

PINN Phasor Fault Localization: Mathematical Derivation and Calibration

1 Scope

This document derives the method implemented in:

- `projects/pinn_phasor_localization/model.py`,
- `projects/pinn_phasor_localization/phasor.py`,
- `projects/pinn_phasor_localization/trainer.py`,
- `projects/pinn_phasor_localization/run.py`.

The pipeline has two layers:

1. **Physics inversion** from COMTRADE waveforms to $\hat{x}_f \in (0, 1)$ and Z_f .
2. **Optional supervised calibration** mapping \hat{x}_f to distance labels.

2 Phasor telegrapher model with a localized shunt fault

Let $x \in [0, 1]$ be normalized line position ($x = 0$ left terminal, $x = 1$ right terminal). At fixed system frequency $\omega = 2\pi f$, define complex phasors

$$V(x) = V_r(x) + jV_i(x), \quad I(x) = I_r(x) + jI_i(x). \quad (1)$$

The model is

$$\frac{dV}{dx} = -z_n I, \quad (2)$$

$$\frac{dI}{dx} = -y_n V - I_f G_\sigma(x - x_f), \quad (3)$$

with

$$z_n = R_n + jX_n, \quad y_n = G_n + jB_n, \quad (4)$$

$$I_f = \frac{V(x_f)}{Z_f}, \quad Z_f = Z_{f,r} + jZ_{f,x}. \quad (5)$$

G_σ is a Gaussian approximation of $\delta(x - x_f)$:

$$G_\sigma(\xi) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left(-\frac{\xi^2}{2\sigma^2}\right). \quad (6)$$

In code, $\sigma = 0.04$ in normalized line units.

2.1 Real-imaginary residual form

Using

$$z_n I = (R_n I_r - X_n I_i) + j(R_n I_i + X_n I_r), \quad (7)$$

$$y_n V = (G_n V_r - B_n V_i) + j(G_n V_i + B_n V_r), \quad (8)$$

equation (2) gives

$$\frac{dV_r}{dx} + R_n I_r - X_n I_i = 0, \quad (9)$$

$$\frac{dV_i}{dx} + R_n I_i + X_n I_r = 0. \quad (10)$$

Let $I_f = I_{f,r} + jI_{f,i}$. Equation (3) gives

$$\frac{dI_r}{dx} + G_n V_r - B_n V_i + I_{f,r} G_\sigma(x - x_f) = 0, \quad (11)$$

$$\frac{dI_i}{dx} + G_n V_i + B_n V_r + I_{f,i} G_\sigma(x - x_f) = 0. \quad (12)$$

These are exactly the four PDE residual channels minimized by the PINN.

3 Parameterization and constraints

The trainable raw parameters are transformed as:

$$x_f = \sigma(\text{raw_xf}) \in (0, 1), \quad (13)$$

$$Z_{f,r} = \text{softplus}(\text{raw_Zf_r}) + \varepsilon > 0, \quad (14)$$

$$Z_{f,x} = \text{raw_Zf_x} \in \mathbb{R}, \quad (15)$$

$$R_n = \text{softplus}(\text{raw_R}) > 0, \quad X_n = \text{softplus}(\text{raw_X}) > 0, \quad (16)$$

$$G_n = \text{softplus}(\text{raw_G}) > 0, \quad B_n = \text{softplus}(\text{raw_B}) > 0. \quad (17)$$

By default, line parameters are frozen to physical priors:

$$R_n^0 = 0.0233178327, \quad X_n^0 = 0.4224245054, \quad G_n^0 = 3.0 \times 10^{-4}, \quad B_n^0 = 0.4224245054. \quad (18)$$

4 COMTRADE preprocessing and boundary phasors

4.1 Analog reconstruction

For each channel y :

$$y[n] = a_y y_{\text{raw}}[n] + b_y. \quad (19)$$

4.2 Fault inception and arrival picks

Combined current magnitude:

$$I_{\text{mag}}(t) = \sqrt{\sum_{p \in \{L,R\}} \sum_{\phi \in \{1,2,3\}} I_{p,\phi}(t)^2}. \quad (20)$$

Fault inception t_0 is detected from a smoothed derivative threshold:

$$\left| \frac{d}{dt} \text{MA}(I_{\text{mag}}) \right| > \mu + 8\sigma. \quad (21)$$

Arrival times per terminal use a local derivative threshold:

$$t_L : \left| \frac{dI_L^{\text{abs}}}{dt} \right| > \mu_L + 6\sigma_L, \quad t_R : \left| \frac{dI_R^{\text{abs}}}{dt} \right| > \mu_R + 6\sigma_R, \quad (22)$$

with sub-sample interpolation at first crossing.

