

# MAE 3128 : BIOMECHANICS HW 1 SOLUTIONS

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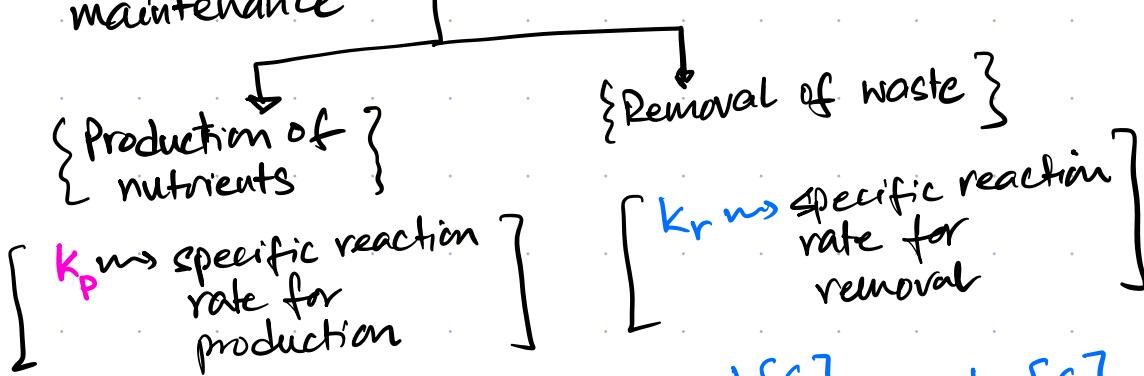
## SOLUTION HW1 P1

Given:

$$\frac{d[c]}{dt} = -k[c]$$

where  $[c] \rightarrow$  concentration $k \rightarrow$  specific reaction rate

$\Rightarrow$  There are two reactions affecting tissue maintenance



$$\therefore \frac{d[c]_p}{dt} = +k_p [c]$$

$$\frac{d[c]_r}{dt} = -k_r [c]$$

Total  $\rightarrow$   
change in  
concentration

$$\frac{d[c]}{dt} = \frac{d[c]_p}{dt} + \frac{d[c]_r}{dt}$$

$$\Rightarrow \frac{d[c]}{dt} = (k_p - k_r) [c]$$

$$= k_o [c]$$

where  $k_o = (k_p - k_r)$

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$$\therefore \frac{d[C]}{dt} = k_0 [C]$$

$$\Rightarrow \int \frac{d[C]}{[C]} = \int k_0 dt$$

$$\Rightarrow \ln [C] = k_0 t + C$$

$$\Rightarrow [C] = A e^{k_0 t}$$

$$\Rightarrow [C] = A e^{(k_p - k_r)t}$$

where  
 A is a  
 constant  
 based on  
 the initial  
 condition  
 at  $t = 0$

SOLUTION HW1 P2:

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Given:

$$\vec{A} = A_x \hat{i} + A_y \hat{j} + A_z \hat{k}$$

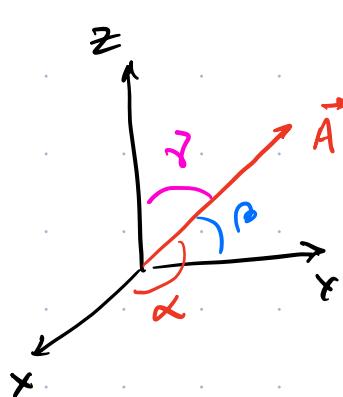
$$\cos \alpha = \frac{A_x}{|\vec{A}|}, \quad \cos \beta = \frac{A_y}{|\vec{A}|}, \quad \cos \gamma = \frac{A_z}{|\vec{A}|}$$

