

AIC Project

1 Design specifications

Design a differential input, single ended output operational transimpedance amplifier (OTA) with the lowest possible power consumption for the following specifications :

- DC gain $\geq 80\text{dB}$.
- Unity gain frequency $\geq 10\text{ MHz}$.
- Output voltage swing $\geq 1V_{pp}$.
- Slew rate $\geq 250\text{V}/\mu\text{s}$.
- Phase Margin $\geq 65^\circ$.
- Input referred noise (Thermal only) $= 10\text{nv}/\sqrt{Hz}$.
- Input Common mode voltage $= 0.9\text{V}$.
- Output load capacitance $= 1\text{pF}$.

Topology:

Since we were required a gain of 80 dB and the design also asks for low power consumption so I went to choose the telescopic configuration as the gain is maximum in this also since folded-cascode requires an extra biasing so it consumes more power as compared to telescopic and furthermore the gain is also less than telescopic so I choose the Telescopic configuration.

Notice how my topology (fig1) is slightly different from conventional telescopic as this offers more swing than the traditional telescopic configuration in which the PMOS are connected in diode connected fashion.

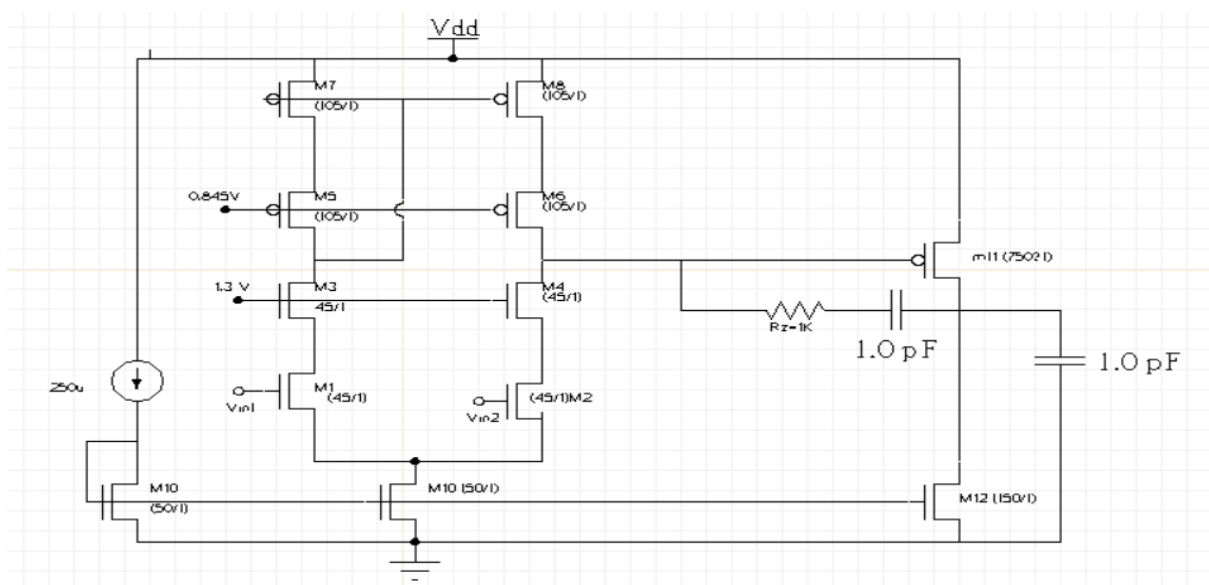


Figure 1

Hand Calculations Results Vs the values used in Simulation(Table1)

| Mosfet | Hand Calculations(W/L) | Actuals Used (W/L) | |
|--------|------------------------|--------------------|-----------|
| M1 | 41 | 45 | Ln=0.18um |
| M2 | 41 | 45 | Ln=0.18um |
| M3 | 41 | 45 | Ln=0.18um |
| M4 | 41 | 45 | Ln=0.18um |
| M5 | 120 | 105 | Lp=0.36um |
| M6 | 120 | 105 | Lp=0.36um |
| M7 | 120 | 105 | Lp=0.36um |
| M8 | 120 | 105 | Lp=0.36um |
| M9 | 45 | 50 | Ln=0.18um |
| M10 | 45 | 50 | Ln=0.18um |
| M11 | 800 | 750 | Lp=0.36um |
| M12 | 150 | 150 | Ln=0.18um |

Table -1

(The length of P channel I increased as lambda is inversely to length so in order to make both rds of NMOS and PMOS equal to increase the Overall Gain)

