

# I. Governing equations of GFD

## Objectives:

1. Know the governing equations (momentum, continuity, tracer, density) and how their terms are derived
2. Boussinesq approximation and Reynolds average
3. Scale analysis (dimensionless numbers)

# Momentum equation

**Newton's second Law:**

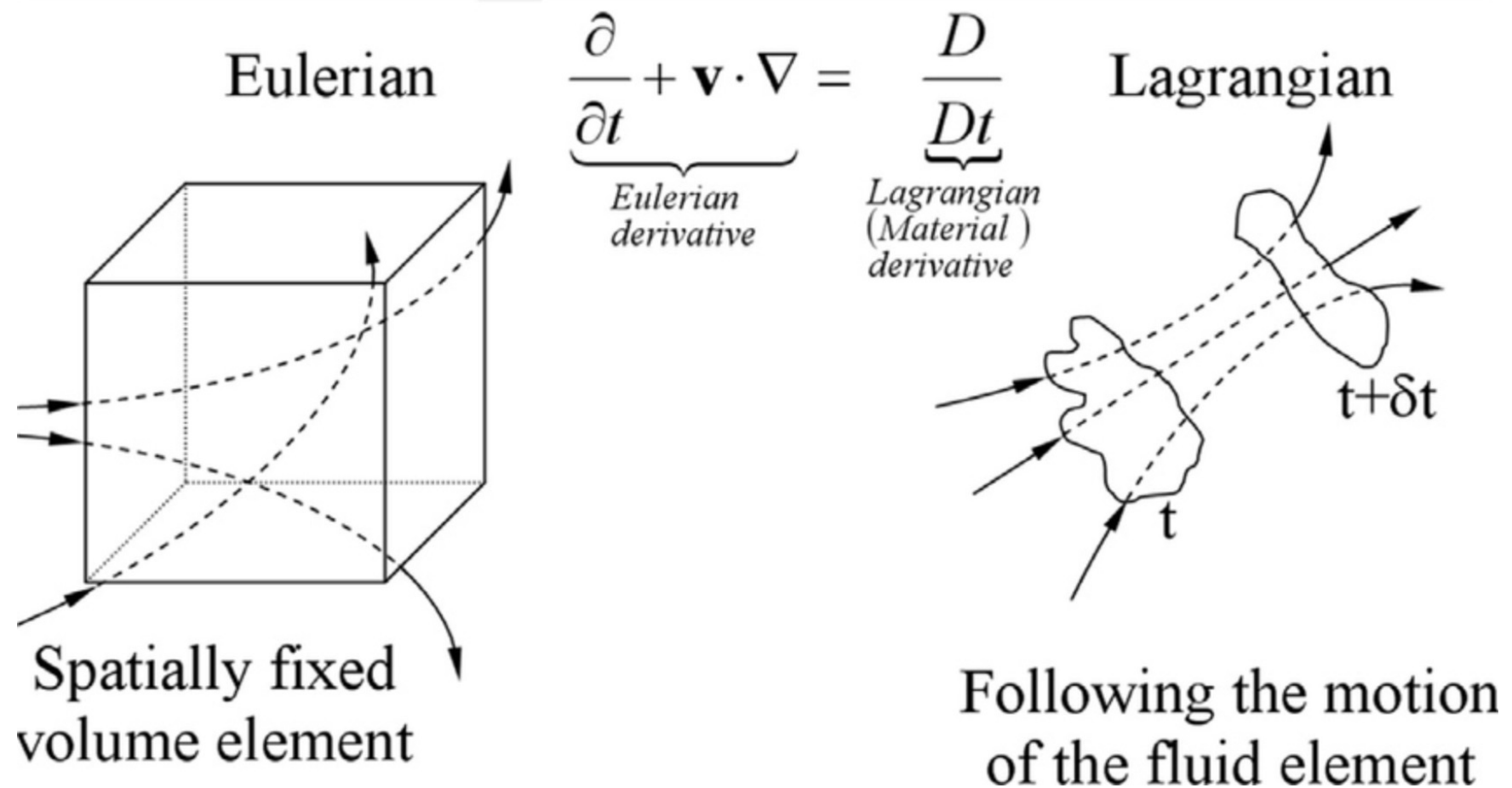
$$m\mathbf{a} = \mathbf{F}$$

For unit volume:

$$\rho \, d\mathbf{u}/dt = \mathbf{F}$$


$$d\mathbf{u}/dt = \mathbf{F}/\rho$$

# Eulerian and Lagrangian methods



$$\mathbf{u} = (u, v, w)$$

$$\frac{d\mathbf{u}}{dt} = \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \longrightarrow \text{non-linear advection term}$$

  
**local acceleration term**

$$\text{x direction: } \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$$

$$\text{y direction: } \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z}$$

$$\text{z direction: } \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$$

## Pressure gradient force

**Derivation of Pressure Term** Consider the forces acting on the sides of a small cube of fluid (Figure 7.4). The net force  $\delta F_x$  in the  $x$  direction is