where

$$|\vec{A}| = \sqrt{A_x^2 + A_y^2 + A_z^2}$$

↳ If  $\hat{e} = \cos \alpha \hat{i} + \cos \beta \hat{j} + \cos \gamma \hat{k}$

$$|\hat{e}| = \sqrt{\cos^2 \alpha + \cos^2 \beta + \cos^2 \gamma}$$



$$\therefore |\hat{e}| = 1$$

we have  $\sqrt{\cos^2 \alpha + \cos^2 \beta + \cos^2 \gamma} = 1$

$$\Rightarrow \cos^2 \alpha + \cos^2 \beta + \cos^2 \gamma = 1$$

$$\Rightarrow \left( \frac{A_x}{|\vec{A}|} \right)^2 + \left( \frac{A_y}{|\vec{A}|} \right)^2 + \left( \frac{A_z}{|\vec{A}|} \right)^2 = 1$$

$$\Rightarrow \frac{A_x^2 + A_y^2 + A_z^2}{|\vec{A}|^2} = \frac{|\vec{A}|^2}{|\vec{A}|^2} = 1$$

$$\therefore \cos^2\alpha + \cos^2\beta + \cos^2\gamma = 1$$

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we have the following inter-relationships

$$\alpha = \cos^{-1}(\sqrt{1 - \cos^2\beta - \cos^2\gamma})$$

$$\beta = \cos^{-1}(\sqrt{1 - \cos^2\alpha - \cos^2\gamma})$$

$$\gamma = \cos^{-1}(\sqrt{1 - \cos^2\alpha - \cos^2\beta})$$

These relationships work in 2D case  
where  $\cos\gamma = 0$  or  $\gamma = 90^\circ$

Consider:  $\cos^2\alpha + \cos^2\beta + \cos^2\gamma = 1$

$$\Rightarrow \cos^2\alpha + \cos^2\beta + \cos^2(90^\circ) = 1$$

$$\Rightarrow \boxed{\cos^2\alpha + \cos^2\beta = 1}$$

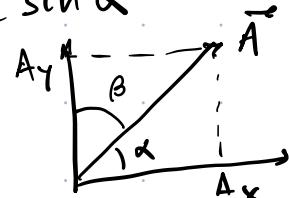
This recovers 2D unit vector

$$|\hat{r}| = 1 = \cos^2\alpha + \cos^2\beta \checkmark$$

Furthermore: In 2D space  $\vec{A} = A_x \hat{i} + A_y \hat{j}$

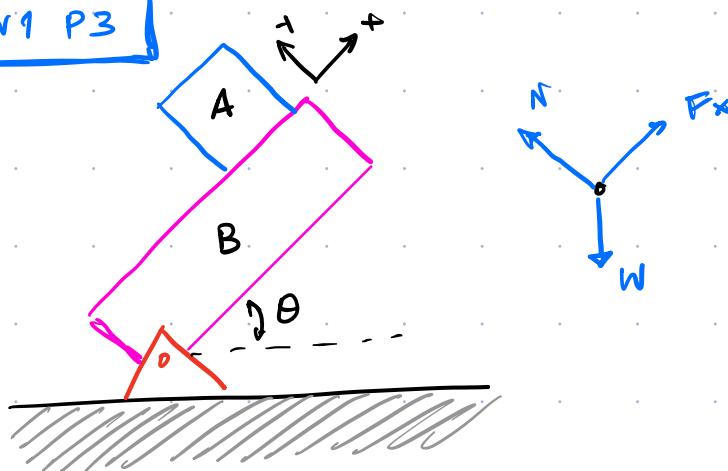
$$\cos\alpha = \frac{A_x}{|\vec{A}|}; \cos\beta = \frac{A_y}{|\vec{A}|}; \text{ But, } \frac{A_y}{|\vec{A}|} = \sin\alpha$$

$$\therefore \cos^2\alpha + \cos^2\beta = 1 \Rightarrow \cos^2\alpha + \sin^2\alpha = 1$$



