabling and complicated troubleshooting. Future designs should use a custom PDB with integrated connectors, breakers, and status LEDs, with silk-screened labels marking each output (e.g. “Motor,” “MPPT,” “Servo”). A dedicated PCB, designed from the ground up, could consolidate off-the-shelf power components (amplifiers, signal generators, buck converters) into a single compact board, significantly reducing wiring complexity and system footprint.
- **Outputting Sine Wave from SpeedyBee:** If the SpeedyBee is to be used for a future iteration, it would be beneficial to test if it is possible to output the sine wave directly from the onboard ESC. The ESC outputs a 3 phase voltage to drive a brushless motor, and if the frequency of the sine wave is low enough, it may be possible to use the ESC to drive the coil directly. This would reduce the number of components needed and simplify the design. However, if an entire PCB were to be made, then this step is not as necessary. Additionally, if more motors were to be purchased, buying brushless motors would be cheaper than motors with a built in ESC, as the SpeedyBee fv405 V4 stack comes with an ESC to drive these motors.
- **Adding Second Coil to Improve GPS:** The GPS module was subject to interference from the coil, which made it difficult to get a good GPS signal. With a second coil emitting a magnetic field in the opposite direction, it would be possible to cancel out the interference from the first coil. This would allow for a much better GPS signal. The second coil would need to be placed at a distance from the first coil, and it could be in series with the first coil and just wound in the opposite direction. Placing the coils in series ensures that the coils are in phase with each other, but the output would cancel out the field from the first coil.

9.3. Software

Our iNav configuration was a basic setup, and future teams should consider utilizing the software ArduPilot, which is a more robust but complex system.

- **Space Filling Curve Algorithm:** We used simple waypoint-following, but future teams should consider implementing a space-filling curve algorithm to optimize the ASV's path. This would allow the ASV to cover more area in less time, improving efficiency and data collection. The current system requires users to manually set waypoints, which is time-consuming and inefficient. A space-filling curve algorithm would allow the ASV to autonomously navigate a given area, reducing the need for manual waypoint setting and improving the user's experience.

9.4. Testing

Testing was one of our biggest challenges, as we did not get enough time to test the ASV in the water, because by the time we were ready to test, we realized that it was likely not worth the difficulty of waterproofing the bolt connections, which would also make the handoff of the project significantly more difficult. The following are some suggestions for future teams to consider when testing the ASV:

- **Testing the Coil:** We were unable to test the coil in the water to ensure that it actually reached the depth we calculated. Above the water the coil was able to produce a magnetic field, but our simulations showed that the field would be detectable at a depth of 80 feet underwater. Future teams should consider a methodology for testing the coil, even if it is not in the water.
- **Testing in a Real Environment:** Future teams should consider testing the ASV in a controlled environment, such as a pool, before taking it out into somewhere like Lake Mendota. This would allow for easier troubleshooting and debugging of the system, as well as providing a safer environment for testing. Testing in a large lake would be beneficial to see how the ASV performs in a real environment, but it would be much more difficult to troubleshoot and debug the system.

A. Isometric Views of all 3D-Printed Parts

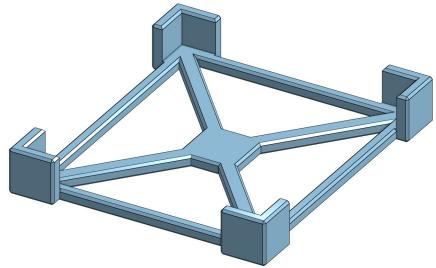


Figure 10: Base to hold batteries in place.

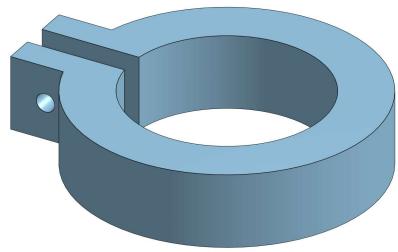


Figure 11: Bushing that clamps to PVC.

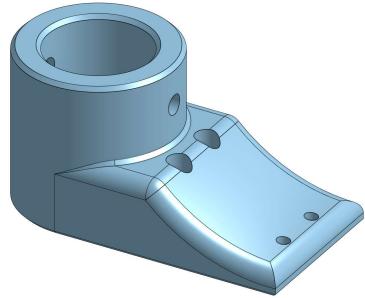


Figure 12: Motor to PVC attachment.

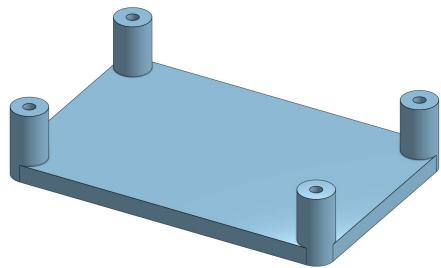


Figure 13: Base for perfboard to mount to with M2 screws.

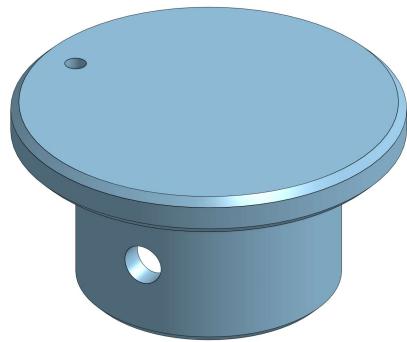


Figure 14: Servo to PVC attachment to align axis of rotation.