
Lab 1

ELECENG 2EJ4

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Part 1

For the NPN-BJT 2N3904 characterized, if we want to bias this device to conduct a collector current $I_C \approx 1.0 \text{ mA}$ at the lowest V_{CE} value, answer the following questions.

1. (7 Points) Based on the simulated data in Steps 1.2-1.4, use the bias condition giving the closest I_C value to the desired collector current, find out
 - a. What are the simulated V_{BEon} in volt and the base current I_B in μA ?
 $V_{BEon} = 0.621\text{V}$
 $I_B = 8.79\mu\text{A}$
 - b. What is the $\beta = I_C/I_B$ value at this I_C ?
117
 - c. What is the early voltage $|V_A|$ in volt?
1000V
 - d. What is the output resistance r_o in $\text{k}\Omega$?
976k Ω
 - e. What is the transconductance g_m in mS?
41 mS
 - f. What is the input resistance r_π in $\text{k}\Omega$?
2.845k Ω
2. (8 Points) Based on the measured data in Step 1.8, use the same bias condition used in Q1 (or the first reliable data if that bias condition is an outlier), find out
 - a. How much is the measured collector current I_C in mA?
1.74mA
 - b. What are the measured V_{BEon} in volt and the base current I_B in μA ?
 $V_{BEon} = 0.675\text{V}$
 $I_B = 8.25\mu\text{A}$
 - c. What is the $\beta = I_C/I_B$ value at this I_C ?
211
 - d. What is the early voltage $|V_A|$ in volt?
360V
 - e. What is the output resistance r_o in $\text{k}\Omega$?
207k Ω
 - f. What is the transconductance g_m in mS?
69.6mS
 - g. What is the input resistance r_π in $\text{k}\Omega$?
3.03k Ω

Part 2

For the PNP-BJT 2N3906 characterized, if we want to bias this device to conduct a collector current $I_C \approx 1.0 \text{ mA}$ at the lowest V_{EC} value, answer the following questions.

3. (7 Points) Based on the simulated data in Steps 2.2-2.4, use the bias condition giving the closest I_C value to the desired collector current, find out
- What are the simulated V_{BEon} in volt and the base current I_B in μA ?
 $V_{BEon} = 0.66V$
 $I_B = 8.4\mu A$
 - What is the $\beta = I_C/I_B$ value at this I_C ?
123
 - What is the early voltage $|V_A|$ in volt?
133
 - What is the output resistance r_o in $k\Omega$?
139k Ω
 - What is the transconductance g_m in mS?
41.2mS
 - What is the input resistance r_π in $k\Omega$?
2.976k Ω
4. (8 Points) Based on the measured data in Step 2.8, use the same bias condition used in Q1 (or the first reliable data if that bias condition is an outlier), find out
- How much is the measured collector current I_C in mA?
1.24mA
 - What are the measured V_{BEon} in volt and the base current I_B in μA ?
 $V_{BEon} = 0.64V$
 $I_B = 3.56\mu A$
 - What is the $\beta = I_C/I_B$ value at this I_C ?
348
 - What is the early voltage $|V_A|$ in volt?
40V
 - What is the output resistance r_o in $k\Omega$?
32.2k Ω
 - What is the transconductance g_m in mS?
49.7mS
 - What is the input resistance r_π in $k\Omega$?
7.015k Ω

Part 3

5. (10 Points) Express the base current I_B as a function of V_{BB} , R_{BB} , V_{BEon} , R_3 , V_{EE} , and β .

$$i_B = i_e - i_c$$

$$i_c = \beta i_B$$

$$i_B = i_e - \beta i_B$$

$$i_e = i_B(\beta + 1)$$

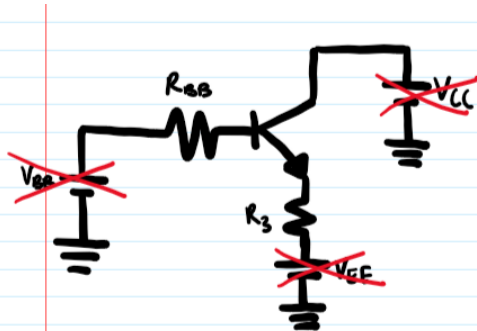
$$\begin{aligned}
V_{BB} - i_B R_{BB} - V_{BEon} - i_e R_3 - V_{EE} &= 0 \\
V_{BB} - i_B R_{BB} - V_{BEon} - i_B (\beta + 1) R_3 - V_{EE} &= 0 \\
V_{BB} - i_B [R_{BB} + (\beta + 1) R_3] - V_{BEon} - V_{EE} &= 0 \\
i_B = \frac{V_{BB} - (V_{BEon} + V_{EE})}{R_{BB} + R_3(\beta + 1)}
\end{aligned}$$

6. (10 Points) Comparing the I_B expression obtained in Q5 with (3), what is the difference between these two equations? For a change ΔV_{EE} in the power supply V_{EE} , derive equations for the resulted change in the base current ΔI_B using (3) and the I_B expression obtained in Q5. Show that the emitter resistor R_3 reduces the change in the base current ΔI_B as a result of the change ΔV_{EE} in the power supply V_{EE} .

