		Geometry:		Physics:	
Run title>	> example qh-mode plasma scena	rio R ₀	= 9.299 m	$I_{\mathcal{P}}$	= 18.49 MA
PROCESS Version>	> 1.0.16	a	= 3 m	Vacuum B_T at R_0	= 5.316 T
Date:>	> 16/08/2019	Α	= 3.1	9 95	= 3.5
Time:>	> 15:15	K ₉₅	= 1.65	$oldsymbol{eta}_{N}$, thermal	$= 2.337 \% \text{ m T MA}^{-1}$
User:>	> apearce	δ_{95}	= 0.3333	$oldsymbol{eta}_N$, total	$= 2.816 \% \text{ m T MA}^{-1}$
Optimising:>	> Plasma major radius	Surface area	$= 1535 \text{ m}^2$	$oldsymbol{eta_P}$, thermal	= 1.066
Plasma composition:		Plasma volume	$= 2776 \text{ m}^3$	$oldsymbol{eta_P}$, total	= 1.285
Number densities relative to electron density:		No. of TF coils	= 16	< t _e >	= 12.87 keV
D + T	= 0.8377	inboard blanket+shield	= 1.055 m	< n _e >	$= 7.172e + 19 \text{ m}^{-3}$
Не	= 0.06839	ouboard blanket+shield	= 1.782 m	$< n_{\rm e, line} > /n_G$	= 1.2
Xe	= 0.0004622	Fusion power	= 2167 MW	$T_{e0}/ < T_e >$	= 2.275
W	= 5e-05			$n_{\rm e0}/< n_{\rm e,vol}>$	= 1.275
				$Z_{ m eff}$	= 2.387
Colour Legend: ITR				$n_Z/ < n_{\rm e, vol} >$	= 0.0005122
OP				$ au_e$	= 3.546 s
				H-factor	= 1.1
				Scaling law	= IPB98(y,2)
Cail augmenta ata		Power flows:		Neutral Beam Current Drive:	
Coil currents etc: PF 1	= 16.27 MA	Nominal neutron wall load	= 1.038 MW m ⁻²		= 76 MW
PF 3	= 16.27 MA = -8.484 MA			Steady state auxiliary power	= 76 MW = 76 MW
PF 5	= -0.464 MA = -5.588 MA	Normalised radius of 'core' req Electron density at pedestal	$= 5.887e + 19 \text{ m}^{-3}$	Power for heating only Bootstrap fraction	= 76 MeV = 0.3846
Startup flux swing	= -5.566 MA = 375 Wb	r/a at density pedestal	= 0.94	Auxiliary fraction	= 0.3646 = 5.521e-05
Available flux swing	= -649.2 Wb	Helium fraction	= 0.94	Inductive fraction	= 5.521e-05 = 0.6153
Burn time	= -049.2 Wb	Core radiation	= 0.00839 = 122.5 MW	NB gamma	= 0.0133 = 0.285 10 ²⁰ A W ⁻¹ m ⁻²
burn time	– 2 IIIS	Total radiation	= 315.1 MW	NB energy	= 1000 keV
TF coil type is WST Nb3Sn		Nuclear heating in blanket	= 1674 MW	Plasma heating used for H fact	
Poak field at conduct	or (w. rip.) = 12.01 T	Nuclear heating in shield	= 1.634 MW	P _{div}	$= 18.78 \text{ MW m}^{-1}$
I/I _{crit}	or $(w. 11p.) = 12.01 1$ = 0.6444	Power to divertor	= 1.034 MW = 174.6 MW	P _{div} R ₀ P _{div}	$= 26.18 \times 10^{-20} \text{ MW m}^2$
TF Temperature marg		H-mode threshold	= 174.8 MW = 116.4 MW		= 20.18 × 10 -4 MW 111- = 1.501
CS Temperature marg	=	Divertor life	= 116.4 MW = 4.26 years	P _{div} P _{LH} H* (non-rad. corr.)	= 1.501 = 0.9893
•	_		= 4.26 years = 2879 MW	п· (поп-тац. соп. <i>)</i>	- U.YOYO
Conduit Von Mises st	ress = $4.467e + 08 Pa$	Primary (high grade) heat	= 28/9 MVV	Costs	

Gross cycle efficiency

Net cycle efficiency

Gross electric power

Fusion-to-electric efficiency $\frac{P_{e, net}}{P_{fus}} = 23.07 \%$

Net electric power

Case Von Mises stress

Allowable stress

Mass per TF coil

= 5.8e + 08 Pa

= 5.8e+08 Pa

= 1.528e + 06 kg

Costs

Cost of electricity

=ERROR! Var missing

= 37.5 %

= 31.41 %

= 1080 MW

= 500 MW