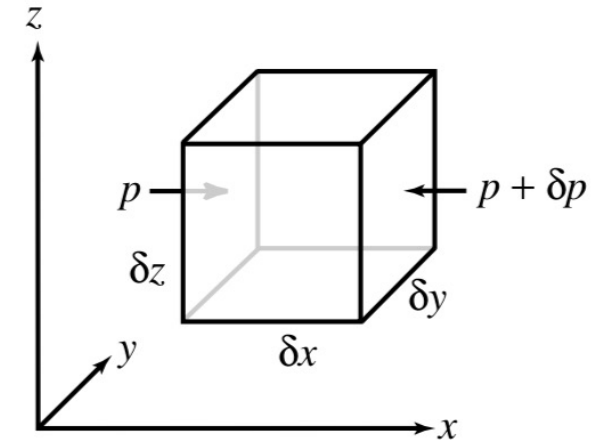
$$\begin{aligned}\delta F_x &= p \delta y \delta z - (p + \delta p) \delta y \delta z \\ \delta F_x &= -\delta p \delta y \delta z\end{aligned}$$

But

$$\delta p = \frac{\partial p}{\partial x} \delta x$$

and therefore

$$\begin{aligned}\delta F_x &= -\frac{\partial p}{\partial x} \delta x \delta y \delta z \\ \delta F_x &= -\frac{\partial p}{\partial x} \delta V\end{aligned}$$



$$f(x) = f(x_0) + \left. \frac{df(x)}{dx} \right|_{x=x_0} (x - x_0) + \frac{d^2 f(x)}{2! dx^2} \bigg|_{x=x_0} (x - x_0)^2 + \dots$$

Dividing by the mass of the fluid  $\delta m$  in the box, the acceleration of the fluid in the  $x$  direction is:

$$a_x = \frac{\delta F_x}{\delta m} = -\frac{\partial p}{\partial x} \frac{\delta V}{\delta m}$$

$$\boxed{a_x = -\frac{1}{\rho} \frac{\partial p}{\partial x}}$$

(7.13)

## The momentum equations

x direction: 
$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \dots$$

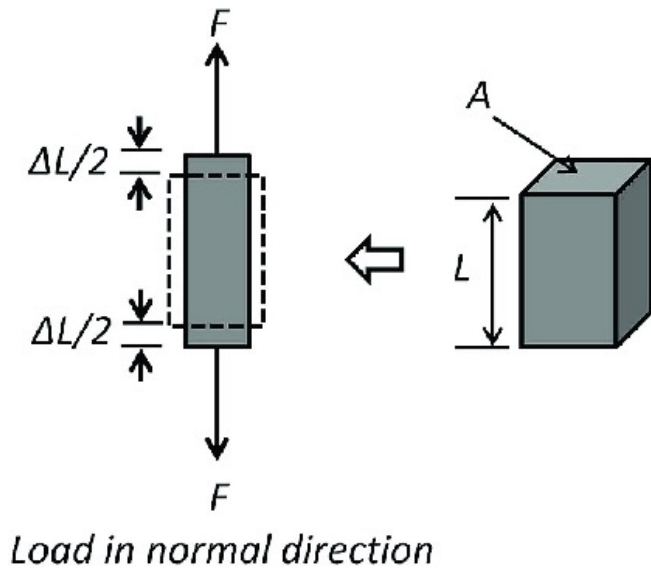
y direction: 
$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \dots$$

z direction: 
$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial z} + \dots$$

