

Quasi-geostrophic dynamics for frictional flows

Assumptions: homogeneous, rotational, viscous fluids, flat surface and bottom

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} - f v = -\frac{1}{\rho_0} \frac{\partial p}{\partial x} + \frac{\partial}{\partial z} \left(A_V \frac{\partial u}{\partial z} \right)$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + f u = -\frac{1}{\rho_0} \frac{\partial p}{\partial y} + \frac{\partial}{\partial z} \left(A_V \frac{\partial v}{\partial z} \right)$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

$z' = 0$ SBL
interior

Define the non-dimensional variables:

$z' = -1$ BBL

$$(u, v) = U(u', v') \quad w = W w' \quad (x, y) = L(x', y') \quad z = H z' \quad p = P p'$$

$$\frac{U}{T} \frac{\partial u'}{\partial t'} + \frac{U^2}{L} u' \frac{\partial u'}{\partial x'} + \frac{U^2}{L} v' \frac{\partial u'}{\partial y'} + \frac{U^2}{L} w' \frac{\partial u'}{\partial z'} - f U v' = -\frac{P}{\rho_0 L} \frac{\partial p'}{\partial x'} + \frac{A_V U}{H^2} \frac{\partial^2 u'}{\partial z'^2}$$

$$\frac{U}{T} \frac{\partial u'}{\partial t'} + \frac{U^2}{L} u' \frac{\partial u'}{\partial x'} + \frac{U^2}{L} v' \frac{\partial u'}{\partial y'} + \frac{U^2}{L} w' \frac{\partial u'}{\partial z'} - f U v' = -\frac{P}{\rho_0 L} \frac{\partial p'}{\partial x'} + \frac{A_V U}{H^2} \frac{\partial^2 u'}{\partial z'^2}$$

Divide the equation by fU , and remove the symbol ':

$$\varepsilon \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) - v = -\frac{\partial p}{\partial x} + \frac{E_v}{2} \frac{\partial^2 u}{\partial z^2} \quad E_v = \frac{2A_V}{fH^2} \sim \varepsilon^2$$

$$\varepsilon \left(\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) + u = -\frac{\partial p}{\partial y} + \frac{E_v}{2} \frac{\partial^2 v}{\partial z^2}$$

Now take the asymptotic expansion of the non-dimensional variables:

$$u = u_0 + \varepsilon u_1 + \varepsilon^2 u_2$$

$$v = v_0 + \varepsilon v_1 + \varepsilon^2 v_2$$

$$w = w_0 + \varepsilon w_1 + \varepsilon^2 w_2$$

$$p = p_0 + \varepsilon p_1 + \varepsilon^2 p_2$$

Substitution into the momentum equation, and to the order of $O(1)$:

$$-v_0 = -\frac{\partial p}{\partial x} \quad u_0 = -\frac{\partial p}{\partial y}$$

To the order of $O(\varepsilon)$:

$$\varepsilon \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) - v = -\frac{\partial p}{\partial x} + \frac{E_v}{2} \frac{\partial^2 u}{\partial z^2}$$

$$\frac{\partial u_0}{\partial t} + u_0 \frac{\partial u_0}{\partial x} + v_0 \frac{\partial u_0}{\partial y} + w_0 \cancel{\frac{\partial u_0}{\partial z}} - v_1 = -\frac{\partial p_1}{\partial x} \quad (1)$$

$$\frac{\partial v_0}{\partial t} + u_0 \frac{\partial v_0}{\partial x} + v_0 \frac{\partial v_0}{\partial y} + w_0 \cancel{\frac{\partial v_0}{\partial z}} + u_1 = -\frac{\partial p_1}{\partial y} \quad (2)$$

$$\frac{\partial u_1}{\partial x} + \frac{\partial v_1}{\partial y} + \frac{\partial w_1}{\partial z} = 0$$

$$z' = 0 \quad \text{SBL}$$

interior

$$\frac{\partial(2)}{\partial x} - \frac{\partial(1)}{\partial y} :$$

$$\frac{d\zeta_0}{dt} = - \left(\frac{\partial u_1}{\partial x} + \frac{\partial v_1}{\partial y} \right) = \frac{\partial w_1}{\partial z} = \frac{w_1|_{z'=0} - w_1|_{z'=-1}}{1}$$

$$z' = -1 \quad \text{BBL}$$

$$\frac{d\zeta_0}{dt} = w_1|_{z=0} - w_1|_{z=-1}$$

The Ekman pumping velocity in the bottom boundary layer is:

$$w|_{z'=-1} = \frac{d}{2} \left(\frac{\partial \bar{v}}{\partial x} - \frac{\partial \bar{u}}{\partial y} \right) = \frac{1}{2} \sqrt{\frac{2A_v}{f}} \bar{\zeta} = \frac{H}{2} E_v^{1/2} \bar{\zeta} \quad E_v = \frac{2A_v}{fH^2}$$

$$Ww'|_{z'=-1} = \frac{H}{2} E_v^{1/2} \frac{U}{L} \left(\frac{\partial v_0}{\partial x'} - \frac{\partial u_0}{\partial y'} \right)$$

$$w'|_{z'=-1} = \frac{1}{2} \cancel{\frac{H}{W}} \cancel{\frac{U}{L}} E_v^{1/2} \left(\frac{\partial v_0}{\partial x'} - \frac{\partial u_0}{\partial y'} \right)$$

