# A Bootstrapped Switch with Accelerated Rising Speed and Reduced On-Resistance

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Abstract—This paper presents a bootstrapped switch with an accelerated gate-voltage rising speed and a reduced onresistance for high-speed ADCs. Compared to the classic bootstrapped switch, this design accelerates the rising speed of gate voltage through four novel techniques. First, an extra NMOS transistor is added to pull up the gate voltage by injecting extra charges into the gate node. Second, the parasitic capacitance at the gate node is reduced by simplifying the circuit structure, leading to a faster speed. Third, transmission gates are used to reduce the two delays to one delay. Fourth, the voltage stored on the capacitor is increased to slightly larger than  $V_{DD}$ , which leads to a faster gate-voltage rising speed as well as a larger value of gate voltage (about  $V_{in}+1.05V_{DD}$ ). The larger gate voltage also helps reduce the on-resistance of the bootstrapped switch, which is helpful for the high-speed sampling of ADCs. In a 40 nm CMOS process, post-layout simulation results show that the rising speed of gate voltage is increased by 3.3 times compared to the classic thin-oxide bootstrapped switch circuit. And the on-resistance of the bootstrapped switch is reduced by 2.2 times compared to the classic structure, due to the larger gate voltage value.

Keywords—Bootstrapped Switch; High-Speed; Reduced On-Resistance; Rising Speed Acceleration.

### I. INTRODUCTION

Due to the development of communication industry, high-speed analog-to-digital converter (ADC) is of great interest over the past decade. In such ADCs, the sample-and-hold circuit is indispensable and has a significant influence on the ADC performance, such as the sampling rate and resolution. To improve resolution, bootstrapped switches, instead of CMOS switches, are widely used, thanks to the low and constant on-resistance.

In recent years, there are many techniques reported to enhance the performance of bootstrapped switches, such as [1]-[14]. These works mainly focus on the sampling accuracy, rather than the sampling rate, of bootstrapped switch circuits. However, in high-speed medium-resolution ADCs (6~8 bits, several GHz), such as [15]-[18], the sampling rate is the top priority, while the sampling accuracy is secondary. Thus, the goal of this paper is to increase the sampling rate.

The sampling rate of a bootstrapped switch depends on three factors: the size of sampling capacitor, the on-resistance of the bootstrapped switch, and the gate-voltage rising speed of bootstrapped switch (rises from 0 to  $V_{in}+V_{DD}$ ). Among them, the first factor can hardly be improved for faster sampling rate, because this factor is already determined by the allowed maximum kT/C noise and capacitance mismatch due to the target ADC resolution. By contrast, the last two factors can be easily improved for faster sampling rate. For example, we can increase the gate voltage value to slightly larger than  $V_{in}+V_{DD}$  (for example  $V_{in}+1.05V_{DD}$ ), rather than slightly smaller than  $V_{in}+V_{DD}$  (for example  $V_{in}+0.8V_{DD}$ ) as in a conventional structure (due to the coupling of parasitic capacitance). This

helps reduce the on-resistance of the bootstrapped switch. Note that the slightly larger gate voltage value will not cause the aging effect of transistor, because the voltage across transistor is at most  $1.05\,V_{DD}$  and thus it is still much smaller than the upper limit of valid bias range, according to the PDK. In sum, this paper focuses on how to improve the last two factors for a faster sampling rate.

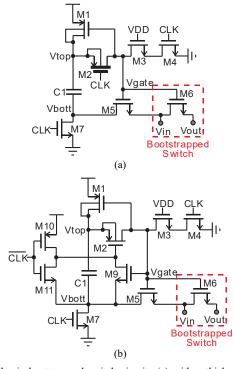


Fig. 1. Classic bootstrapped switch circuits (a) with a thick-oxide MOS transistor and (b) with thin-oxide MOS transistors only.