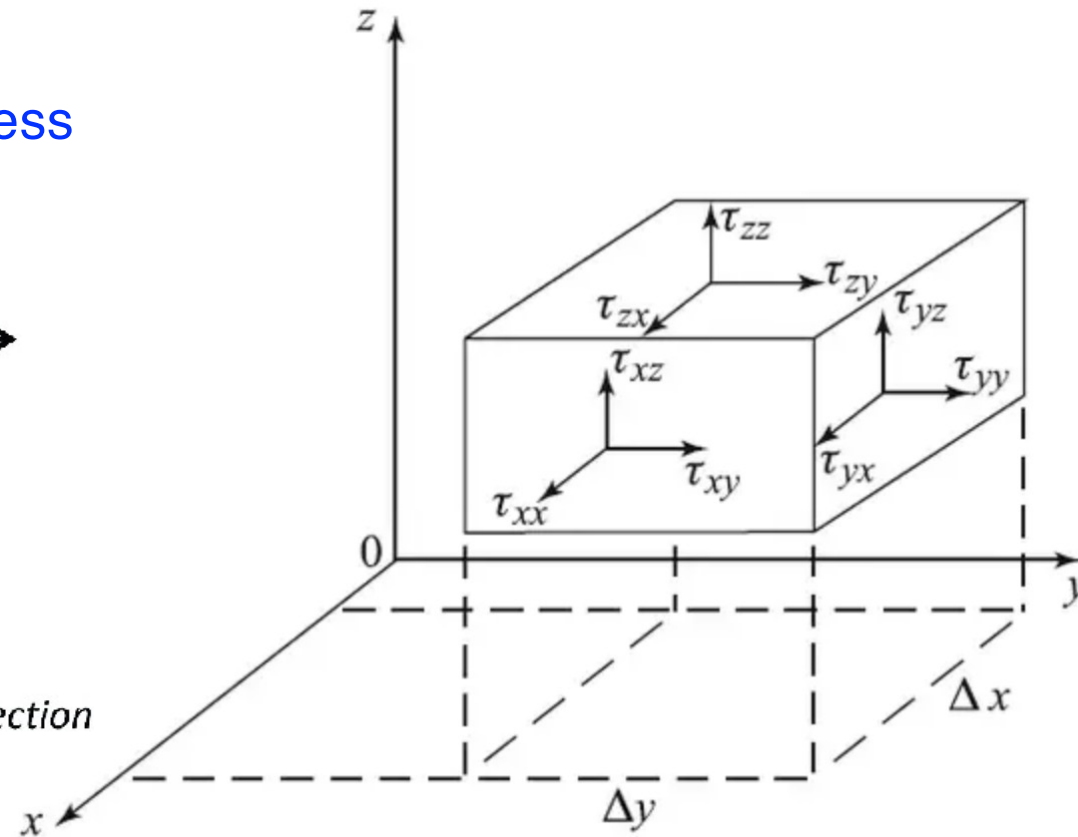
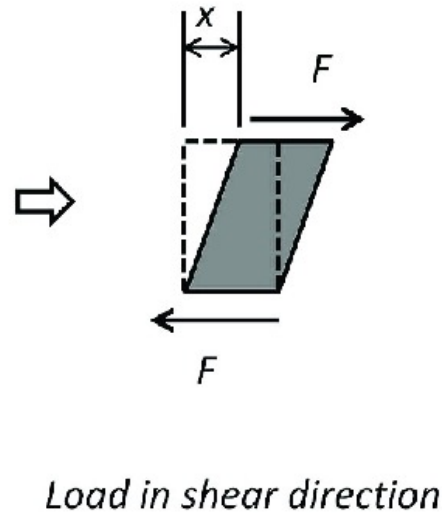
## Frictional force term

**Stress** – second-order tensor ( $\text{N m}^{-2}$ )

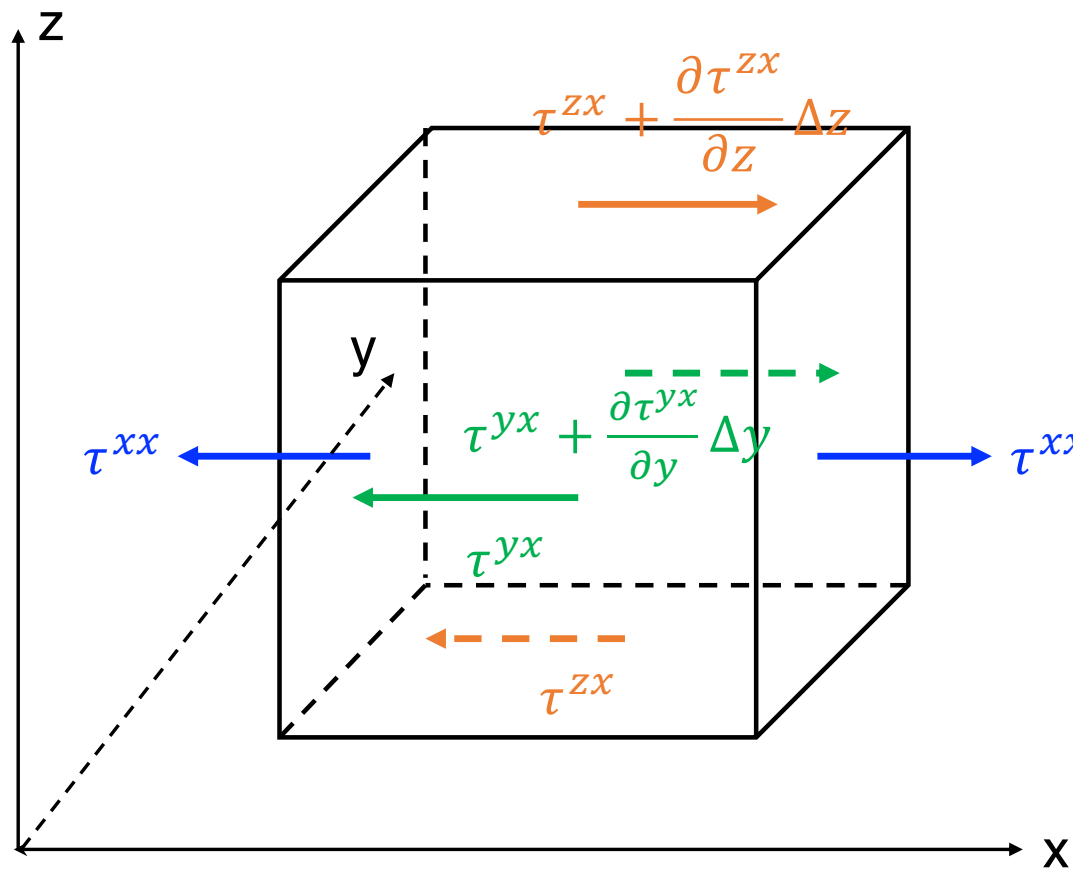
normal stress



shear stress



9 components



$$\begin{aligned}
 F^x = & \left( \tau^{xx} + \frac{\partial \tau^{xx}}{\partial x} \Delta x \right) \Delta y \Delta z - \tau^{xx} \Delta y \Delta z \\
 & + \left( \tau^{yx} + \frac{\partial \tau^{yx}}{\partial y} \Delta y \right) \Delta x \Delta z - \tau^{yx} \Delta x \Delta z \\
 & + \left( \tau^{zx} + \frac{\partial \tau^{zx}}{\partial z} \Delta z \right) \Delta x \Delta y - \tau^{zx} \Delta x \Delta y
 \end{aligned}$$