Remove the symbol ':

$$w|_{z=-1} = \frac{1}{2} E_v^{1/2} \zeta_0 = w_0|_{z=-1} + \varepsilon w_1|_{z=-1}$$

$$\frac{\partial w_0}{\partial z} = 0$$

$$w_0|_{z=-1} = 0 \quad \longrightarrow \quad w_0 = 0$$



$$w_1|_{z=-1} = \frac{E_v^{1/2}}{2\varepsilon} \zeta_0$$

The Ekman pumping velocity for the surface boundary layer is:

$$\begin{aligned}
 w|_{z=0} &= \frac{1}{\rho_0 f} \left(\frac{\partial \tau^y}{\partial x} - \frac{\partial \tau^x}{\partial y} \right) = \frac{1}{\rho_0 f} \left(\frac{\partial}{\partial x} \left(\rho_0 A_v \frac{\partial v}{\partial z} \right) - \frac{\partial}{\partial y} \left(\rho_0 A_v \frac{\partial u}{\partial z} \right) \right) \\
 &= \frac{A_v}{f} \left(\frac{\partial}{\partial x} \left(\frac{v_s - \bar{v}}{d} \right) - \frac{\partial}{\partial y} \left(\frac{u_s - \bar{u}}{d} \right) \right) \\
 &= \frac{A_v}{fd} (\zeta_s - \bar{\zeta}) \quad d = \sqrt{\frac{2A_v}{f}}
 \end{aligned}$$

$$E_v = \frac{2A_v}{fH^2} = \frac{1}{2} \sqrt{\frac{2A_v}{f}} (\zeta_s - \bar{\zeta}) = \frac{1}{2} E_v^{\frac{1}{2}} H (\zeta_s - \bar{\zeta})$$

$$Ww'|_{z'=0} = \frac{1}{2} E_v^{\frac{1}{2}} H \frac{U}{L} (\zeta_s' - \zeta_0) \quad \longrightarrow \quad w'|_{z'=0} = \frac{1}{2} E_v^{\frac{1}{2}} (\zeta_s' - \zeta_0)$$

$w_0 = 0$

Remove the symbol ':

$$w|_{z=0} = w_0|_{z=0} + \varepsilon w_1|_{z=0} = \frac{1}{2} E_v^{\frac{1}{2}} (\zeta_s - \zeta_0)$$

$$w_1|_{z=0} = \frac{E_v^{\frac{1}{2}}}{2\varepsilon} (\zeta_s - \zeta_0)$$

$$\frac{d\zeta_0}{dt} = w_1|_{z=0} - w_1|_{z=-1}$$

$$w_1|_{z=0} = \frac{E_v^{\frac{1}{2}}}{2\varepsilon} (\zeta_s - \zeta_0)$$

$$w_1|_{z=-1} = \frac{E_v^{\frac{1}{2}}}{2\varepsilon} \zeta_0$$

$$\frac{d\zeta_0}{dt} = -\frac{E_v^{\frac{1}{2}}}{\varepsilon} \left(\zeta_0 - \frac{1}{2} \zeta_s \right) = -r \left(\zeta_0 - \frac{1}{2} \zeta_s \right)$$

If the surface forcing disappears ($\zeta_s = 0$) : $\frac{d\zeta_0}{dt} = -r\zeta_0$ $\zeta_0 = \zeta_c e^{-rt}$

Circulation:

$$C = \oint \mathbf{u}_0 d\mathbf{r} = \iint \zeta_0 dS$$

geostrophic flow is non-divergent

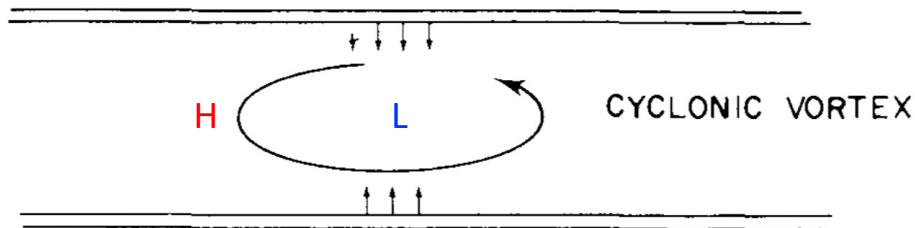
$$\frac{dC}{dt} = \iint \frac{d\zeta_0}{dt} dS + \iint \zeta_0 \frac{d}{dt} (dS) = \iint -r\zeta_0 dS = -rC \quad \longrightarrow \quad C = C_0 e^{-rt}$$

Spindown time (decay timescale of the flow or vorticity):

$$\zeta_0 = \zeta_c e^{-rt} = \zeta_c e^{-\frac{t}{1/r}}$$

The e-folding decay timescale: $\tau = \frac{1}{r} = \frac{\varepsilon}{E_v^{\frac{1}{2}}} = \frac{U/fL}{E_v^{\frac{1}{2}}} = \frac{1/fT}{E_v^{\frac{1}{2}}} \sim O(1)$ $T \sim \frac{1}{f E_v^{\frac{1}{2}}}$