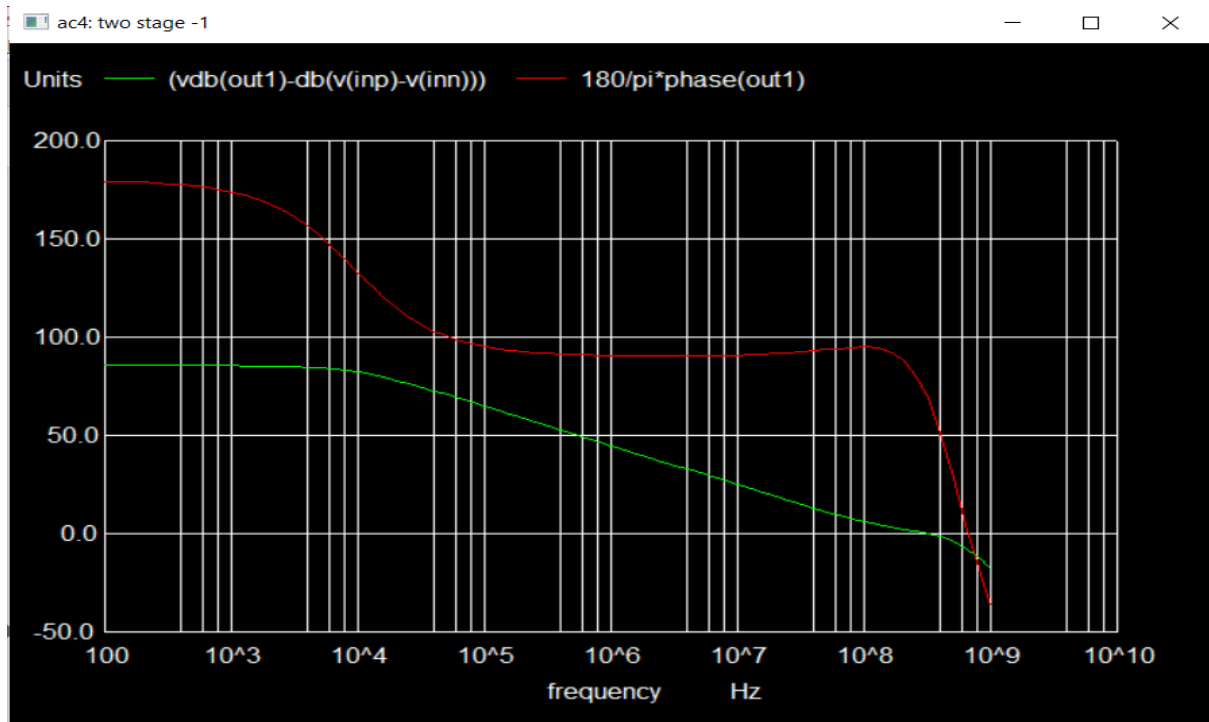
Hand Calculations:

$\phi_m \geq 65^\circ$
 $\phi_m = 180^\circ - \tan^{-1}\left(\frac{g_{B\omega}}{P_i}\right) - \tan^{-1}\left(\frac{g_{B\omega}}{P_i}\right) - \tan^{-1}\left(\frac{g_{B\omega}}{2}\right)$
 $\frac{g_{B\omega}}{2} = 0.1$
 Let say $\boxed{w_{01} = 10 \cdot g_{B\omega}}$
 $115^\circ = \tan^{-1}\left(\frac{g_{B\omega}}{P_i}\right) + \tan^{-1}\left(\frac{g_{B\omega}}{P_i}\right) + \tan^{-1}(0.1)$
 $\frac{g_{B\omega}}{P_i} = \frac{g_{B\omega}}{g_{m10} \cdot P_i} = g_{m10} = 10^4$
 $= 90^\circ + \tan^{-1}\left(\frac{g_{B\omega}}{P_i}\right) + 5.2$
 $\tan(19.3) = \frac{g_{B\omega}}{P_i}$
 $\boxed{P_i = \frac{g_{B\omega}}{0.35} = 2.85 \cdot g_{B\omega}} \quad \text{--- (1)}$
 $P_i \geq 2.85 \cdot g_{B\omega}$
 $\frac{g_{m10}}{C_c} \geq 2.85 \left(\frac{g_{m2}}{C_c}\right) \quad \text{--- (2)}$
 further $\frac{g_{m10}}{C_c} \geq 10 \cdot g_{B\omega}$
 $\left(\frac{g_{m10}}{g_{m2}}\right) \geq 10 \quad \text{--- (3)}$
 $C_c \geq C_2 \left(\frac{g_{m1}}{g_{m2}}\right) 2.85$
 $\boxed{C_c \geq \text{out } P} \quad \boxed{C_2 \geq 0.285 \cdot P} \quad \text{--- (4)}$