For per unit volume

$$F^x = \frac{\partial \tau^{xx}}{\partial x} + \frac{\partial \tau^{yx}}{\partial y} + \frac{\partial \tau^{zx}}{\partial z}$$



For Newtonian fluids, viscous stress is:  $\tau^{zx} = \mu \frac{\partial u}{\partial z}$

$\mu$ : dynamic viscosity coefficient

Assumption:  
 $\mu$  is constant

$$\begin{aligned} F^x &= \frac{\partial \tau^{xx}}{\partial x} + \frac{\partial \tau^{yx}}{\partial y} + \frac{\partial \tau^{zx}}{\partial z} \\ &= \frac{1}{\partial x} \left( \mu \frac{\partial u}{\partial x} \right) + \frac{1}{\partial y} \left( \mu \frac{\partial u}{\partial y} \right) + \frac{1}{\partial z} \left( \mu \frac{\partial u}{\partial z} \right) \\ &= \mu \nabla^2 u \end{aligned}$$

Laplacian operator

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

$$\begin{aligned} F^y &= \frac{\partial \tau^{xy}}{\partial x} + \frac{\partial \tau^{yy}}{\partial y} + \frac{\partial \tau^{zy}}{\partial z} \\ &= \frac{1}{\partial x} \left( \mu \frac{\partial v}{\partial x} \right) + \frac{1}{\partial y} \left( \mu \frac{\partial v}{\partial y} \right) + \frac{1}{\partial z} \left( \mu \frac{\partial v}{\partial z} \right) \\ &= \mu \nabla^2 v \end{aligned}$$

$$\begin{aligned} \frac{F^x}{\rho} &= \frac{\mu}{\rho} \nabla^2 u \\ &= \nu \nabla^2 u \end{aligned}$$

$\nu$  : kinematic viscosity coefficient

$$\begin{aligned} F^z &= \frac{\partial \tau^{xz}}{\partial x} + \frac{\partial \tau^{yz}}{\partial y} + \frac{\partial \tau^{zz}}{\partial z} \\ &= \frac{1}{\partial x} \left( \mu \frac{\partial w}{\partial x} \right) + \frac{1}{\partial y} \left( \mu \frac{\partial w}{\partial y} \right) + \frac{1}{\partial z} \left( \mu \frac{\partial w}{\partial z} \right) \\ &= \mu \nabla^2 w \end{aligned}$$

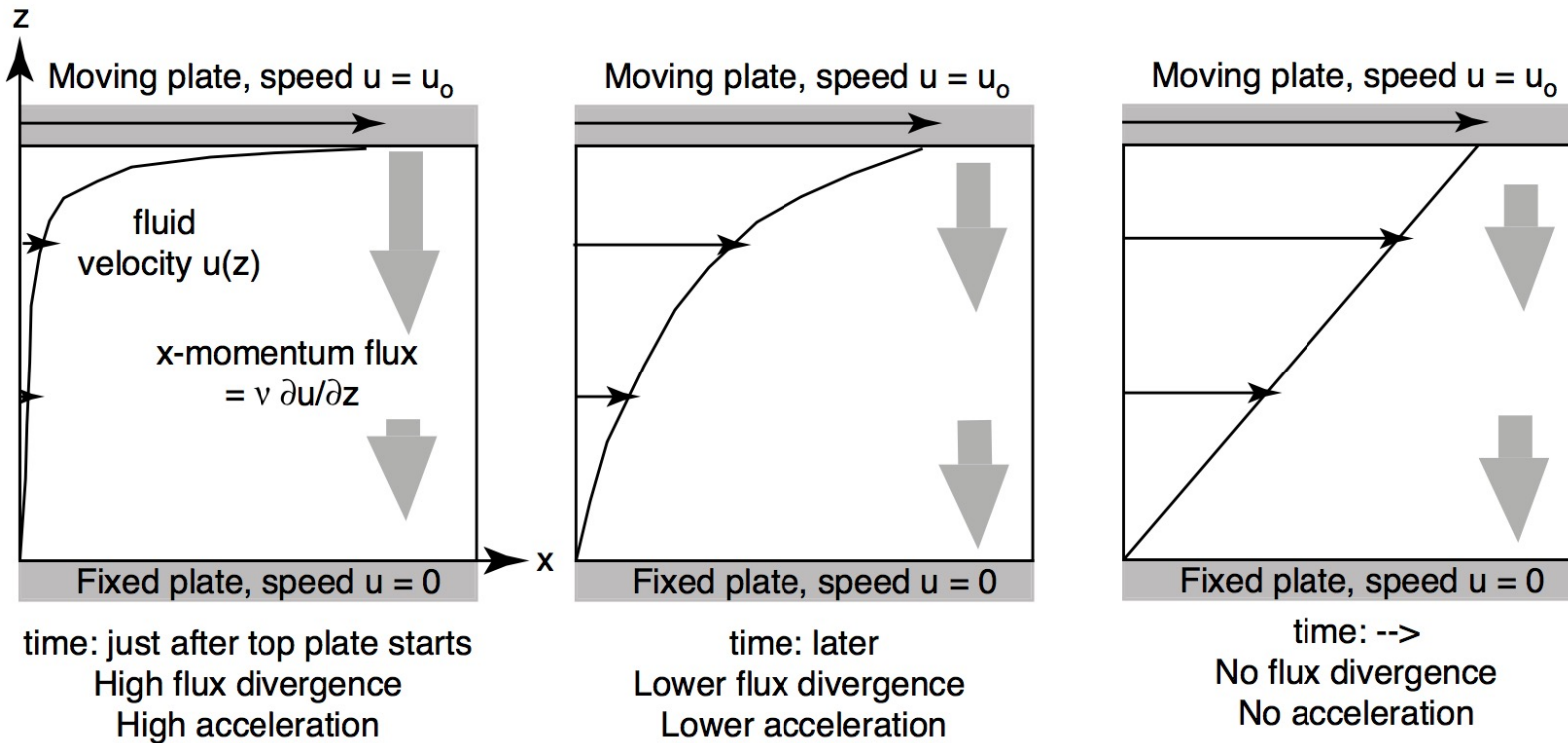
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	$\mu$ (kg m <sup>-1</sup> s <sup>-1</sup> )	$\nu$ (m <sup>2</sup> s <sup>-1</sup> )
Air	$1.8 \times 10^{-5}$	$1.5 \times 10^{-5}$
Water	$1.1 \times 10^{-3}$	$1.1 \times 10^{-6}$
Mercury	$1.6 \times 10^{-3}$	$1.2 \times 10^{-7}$