larger E_v , smaller T , faster dissipation of vorticity and kinetic energy

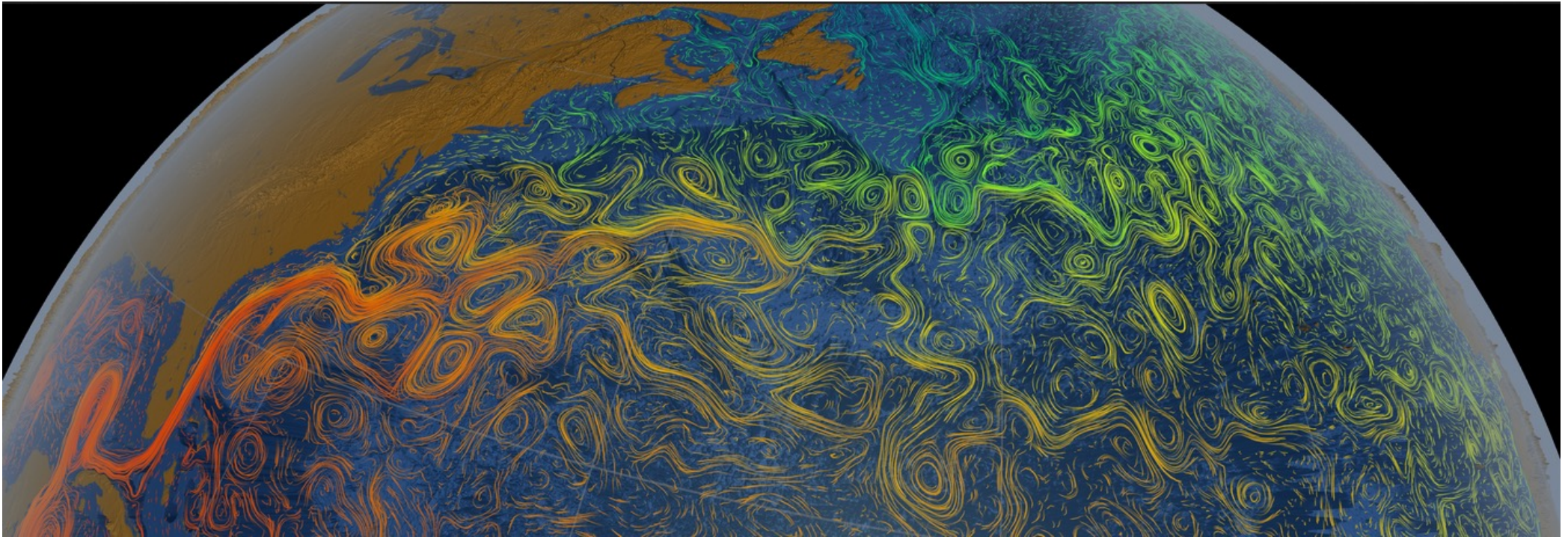


$$w_1|_{z=-1} = \frac{E_v^{\frac{1}{2}}}{2\varepsilon} \zeta_0 > 0 \quad w_1|_{z=0} = -\frac{E_v^{\frac{1}{2}}}{2\varepsilon} \zeta_0 < 0$$

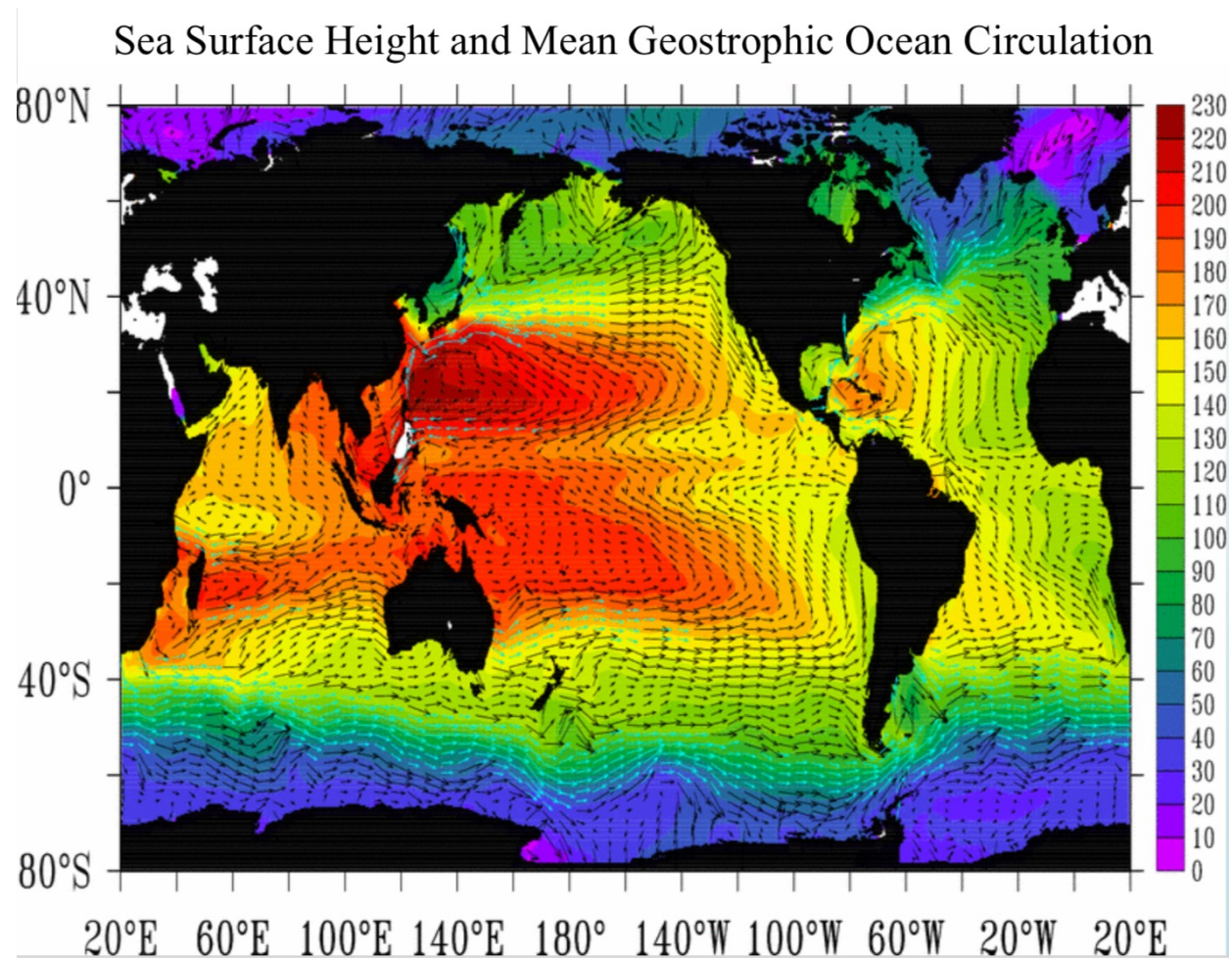
The water column is squeezed ($h \downarrow$), and for PV conservation, $\zeta_0 \downarrow$

