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STREAM FUNCTION-VORTICITY FORMULATION AND HEAT TRANSPORT USING FEM FOR UNSTRUCTURED MESHES AND COMPLEX DOMAINS

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ABSTRACT – The stream function-vorticity formulation is a useful alternative to solving the Navier-Stokes equations in two dimensional domain. One of its major difficulties is the lack of boundary conditions for vorticity, and several schemes are proposed to satisfy such a condition. In this paper we propose a finite element scheme for solving the couple problem of the stream function-vorticity formulation using linear triangle elements. A possible application of the method is also demonstrated using the calculated velocity field from the formulation in the heat transport equation to study the temperature distribution in a incompressible single-phase fluid medium. The results obtained were satisfactory when using low to moderate Reynolds number.

1. INTRODUCTION

In computational fluid dynamics (CFD), solving the incompressible Navier-Stokes equation is of utmost interst in various applications. The stream function-vorticity (ψ , ω_z) formulation is a way to express the Navier-Stokes equation in terms of ψ and ω_z instead of the primitives pressure and velocity (Peeters et al., 1987). The advantage of using the stream function-vorticity formulation is that the pressure does not appear in the equation and, thus, we do not need to solve the pressure-velocity problem, therefore the use of linear element is suitable. The formulation has been proved to be of great use when considering a two dimensional domain (Hoffmann e Chiang, 2000) and in this paper it is proposed an algorithm based on (Salih, 2013) to combine the (ψ , ω_z) formulation results with the heat transport equation.

2. MATHEMATICAL MODEL

For a two dimensional analysis using FEM with unstructured meshes, the proposed method for solving the heat transport equation in a fluid system makes use of the stream function-vorticity formulation (Hoffmann e Chiang, 2000) to obtain a more precise description of the velocity field in a single-phase incompressible flow.

The equations used in this method are:

$$\omega_z = \frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \tag{1}$$



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$$\frac{\partial \omega_z}{\partial t} + \mathbf{v} \cdot \nabla \omega_z = \frac{1}{Re} \nabla^2 \omega_z \tag{2}$$

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = \omega_z \tag{3}$$

$$\frac{\partial \psi}{\partial y} = v_x \ , \quad \frac{\partial \psi}{\partial x} = -v_y \tag{4}$$

$$\frac{\partial T}{\partial t} + \mathbf{v} \cdot \nabla T = \frac{1}{RePr} \nabla^2 T + Q \tag{5}$$

Where T is the scalar field of temperature, the Reynolds number is $Re = \rho u D/\mu$ (ρ is the density, u is the reference velocity, μ , is the viscosity and D is a characteristic linear dimension), the Prandtl number is $Pr = \nu/\alpha$ (ν is the kinematic viscosity and α is the thermal diffusivity), ω_z is the vorticity field, x and y are the independent spatial variables, $\mathbf{v} = (v_x, v_y)$ is the velocity field, ψ is the stream function, Q is the generation of heat, and t is the time variable.

The algorithm developed to solve the stream function-vorticity problem was based on the algorithm proposed on (Salih, 2013). At first an initial \mathbf{v} field is initialized, respecting the boundary conditions for velocity, and the initial ω_z is calculated with equation (1). After that, the initial ψ function is obtained by solving equation(3) with Dirichlet boundary conditions for ψ .

The next step is to obtain the boundary conditions for the vorticity that are needed to solve equation (2). Various finite differences schemes can be derived for that, such as in (Peeters et al., 1987), however this schemes need a structured mesh to be implemented. The proposed way to calculate the boundary conditions when using unstructured meshes is to calculate ω_z with equation (1) in each time step as the velocity field changes.

With the initial values for \mathbf{v} , ω_z and ψ and the boundary conditions calculated, the vorticity transport equation (2) is solved for the next time step, than with the new ω_z field, equation (3) is solved for the new ψ field. Afterwards the new velocity field is obtained by equations in (4). This repeats over a defined number of steps.

In the equations (1) and (4) we use the Lumped Mass matrix to reduce the computational cost of inverting the original Mass matrix (\mathbf{M}). The Lumped matrix is constructed adding all the elements for each line of \mathbf{M} and placing the results in the main diagonal and its use is valid when the original matrix elements have higher values when closer to its diagonal.

The FEM algorithm was developed for the use of linear triangular elements in the discretization of the spatial domain and for the time it was used a finite differences method with a forward difference approximation and an implicit approach. The linear systems of equations were solved by a direct solver. To build the geometric model and mesh of the different spatial domains an open source software called "GMSH" Geuzaine e Remacle (2009) was used.

3. RESULTS

3.1. Poiseuille Flow in Heated Plates

A validation for the temperature equation (5) was constructed based on the analytic solution shown in (Pontes e Mangiavacchi, 2010). After applying all the coeficient values, the temperature solution can be described by equation (6).

$$T = \frac{-15}{48}q + \frac{2}{Re(-\partial P/\partial x)}qx + 3q\left(\frac{y^2}{2} - \frac{y^4}{3}\right)$$
 (6)

The top and bottom plates had a heat flux boundary condition of q=1 perpendicular to the boundary. For the stream function $\psi=0$ on the bottom plate and $\psi=1$ on the top plate, $Re=10,\ Pr=1,\ {\rm and}\ (-\partial P/\partial x)=12$. The exact solution for temperature and numerical solutions are shown in Figure 1 and Figure 2 after 60 iterations with $\Delta t=0.1$.

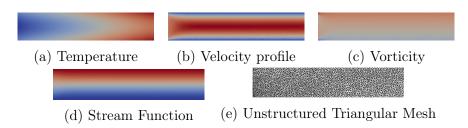


Figure 1 – Numerical solutions obtained by the stream function-vorticity FEM code

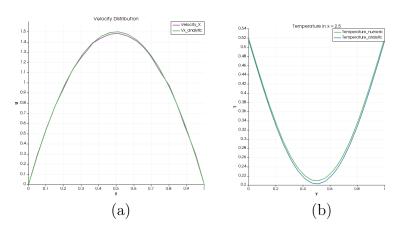


Figure 2 – Comparison of the numerical solution obtaind with the stream function-vorticity finite element solver and the exact solution for (a) Velocity comparison; (b) Temperature comparison



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3.2. Heat Transport Between Non-Smooth Plates

The results presented in figure Figure 3 are for a similar case as the above, however now the heat flux q=1 is only defined on the rectangular shapes along the top and bottom boundaries with the intent to observe how a perturbation on the boundary would affect the solution. Each rectangle has a 0.1 height and 0.5 width. The other boundary conditions and simulation parameters were set as the same for the plane Poiseuille case.

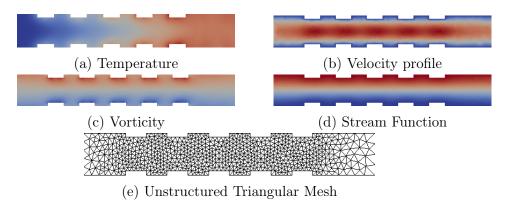


Figure 3 – Numerical solutions obtained by the stream function-vorticity FEM code for the complex geometry proposed

4. CONCLUSION

The proposed method for solving the stream function-vorticity system using the FEM on two dimensional unstructured meshes has shown good results when compared with the literature on the case of low Reynolds. Moreover, it has also been demonstrated its aplication alongside the temperature distribution equation. The algorithm is in continuous development to acomodate higher Re values, thus simulating more challenging problems.

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