$C_c = 0.8 \cdot P$
 $I_D = C_c \cdot KSR$
 $I_D = 200 \mu A$
 $M_5 - M_6$ are identical
 $M_1 - M_4$ are identical
 $(V_{out})_{5-6} = 0.2$
 $(V_{out})_{1-4} = 0.1$
 $(V_{out})_A = 0.2$
 $\left(\frac{W}{L}\right)_{1-4} = \frac{200}{210 \times (0.1)^2} = 41$
 $\left(\frac{W}{L}\right)_{5-6} = \frac{200}{95 \times (0.1)^2} = 52.6$
 $\left(\frac{W}{L}\right)_A = 45.74$
 $(g_m)_{1-4} = \frac{2I_D}{V_{ov}} = 1.33 \text{ mA/V}$
 $(g_m)_{5-6} = \frac{2I_D}{V_{ov}} = 1 \text{ mA/V}$
 $g_m = g_{m1} \left[g_{m1} + g_{m2} \parallel g_{m3} \parallel g_{m4} \right]$
 $g_{on} = \frac{1}{\lambda_n I_{Dn}} \quad \boxed{\gamma \propto \frac{1}{\lambda}}$
 $L_p = 2 L_n$
 $\text{to make } g_{mp} = g_{mn}$
 $\boxed{W' = 2W}$
 $\left(\frac{W}{L}\right)_{5-6} = 120$
 $(V_{out})_{5-6} = 0.13 \text{ V}$
 $L_p = 836 \text{ nm}$

3) Simulations :