The pressure gradient force does negative work, flow deaccelerates

The spindown timescale determines the life time of eddies



Dynamics for the subtropical gyre



For the interior ocean (shallow-water model):

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} - f v = -\frac{1}{\rho_0} \frac{\partial p'}{\partial x}$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + f u = -\frac{1}{\rho_0} \frac{\partial p'}{\partial y}$$

Take the curl of the equation:

$$\frac{\partial}{\partial t} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) + \frac{\partial u}{\partial x} \frac{\partial v}{\partial x} + u \frac{\partial^2 v}{\partial x^2} - \frac{\partial u}{\partial y} \frac{\partial u}{\partial x} - u \frac{\partial^2 u}{\partial x \partial y} + \frac{\partial v}{\partial x} \frac{\partial v}{\partial y} + v \frac{\partial^2 v}{\partial x \partial y} - \frac{\partial v}{\partial y} \frac{\partial u}{\partial y} - v \frac{\partial^2 u}{\partial y^2} + f \frac{\partial u}{\partial x} + \frac{\partial f}{\partial y} v + f \frac{\partial v}{\partial y} = 0$$

$$\frac{\partial \zeta}{\partial t} + \frac{\partial u}{\partial x} \zeta + u \frac{\partial \zeta}{\partial x} + \frac{\partial v}{\partial y} \zeta + v \frac{\partial \zeta}{\partial y} + f \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + \beta_0 v = 0$$

$$\frac{d\zeta}{dt} + \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) (f + \cancel{\zeta}) + \beta_0 v = 0 \quad \text{large scale: } \zeta \ll f$$

$$\frac{d\zeta}{dt} + \beta_0 v = f \frac{\partial w}{\partial z}$$

$$\frac{d\zeta}{dt} + \beta_0 v = f \frac{\partial w}{\partial z}$$

$$z = z_1$$

SBL

interior

Take the vertical integral, and given that $\frac{\partial u}{\partial z} = \frac{\partial v}{\partial z} = 0, \frac{\partial \zeta}{\partial z} = 0$

$$z = z_0$$

BBL

$$\begin{aligned} \left(\frac{d\zeta}{dt} + \beta_0 v \right) H &= f (w|_{z_1} - w|_{z_0}) \\ &= f \left\{ \frac{1}{\rho_0} \left[\frac{\partial}{\partial x} \left(\frac{\tau^y}{f} \right) - \frac{\partial}{\partial y} \left(\frac{\tau^x}{f} \right) \right] - \frac{d}{2} \zeta \right\} \\ &= f \left\{ \frac{1}{\rho_0 f} \frac{\partial \tau^y}{\partial x} - \frac{1}{\rho_0 f} \frac{\partial \tau^x}{\partial y} + \frac{\tau^x}{\rho_0 f^2} \beta_0 - \frac{d}{2} \zeta \right\} \end{aligned}$$

Define non-dimensional variables:

$$(u, v) = U(u', v') \quad (x, y) = L(x', y') \quad t = T t' \quad \tau = \tau_0 \tau'$$

$$H \left(\frac{U}{LT} \frac{d\zeta'}{dt'} + \beta_0 U v' \right) = \frac{1}{\rho_0} \frac{\tau_0}{L} \text{curl} \tau' + \frac{\tau_0}{\rho_0 f} \beta_0 \tau^{x'} - \frac{d}{2} f \frac{U}{L} \zeta'$$

$$H \left(\frac{U}{LT} \frac{d\zeta'}{dt} + \beta_0 U v' \right) = \frac{1}{\rho_0} \frac{\tau_0}{L} \text{curl} \tau' + \frac{\tau_0}{\rho_0 f} \beta_0 \tau^{x'} - \frac{d}{2} f \frac{U}{L} \zeta'$$

$$H \frac{U^2}{L^2} \left(\frac{d\zeta'}{dt} + \frac{\beta_0 L^2}{U} v' \right) = \frac{\tau_0}{\rho_0 L} \left(\text{curl} \tau' + \frac{\beta_0 L}{f} \tau^{x'} \right) - \frac{d}{2} f \frac{U}{L} \zeta'$$

$$\frac{d\zeta'}{dt} + \frac{\beta_0 L^2}{U} v' = \frac{\tau_0 L}{\rho_0 H U^2} \left(\text{curl} \tau' + \frac{\beta_0 L}{f} \tau^{x'} \right) - \frac{1}{2} \frac{f L}{U} \frac{d}{H} \zeta'$$