Fig. 1 shows two classic bootstrapped switch circuits, where Fig. 1(a) [2] shows the bootstrapped switch with a thick-oxide MOSFET M2, and Fig. 1(b) [3] shows the bootstrapped switch with thin-oxide MOSFETs only. In Fig. 1(a), the thick oxide of M2 is used to prevent M2 from being broken down, because the voltage across M2 can be as large as  $2V_{DD}$ , and a thick-oxide MOSFET has a larger breakdown voltage of  $4V_{DD}$ . By contrast, in Fig. 1(b), a more complicated structure is used to prevent the voltage across M2 from being as large as  $2V_{DD}$ , thus the thick oxide is no longer needed for M2. The principle of Fig. 1(a) and Fig. 1(b) are similar. During the reset phase (CLK=1), the voltage across the capacitor C1 is reset to  $V_{DD}$ , and the gate voltage  $V_{gate}$  of the bootstrapped switch is reset to 0V. During the bootstrap phase (CLK=0), M5 is turned on to connect the bottom plate of capacitor C1 to  $V_{in}$ , so that the top plate of capacitor C1 is  $V_{in}+V_{DD}$ . And then, M2 is turned on to transmit  $V_{in}+V_{DD}$  to the gate voltage  $V_{gate}$ of the switch. Since the on-resistance of a thin-oxide MOSFET is much smaller (3.7 times) than a thick-oxide MOSFET, the gate-voltage rising speed of Fig. 1(b) is much faster than Fig. 1(a). Simulation results in 40 nm CMOS show

that the gate-voltage rising speed of Fig. 1(b) is 2.1 times faster than Fig. 1(a). Thus, the proposed structure in this paper is based on the thin-oxide version of Fig. 1(b).

For a faster sampling rate, this paper proposes four novel techniques. Firstly, an additional NMOS transistor is added to pull up the gate voltage of the bootstrapped switch, by injecting extra charges into the gate node. Secondly, the parasitic capacitance at the gate node is reduced by simplifying the circuit structure, thus leading to a faster speed. Thirdly, transmission gates are used to further reduce the delay. Fourthly, the voltage stored on the capacitor is increased to slightly larger than  $V_{DD}$ , which helps increase the gate-voltage rising speed as well as reduce the on-resistance of the bootstrapped switch. Designed in a 40nm CMOS process, the proposed bootstrapped switch circuit increases the gate voltage value to  $V_{in}+1.05V_{DD}$ . Compared to the conventional structure of Fig. 1(b), the gate-voltage rising speed is increased by 3.3 times, and the on-resistance of bootstrapped switch is decreased by 2.2 times.

This paper is organized as follows. Section II discusses the proposed bootstrapped switch and analyses the circuit principle. Section III shows the post-layout simulation results and compares with the state-of-the-art work. Section IV concludes the paper.

#### II. THE PROPOSED BOOTSTRAPPED SWITCH

#### A. First Version of the Proposed Bootstrapped Switch

For a faster sampling rate, Fig. 2 shows the first version of the proposed bootstrapped switch. Compared to the classic structure of Fig. 1(b), the only difference is the addition of M8 in Fig. 2 for accelerating the gate-voltage rising speed of  $V_{gate}$ . To understand the reason of adding M8, let us first review the operation of Fig. 1(b) as well as its drawbacks.

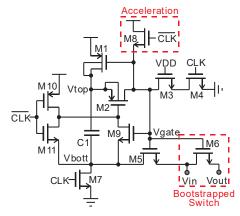


Fig. 2. First version of the proposed bootstrapped switch.

In the bootstrap phase of Fig. 1(b),  $\overline{\text{CLK}}$  rises and turns on M11, which pulls down the gate  $V_{g2}$  of M2 to the bottom plate  $V_{bott}$  of capacitor C1. At this moment, the voltage across capacitor C1 (equal to  $V_{DD}$ ) is applied onto the source-gate of M2, which turns on M2 for pulling up the gate voltage  $V_{gate}$ . This process, from the rising of  $\overline{\text{CLK}}$  to the rising of  $\overline{\text{Vgate}}$ , can be divided into two delays: the delay from the rising of  $\overline{\text{CLK}}$  to the falling of  $V_{g2}$  (pulled down by M11), and the delay from the falling of  $V_{g2}$  to the rising of  $V_{gate}$  (pulled up by M2). More seriously, before the rising of  $V_{gate}$ , M5 cannot be turned on to pull up  $V_{bott}$  to  $V_{in}$ , which means more delay required before the bootstrap process finishes.