SOLUTION HW1 P3

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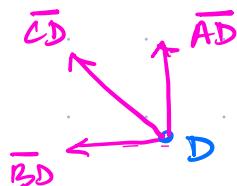
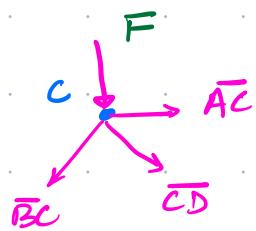
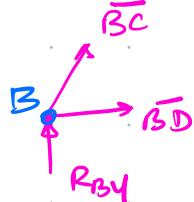
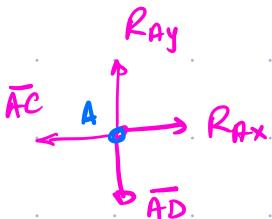
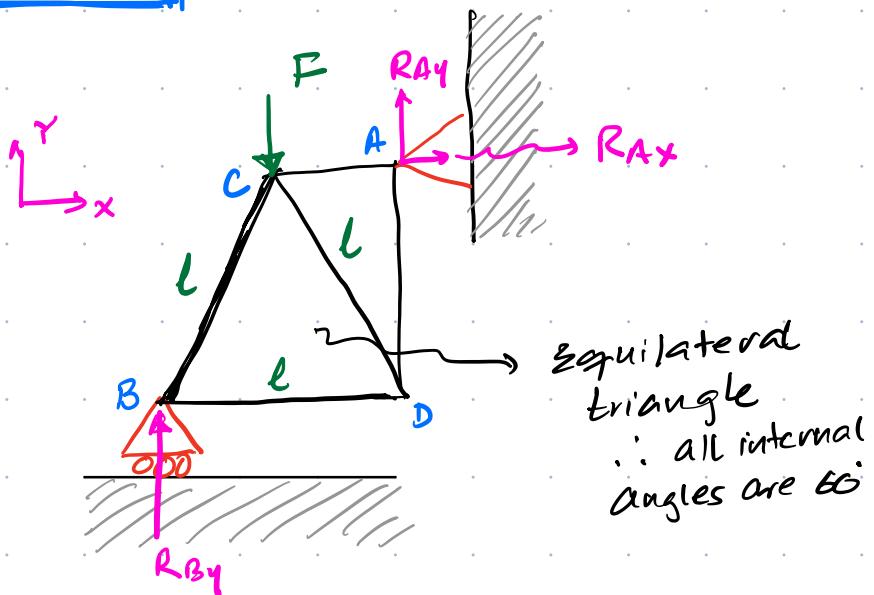


↳ Just before the block A slips, we have equilibrium

$$\begin{aligned} \sum F_x = 0 &\Rightarrow \mu N - W \sin \theta = 0 \\ &\Rightarrow \mu N \cos \theta - W \sin \theta = 0 \quad | \quad \sum F_y = 0 \\ &\Rightarrow N - W \cos \theta = 0 \\ &\Rightarrow N = W \cos \theta \\ \Rightarrow \mu &= \frac{W \sin \theta}{W \cos \theta} \quad \Rightarrow \boxed{\mu = \tan \theta} \end{aligned}$$

(6)

SOLUTION HW1 P4



Reaction forces and Applied forces across the entire truss:

$$\sum F_x = 0$$

$$R_{Ax} = 0 \rightarrow (1)$$

$$\sum M_B = 0$$

$$R_{Ay}(l) - F(l/2) = 0$$

$$\sum F_y = 0$$

$$F - R_{By} - R_{Ay} = 0$$

$$\Rightarrow F = R_{By} + R_{Ay}$$

$$\Rightarrow R_{By} = F/2 \rightarrow (2)$$

$$\Rightarrow R_{Ay} = \frac{F}{2} \rightarrow (2)$$

At point A :

$$\begin{aligned} \sum F_x = 0 &\Rightarrow R_{Ax} - \bar{AC} = 0 \Rightarrow \boxed{\bar{AC} = 0} & \text{From eq (1)} \\ \sum F_y = 0 &\Rightarrow R_{Ay} - \bar{AD} = 0 \Rightarrow \boxed{\bar{AD} = \frac{F}{2}} & \text{From eq (2)} \end{aligned}$$

(7)

(4)

