

Linear Stability Analysis for Planar Interface - Solidification of Dilute Binary Alloy

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1 Directional Solidification

Assume a planar interface moving at a constant velocity 'V'. The steady state Species Transfer Equation,

$$\frac{\partial C_i}{\partial t} = D_{ii} \nabla^2 C_i = 0 \quad (1)$$

Transforming to a moving co-ordinate system,

$$D_{ii} \nabla^2 C_i + V \frac{dC_i}{dz} = 0 \quad (2)$$

Boundary Conditions,

$$C_i = C_{i,eq}^l \quad \text{at } z = 0 \quad (3)$$

$$VC_{i,eq}^l(1 - k_i) = -D_{ii} \left. \frac{dC_i}{dz} \right|_{z=0} = -D_{ii} G_{c,i} \quad \text{at } z = 0 \quad (4)$$

Solution is given by,

$$C_i = C_{i,eq}^l + \frac{G_{c,i} D_{ii}}{V} \left[1 - \exp \left(\frac{-Vz}{D_{ii}} \right) \right] \quad (5)$$

Adding a linear perturbation

Assume a infinitesimally small sinusoidal noise on the planar interface normal to 'z'. Now the interface is no more $z = 0$ rather it is at $z = \Phi$ where,

$$z = \Phi = \delta(t) \sin(\omega x) \quad (6)$$

Now the diffusion equation becomes,

$$D_{ii} \nabla^2 \tilde{C}_i + V \frac{\partial \tilde{C}_i}{\partial z} = 0 \quad (7)$$

Boundary Conditions,

$$C_{i,\Phi} = C_{i,eq}^l + b_i \delta \sin(\omega x) \quad \text{at } z = \Phi \quad (8)$$

$$(V + \delta \sin(\omega x)) C_{i,\Phi}^l (1 - k_i) = -D_{ii} \left. \frac{d\tilde{C}_i}{dz} \right|_{z=\Phi} \quad \text{at } z = \Phi \quad (9)$$

The interface equilibrium concentration will be no longer constant and will be a function of the curvature at the interface (Gibb's Thompson Condition).

The solution to these equations will be similar to Eq. 5 along with a term that ensures that the perturbation provided at the interface will die down as $z \rightarrow \infty$

$$\tilde{C}_i = C_{i,eq}^l + \frac{G_{c,i} D_{ii}}{V} \left[1 - \exp\left(\frac{-Vz}{D_{ii}}\right) \right] + E_i \sin(\omega x) \exp(-k_{w,i} z) \quad (10)$$

Substituting this in Eq. 7 we get a relation between E_i and $k_{w,i}$,

$$k_{w,i} = \frac{V}{2D_{ii}} + \sqrt{\left(\frac{V}{2D_{ii}}\right)^2 + \omega^2} \quad (11)$$

We can write E_i in terms of b_i , by equating Eq.8 and Eq.10 and using the approximation $\exp(x) = 1 + x$ for small x ,

$$E_i = \delta(b_i - G_{c,i}) \quad (12)$$

Now, we solve for the other boundary condition (i.e Stefan condition, Eq. 9). Before this a small simplification using binomial approx. can be performed on Eq. 8,

$$\frac{1}{C_{i,\Phi}^l} = \frac{1}{C_{i,eq}^l (1 + \frac{b_i \delta}{C_{i,eq}^l} \sin(\omega x))} \quad (13)$$

$$\frac{1}{C_{i,\Phi}^l} = \frac{1}{C_{i,eq}^l} \left(1 - \frac{b_i \delta}{C_{i,eq}^l} \sin(\omega x) \right) \quad (14)$$

Finally, on solving Eq. 9, we arrive at,

$$\left. \frac{d\tilde{C}_i}{dz} \right|_{z=\Phi} = G_{c,i} \left(1 - \frac{V \delta \sin(\omega x)}{D_{ii}} \right) - k_{w,i} E_i \sin(\omega x) (1 - \delta \sin(\omega x)) \quad (15)$$

$$\left. \frac{d\tilde{C}_i}{dz} \right|_{z=\Phi} = G_{c,i} - \left(\frac{G_{c,i} V}{D_{ii}} + k_{w,i} (b_i - G_{c,i}) \right) \delta \sin(\omega x) \quad (16)$$

$$V + \delta \sin(\omega x) = \frac{-D_{ii}}{C_{i,eq}^l (1 - k_i)} \left(1 - \frac{b_i \delta}{C_{i,eq}^l} \sin(\omega x) \right) \left(G_{c,i} - \left(\frac{G_{c,i} V}{D_{ii}} + k_{w,i} (b_i - G_{c,i}) \right) \delta \sin(\omega x) \right) \quad (17)$$

$$\frac{\dot{\delta}}{\delta} = V\tilde{\omega} \left[-\frac{b_i}{G_{c,i}} + \frac{1}{\tilde{\omega}} \left(k_{\omega,i} - \frac{V}{D_{ii}} \right) \right] \quad (18)$$

where $\tilde{\omega} = k_{\omega,i} - \frac{V}{D_{ii}}(1 - k_i)$. Now the only unknown is b_i . But, the term $\frac{\dot{\delta}}{\delta}$ is constant for all the components, so any component $i! = 1$ should be equal to $i = 1$,

$$V\tilde{\omega} \left[-\frac{b_i}{G_{c,i}} + \frac{1}{\tilde{\omega}} \left(k_{\omega,i} - \frac{V}{D_{ii}} \right) \right] = V\tilde{\omega} \left[-\frac{b_1}{G_{c,1}} + \frac{1}{\tilde{\omega}} \left(k_{\omega,1} - \frac{V}{D_{11}} \right) \right] \quad (19)$$

$$b_i = \frac{G_{c,i}}{\tilde{\omega}_i} \left[\frac{b_1}{G_{c,1}} \tilde{\omega}_i + \left(k_{w,i} - \frac{V}{D_{ii}} \right) - \left(k_{w,1} - \frac{V}{D_{11}} \right) \right] \quad (20)$$

Now the only unknown is b_1 and this can be found with the condition of local equilibrium,

$$T|_{z=\phi} - (T_{pure} + \sum_i m_i^l (C_{i,\phi}^{\tilde{l}})) = -\Gamma\kappa \quad (21)$$

$$T|_{z=0} + G\delta \sin(\omega z) - (T_m + \sum_i m_i^l b_i \delta \sin(\omega x)) = -\Gamma\delta\omega^2 \sin(\omega x) \quad (22)$$

Comparing the coefficients of $\delta \sin(\omega x)$ on both sides,

$$G + \Gamma\omega^2 = \sum_i m_i^l b_i \quad (23)$$

Now that all the values are known, we can calculate the critical frequency ω_{crit} for the stability by $\frac{\dot{\delta}}{\delta} = 0$,

$$b_i = G_{c,i} \frac{k_{w,i} - \frac{V}{D_{ii}}}{\tilde{\omega}_i} \quad (24)$$

The critical wavelength $\lambda_{crit} = 2\pi/\omega_{crit}$ and this turns out to be,

$$TBD \quad (25)$$

2 Assumptions

1. The bulk and surface parameters are assumed to be isotropic
2. Analysis carried out when the system is in a steady state in both temperature and composition. (These calculations are valid only when the dendrite shape changes slowly)