β $<< 1$ $-\frac{1}{2} \frac{1}{R_o} E_k^{1/2} \zeta'$

$$E_k = \frac{v_E}{f H^2}$$

$$d = \sqrt{\frac{v_E}{f}} = E_k^{1/2} H$$

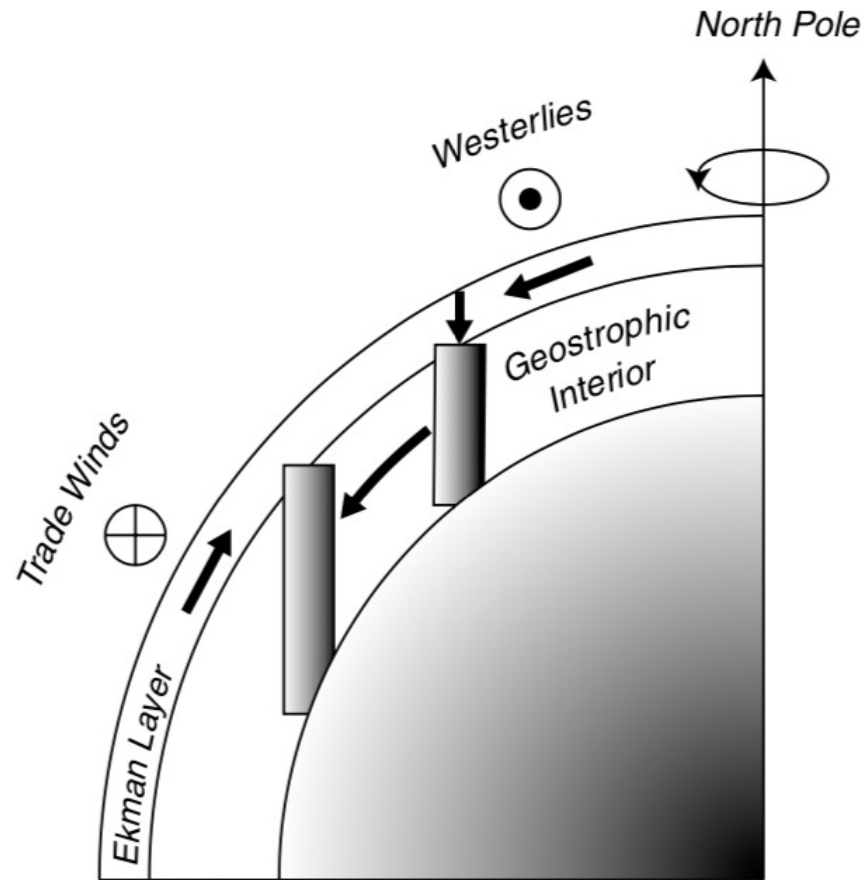
Remove the prime symbol '

$$\cancel{\frac{d\zeta}{dt}} + \beta v = \frac{\tau_0 L}{\rho_0 H U^2} \text{curl} \tau - \cancel{r \zeta}$$

For steady, large-scale flow, and assuming the bottom friction is negligible:

$$v = \text{curl} \tau$$

Sverdrup balance



$$\frac{d}{dt} \left(\frac{f + \zeta}{h} \right) = 0$$

Figure 12.7 Ekman pumping that produces a downward velocity at the base of the Ekman layer forces the fluid in the interior of the ocean to move southward. (From Niiler, 1987)

How about at the lateral boundaries?

Lateral boundaries:

$$\text{West: } x = X_w(y)$$

$$\text{East: } x = X_E(y)$$

$$x - X_w(y) = 0$$

$$x - X_E(y) = 0$$

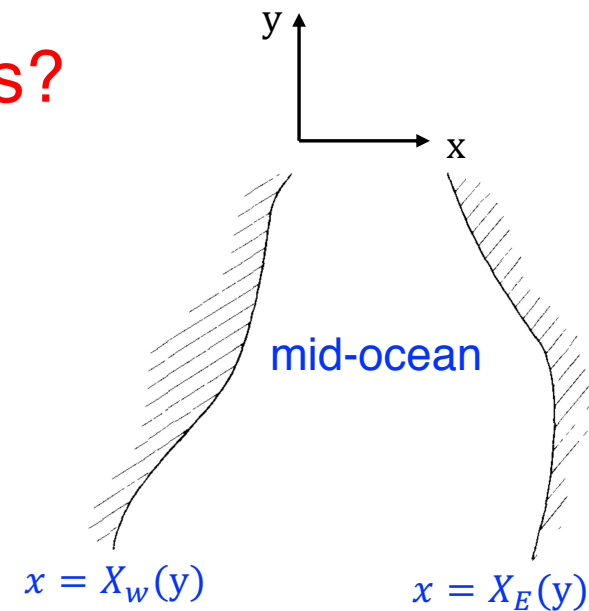
No normal flows:

$$\mathbf{u} \cdot \nabla(x - X_w(y)) = 0 \longrightarrow u - v \frac{\partial X_w}{\partial y} = 0 \text{ at } x = X_w$$

$$\mathbf{u} \cdot \nabla(x - X_E(y)) = 0 \longrightarrow u - v \frac{\partial X_E}{\partial y} = 0 \text{ at } x = X_E$$