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At point B :

$$\begin{aligned} \sum F_x = 0 &\Rightarrow \bar{BD} + \bar{BC} \cos 60^\circ = 0 \Rightarrow \bar{BD} = \frac{F}{\sqrt{3}} \cos 60^\circ \Rightarrow \boxed{\bar{BD} = \frac{F}{2\sqrt{3}}} \\ \sum F_y = 0 &\Rightarrow \bar{BC} \sin 60^\circ + R_{By} = 0 \Rightarrow \boxed{\begin{aligned} \bar{BC} &= -\frac{F}{(\sqrt{3})/2} \\ &= -F/\sqrt{3} \end{aligned}} & \text{From eq (3)} \end{aligned}$$

(7)

$$\boxed{\bar{BD} = \frac{F}{2\sqrt{3}}}$$

(6)

At point C :

$$\begin{aligned} \sum F_x = 0 &\Rightarrow \bar{AC} + \bar{CD} \cos 60^\circ - \bar{BC} \cos 60^\circ = 0 \\ &\Rightarrow \boxed{\bar{CD} = \bar{BC}} \quad \because \bar{AC} = 0 \text{ from Eq (4)} \\ \sum F_y = 0 &\Rightarrow F + \bar{BC} \sin 60^\circ + \bar{CD} \sin 60^\circ = 0 \\ &\Rightarrow \boxed{F = -2\bar{BC} \sin 60^\circ} \quad \because \bar{CD} = \bar{BC} \text{ from Eq (7)} \end{aligned}$$

At point D :

$$\begin{aligned} \sum F_x = 0 &\Rightarrow \bar{BD} + \bar{CD} \cos 60^\circ = 0 \Rightarrow \frac{F}{2\sqrt{3}} + \left(\frac{F}{\sqrt{3}}\right)\frac{1}{2} = 0 & \text{From eqs (4) \& (7)} \\ \sum F_y = 0 &\Rightarrow \bar{AD} + \bar{CD} \sin 60^\circ = 0 \Rightarrow \bar{AD} = -\frac{F}{\sqrt{3}} \frac{\sqrt{3}}{2} \\ &\Rightarrow \boxed{\bar{AD} = -\frac{F}{2}} \end{aligned}$$

(4)  
(7)

(8)

SOLUTION HWI PS

$$\text{Given: } \sigma_{xy} = \sigma_{yx} = 5 \text{ MPa}$$

$$\sigma_{xx} = \sigma_{yy} = 0$$

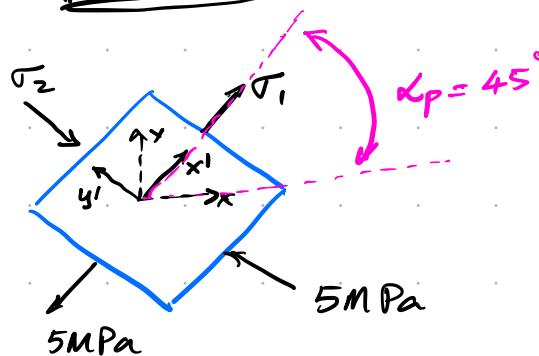
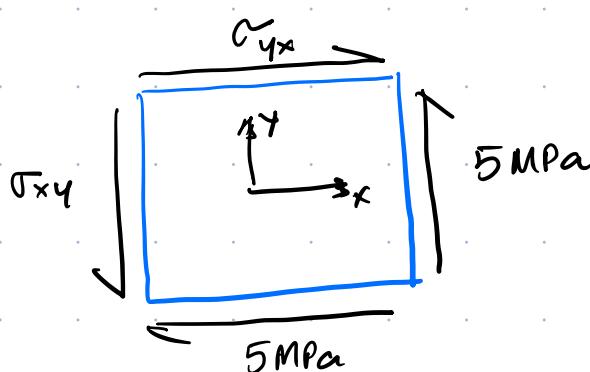
$$\sigma_{1,2} = \frac{\sigma_{xx} + \sigma_{yy}}{2} \pm \sqrt{\frac{\sigma_{xx}^2 - \sigma_{xy}^2}{2} + \sigma_{xy}^2}$$

$$= \pm \sqrt{\sigma_{xy}^2} \Rightarrow \sigma_{1,2} = \pm 5 \text{ MPa}$$

Orientation:

$$\alpha_p = \frac{1}{2} \tan^{-1} \left( \frac{2\sigma_{xy}}{\sigma_{xx} - \sigma_{yy}} \right)$$

$$= \frac{1}{2} \tan^{-1}(0) \Rightarrow \alpha_p = \frac{\pi}{4} = 45^\circ$$



(9)

