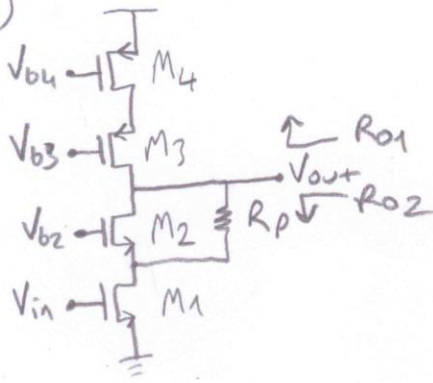
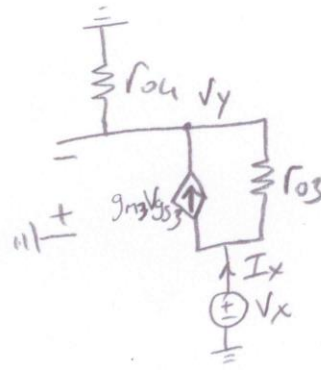


①

a)



=>



$$R_{O2} = g_{m2} \cdot r_{o1} \cdot r_{o2} \parallel R_p + r_{o2} \parallel R_p + r_{o1}$$

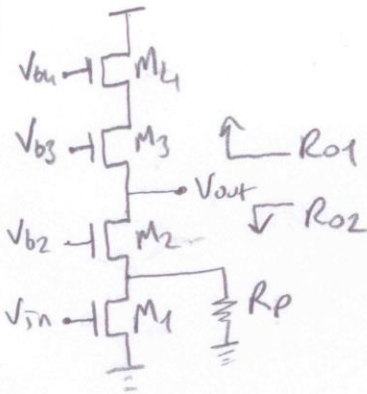
$$A_v = -g_{m1} \cdot R_{O1} \parallel R_{O2}$$

$$V_{gs3} = -I_x \cdot r_{o4}$$

$$V_x - (I_x + I_x \cdot r_{o4} \cdot g_{m3}) r_{o3} = I_x \cdot r_{o4}$$

$$\Leftrightarrow R_{O1} = \frac{V_x}{I_x} = g_{m3} \cdot r_{o4} \cdot r_{o3} + r_{o3} + r_{o4}$$

b)

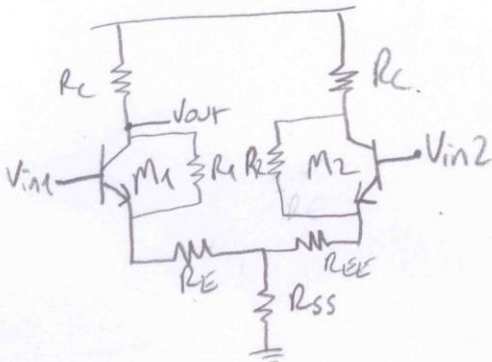


$$R_{O1} = g_{m3} \cdot r_{o4} \cdot r_{o3} + r_{o3} + r_{o4}$$

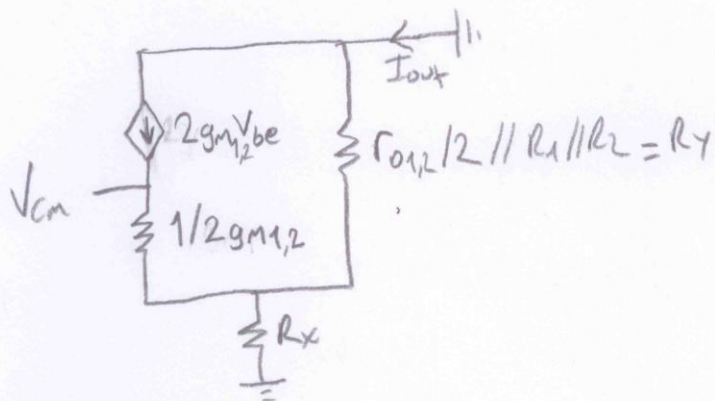
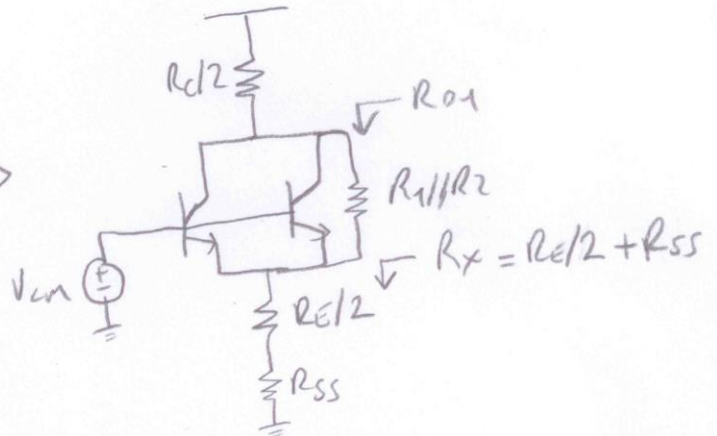
$$R_{O2} = g_{m2} \cdot r_{o2} \cdot r_{o1} \parallel R_p + r_{o1} \parallel R_p + r_{o2}$$