4.3 Arrival-time geometry prior

Using one-way travel identity

$$t_L = t_0 + x_f \tau, \quad t_R = t_0 + (1 - x_f) \tau, \quad (23)$$

we obtain

$$\tau_{\text{arr}} = t_L + t_R - 2t_0, \quad (24)$$

$$x_{\text{arr}} = \frac{1}{2} + \frac{t_L - t_R}{2\tau_{\text{arr}}}. \quad (25)$$

If $\tau_{\text{arr}} \leq 0$, the prior is treated as invalid.

4.4 Multi-window phasor extraction

For window $k = 0, \dots, K - 1$:

$$t_k^{(s)} = t_0 + (\text{skip_cycles} + k \text{ stride_cycles}) T_0, \quad (26)$$

$$t_k^{(e)} = t_k^{(s)} + \text{post_cycles} T_0, \quad T_0 = \frac{1}{f}. \quad (27)$$

For any signal $s(t)$ in the window:

$$\hat{s} = 2 \overline{s(t) e^{-j\omega t}} = 2 (\overline{s \cos \omega t} - j \overline{s \sin \omega t}). \quad (28)$$

Apply this to phase voltages/currents at both terminals.

4.5 Sequence decomposition and fault-type weighting

For phase phasors (P_a, P_b, P_c) , with $a = e^{j2\pi/3}$:

$$P_0 = \frac{P_a + P_b + P_c}{3}, \quad (29)$$

$$P_1 = \frac{P_a + a P_b + a^2 P_c}{3}, \quad (30)$$

$$P_2 = \frac{P_a + a^2 P_b + a P_c}{3}. \quad (31)$$

Weighted equivalent (fault-type dependent (w_0, w_1, w_2)):

$$P_{\text{eq}} = w_0 P_0 + w_1 P_1 + w_2 P_2. \quad (32)$$

Right-terminal current sign convention is unified as line-forward:

$$I_R^{\text{eq}} \leftarrow -I_R^{\text{eq}}. \quad (33)$$

4.6 Normalization

Across windows:

$$v_{\text{scale}} = \max \left(\max_k |V_{L,k}|, \max_k |V_{R,k}|, 1 \right), \quad (34)$$

$$i_{\text{scale}} = \max \left(\max_k |I_{L,k}|, \max_k |I_{R,k}|, 1 \right). \quad (35)$$

Boundary phasors used by training are normalized:

$$\tilde{V}_{(\cdot),k} = \frac{V_{(\cdot),k}}{v_{\text{scale}}}, \quad \tilde{I}_{(\cdot),k} = \frac{I_{(\cdot),k}}{i_{\text{scale}}}. \quad (36)$$

5 PINN objective

Let K be number of valid windows and N_c collocation points.

5.1 Boundary loss (multi-window)

$$\begin{aligned} \mathcal{L}_{\text{bc}} = \frac{1}{K} \sum_{k=1}^K & \left(|V_r(0) - \tilde{V}_{L,r}^{(k)}|^2 + |V_i(0) - \tilde{V}_{L,i}^{(k)}|^2 + |I_r(0) - \tilde{I}_{L,r}^{(k)}|^2 + |I_i(0) - \tilde{I}_{L,i}^{(k)}|^2 \right. \\ & \left. + |V_r(1) - \tilde{V}_{R,r}^{(k)}|^2 + |V_i(1) - \tilde{V}_{R,i}^{(k)}|^2 + |I_r(1) - \tilde{I}_{R,r}^{(k)}|^2 + |I_i(1) - \tilde{I}_{R,i}^{(k)}|^2 \right). \end{aligned} \quad (37)$$

5.2 PDE loss

With residuals (9)–(12) at random $x_m \sim U(0, 1)$:

$$\mathcal{L}_{\text{pde}} = \frac{1}{N_c} \sum_{m=1}^{N_c} \left(r_1(x_m)^2 + r_2(x_m)^2 + r_3(x_m)^2 + r_4(x_m)^2 \right). \quad (38)$$

5.3 Arrival anchor loss

If x_{arr} from (25) is valid:

$$\mathcal{L}_{x_{\text{arr}}} = (x_f - x_{\text{arr}})^2. \quad (39)$$

Otherwise $\mathcal{L}_{x_{\text{arr}}} = 0$.