DC gain and Phase Plot : From AC Analysis

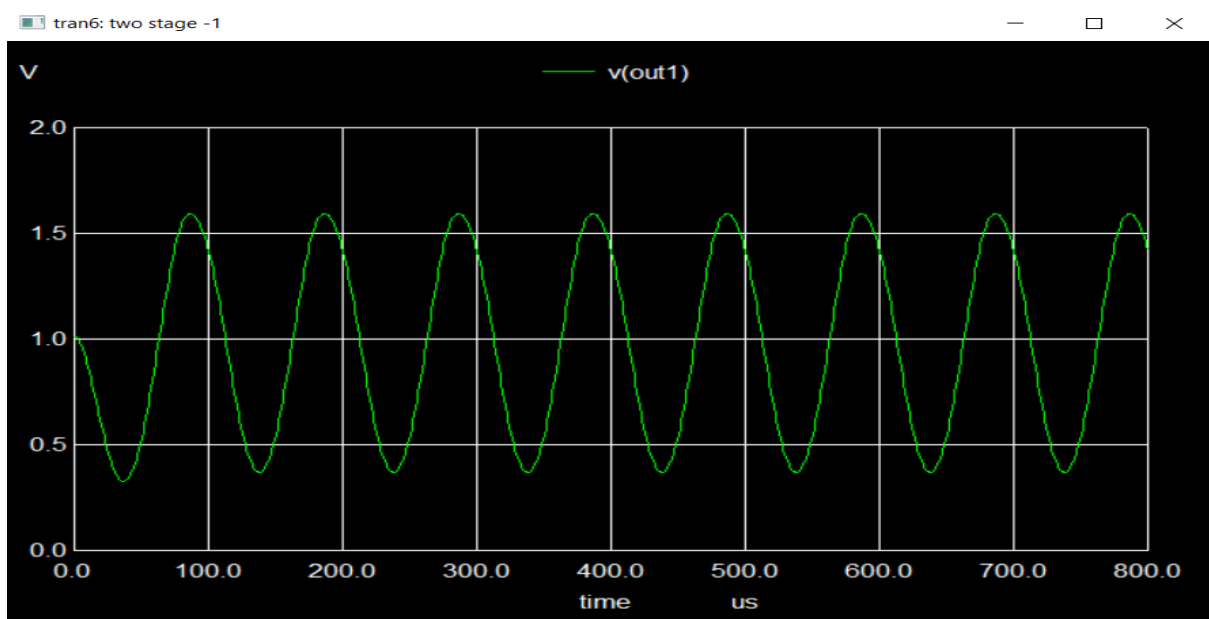


DC gain: 84.2 dB

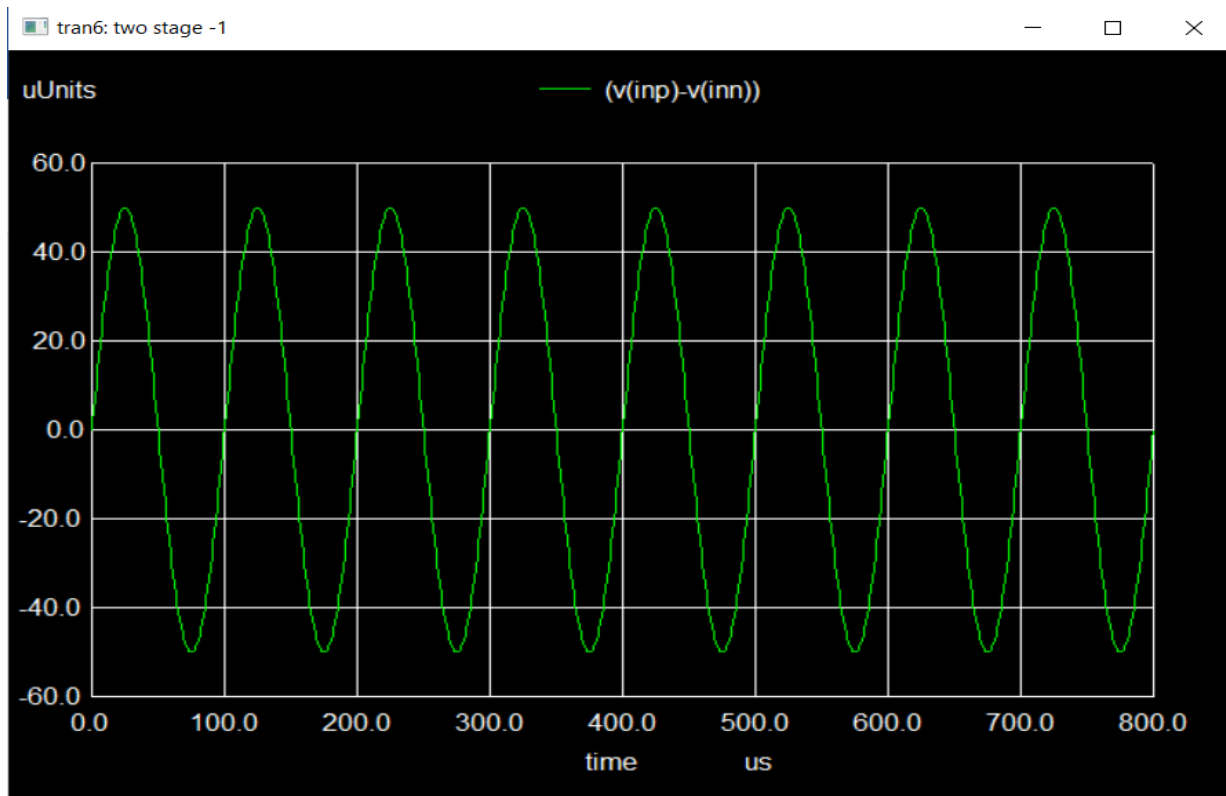
Phase Margin: 71.2 degrees

Unity Gain frequency: 3.01×10^8 Hz

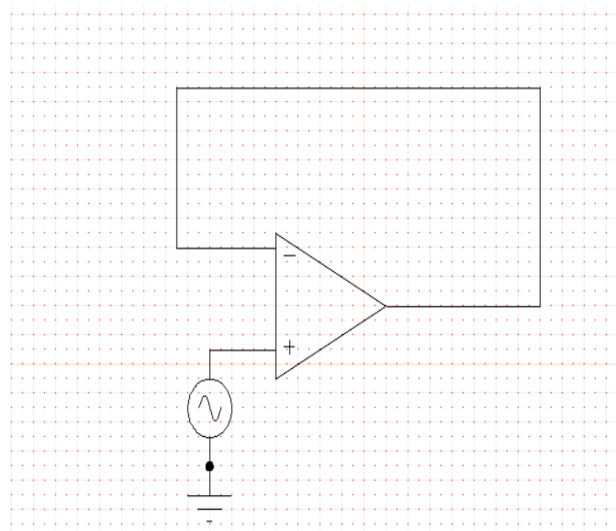
Output Swing: Maximum output swing before clipping 1.23v(>1Vp-p)



Differential Input of 100micro volts peak to peak.