$$A_v = -g_{m1} \cdot R_{O1} \parallel R_{O2}$$

②



=>



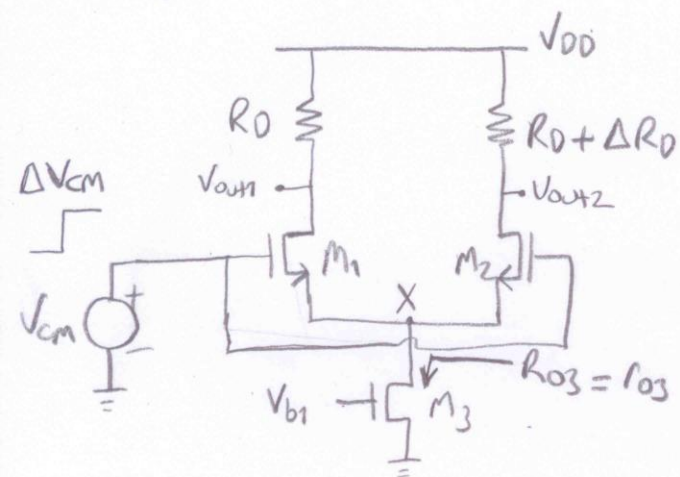
If we assume that $1/2 g_{m1,2} \ll R_y$

$$G_m = \frac{I_{out}}{V_{cm}} = \frac{1}{1/2 g_{m1,2} + R_x}$$

$$R_{O1} = g_{m1,2} \cdot R_y \cdot R_x + R_y + R_x$$

$$A_{cm} = -G_m \cdot R_{O1} \parallel R_{cd/2}$$

③ a)



$$\Delta V_{GS} = \Delta V_{GS1} = \Delta V_{GS2}$$

$$\Delta I_D = \Delta I_{D1} = \Delta I_{D2}$$

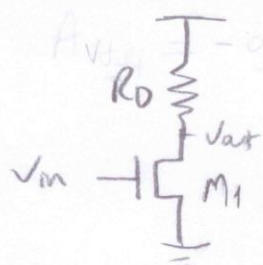
$$\Delta V_{cm} = \Delta V_{GS} + 2\Delta I_D \cdot R_{03} = \frac{\Delta I_D}{g_{m1}} + 2\Delta I_D \cdot r_{03}$$

$$\Delta V_{out} = \Delta V_{out1} - \Delta V_{out2} = -\Delta R_D \cdot \Delta I_D$$

$$A_{vcm} = \left| \frac{\Delta V_{out}}{\Delta V_{cm}} \right| = \frac{\Delta R_D}{\frac{1}{g_{m1}} + 2r_{03}}$$

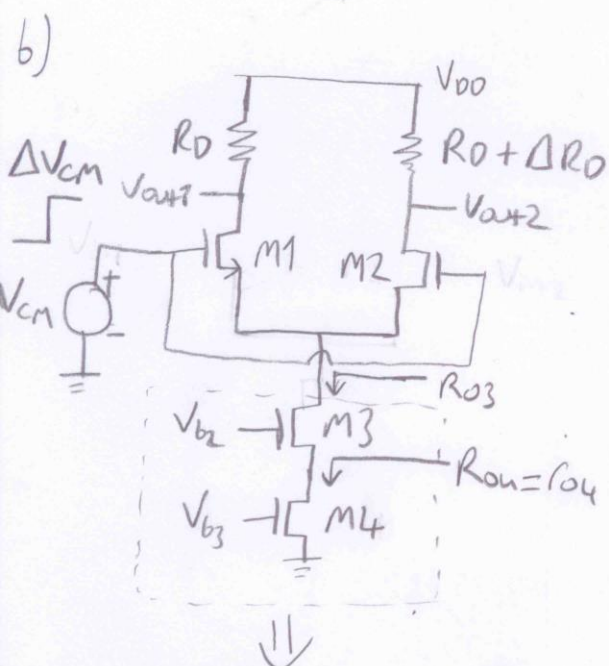
X node appears as virtual ground when differential input signals are applied.