To reduce delay, an additional transistor M8 is added into Fig. 2. Thus, at the rising edge of  $\overline{\text{CLK}}$ , M8 is turned on to pull up  $V_{gate}$  immediately. This means that, from the rising of  $\overline{\text{CLK}}$ to the rising of  $V_{gate}$ , there is only one transistor delay left. This is how M8 accelerates the  $V_{gate}$  rising speed. After that, when  $V_{gate}$  rises to above  $V_{DD}$ , M8 is turned off automatically, and no longer affects the bootstrap process. And finally,  $V_{gate}$  will rise to approximately  $V_{in}+V_{DD}$ . Another advantage of M8 is that, M8 is an NMOS transistor, and the NMOS electron mobility is 2 to 3 times larger than the PMOS hole mobility. Thus, compared to the case where only PMOS M2 is used to pull up  $V_{gate}$  as in Fig. 1(b), an additional NMOS M8 can effectively accelerate the  $V_{gate}$  rising speed. The only cost is that, M8 injects additional charges into the  $V_{gate}$  node, causing  $V_{gate}$  to slightly deviate from the desired value. And this deviation is dependent on  $V_{in}$ , which will slightly influence the ADC sampling accuracy. Nevertheless, for high-speed medium-resolution ADCs (6~8 bits, several GHz) [15]-[18], the sampling speed is the top priority, while the sampling accuracy is secondary, thus this cost can be neglected.

Under a 40nm CMOS process, simulation results show that the gate-voltage rising speed is increased by 1.1 times compared to Fig. 1(b). (see Section III for more details)

#### B. Second Version of the Proposed Bootstrapped Switch

For an even faster sampling rate, Fig. 3 shows the second version of the proposed bootstrapped switch. Compared to the first version in Fig. 2, the difference is the three modifications below.

Firstly, transistors M3, M4, and M8 in Fig. 2 are combined into one transistor M3 in Fig. 3, which realizes the same function as M3, M4, and M8. This modification helps simplify the circuit structure and reduce the parasitic capacitance at the  $V_{gate}$  node, thus accelerating the gate-voltage rising speed. The principle of this M3 in Fig. 3 is as follows. During the reset phase ( $\overline{\text{CLK}}$ =0), M3 is turned on for resetting  $V_{gate}$  to 0. During the bootstrap phase ( $\overline{\text{CLK}}$ =1), M3 is turned on for pulling up  $V_{gate}$ . After  $V_{gate}$  rises to above  $V_{DD}$ , M3 is turned off automatically, and no longer affects the bootstrap process. Finally,  $V_{gate}$  rises to approximately  $V_{in}+V_{DD}$ .

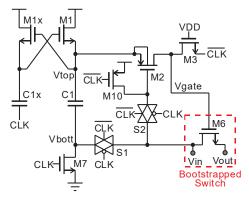


Fig. 3. Second version of the proposed bootstrapped switch.

Secondly, M5, M9, and M11 in Fig. 2 are replaced by the transmission gates S1 and S2 in Fig. 3. This modification accelerates the connection of both  $V_{g2}$  and  $V_{bott}$  to  $V_{in}$ , which further increases the gate-voltage rising speed. For easy understanding, let us first review the operation of Fig. 2. In Fig. 2, after  $\overline{\text{CLK}}$  rises, M8 is turned on to pull up  $V_{gate}$ . The rising of  $V_{gate}$  turns on M5 to pull up  $V_{bott}$  to  $V_{in}$ . This process can be divided into two delays: the delay from the rising of

 $\overline{\text{CLK}}$  to the rising of  $V_{gate}$  (pulled up by M8), and the delay from the rising of  $V_{gate}$  to the rising of  $V_{bott}$  (pulled up by M5). By contrast, in Fig. 3, after  $\overline{\text{CLK}}$  rises, the transmission gate S1 is turned on immediately to pull up  $V_{bott}$  to  $V_{in}$ , which means only one transistor delay. This helps accelerate the gate-voltage rising speed. Furthermore, in Fig. 2, after  $V_{gate}$  rises, both M5 and M9 are turned on to connect  $V_{g2}$  to  $V_{in}$ . By contrast, in Fig. 3, after  $\overline{\text{CLK}}$  rises, the transmission gate S2 is turned on immediately to connect  $V_{g2}$  to  $V_{in}$ . This realizes the same operation, while simplifying the circuit structure.