For interior geostrophic flow:

$$\frac{\partial u}{\partial x} = -\frac{\partial v}{\partial y} = -\frac{\partial \text{curl} \tau}{\partial y}$$



For a point in the mid-ocean x_0 :

$$\int_{x_0}^x \frac{\partial u}{\partial x} dx' = - \int_{x_0}^x \frac{\partial \text{curl} \tau}{\partial y} dx'$$

$$u(x, y) = - \int_{x_0}^x \frac{\partial \text{curl} \tau}{\partial y} dx' + U(x_0, y) \quad \text{unknown, and needs to be determined}$$

If the Sverdrup relation is valid at the eastern boundary: $u = v \frac{\partial X_E}{\partial y}$ at $x = X_E$

$$- \int_{x_0}^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + U(x_0, y) = v \frac{\partial X_E}{\partial y} = \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y}$$

$$U(x_0, y) = \int_{x_0}^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y}$$

$$u(x, y) = - \int_{x_0}^x \frac{\partial \text{curl} \tau}{\partial y} dx' + \int_{x_0}^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y}$$

$$= \int_x^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y}$$

$$u(x, y) = \int_x^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y}$$

If the Sverdrup relation is also valid at the western boundary: $u = v \frac{\partial X_W}{\partial y}$ at $x = X_W$

$$u(X_W, y) = \int_{X_W}^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y} = v \frac{\partial X_W}{\partial y} = \text{curl} \tau(X_W, y) \frac{\partial X_W}{\partial y}$$

$$\int_{X_W}^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y} - \text{curl} \tau(X_W, y) \frac{\partial X_W}{\partial y} = 0$$

$$\frac{\partial}{\partial y} \int_{X_W}^{X_E} \text{curl} \tau dx' = 0$$

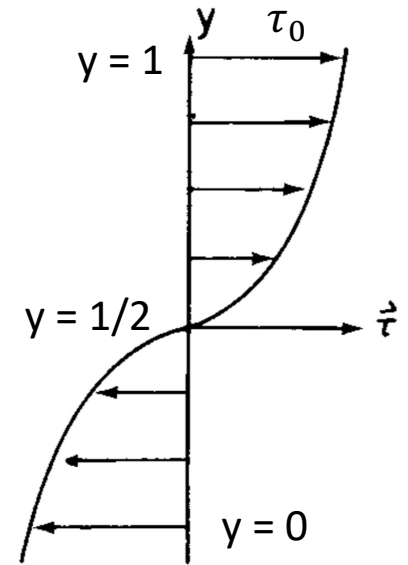
condition for Sverdrup relation to be valid at both boundaries

$$\frac{\partial}{\partial y} \int_{X_W}^{X_E} \text{curl} \tau dx' = 0$$

For the trade wind and westerly wind:

$$\tau = (-\tau_0 \cos \pi y, \quad 0) \quad \begin{array}{l} 0 < y < 1 \\ 0 < \pi y < \pi \end{array}$$

$$v = \text{curl} \tau = -\frac{\partial \tau^x}{\partial y} = -\pi \tau_0 \sin \pi y < 0$$



$$\frac{\partial}{\partial y} \int_{X_W}^{X_E} \text{curl} \tau dx' = \frac{\partial}{\partial y} \int_{X_W}^{X_E} -\pi \tau_0 \sin \pi y dx' = -\pi^2 \tau_0 \cos \pi y (X_E - X_W)$$

only =0 at $y=1/2$

Sverdrup relation cannot hold at both boundaries

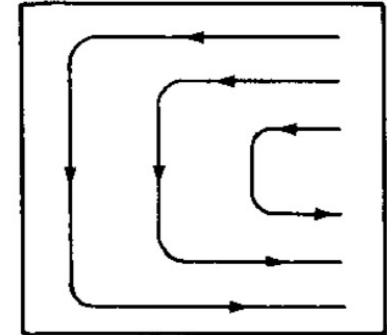
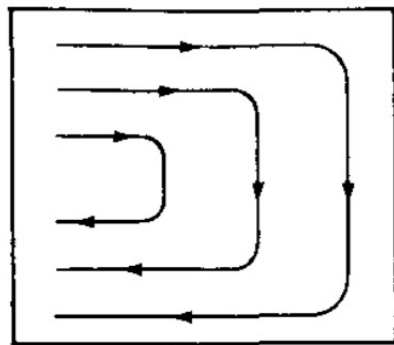
If Sverdrup relation holds at the eastern boundary:

$$u(x, y) = \int_x^{X_E} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_E, y) \frac{\partial X_E}{\partial y}$$

straight coastline $X_E = C$

$$\text{curl} \tau = -\frac{\partial \tau^x}{\partial y} = -\pi \tau_0 \sin \pi y$$

$$= \frac{\partial}{\partial y} \int_x^{X_E} \text{curl} \tau dx' = -\pi^2 \tau_0 \cos \pi y (X_E - x) \quad \begin{cases} > 0, y > 1/2 \\ < 0, y < 1/2 \end{cases}$$



If Sverdrup relation holds at the western boundary:

opposite to the wind direction (X)

$$u(x, y) = \int_x^{X_W} \frac{\partial \text{curl} \tau}{\partial y} dx' + \text{curl} \tau(X_W, y) \frac{\partial X_W}{\partial y}$$

straight coastline $X_W = C$

$$= \frac{\partial}{\partial y} \int_x^{X_W} \text{curl} \tau dx' = -\pi^2 \tau_0 \cos \pi y (X_W - x) \quad \begin{cases} < 0, y > 1/2 \\ > 0, y < 1/2 \end{cases}$$