5.4 Line-prior regularization

When line parameters are trainable:

$$\mathcal{L}_{\text{line}} = (R_n - R_n^0)^2 + (X_n - X_n^0)^2 + (G_n - G_n^0)^2 + (B_n - B_n^0)^2. \quad (40)$$

If line parameters are frozen, $\mathcal{L}_{\text{line}} = 0$.

5.5 Total loss

$$\mathcal{L} = w_{\text{bc}} \mathcal{L}_{\text{bc}} + w_{\text{pde}} \mathcal{L}_{\text{pde}} + w_{x_{\text{arr}}} \mathcal{L}_{x_{\text{arr}}} + w_{\text{line}} \mathcal{L}_{\text{line}}. \quad (41)$$

6 Optimization schedule

Warmup (Adam, low lr). Optimize boundary + arrival (+ line reg if enabled), effectively without PDE.

Main Adam stage. Optimize full weighted objective.

LBFGS stage. Deterministic refinement with fixed collocation samples.

7 Recovered physical quantities

Predicted distance for known line length L_{km} :

$$\hat{d}_{\text{km}} = x_f L_{\text{km}}. \quad (42)$$

Fault impedance in ohms is obtained by undoing normalization:

$$Z_0 = \frac{v_{\text{scale}}}{i_{\text{scale}}}, \quad \hat{Z}_{f,\Omega} = (Z_{f,r} + jZ_{f,x}) Z_0. \quad (43)$$

8 Affine calibration layer

8.1 Need for calibration

If inversion output x_f is monotone but biased versus labels, use a global affine calibrator.

8.2 Model

Let labeled samples be (x_j, y_j) with

$$x_j = \hat{x}_{f,j}, \quad y_j = \frac{FD_j}{L_{\text{km}}}. \quad (44)$$

Fit

$$\hat{y}_j = ax_j + b, \quad (a, b) = \arg \min_{a,b} \sum_{j=1}^N (ax_j + b - y_j)^2. \quad (45)$$

Matrix form:

$$\boldsymbol{\theta} = \begin{bmatrix} a \\ b \end{bmatrix} = (X^\top X)^{-1} X^\top \mathbf{y}, \quad X = \begin{bmatrix} x_1 & 1 \\ \vdots & \vdots \\ x_N & 1 \end{bmatrix}. \quad (46)$$

Calibrated prediction:

$$x_j^{\text{cal}} = \text{clip}(ax_j + b, 0, 1), \quad \hat{d}_{j,\text{km}}^{\text{cal}} = x_j^{\text{cal}} L_{\text{km}}. \quad (47)$$

8.3 Leave-one-out (LOO) estimate

For each j , fit $(a^{(-j)}, b^{(-j)})$ on all samples except j :

$$x_{j,\text{loo}}^{\text{cal}} = \text{clip}(a^{(-j)}x_j + b^{(-j)}, 0, 1), \quad \hat{d}_{j,\text{km}}^{\text{cal,loo}} = x_{j,\text{loo}}^{\text{cal}} L_{\text{km}}. \quad (48)$$

LOO gives a less optimistic estimate than fitting and testing on the same set.

9 Metrics

For residuals $e_j = \hat{d}_j - d_j$:

$$\text{MAE} = \frac{1}{N} \sum_j |e_j|, \quad (49)$$

$$\text{RMSE} = \sqrt{\frac{1}{N} \sum_j e_j^2}, \quad (50)$$

$$\text{Bias} = \frac{1}{N} \sum_j e_j, \quad (51)$$

$$\text{MaxAbs} = \max_j |e_j|. \quad (52)$$

The same definitions are used for raw, calibrated, and LOO-calibrated predictions.

10 Interpretation

The pipeline is intentionally hybrid:

1. physics-constrained inversion gives structured latent estimates (x_f, Z_f) ,
2. calibration corrects systematic mapping bias from latent coordinate to distance.

Hence, calibration improves absolute distance accuracy but does not replace the physics layer.