Thirdly, the PMOS M1 in Fig. 2 is replaced by an NMOS M1 in Fig. 3, whose gate voltage is generated by additional M1x and C1x. The reason for this modification is as follows. If Fig. 3 still uses a PMOS for M1, and if the gate of M1 in Fig. 3 is still connected to  $V_{gate}$  as Fig. 2 does, then M1 in Fig. 3 will be unexpectedly turned on during the bootstrap phase (CLK=1). This is because, after CLK rises, the switch S1 in Fig. 3 is immediately turned on to pull up  $V_{bott}$  to  $V_{in}$ , and pull up  $V_{top}$  to  $V_{in}+V_{DD}$  though capacitor C1. Meanwhile,  $V_{gate}$  is also pulled up to  $V_{DD}$ - $V_{th}$  by M3. This means that, M1 is turned on unexpectedly at this moment, because its drain voltage  $(V_{in}+V_{DD})$  is much larger than the gate voltage  $(V_{DD}-V_{th})$ . This unexpected state of M1 will pull down  $V_{top}$ , destroying the voltage stored on the capacitor C1. To solve this problem in Fig. 3, we replace the PMOS of M1 with an NMOS. Because the gate voltage of NMOS M1 is  $V_{DD}$  at this moment, M1 is turned off, preventing the above problem from happening again.

Under a 40nm CMOS process, simulation results show that the gate-voltage rising speed is increased by 2.6 times compared to Fig. 1(b). Furthermore, compared to Fig. 1(b) where  $V_{gate}$  only rises to  $V_{in}$ +0.71 $V_{DD}$  due to the parasitic capacitance,  $V_{gate}$  in Fig. 3 rises to  $V_{in}$ +0.81 $V_{DD}$  due to the reduced parasitic capacitance at the nodes  $V_{gate}$  and  $V_{top}$ . (see Section III for more details)

## C. Final Version of the Proposed Bootstrapped Switch

To further increase the sampling rate, Fig. 4 shows the final version of the proposed bootstrapped switch. Compared to the second version of Fig. 3, the difference is the two modifications as discussed below.

Firstly, the drain of M1 is no longer connected to  $V_{DD}$ . Instead, it is connected to VY which is larger than  $V_{DD}$ . This is to reset the top plate  $V_{top}$  of capacitor C1 to slightly larger than  $V_{DD}$  in the reset phase. As a result, during the bootstrap phase,  $V_{gate}$  can rise to slightly larger than  $V_{in}+V_{DD}$ , rather than slightly smaller than  $V_{in}+V_{DD}$  as in a conventional structure. This can effectively reduce the on-resistance of the bootstrapped switch M6.

Secondly, the source of M10 is no longer connected to  $V_{DD}$ . Instead, it is connected to  $V_{top}$  through M12. To understand the reason for this modification, let us first review Fig. 3 again. In the reset phase ( $\overline{\text{CLK}}$ =0) of Fig. 3, M10 is turned on to pull up  $V_{g2}$  to  $V_{DD}$ . This makes M2 turned off, because both the gate and source of M2 are at  $V_{DD}$  at this moment. However, in Fig. 4, the case is different, where the source of M2 (node  $V_{top}$ ) is slightly larger than  $V_{DD}$ , rather than equal to  $V_{DD}$ , making M2 fail to be turned off. To address this issue, we connect the gate of M2 to  $V_{top}$  through M10 and M12 (M10 and M12 are turned on at this moment). This ensures that M2 is turned off.

The operation of Fig. 4 is as follows. During the reset phase (CLK=1,  $\overline{\text{CLK}}$ =0), VY raises to  $2V_{DD}$  to charge  $V_{top}$ 

through M1. This makes  $V_{top}$  raise to larger than  $V_{DD}$ . Note that,  $V_{top}$  can only be charged to slightly larger than  $V_{DD}$ , rather than equal to  $2V_{DD}$ . This is because VY will decrease after the charge sharing, and the voltage across M1 is as large as  $V_{th} \approx 0.45 \text{V}$ . During the bootstrap phase (CLK=0,  $\overline{\text{CLK}}$ =1),  $V_{top}$  rises to slightly larger than  $V_{in} + V_{DD}$ , while  $V_{g2}$  is connected to  $V_{in}$ . This makes the source-gate voltage of M2 slightly larger than  $V_{DD}$  so that M2 can pull up  $V_{gate}$  at a higher speed than Fig. 3. This is another advantage of this circuit.