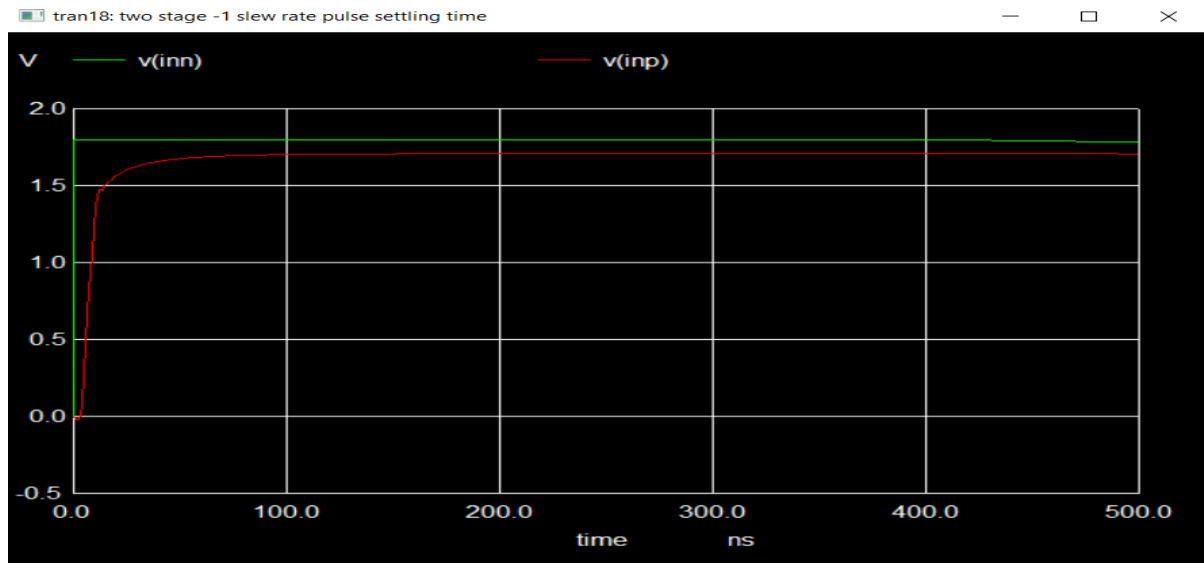


Slew Rate : We applied a step input of 1.8 V and will check the O/p voltage at other node .



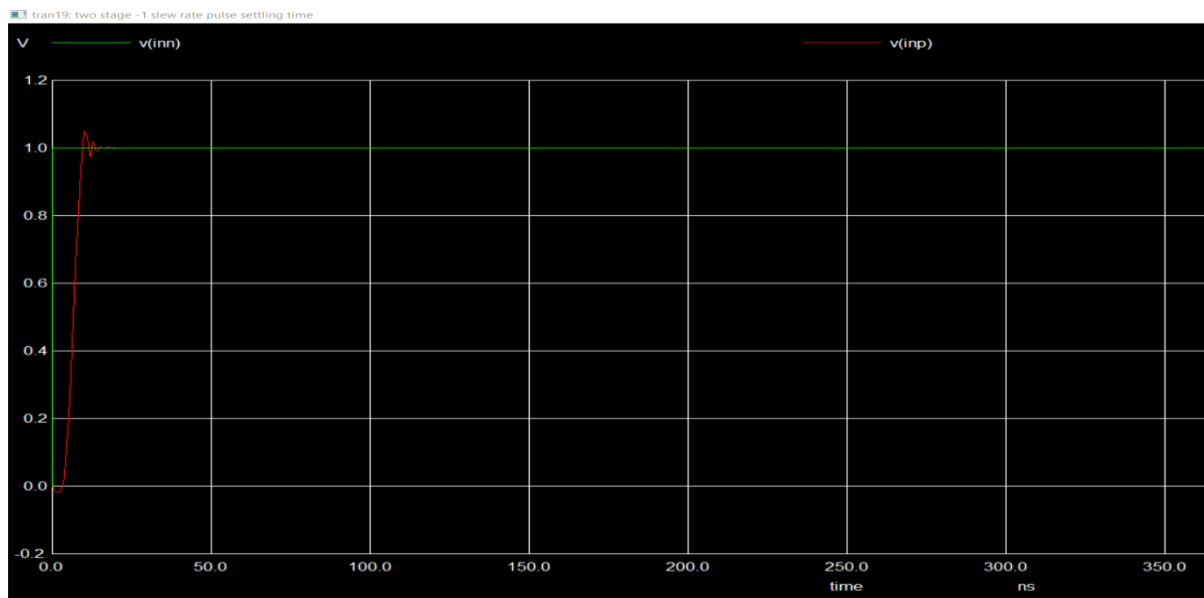
We will now find the maximum Slope by Output voltage for calculation of Slew Rate.

