

## Solutions of Transmission-Line Equations

### Frequency-Domain Solution: (Steady-state solution)

Lossless-Line Case: For a lossless line, the equations in fr. domain are,

$$\frac{d^2 V}{dz^2} = -\omega^2 LC V \quad \text{and} \quad \frac{d^2 I}{dz^2} = -\omega^2 LC I$$

The general solution for the first eq. is:

$$V(z) = V_+ e^{-j\beta z} + V_- e^{+j\beta z}$$

The first term satisfies the second order diff. eq., and the second term also satisfies. So the sum of two terms also satisfies the equation.

$V_+$ : complex voltage phasor in the  $+z$  direction

$V_-$ : " " " "  $-z$  "

$e^{-j\beta z}$ : travelling wave " "  $+z$  "

$e^{+j\beta z}$ : " " " "  $-z$  "

$\beta = \omega \sqrt{LC}$  (rad/m) is the phase constant

$\beta z$ : electrical length (rad)

According to Eq.  $\frac{dV}{dz} = -j\omega L I$  (the first eq. on the top of this page) the current  $I$  is determined by,

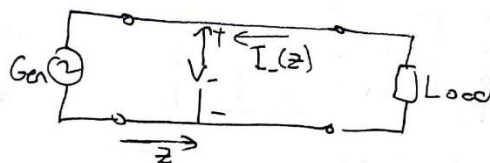
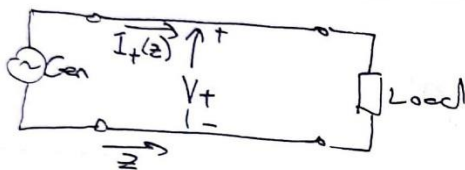
$$I = -\frac{1}{j\omega L} \frac{dV}{dz}$$

using the  $V(z)$  solution in this eq. we obtain,

$$I = Y_0 V_+ e^{-j\beta z} - Y_0 V_- e^{+j\beta z} = I_+ e^{-j\beta z} - I_- e^{+j\beta z}$$

in which we define the characteristic impedance of the line for lossless case as  $Z_0 = \frac{1}{Y_0} \equiv \sqrt{\frac{L}{C}}$

The factors  $I_+$  and  $I_-$  represent complex currents travelling in the  $+z$  and  $-z$  direction respectively.



Line voltages and currents

Lossy-Line Case: ( $R \neq 0, G \neq 0$ ), for the lossy case, we have

$$\frac{d^2 V}{dz^2} = \gamma^2 V \quad \text{and} \quad \frac{d^2 I}{dz^2} = \gamma^2 I$$

$$\gamma = \alpha + j\beta = \sqrt{ZY} = \sqrt{(R+j\omega L)(G+j\omega C)} \quad \text{is the propagation constant}$$

$\alpha$ : attenuation constant (Np/m)  
 $\beta$ : phase " (rad/m)

We can rearrange the  $\gamma$  relation as,

$$\gamma = \sqrt{(j\omega)^2 LC} \sqrt{\left(1 + \frac{R}{j\omega L}\right) \left(1 + \frac{G}{j\omega C}\right)}$$

and at high frequencies (or <sup>with</sup> low losses), when  $R \ll \omega L$  and  $G \ll \omega C$  and by using the binomial expansion of  $(1+b)^{\pm 1/2} = 1 \pm b/2$  for  $b \ll 1$ , we can express the  $\gamma$  as,

$$\begin{aligned} \gamma &\approx j\omega\sqrt{LC} \left[ \left(1 + \frac{1}{2} \frac{R}{j\omega L}\right) \left(1 + \frac{1}{2} \frac{G}{j\omega C}\right) \right] \approx j\omega\sqrt{LC} \left[ 1 + \frac{1}{2} \left( \frac{R}{j\omega L} + \frac{G}{j\omega C} \right) \right] \\ &= \frac{1}{2} \left( R\sqrt{\frac{C}{L}} + G\sqrt{\frac{L}{C}} \right) + j\omega\sqrt{LC} = \alpha + j\beta \end{aligned}$$