SOLUTION HW1 P6

Given:  $\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = -P$  <sup>pressure</sup>

$$\begin{aligned}\sigma_{1,2} &= \frac{\sigma_{xx} + \sigma_{yy}}{2} \pm \sqrt{\left(\frac{\sigma_{xx} - \sigma_{yy}}{2}\right)^2 + \sigma_{xy}^2} \\ &= \frac{-P - P}{2} \pm \sqrt{\left(\frac{-P - (-P)}{2}\right)^2 + 0}\end{aligned}$$

$$\Rightarrow \boxed{\sigma_{1,2} = \frac{-2P}{2} = -P}$$

$$\begin{aligned}\sigma_{x,y,\max} &= \pm \sqrt{\left(\frac{\sigma_{xx} - \sigma_{yy}}{2}\right)^2 + \sigma_{xy}^2} = \sigma_m \\ &= \pm \sqrt{\left(\frac{-P - (-P)}{2}\right)^2 + 0}\end{aligned}$$

$$\Rightarrow \boxed{\sigma_m = 0}$$

SOLUTION HW1 P7

(10)

Given:  $\sigma_{xx} = 3 \text{ MPa}$

$\sigma_{yy} = -3 \text{ MPa}$

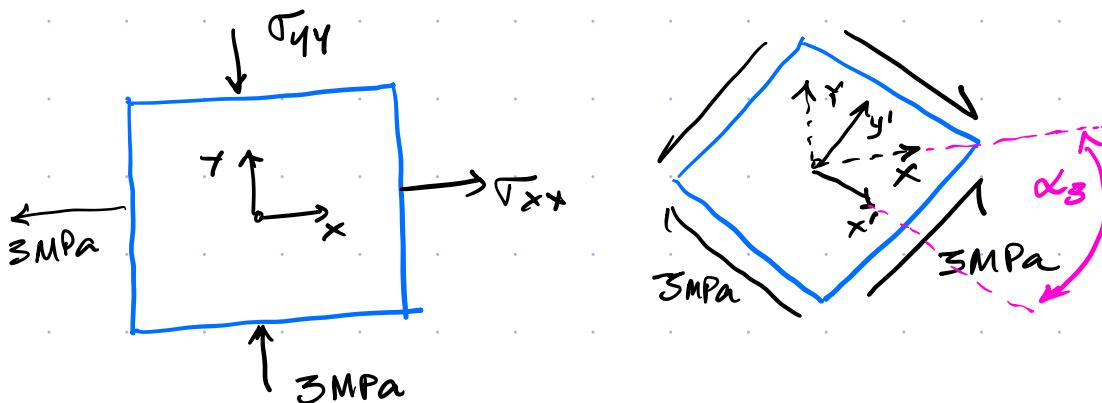
$$\begin{aligned}\tau_m &= \pm \sqrt{\left(\frac{\sigma_{xx} - \sigma_{yy}}{2}\right)^2 + \sigma_{xy}^2} \\ &= \sqrt{\left(\frac{3 - (-3)}{2}\right)^2 + 0^2}\end{aligned}$$

$\boxed{\tau_m = 3 \text{ MPa}}$

$$\alpha_s = \frac{1}{2} \tan^{-1} \left( \frac{\sigma_{yy} - \sigma_{xx}}{2\sigma_{xy}} \right)$$

$$= \frac{1}{2} \tan^{-1}(\infty)$$

$\Rightarrow \boxed{\alpha_s = \frac{\pi}{4} \text{ or } 45^\circ}$



(11)