SR=230V/us from the below simulations.

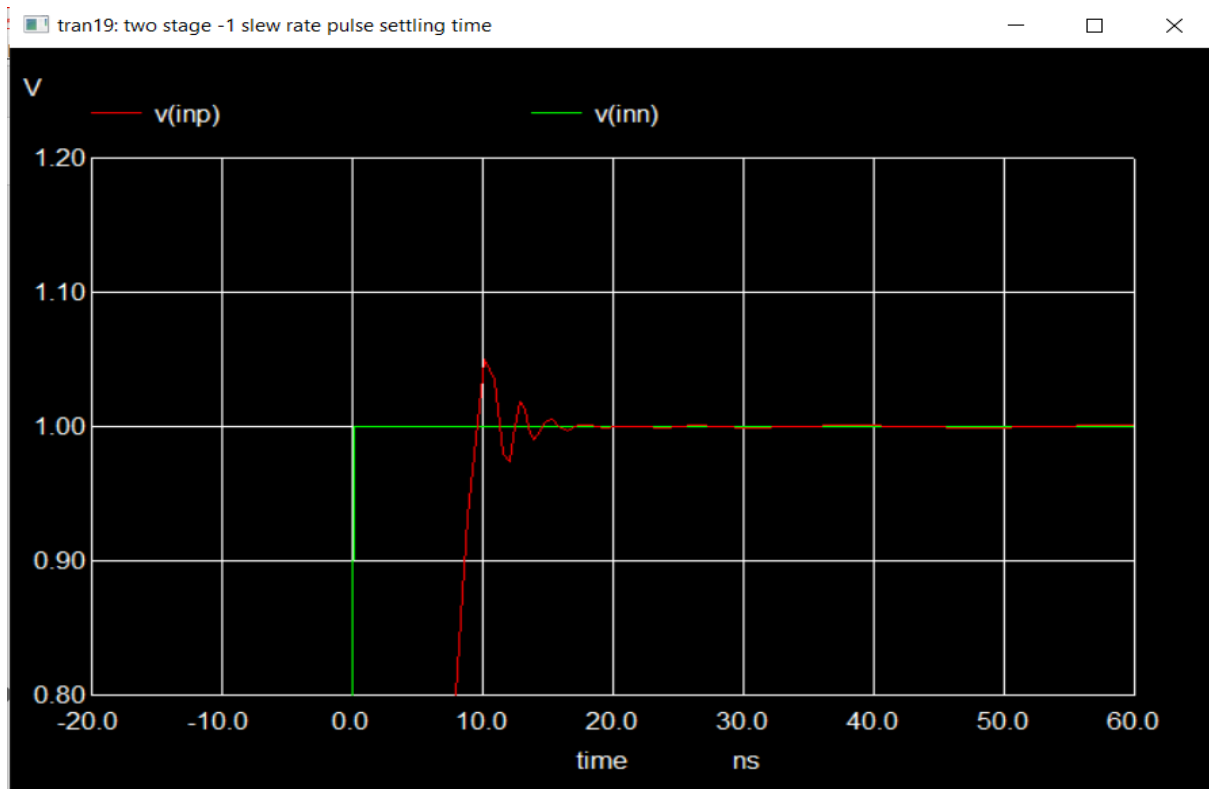


Settling Time: This is due to effect of Phase Margin the more the Phase Margin the less will be the overshoots since my PM is around 71degrees so it has very low peaks.