Thus, we obtain for  $\alpha$  and  $\beta$  as,

$$\alpha = \frac{1}{2} \left( R\sqrt{\frac{C}{L}} + G\sqrt{\frac{L}{C}} \right) \quad \text{and} \quad \beta = \omega\sqrt{LC}$$

The general solution for the second order <sup>diff.</sup> voltage eq. in lossy case is,

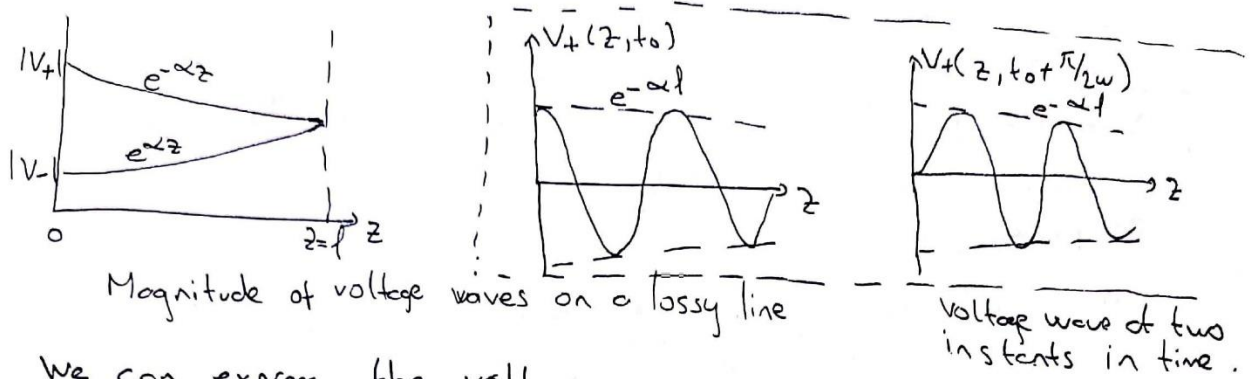
$$V = V_+ e^{-\gamma z} + V_- e^{\gamma z}$$

and using the relation  $I = -\frac{1}{Z} \frac{dV}{dz}$ , we can obtain,

$$I = Y_0 (V_+ e^{-\gamma z} - V_- e^{\gamma z})$$

where the characteristic impedance is,

$$Z_0 = \frac{1}{Y_0} = \sqrt{\frac{Z}{Y}} = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = R_0 \pm jX_0$$



We can express the voltage wave as,

$$\begin{aligned} v_+(z, t) &= \text{Re} [V_+(z) e^{j\omega t}] = \text{Re} [V_+ e^{-\gamma z} e^{j\omega t}] = \text{Re} [V_+ e^{-\alpha z} e^{j\omega t} e^{-j\beta z}] \\ &= |V_+| e^{-\alpha z} \cos(\omega t - \beta z + \theta_+) \end{aligned}$$

where  $V_+ = |V_+| e^{j\theta_+}$

When the voltage wave moves from  $z_1$  to  $z_2$  position ( $l = z_2 - z_1$ ), the ratios of the magnitudes of voltage  $V_+$  and current  $I_+$  of the two points are,

$$\left| \frac{V_2}{V_1} \right| = \left| \frac{I_2}{I_1} \right| = e^{-\alpha l}$$

Taking the  $\ln$  of both sides, we obtain the attenuation in Nepers

$$\ln \left| \frac{V_2}{V_1} \right| = \ln e^{-\alpha l} = -\alpha l \quad (\text{Np})$$

The dB is defined as the logarithm <sup>(to the base 10)</sup> of a power ratio. ( $1 \text{ Np} = 8.686 \text{ dB}$ )

$$(\text{dB}) : 10 \log \frac{P_2}{P_1}$$

Since  $P_1 = V_1^2/R_1$  and  $P_2 = V_2^2/R_2$  and if  $R_1 = R_2$ ,  $\text{dB} = 20 \log \left| \frac{V_2}{V_1} \right|$

Since the voltage  $V_2$  is smaller than  $V_1$ , the ratio in dB is negative.

That means the traveling wave is attenuated by that number of dBs. The curve above represents a moving wave with an amplitude attenuated by a factor of  $e^{-\alpha l}$ .