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$$\tau^{zx} = \mu \frac{\partial u}{\partial z}$$

**(e)** Acceleration associated with friction and viscosity



Acceleration is finally determined by the divergence of the viscous stress.

$$\frac{\partial}{\partial z} \left( \nu \frac{\partial u}{\partial z} \right)$$

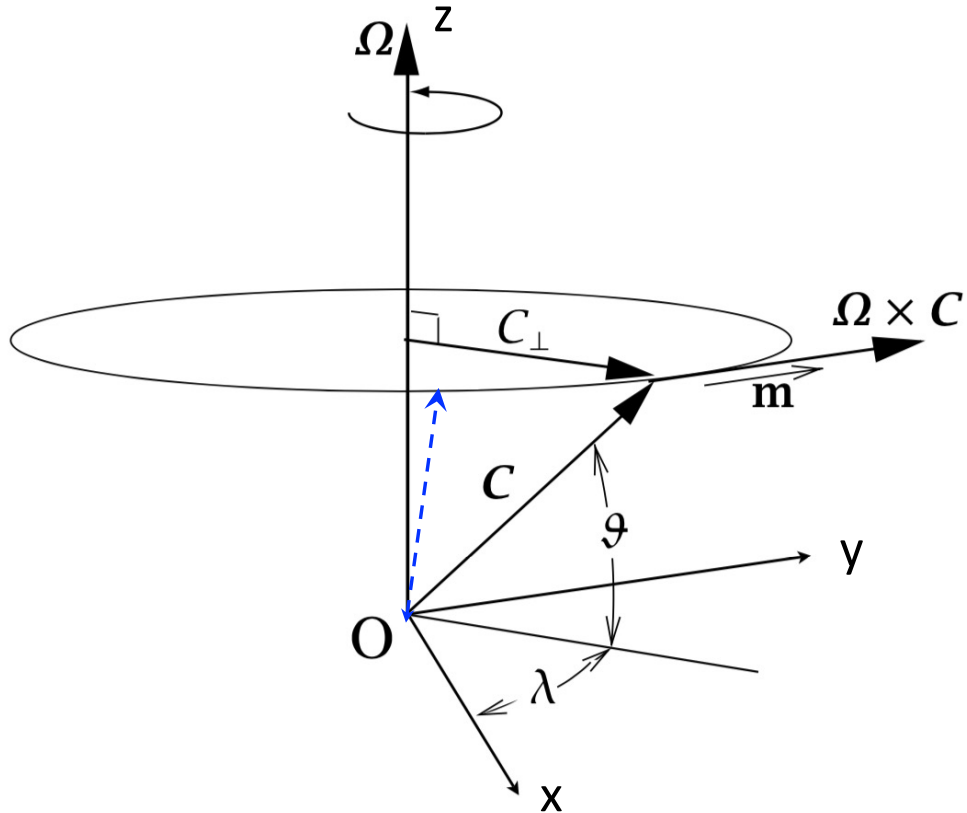
## The momentum equations

x direction: 
$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \underbrace{v \nabla^2 u}_{v \nabla^2 u \text{ (for constant } v)} + \underbrace{\frac{\partial}{\partial x} \left( v \frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial y} \left( v \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial z} \left( v \frac{\partial u}{\partial z} \right)}_{\text{red terms}} + \dots$$