**SOLUTION HW1 PG**

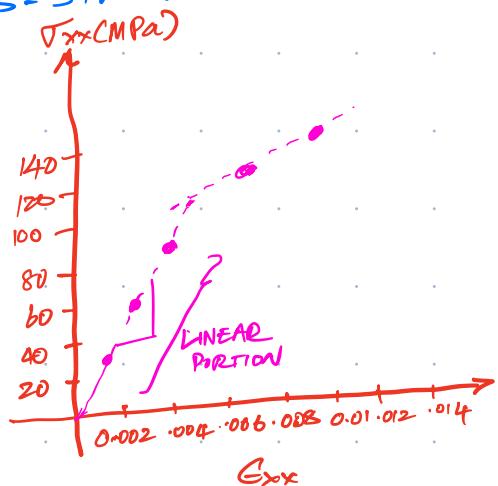
Axial force (N)	94	190	284	376	440
Change in Length (nm)	0.009	0.018	0.027	0.050	0.094

a) Plot the associated stress-strain relationship

$$\sigma_{xx} = \frac{F}{A}$$

$$G_{xx} = \frac{\Delta u_x}{\Delta x}$$

$G_{xx}$	$\sigma_{xx}$ (MPa)
0.0015	29.921
0.003	60.479
0.0045	90.4
0.0083	119.68
0.0154	140.06



b) Calculate the Young's Modulus

↳ E is the slope of the line on the linear portion  
of the stress-strain curve (first 3 points)

↳ The trend line for the linear portion

↳ The trend line for the linear portion  
is fit by  $y = 20176x$  (i.e.,  $\sigma_{xx} = E G_{xx}$ )

So,  $E = 20.176 \text{ GPa}$

c) Show that the yield stress is 118 MPa (recall that  
the yield stress reveals the transition from  
elastic to plastic deformation)

↳ The bone will yield before the 4th point but after  
the 3rd point on the stress-strain data shown in the  
figure.

$90 < \sigma_{yield} < 119$

↳ We can estimate that to be approximately

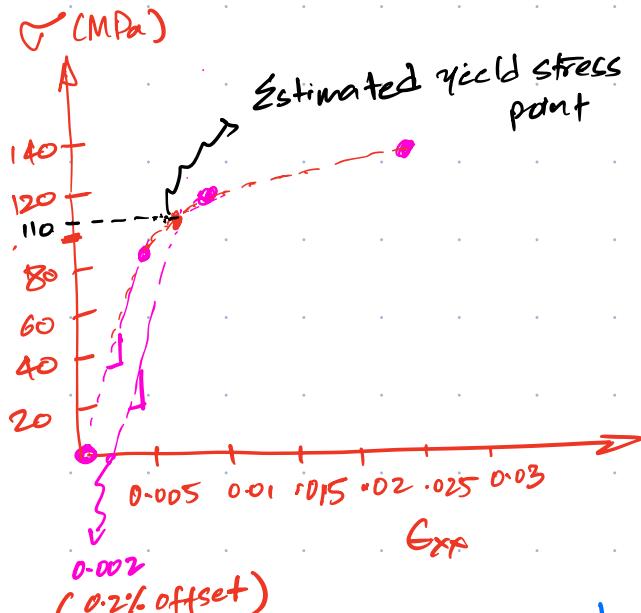
118 MPa

↳ OR we can draw a 0.2%  
strain offset line parallel to the  
linear portion & look for the point of  
intersection.

**SOLUTION HWI PQ**

(12)

- ② Plot the data given. Interpret the plot



↳ Linear region is upto 85 MPa  
↳ Material may be brittle-based on the data shown

- ③ Estimate the Young's modulus, yield stress and ultimate stress

↳ Young's modulus is the slope of the linear portion of the data

$$y_1 = Ex \Rightarrow 8.5 \times 10^6 \text{ Pa} = E \quad (6.005) \\ \Rightarrow E = 17 \text{ GPa}$$

↳ Yield stress: Point of intersection of 0.2% strain offset line, drawn parallel to the linear portion of the data, i.e.,  $\approx 110 \text{ MPa}$

↳ Ultimate stress: Stress value where the material fails.

↳ From the problem statement that is  $128 \text{ MPa}$