## Time-Domain Solution:

### Lossless-Line Case:

solution are,

$$\frac{\partial^2 u}{\partial z^2} = LC \frac{\partial^2 u}{\partial t^2} \quad \text{and} \quad \frac{\partial^2 i}{\partial z^2} = LC \frac{\partial^2 i}{\partial t^2}$$

Let, the following voltage function be a solution to the wave equations:

$$u_+ = f_+(t - \sqrt{LC} z), \quad v_p = 1/\sqrt{LC} \text{ is the phase velocity}$$

defining the argument of the function as  $A = (t - \sqrt{LC} z)$ , then

$$u_+ = f_+(A)$$

and we can write the partial differentiation as,

$$\frac{\partial u_+}{\partial z} = \frac{df_+}{dA} \frac{\partial A}{\partial z} = -\sqrt{LC} \frac{df_+}{dA}$$

Differentiating this eq. with respect to  $z$  once again,

$$\frac{\partial^2 u_+}{\partial z^2} = LC \frac{d^2 f_+}{dA^2}$$

$$\text{Similarly, } \frac{\partial u_+}{\partial t} = \frac{df_+}{dA} \left( \frac{\partial A}{\partial t} \right) = \frac{df_+}{dA} \quad \text{and} \quad \frac{\partial^2 u_+}{\partial t^2} = \frac{d^2 f_+}{dA^2}$$

and comparing the results, we can obtain:  $\frac{\partial^2 u_+}{\partial z^2} = LC \frac{\partial^2 u_+}{\partial t^2}$

Therefore  $u_+$  is one solution of voltage wave equation.

Similarly  $u_- = f_-(t + \sqrt{LC} z)$  is also one solution of this equation.

Since the wave equation is linear, the sum of the solutions is also a solution:

$$u = f_+(t - \sqrt{LC} z) + f_-(t + \sqrt{LC} z)$$

Similarly for the current wave eq.

$$i = g_+(t - \sqrt{LC} z) + g_-(t + \sqrt{LC} z) \text{ is surely a solution.}$$

For example, we can replace the solution with the cosine function:  $u_+ = V_+ \cos \omega(t - \sqrt{LC} z)$

if we use this solution in wave equation, we <sup>(prove that)</sup> see that the wave equation is satisfied. So,  $u_+$  is a solution to the wave eq.



Lossy-Line Case: The wave eq.s for the time-domain on lossy line are,  

$$\frac{\partial^2 u}{\partial z^2} = RG u + (RC + LG) \frac{\partial u}{\partial t} + LC \frac{\partial^2 u}{\partial t^2} \quad \text{and similar eq. for current.}$$

Let's assume the following solution,

$$u_+ = V_+ e^{-\alpha z} \cos(\omega t - \beta z) = \frac{V_+}{2} [e^{-(\alpha + j\beta)z} e^{j\omega t} + e^{-(\alpha - j\beta)z} e^{-j\omega t}]$$

Then,

$$\frac{\partial^2 u_+}{\partial z^2} = \frac{V_+}{2} [(\alpha + j\beta)^2 e^{-(\alpha + j\beta)z} e^{j\omega t} + (\alpha - j\beta)^2 e^{-(\alpha - j\beta)z} e^{-j\omega t}]$$

$$\text{and } \frac{\partial u_+}{\partial t} = \frac{V_+}{2} [j\omega e^{-(\alpha + j\beta)z} e^{j\omega t} - j\omega e^{-(\alpha - j\beta)z} e^{-j\omega t}]$$

$$\frac{\partial^2 u_+}{\partial t^2} = \frac{V_+}{2} [-\omega^2 e^{-(\alpha + j\beta)z} e^{j\omega t} - \omega^2 e^{-(\alpha - j\beta)z} e^{-j\omega t}]$$

Substituting the results into wave eq., dividing both sides by  $(V_+/2)$ , and rearranging terms, we get

$$[(\alpha + j\beta)^2 - RG - (RC + LG)j\omega - LC(j\omega)^2] + [(\alpha - j\beta)^2 - RG - (RC + LG)j\omega - LC(j\omega)^2]^* e^{-j2\omega t - 2\beta z} = 0$$