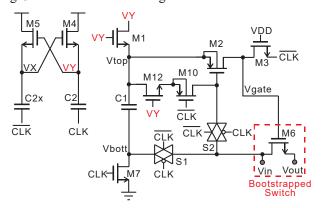


Fig. 4. Final version of the proposed bootstrapped switch.

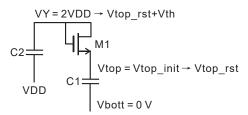


Fig. 5. Voltage values at the beginning and the end of reset phase.

For easy understanding, we derive formulas to quantitatively discuss the circuit in detail, as follows.

Ideally, for a conventional bootstrapped switch circuit, the gate voltage should rise to  $V_{in}+V_{DD}$ . However, in reality, the gate voltage can only rise to a smaller value  $V_{in}+\Delta V$  ( $\Delta V < V_{DD}$ ), due to the parasitic capacitances in the conventional circuit. Here,  $\Delta V$  can be calculated as follows:

$$\Delta V = V_{top\_rst} \frac{C1 + C_{p\_top}}{C1 + C_{p\_top} + C_{p\_gate}} - V_{in} \frac{C_{p\_top} + C_{p\_gate}}{C1 + C_{p\_top} + C_{p\_gate}}$$
(1)

where  $V_{top\_rst}$  is the  $V_{top}$  value at the end of reset phase,  $C_{p\_top}$  is the parasitic capacitance at node  $V_{top}$ , and  $C_{p\_gate}$  is the parasitic capacitance at node  $V_{gate}$ . For the conventional structure of Fig. 1(b),  $V_{top\_rst}$  is equal to  $V_{DD}$ . For the proposed circuit of Fig. 4,  $V_{top\_rst}$  is slightly larger than  $V_{DD}$ . Thus, according to Eq. (1), if the parasitic capacitances are 0, then  $\Delta V$  of Fig. 1(b) will be  $V_{DD}$ , and  $\Delta V$  of Fig. 4 will be slightly larger than  $V_{DD}$ . Simulation results show that  $\Delta V$  of Fig. 1(b) is  $0.71V_{DD}$  due to the parasitic capacitances, and  $\Delta V$  of Fig. 4 is  $1.05V_{DD}$ .

To calculate  $V_{top\_rst}$  for Fig. 4, Fig. 5 shows the voltage values at the beginning and the end of reset phase (CLK=1). At the beginning of reset phase, VY rises to about  $2V_{DD}$ , while  $V_{top}$  is at its initial value  $V_{top\_init}$ . This makes M1 turned on which transfers charges from C2 to C1. As a result, at the end of reset phase,  $V_{top}$  rises to  $V_{top\_rst}$ , while VY falls to  $V_{top\_rst}+V_{th}$ , where  $V_{th}$  is the threshold voltage of M1. Thus, according to

the law of conservation of charges,  $V_{top\_rst}$  can be calculated as follows:

$$V_{top\_rst} = \frac{2 \cdot V_{DD} \cdot C2 + V_{top\_init} \cdot C1 - V_{th} \cdot C2}{C1 + C2}$$
 (2)

With a proper ratio between C1 and C2, the  $V_{top\_rst}$  can be set to slightly larger than  $V_{DD}$ .

As mentioned before, one advantage of this circuit is the increased driving ability of M2 and thus a faster rising speed of  $V_{gate}$ , because the source-gate voltage of M2 is increased to slightly larger than  $V_{DD}$  in the bootstrap phase. Due to the squared relationship in I-V of MOSFET in saturation region, the increased source-gate voltage of M2 leads to an increase in its current  $I_2$ . Simulation results show that the current  $I_2$  of Fig. 4 is increased by 2.1 times compared to Fig. 3.

Besides, as mentioned before, the  $V_{gate}$  slightly larger than  $V_{in}+V_{DD}$  leads to a reduced on-resistance of the bootstrapped switch M6. Simulation results show that the on-resistance of M6 is reduced by 2.2 times compared to the classic structure of Fig. 1(b), and 1.6 times compared to Fig. 3.

