## Standing Wove and Standing Ware Ratio

The general solutions of the transmission-line voltage and current equations are:

We can rewrite the voltage solution as,

$$V = V_{+}e^{-\alpha z} - ikz_{+} V_{-}e^{\alpha z} e^{ikz}$$

$$= V_{+}e^{-\alpha z} \left[ \cos(\beta z) - j\sin(\beta z) \right] + V_{-}e^{\alpha z} \left[ \cos(\beta z) + j\sin(\beta z) \right]$$

$$= (V_{+}e^{-\alpha z} + V_{-}e^{\alpha z}) \cos(\beta z) - j(V_{+}e^{-\alpha z} - V_{-}e^{\alpha z}) \sin(\beta z)$$

we can assume that Vte-2 and Vedz are real; we can then obtain the voltage standing were equation by expessing the above equation as,

where Vo is the standing-war pottern, or the amplitude of the standing wave;

and to is the phase pottern at the standing ware,  $\phi_n = \arctan \left[ \frac{V_{te^{-d^2}} - V_{-e^{d^2}}}{(n)^2} \right]$ 

$$\phi_0 = \operatorname{orcton} \left[ \frac{V_{+}e^{-\alpha z} - V_{-}e^{\alpha z}}{V_{+}e^{-\alpha z} + V_{-}e^{\alpha z}} \operatorname{ton}(\beta z) \right]$$

We can find the max. and min. values of Vo by differtiating the Vo with respect to \$2 and equating the result to zero. When we do so and substitute the proper values of \$2 into Vo; the max. amplitude is: \frac{V\_{max}}{max} = \frac{V\_{+}e^{-\alpha 2} + V\_{-}e^{\alpha 2}}{max} \text{ which occurs at \$\beta 2 = nrc & 1 & n = 0, \pm 1, \pm 12... \text{ the min. amplitude is: } \frac{V\_{max}}{V\_{min}} = \frac{V\_{+}e^{-\alpha 2} - V\_{-}e^{\alpha 2}}{V\_{-}e^{-\alpha 2}} \text{ which occurs at \$\beta 2 = (2n-1)(\pi I/2), \$n = 0, \pm 1, \pm 12...

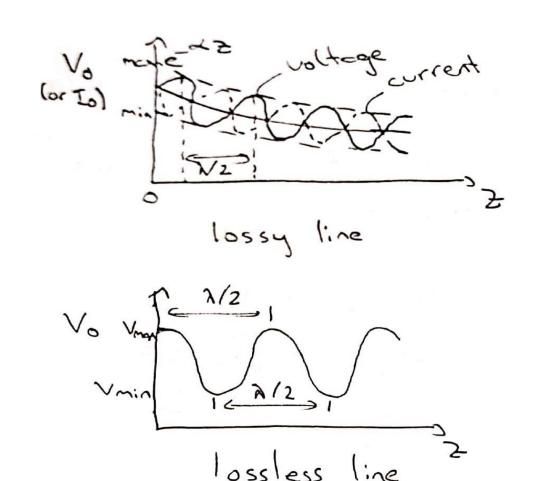
The distance between any two maxima or minima is one-holf wavelength, since \$2=n\pi, n=0, \pi 1, \pi 2, ..., so

$$\frac{7}{3} = \frac{9\pi}{3} = \frac{1}{(2\pi)/3} = \frac{1}{2}$$

Similarly, the maximum and minimum currets are,

Imex = I+e-x2+I-ex2 and Imin = I+e-x2-I-ex2

The figures below show the standing wave patterns in a lossy



In the lossy-line case, the maxima and minimo are functions of position 2 and reflection coefficient  $\Gamma'$  ( $\Gamma = \frac{V - e^{\gamma z}}{V + e^{\gamma z}}$ )  $|\Gamma| = \frac{V - e^{\gamma z}}{V + e^{\gamma z}}$ )

Vmox = V+ e-d= (1+171) and Vmin = V+ e-d= (1-171) Imex = I+ e-d= (1+171) and Imin = I-e-d= (1-171)