← complex conjugate

This eq. can be satisfied for independently chosen values of  $t$  and  $z$  if, and only if, the following two factors are zeros:

$$(\alpha + j\beta)^2 - RG - (RC + LG)j\omega - LC(j\omega)^2 = 0 \quad \text{and the second factor (taking the complex conjugate), } (\alpha - j\beta)^2 - RG - (RC + LG)j\omega - LC(j\omega)^2 = 0$$

Let  $\gamma = \alpha + j\beta$  defines the propagation constant and using ' $\gamma$ ' in the first eq. just above,

$$\gamma = \sqrt{RG + (RC + LG)j\omega + LC(j\omega)^2} = \sqrt{(R + j\omega L)(G + j\omega C)} = \sqrt{ZY}$$

as defined in the previous frequency domain result. Therefore our  $u_+$  solution is surely one solution of the traveling wave equation.

$u_- = V_- e^{\alpha z} \cos(\omega t + \beta z)$  is also a solution. The sum of the two solution  $u = V_+ e^{-\alpha z} \cos(\omega t - \beta z) + V_- e^{\alpha z} \cos(\omega t + \beta z)$  is also a solution.

Similarly

$i = I_+ e^{-\alpha z} \cos(\omega t - \beta z) + I_- e^{\alpha z} \cos(\omega t + \beta z)$  is the solution of the wave equation for current.

## Characteristic Impedance and Line Impedance

### Characteristic Impedance:

We define the characteristic impedance of a transmission line as,

$$Z_0 = \sqrt{\frac{Z}{Y}} = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = R_0 \pm jX_0$$

This impedance is,

- independent of the length of the line
- " " " " termination of " "
- not the impedance that a line itself possesses
- determined only by the parameters of the line per unit length.

At high frequencies or with low losses, since  $R \ll \omega L$  and  $G \ll \omega C$  from the binomial expansion, we can approximate,

$$\begin{aligned} Z_0 &= \sqrt{\frac{L}{C}} \left(1 + \frac{R}{j\omega L}\right)^{1/2} \left(1 + \frac{G}{j\omega C}\right)^{-1/2} \approx \sqrt{\frac{L}{C}} \left(1 + \frac{1}{2} \frac{R}{j\omega L}\right) \left(1 - \frac{1}{2} \frac{G}{j\omega C}\right) \\ &\approx \sqrt{\frac{L}{C}} \left[1 + \frac{1}{2} \left(\frac{R}{j\omega L} - \frac{G}{j\omega C}\right)\right] \end{aligned}$$

but  $Z_0 = \sqrt{\frac{L}{C}}$  for very high frequency.

We define the characteristic admittance as  $Y_0 = \frac{1}{Z_0} = G_0 \pm jB_0$

### Example:

A coaxial line has the following parameters:

$R = 5 \Omega/\text{mi}$ ,  $L = 37 \cdot 10^{-4} \text{ H/mi}$ ,  $G = 6,2 \cdot 10^{-3} \text{ S/mi}$ ,  $C = 0,0081 \cdot 10^{-6} \text{ F/mi}$

The line operates at a frequency of 100 kHz. Determine its  $Z_0$  and  $\gamma$ .

$$\begin{aligned} Z_0 &= \sqrt{\frac{Z}{Y}} = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = \sqrt{\frac{5+j2323}{(0,62+j0,51) \cdot 10^{-2}}} = \sqrt{\frac{2324 \angle 90^\circ}{0,0080 \angle 39,4^\circ}} = 539 \angle 25,3^\circ \\ &= 487 + j230 \Omega \end{aligned}$$

$$\begin{aligned} \gamma &= \sqrt{ZY} = \sqrt{(R+j\omega L)(G+j\omega C)} = \sqrt{(2324 \angle 90^\circ)(0,0080 \angle 39,4^\circ)} = 4,31 \angle 64,7^\circ \\ &= 1,85 + j3,90 \end{aligned}$$

Since  $\gamma = \alpha + j\beta$ ,

$$\alpha = 1,85 \text{ Np/mi}$$

and  $\beta = 3,90 \text{ rad/mi}$