The main difference between the expression obtained in Q5 and (3) is that in (3) we are only dividing by R_{BB} while in Q5 we are dividing by $R_{BB} + R_3(\beta + 1)$. The $R_3(\beta + 1)$

7. (15 Points) Inserting the feedback R_3 at the emitter of the BJT not only stabilizes the I_B but also improves (or increases) the output resistance R_o of the current sink shown in Fig. 6/ Fig. 7 (i.e. I_o is more stable when there is a change in V_{CE}). Using a π -model for the BJT, prove that the output resistance of the current sink is

$$R_o = r_o + [r_3 || (R_{BB} + r_\pi)] \left[1 + g_m r_o \left(\frac{r_\pi}{R_{BB} + r_\pi} \right) \right]$$



$$① R_o = \frac{V_o}{i_o} = \frac{V_o}{i_3}$$

$$② i_2 = g_m V_\pi = g_m r_\pi i_1$$

$$③ V_o - r_o(i_3 - i_2) - R_3(i_3 - i_1) = 0$$

$$i_1 = \frac{V_o - r_o i_3 - R_3 i_3}{r_o g_m r_\pi - R_3}$$

$$④ -R_2(i_1 - i_3) - R_{BB} i_1 - r_\pi i_1 = 0$$

$$i_1 = \frac{R_3 i_3}{r_\pi + R_{BB} + R_3}$$

$$⑤ \frac{R_3 i_3}{r_\pi + R_{BB} + R_3} = \frac{V_o - r_o i_3 - R_3 i_3}{r_o g_m r_\pi - R_3}$$

$$R_o = r_o + \left[\frac{R_3 R_{BB} + R_3 r_\pi}{R_3 + R_{BB} + r_\pi} \right] \left[\frac{1 + g_m r_o r_\pi}{R_{BB} + r_\pi} \right]$$

$$R_o = r_o + (R_3 || R_{BB} + r_\pi) \left[1 + g_m r_o \left(\frac{r_\pi}{R_{BB} + r_\pi} \right) \right]$$

8. (10 Points) Inserting the feedback R_3 at the emitter of the BJT improves the stabilization of the Q-point at the cost of increased $V_{o,min}$. What is the $V_{o,min}$ of the constant current sink when $R_3 \neq 0$?

$R_3 \neq 0$ = voltage drop

$$V_{o,min} = V_E + 0.3V$$

$$V_{R_3} = i_e R_3$$

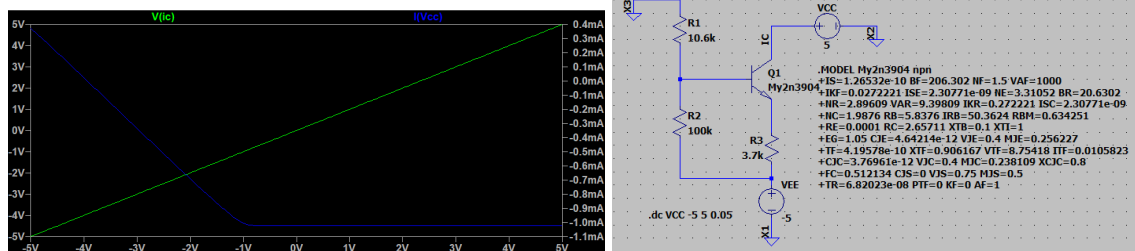
$$V_{o,min} = V_E + 0.3V + i_e R_3$$

9. (15 Points) For $V_{EE} = -5V$, if we want to design a current sink with $I_0 = 1.0 \text{ mA}$ and $V_{o,min} = -1 \text{ V}$ using the NPN-BJT 2N3904 characterized in Q1, what is the resistance value for R_3 ? To reduce the DC power consumption of R_1 and R_2 , we usually choose large resistance values (in tens or hundreds of $k\Omega$) for R_1 and R_2 . Suppose we choose $R_2 = 100 \text{ k}\Omega$, calculate R_1 in $k\Omega$. Verify the I_0 vs. V_{CC} characteristics of the design by sweeping V_{CC} from $-5V$ to $5V$ with a $0.05V$ step and post the screenshot of the simulated I_0 vs. V_{CC} characteristics.

$$V_{o,min} = V_E + 0.3V + i_e R_3$$

$$-1V = -5V + 0.3V + (1mA)R_3$$

$$3.7k = R_3$$



10. (10 Points) When designing the constant current sink shown in Fig. 6, we assume that $|V_{CE}| \geq 0.3V$ and Q_1 works in the active region. Based on the resistance values obtained in Q9, sweep V_{CC} in Fig. 6 from -5 V to $+5V$ with a 0.05 V step and measure V_E and I_C to determine the $|V_{CE}|$ required for Q_1 to work in the active region.

$|V_{CE}|$ and Q_1 are only active when $V < 0V$.