y direction: 
$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \underbrace{v \nabla^2 v}_{v \nabla^2 v} + \underbrace{\frac{\partial}{\partial x} \left( v \frac{\partial v}{\partial x} \right) + \frac{\partial}{\partial y} \left( v \frac{\partial v}{\partial y} \right) + \frac{\partial}{\partial z} \left( v \frac{\partial v}{\partial z} \right)}_{\text{red terms}} + \dots$$

z direction: 
$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial z} + \underbrace{v \nabla^2 w}_{v \nabla^2 w} + \underbrace{\frac{\partial}{\partial x} \left( v \frac{\partial w}{\partial x} \right) + \frac{\partial}{\partial y} \left( v \frac{\partial w}{\partial y} \right) + \frac{\partial}{\partial z} \left( v \frac{\partial w}{\partial z} \right)}_{\text{red terms}} + \dots$$

Expressions for the force terms are given in the inertial frame.  
So is the acceleration term.



**Fig. 2.1** A vector  $\mathbf{C}$  rotating at an angular velocity  $\boldsymbol{\Omega}$ . It appears to be a constant vector in the rotating frame, whereas in the inertial frame it evolves according to  $(d\mathbf{C}/dt)_I = \boldsymbol{\Omega} \times \mathbf{C}$ .

## Coriolis Force

The change in  $\mathbf{C}$  in  $\delta t$  with respect to the Inertial frame

$$\delta \mathbf{C} = |\mathbf{C}| \cos \vartheta \delta \lambda \mathbf{m},$$

$$\delta \lambda = |\boldsymbol{\Omega}| \delta t$$

Let  $\hat{\vartheta} = (\pi/2 - \vartheta)$

$$\delta \mathbf{C} = |\mathbf{C}| |\boldsymbol{\Omega}| \sin \hat{\vartheta} \mathbf{m} \delta t = \boldsymbol{\Omega} \times \mathbf{C} \delta t.$$

$$\left( \frac{d\mathbf{C}}{dt} \right)_I = \boldsymbol{\Omega} \times \mathbf{C}$$

## Non-constant vector in the rotating frame

For a vector  $\mathbf{B}$  that changes in the inertial frame:

$$(\delta \mathbf{B})_I = (\delta \mathbf{B})_R + (\delta \mathbf{B})_{rot}$$

With  $(\delta \mathbf{B})_{rot} = \boldsymbol{\Omega} \times \mathbf{B} \delta t$

$$\delta \mathbf{C} = \boldsymbol{\Omega} \times \mathbf{C} \delta t$$

$$\left( \frac{d\mathbf{C}}{dt} \right)_I = \boldsymbol{\Omega} \times \mathbf{C}$$

$$\left( \frac{d\mathbf{B}}{dt} \right)_I = \left( \frac{d\mathbf{B}}{dt} \right)_R + \boldsymbol{\Omega} \times \mathbf{B} \quad \mathbf{r} \text{ is a vector from the Earth center pointing to the Earth surface}$$

$$\left( \frac{d\mathbf{r}}{dt} \right)_I = \left( \frac{d\mathbf{r}}{dt} \right)_R + \boldsymbol{\Omega} \times \mathbf{r}$$

$$\left( \frac{d\mathbf{v}_I}{dt} \right)_I = \left( \frac{d\mathbf{v}_R}{dt} \right)_R + \boldsymbol{\Omega} \times \mathbf{v}_R + \cancel{\frac{d\boldsymbol{\Omega}}{dt} \times \mathbf{r}} + \boldsymbol{\Omega} \times \left( \frac{d\mathbf{r}}{dt} \right)_I$$

$\mathbf{v}_I$

$$\mathbf{v}_I = \mathbf{v}_R + \boldsymbol{\Omega} \times \mathbf{r}$$

Centrifugal acceleration

$$\left( \frac{d\mathbf{v}_R}{dt} \right)_I = \left( \frac{d\mathbf{v}_R}{dt} \right)_R + \boldsymbol{\Omega} \times \mathbf{v}_R$$

$$\left( \frac{d\mathbf{v}_I}{dt} \right)_I = \left( \frac{d\mathbf{v}_R}{dt} \right)_R + \underline{2\boldsymbol{\Omega} \times \mathbf{v}_R} + \underline{\boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{r})}$$

Coriolis acceleration

$$\left( \frac{d}{dt} (\mathbf{v}_I - \boldsymbol{\Omega} \times \mathbf{r}) \right)_I = \left( \frac{d\mathbf{v}_R}{dt} \right)_R + \boldsymbol{\Omega} \times \mathbf{v}_R$$