So, $A_{vdiff} = -g_{m1} R_D$



$$\Rightarrow A_{vdiff} = -g_{m1} R_D$$

$$CMRR = \frac{|A_{vdiff}|}{|A_{vcm}|} = \frac{R_D}{\Delta R_D} \cdot (1 + 2g_{m1} \cdot r_{03})$$



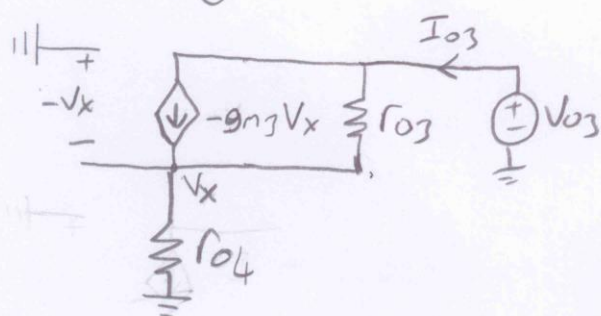
$$\Delta V_{cm} = \Delta V_{GS} + 2\Delta I_D R_{03} = \Delta I_D \left[\frac{1}{g_{m1}} + 2r_{03} \right]$$

$$\Delta V_{out} = -\Delta R_D \cdot \Delta I_D$$

$$A_{vcm} = \left| \frac{\Delta V_{out}}{\Delta V_{cm}} \right| = \frac{\Delta R_D}{\frac{1}{g_{m1}} + 2r_{03}}$$

$$A_{vdiff} = -g_{m1} \cdot R_D$$

$$\Rightarrow CMRR = \left| \frac{A_{vdiff}}{A_{vcm}} \right| = \frac{R_D}{\Delta R_D} \cdot (1 + 2g_{m1}g_{m3}r_{03}r_{04})$$

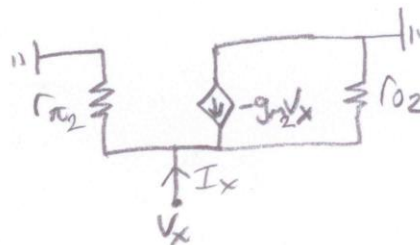
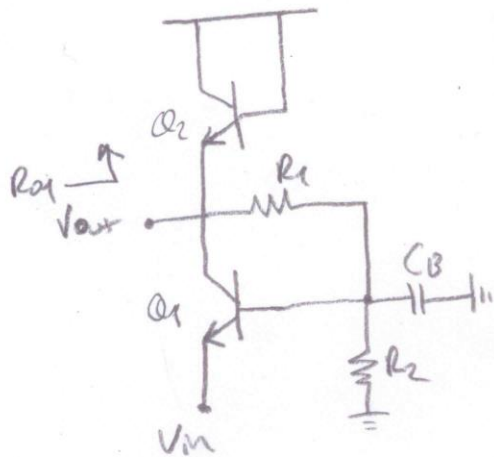


$$V_{03} = (I_{03} + g_{m3}V_x)r_{03} + I_{03} \cdot r_{04}$$

$$V_x = I_{03} \cdot r_{04}$$

$$R_{03} = \frac{V_{03}}{I_{03}} = g_{m3} \cdot r_{03} \cdot r_{04} + r_{04} + r_{03} \approx g_{m3} \cdot r_{03} \cdot r_{04}$$

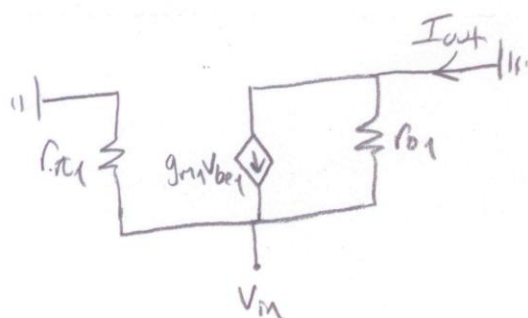
④



$$(I_x - g_{m2} V_x) r_{x2} \parallel r_{o2} = V_x$$

$$R_{o1} = \frac{V_x}{I_x} = \frac{r_{x2} \parallel r_{o2}}{1 + g_{m2} r_{x2} \parallel r_{o2}}$$