In the lossless-line, mex. and min. emplitudes remain constant,

 $V_{max} = V_{+} (1+|\Gamma|)$  and  $V_{min} = V_{+} (1-|\Gamma|)$  $I_{max} = I_{+} (1+|\Gamma|)$  and  $I_{min} = I_{+} (1-|\Gamma|)$ 

when  $V_{-}=0$  ( $\Gamma=0$ ),  $V_{0}$  becomes  $V_{0}=V_{+}e^{-\alpha Z}$  and  $V_{S}=V_{+}e^{-\gamma Z}$  which is a pure traveling move.

when  $|V_te^{-\alpha z}| = |V_e^{\alpha z}|$ ,  $(|\Gamma| = 1)$ ,  $V_s = 2V_te^{-\alpha z}\cos(\beta z)$  which is a pure standing were.

Similarly, for the current, the equation at a pure standing wave is  $\Gamma_s = -i27 \sigma V_+ e^{-dz} \sin{(\beta z)}$ 

We can express the voltage or real function of time and spece:

Us (2,t) = Re [Vs(2) e int] = 2Vt e = 2 cos (B2) cos(W4)

Similarly for current, is(z,t) = Re[Is(z)eint] = 240V+e-~zsin(Bz)sin(ut)

The sum of the two time-overage densities is constant on the line. The complex power in the lossless line is,

 $P = \frac{1}{2} V_s(z) \left[ \frac{1}{5} (z) = \frac{1}{2} \left[ \frac{2 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] \left[ \frac{12 V_0 V_t \sin(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_0 V_t \sin(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta z)} \right] = \frac{1}{3} \left[ \frac{12 V_t \cos(\beta z)}{1 \cos(\beta$ 

## Standing Wore Rotio

Standing-were ratio is defined as, (designated by s)

S = max. voltage or current = 
$$\frac{|V_{max}|}{|V_{min}|} = \frac{|I_{max}|}{|I_{min}|}$$

For the pure traveling wave (V=0), S=1, and for the pure standing wave, we have S+00. The standing-wave ratio (SWR) cannot be defined on a lossy line because the standing-wave pottern changes from one position to another. On a lossless line, SWR stays the same throughout the line.

SWR is related to the reflection coefficient 1 as follows:

$$S = \frac{1+|\Gamma|}{1-|\Gamma|} \quad \text{or} \quad |\Gamma| = \frac{S-1}{S+1} \quad \text{isince } |\Gamma| \leq 1, \, S \geq 1$$

Since  $|V_{+}| = |I_{+}| \geq_{0}$  and  $|V_{-}| = |I_{-}| \geq_{0}$ , we can express  $|V_{\text{mex}}|$  and  $|V_{\text{min}}| = s$ .

|Vnox | = | Imax | Zo and |Vnix | = | Imin | Zo

When the voltage is now. and the current is min., the impedance at that print must be now and purely resisting.

Znox = (Vnox)
Znin = (Vnin)
IInox)

The power transmitted by a line:  $P = |V_{max}| |I_{min}| = |V_{min}| |II_{max}| \qquad clso,$   $P = \frac{|V_{max}| |V_{min}|}{2} = \frac{|V_{max}|^2}{2} = \frac{|V_{min}|^2}{2}$ 

in terms of current,  $P = |I_{max}||I_{min}||_{Z_0} = |I_{max}|^2 \sum_{min} = |I_{min}|^2 \sum_{min} |I_{min}|^$ 

Since  $|V_{max}| = |V_{+}| + |V_{-}|$  and  $|V_{min}| = |V_{+}| - |V_{-}|$   $P = \frac{|V_{max}||V_{min}|}{2\sigma} = \frac{|V_{+}|^{2}}{2\sigma} - \frac{|V_{-}|^{2}}{2\sigma}$ 

also in terms of current, P= II+PZo-II\_PZo

The result says that it the Zo is a pure resistance the power is related (or calculated) with incident and reflected naves.

Example: For a transmission line,  $Z_0 = 50 + j0,010$  and  $Z_L = 73 - j(2502, S=2)$  $P = \frac{Z_L - Z_D}{Z_L + Z_D} = 0,377 \ L - 427^0$   $1 + |P| \qquad 1 + 0,377$ 

$$S = \frac{1+|\Gamma|}{1-|\Gamma|} = \frac{1+0.377}{1-0.377} = 2.21$$