# The Coriolis acceleration

$$2\boldsymbol{\Omega} \times \mathbf{v}_R$$

$$\boldsymbol{\Omega} = \Omega \cos \varphi \mathbf{j} + \Omega \sin \varphi \mathbf{k}$$

$$\text{x: } 2\Omega \cos \varphi w - 2\Omega \sin \varphi v$$

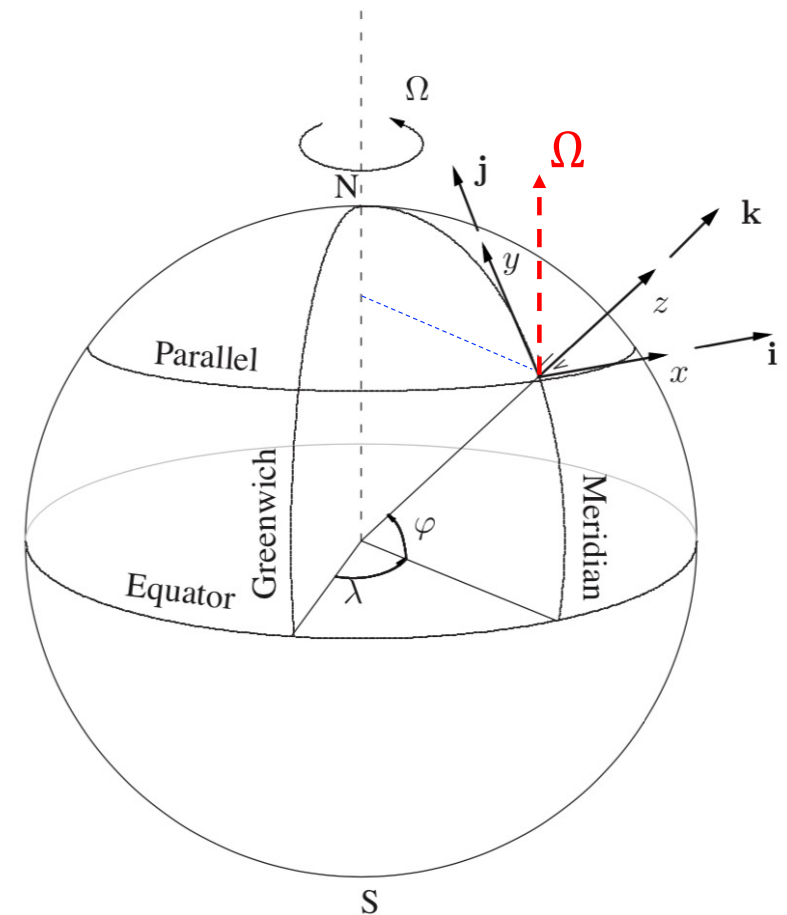
$$\text{y: } 2\Omega \sin \varphi u$$

$$\text{z: } -2\Omega \cos \varphi u.$$

$$f = 2\Omega \sin \varphi$$

$$f_* = 2\Omega \cos \varphi.$$

$f$ : Coriolis parameter



# The momentum equations

$$\left(\frac{d\mathbf{v}_I}{dt}\right)_I = \left(\frac{d\mathbf{v}_R}{dt}\right)_R + 2\boldsymbol{\Omega} \times \mathbf{v}_R + \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{r}) = \text{force terms}$$

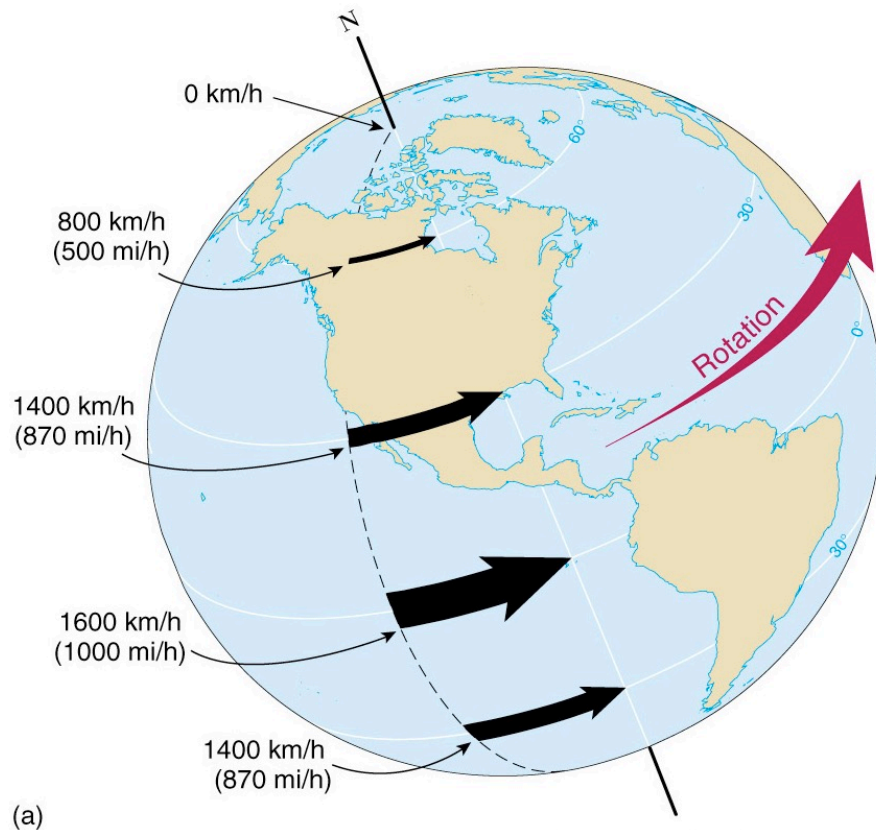
Nonlinear advection term   Coriolis term   Pressure gradient term