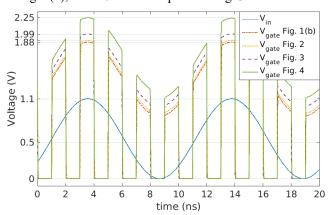


Fig. 6. The curve of  $V_{gate}$  and  $V_{in}$ .

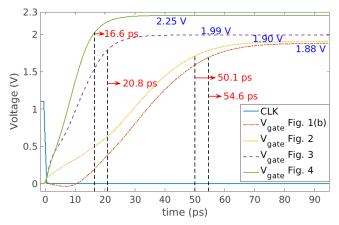


Fig. 7. The rising time of  $V_{gate}$  when  $V_{in}=V_{DD}$ .

## III. POST-LAYOUT SIMULATION RESULTS

All the above bootstrapped switch circuits of Fig. 1 to Fig. 4 are designed in the same 40nm CMOS process. To make a fair comparison, all the circuits use the same MOSFET sizes and the same capacitor sizes.

With a 1.1V  $V_{DD}$ , a 500MHz CLK, and a 1.1V<sub>pp</sub> 100MHz sinusoidal  $V_{in}$ , Fig. 6 shows the curve of  $V_{gate}$  and  $V_{in}$ . As can be seen,  $\Delta V$  of Fig. 1(b) is only 0.71 $V_{DD}$ , while that of Fig. 4 is 1.05 $V_{DD}$ .

Fig. 7 shows the rise time of  $V_{gate}$  when  $V_{in}$ = $V_{DD}$ . This rise time is calculated at the 90% settling of  $V_{gate}$ . As can be seen, the rise time of the classic structure of Fig. 1(b) is 54.6ps, and its  $\Delta V$  is only  $0.71V_{DD}$ . Its slow rising is because of the two delays discussed before and the small current  $I_2$ , while the small  $\Delta V$  is due to the large parasitic capacitance. By contrast, Fig. 2 reduces the rise time by 4.5ps using an additional transistor to inject extra charges. Fig. 3 has a small rise time of 20.8ps and a large  $\Delta V$  of  $0.81V_{DD}$ . Fig. 4 has a rise time of only 16.6ps and a large  $\Delta V$  of  $1.05V_{DD}$ . Note that, Fig. 4 only needs 13.4ps to rise to the same voltage as Fig. 3. This means that, the rising speed of Fig. 4 is 1.55 times faster than Fig. 3.

Table I summarizes the performance of each bootstrapped switch circuit. The key highlight of the proposed circuit of Fig. 4 is the smallest rise time of  $V_{gate}$  as well as the smallest  $R_{on}$ . Compared to Fig. 1(b), it reduces  $V_{gate}$  rise time by 3.3 times, and reduces  $R_{on}$  by 2.2 times.

Table II compares the dynamic performance of sampling-hold (S/H) circuits constituted by the bootstrapped switch circuits, respectively. The S/H circuit using Fig. 4 as the sampling switch achieves the highest ENOB, due to the smallest on-resistance  $R_{on}$  than other structures.

TABLE I
PERFORMANCE OF DIFFERENT STRUCTURES

PERFORMANCE OF DIFFERENT STRUCTURES							
	Fig. 1(b)	Fig. 2	Fig. 3	Fig. 4			
$\Delta V$	$0.71V_{DD}$	$0.73V_{DD}$	$0.81V_{DD}$	$1.05V_{DD}$			
I <sub>2</sub> normalized to Fig. 1(b)	1	1	1	2.1			
rise time of $V_{gate}$	54.6ps	50.1ps	20.8ps	16.6ps			
R <sub>on</sub> normalized to Fig. 1(b)	1	0.93	0.74	0.46			

TABLE II
DYNAMIC PERFORMANCE OF THE S/H CIRCUIT

	Fig. 1(b)	Fig. 2	Fig. 3	Fig. 4
ENOB	11.79	11.74	11.46	12.15
SNDR	72.77	72.60	72.31	75.1

# IV. CONCLUSION

This paper presents a novel bootstrapped switch circuit with an accelerated gate-voltage rising speed and a reduced on-resistance of switch. Several techniques are proposed to realize this improved performance. Designed in a 40nm CMOS process, simulation results show that the gate-voltage rising speed is increased by 3.3 times, and the on-resistance is reduced by 2.2 times.

## V. ACKNOWLEDGMENT

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