Stommel's model for western boundary intensification — **bottom friction**

$$\cancel{\frac{d\zeta}{dt}} + \beta v = \frac{\tau_0 L}{\rho_0 H U^2} \text{curl} \tau - r \zeta$$

For the boundary layers, retain bottom friction, and divide the equation by β :

$$v = \text{curl} \tau - \frac{r}{\beta} \zeta$$

For geostrophic flow:

$$\frac{\partial \psi}{\partial x} = \text{curl} \tau - \varepsilon_s \nabla^2 \psi$$

$$\psi = \underline{\psi_I(x, y)} + \underline{\psi_B(x, y)} \quad \text{boundary layer correction}$$

interior (mid-ocean) solution

$$\frac{\partial \psi_I}{\partial x}(x, y) = \text{curl} \tau$$

$$\varepsilon_s(\nabla^2\psi_I + \nabla^2\psi_B) + \cancel{\frac{\partial\psi_I}{\partial x}} + \frac{\partial\psi_B}{\partial x} = \cancel{\text{curl}\tau}$$

West: $\alpha = \frac{x-0}{\varepsilon} \sim O(1)$ $\frac{\partial}{\partial x} = \frac{1}{\varepsilon} \frac{\partial}{\partial \alpha}$ $\frac{\partial^2}{\partial x^2} = \frac{1}{\varepsilon^2} \frac{\partial^2}{\partial \alpha^2}$ ε : boundary layer thickness ($\ll 1$)

East: $\alpha = \frac{x-1}{\varepsilon} \sim O(1)$

$$\varepsilon_s \left(\cancel{\nabla^2\psi_I} + \frac{1}{\varepsilon^2} \frac{\partial^2\psi_B}{\partial \alpha^2} + \cancel{\frac{\partial^2\psi_B}{\partial y^2}} \right) + \frac{1}{\varepsilon} \frac{\partial\psi_B}{\partial \alpha} = 0$$

Only retain the large terms:

$$\frac{\partial^2\psi_B}{\partial \alpha^2} + \frac{\partial\psi_B}{\partial \alpha} = 0$$

$$\frac{\partial^2 \psi_B}{\partial \alpha^2} + \frac{\partial \psi_B}{\partial \alpha} = 0$$

$$\psi_B = A(y)e^{\lambda\alpha} \longrightarrow \lambda^2 + \lambda = 0 \longrightarrow \lambda = -1$$

$$\psi_B = A(y)e^{-\alpha}$$

If ψ_B applies to the western boundary: $\alpha = \frac{x-0}{\varepsilon} > 0$

ψ_B decays exponentially toward the mid-ocean ✓

If ψ_B applies to the eastern boundary: $\alpha = \frac{x-1}{\varepsilon} < 0$

ψ_B grows exponentially toward the mid-ocean ✗

The correction applies to the western boundary, and Sverdrup relation holds for the eastern boundary

For the interior and the eastern boundary: $\frac{\partial \psi_I}{\partial x}(x, y) = \text{curl} \tau$

$$\int_x^1 \frac{\partial \psi_I}{\partial x} dx' = \int_x^1 \text{curl} \tau dx'$$

$$\text{curl} \tau = -\frac{\partial \tau^x}{\partial y} = -\pi \tau_0 \sin \pi y$$