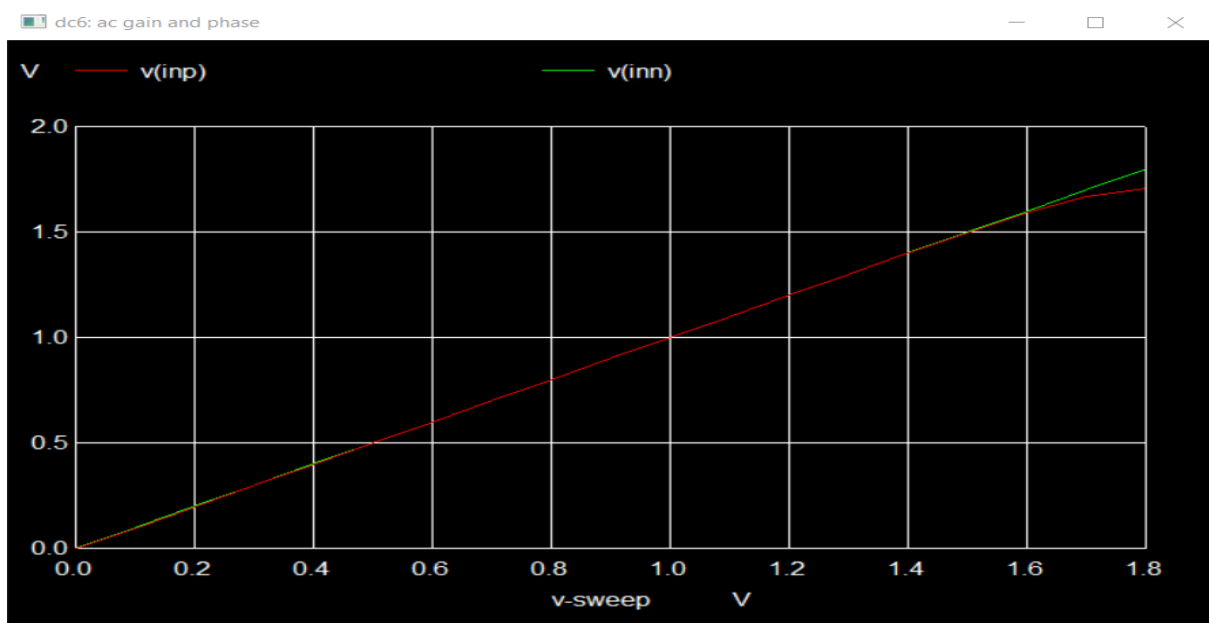
This time instead of applying 1.8V pulse I have applied a 1V peak to see the ringing in my circuit .



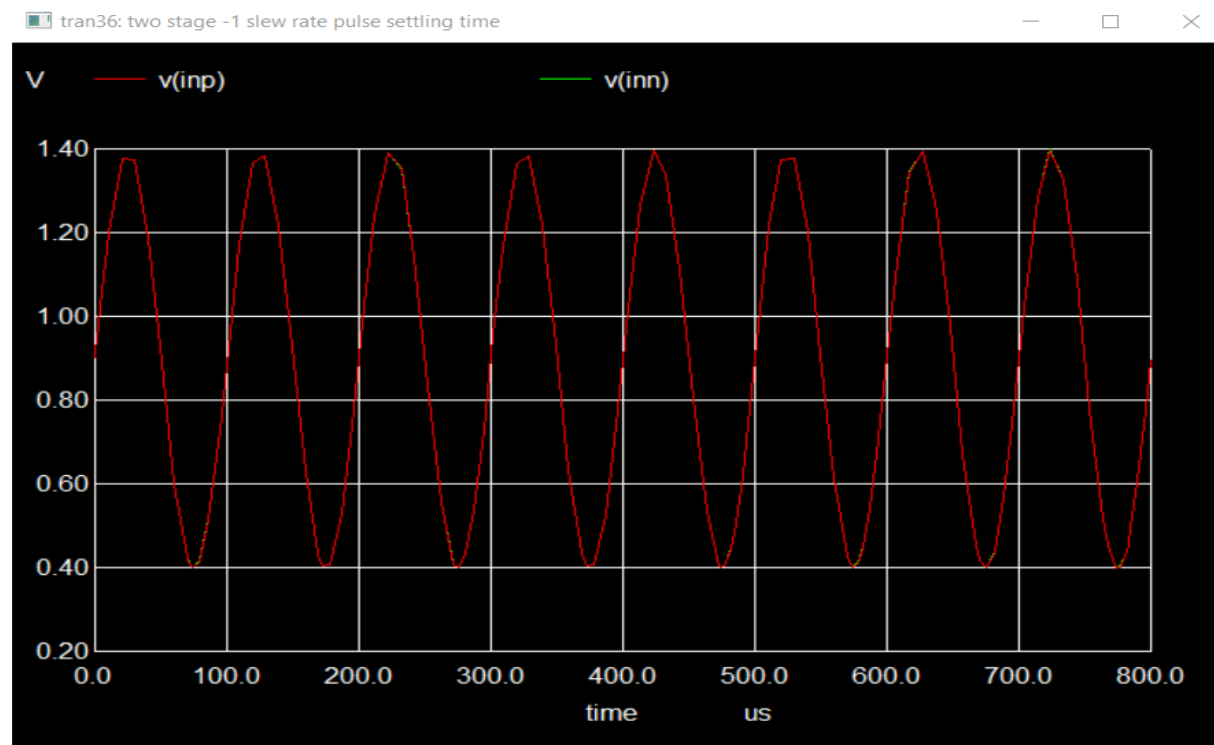
For calculation of settling time we will zoom our previous result to check what time does it take to be in 2% tolerance level so it comes as $t_s=15\text{ns}$.