x direction:  $\underbrace{\frac{\partial u}{\partial t}}_{\text{Local acceleration}} + \underbrace{u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}}_{\text{Nonlinear advection term}} - \underbrace{fv + f_* w}_{\text{Coriolis term}} = -\underbrace{\frac{1}{\rho} \frac{\partial p}{\partial x}}_{\text{Pressure gradient term}} + \underbrace{\nu \nabla^2 u}_{\text{Viscosity term}} + \dots$

y direction:  $\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \underbrace{fu}_{\text{Coriolis term}} = -\underbrace{\frac{1}{\rho} \frac{\partial p}{\partial y}}_{\text{Pressure gradient term}} + \underbrace{\nu \nabla^2 v}_{\text{Viscosity term}} + \dots$

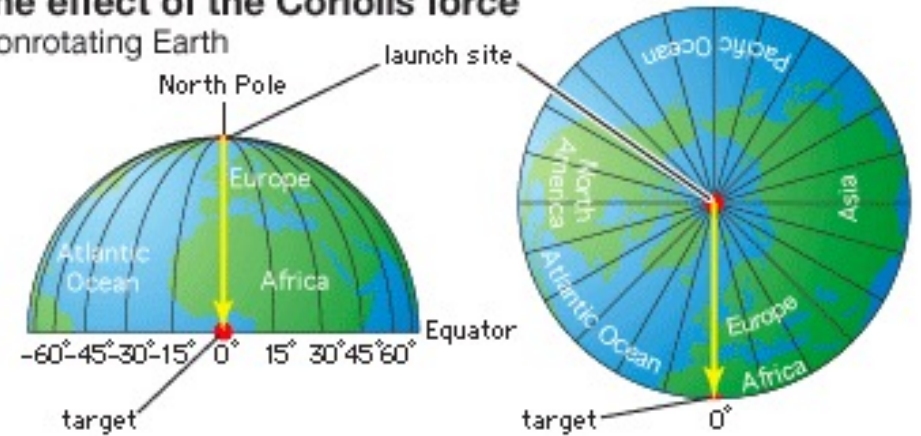
z direction:  $\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} - \underbrace{f_* u}_{\text{Coriolis term}} = -\underbrace{\frac{1}{\rho} \frac{\partial p}{\partial z}}_{\text{Pressure gradient term}} + \underbrace{\nu \nabla^2 w}_{\text{Viscosity term}} + \dots$

# The Coriolis Force

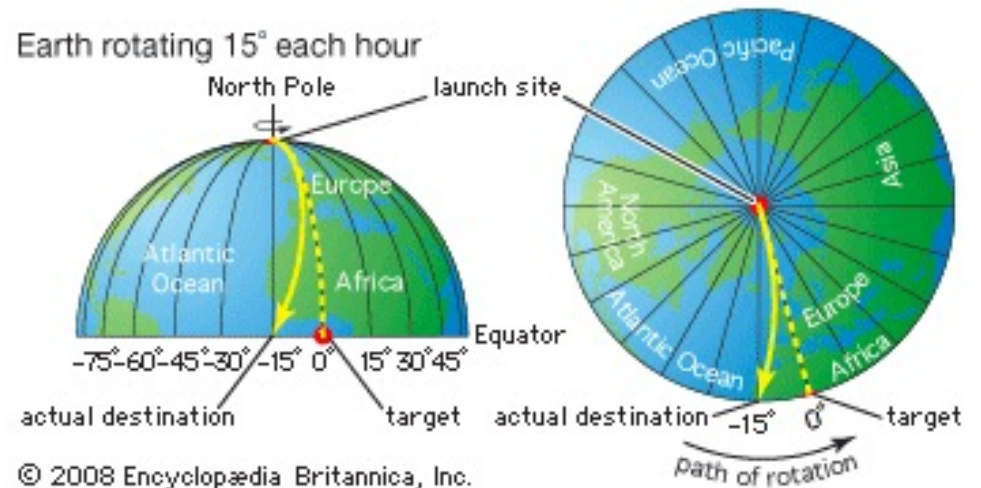


## The effect of the Coriolis force

### Nonrotating Earth



### Earth rotating 15° each hour





# $f$ -plane and $\beta$ -plane

$$f = 2\Omega \sin \varphi = \frac{2\Omega(\sin \varphi_0 + \cos \varphi_0(\varphi - \varphi_0))}{f_0}$$

If  $\varphi - \varphi_0$  is small:

$f$ -plane:  $f = f_0$  is a constant.

If  $\varphi - \varphi_0$  cannot be neglected:

$$\beta\text{-plane: } f = f_0 + 2\Omega \cos \varphi_0 \frac{(\varphi - \varphi_0)}{y/a} = f_0 + \frac{2\Omega \cos \varphi_0}{\beta} y$$