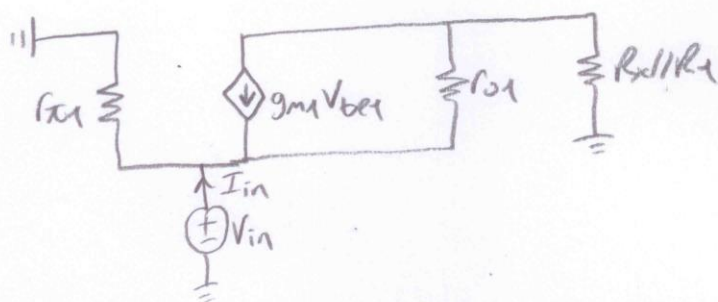
$$R_{out} = R_{o1} \parallel R_1 \parallel r_{o1}$$



$$0 - (I_{out} - g_{m1} V_{in}) r_{o1} = V_{in}$$

$$G_m = \frac{I_{out}}{V_{in}} = \frac{r_{o1}}{1 + g_{m1} r_{o1}}$$

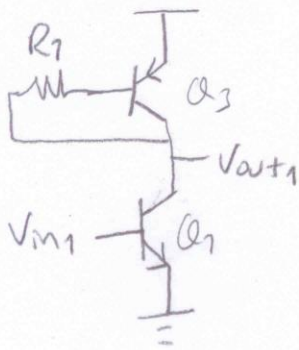
$$A_v = G_m \cdot R_{out}$$



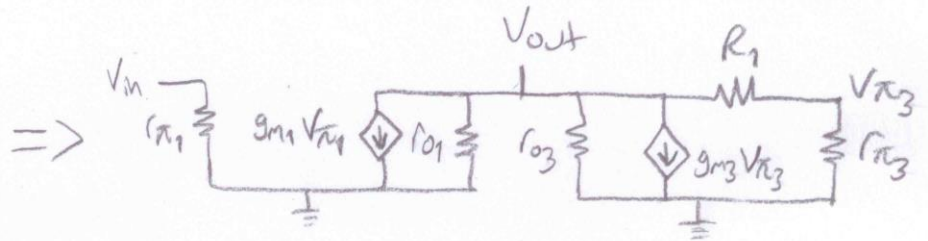
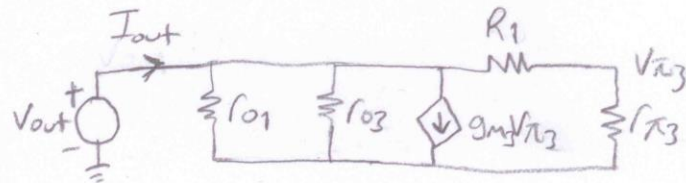
$$\left(I_{in} - \frac{V_{in}}{r_{x1}} - g_{m1} V_{in} \right) r_{o1} + R_x \parallel R_1 \left(I_{in} - \frac{V_{in}}{r_{x1}} \right) = V_{in}$$

$$R_{in} = \frac{V_{in}}{I_{in}} = \frac{r_{x1} r_{o1} + R_x \parallel R_1 \cdot r_{x1}}{r_{x1} + R_x \parallel R_1 + r_{o1} + g_{m1} r_{x1} \cdot r_{o1}}$$

(5)

Half of the amplifier

$$G_m = \frac{I_{out}}{V_{in}} = g_{m1}$$

Small signal equivalent circuitCalculation of Rout

$$\frac{V_{out}}{V_{\pi 3}} = \frac{R_1 + r_{\pi 3}}{r_{\pi 3}} \Rightarrow V_{\pi 3} = \frac{V_{out} r_{\pi 3}}{R_1 + r_{\pi 3}}$$

$$(I_{out} - g_{m3} V_{\pi 3}) (r_{o1} \parallel r_{o3} \parallel (R_1 + r_{\pi 3})) = V_{out}$$

R_{eq}

$$\frac{V_{out}}{I_{out}} = R_{out} = \frac{R_{eq} (R_1 + r_{\pi 3})}{g_{m3} r_{\pi 3} R_{eq} + R_1 + r_{\pi 3}} \approx \frac{R_1 + r_{\pi 3}}{g_{m3} r_{\pi 3}}$$

$$A_v = \frac{V_{out}}{V_{in}} = -g_{m1} \cdot \frac{R_1 + r_{\pi 3}}{g_{m3} r_{\pi 3}}$$

Due to constant current, we can't change value of g_{m1} , g_{m3} and $r_{\pi 3}$.

However, we can increase R_1 to obtain higher gain. Note that after a certain R_1 value, input transistors will go into saturation region leading to gain drop.