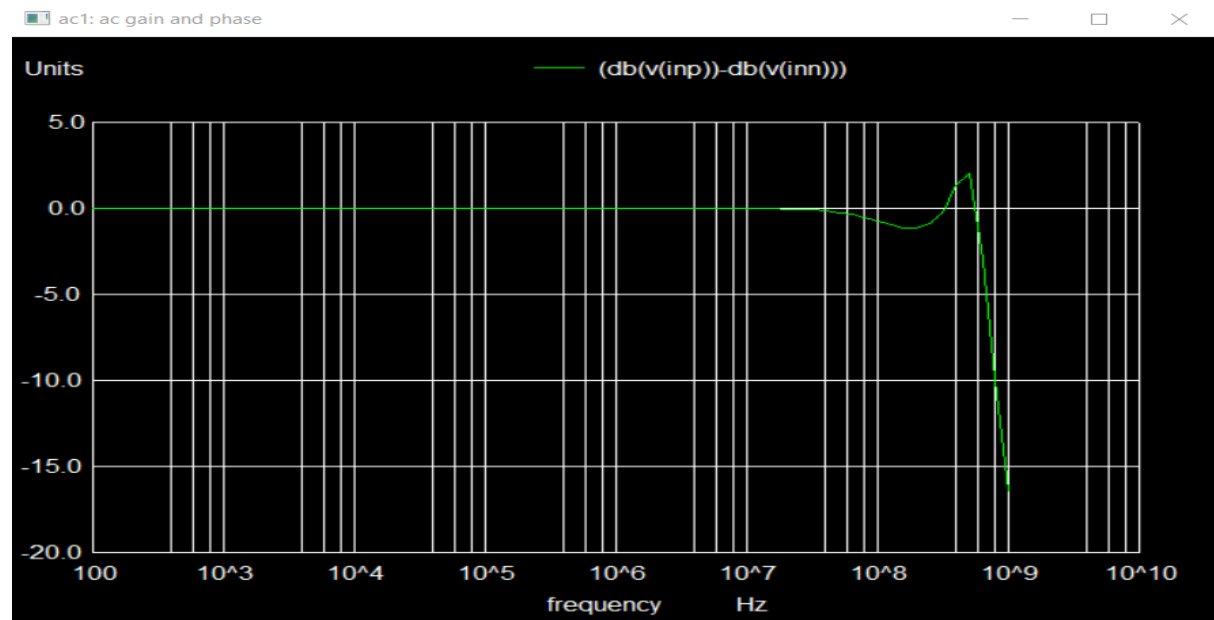
ICMR Calculations: $\text{ICMR}^+=1.45\text{V}$ $\text{ICMR}^- = 0.45\text{V}$



Closed Loop Transient Analysis:



Closed Loop Gain: We used OTA in negative feedback configuration and performed AC simulation for calculation of DC gain and -3db Frequency.



$A_v=1$ which means 0db which was expected .

$F_{-3db}= 0.63\text{Ghz}$

Power Consumption: Total Current from the Vdd supply including the biasing circuitry is 1.2mA .

$P_{\text{total}} = V_{\text{dd}} * I(\text{from Vdd}) = 1.8 * 1.2 = 2.16\text{mW}$.

Conclusions

| Requirements | Results from Simulations |
|----------------------------|--------------------------|
| DC Gain>80dB | 84.2dB |
| UGB>10Mhz | $3 * 10^8$ hz |
| Output Voltage Swing>1Vp-p | 1.23V p-p |
| Slew Rate>=250V/us | 230V/us |
| Phase Margin>65degree | 71.2 |
| Input Referred Noise | - |
| Output Capacitance=1pf | 1pf |
| ICMR ⁺ | 1.45V |