$$\psi_I(1, y) - \psi_I(x, y) = -\pi \tau_0 \sin \pi y (1 - x)$$

$$\psi_I(x, y) = \pi \tau_0 \sin \pi y (1 - x)$$

At the western boundary: $\psi_B = A(y)e^{-\alpha}$

$$\psi(0, y) = \psi_I(0, y) + \psi_B(0, y) = \pi \tau_0 \sin \pi y + A(y) = 0$$

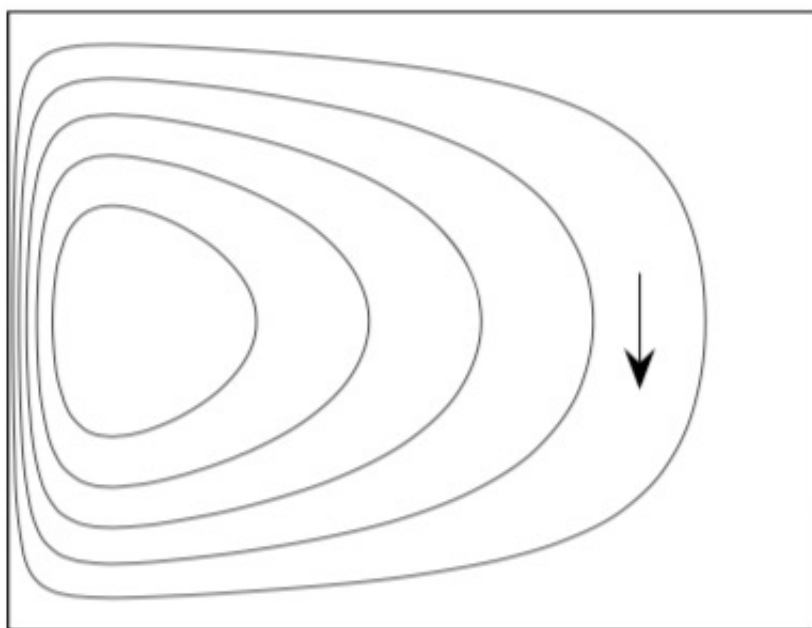
$$A(y) = -\pi \tau_0 \sin \pi y$$

$$\alpha = \frac{x - 0}{\varepsilon}$$

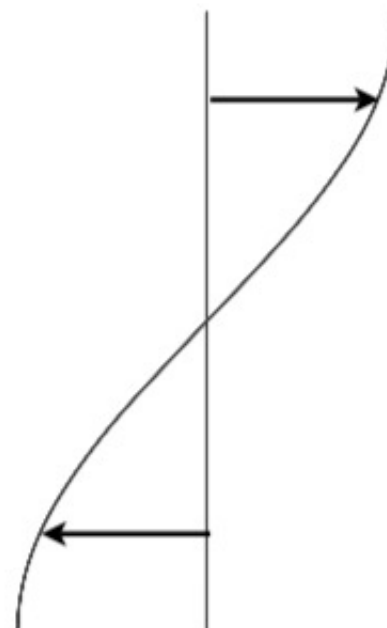
$$\psi(x, y) = \psi_I(x, y) + \psi_B(x, y) = \pi \tau_0 \sin \pi y (1 - x) - \pi \tau_0 \sin \pi y e^{-x/\varepsilon}$$

$$= (1 - x - e^{-x/\varepsilon}) \pi \tau_0 \sin \pi y$$

Streamfunction



Wind stress



Vorticity dynamics

$$\frac{d}{dt} \left(\frac{f + \zeta}{h} \right) = 0$$

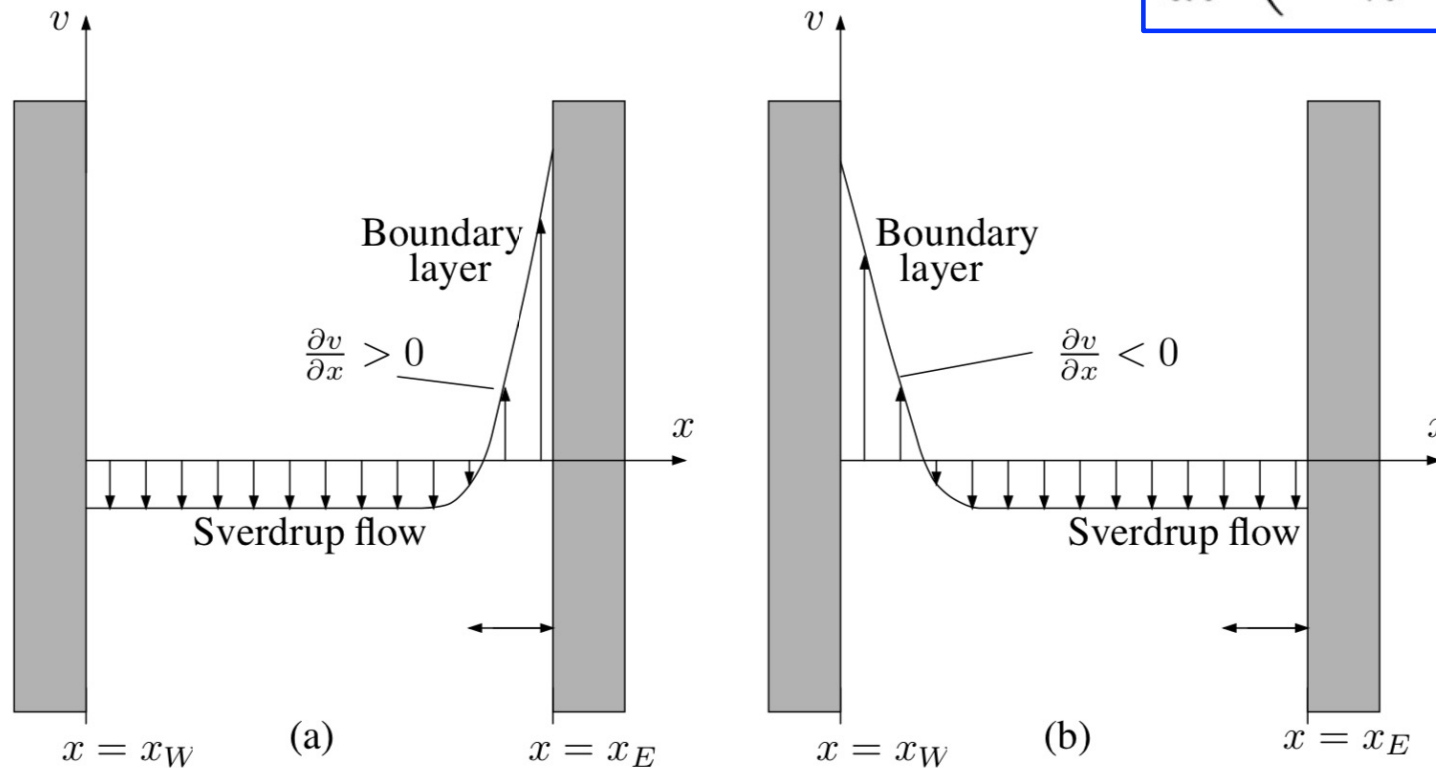


Figure 20-7 The two possible configurations for a northward boundary current to return the southward Sverdrup flow that exists across most of an ocean basin in the mid-latitudes of the Northern Hemisphere: (a) boundary current on the eastern side, (b) boundary current on the western side. The former is to be rejected on dynamic grounds, leaving the latter as the correct configuration.