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***** Question 1 *****

Q1 a) Equations of motion of the Non-Linear system:

cart acceleration, $\ddot{x} =$

$$-(l_1 m_1 \sin(\theta_1) \dot{\theta}_1^2 + l_2 m_2 \sin(\theta_2) \dot{\theta}_2^2 - F + g m_1 \cos(\theta_1) \sin(\theta_1) - g m_2 \cos(\theta_2) \sin(\theta_2)) / (m_1 \sin(\theta_1)^2 + m_2 \sin(\theta_2)^2 + M)$$

pendulum 1 acceleration, $\ddot{\theta}_1 =$

$$-(g \sin(\theta_1) + (\cos(\theta_1) (l_1 m_1 \sin(\theta_1) \dot{\theta}_1^2 + l_2 m_2 \sin(\theta_2) \dot{\theta}_2^2 - F + g m_1 \cos(\theta_1) \sin(\theta_1) - g m_2 \cos(\theta_2) \sin(\theta_2))) / (m_1 \sin(\theta_1)^2 + m_2 \sin(\theta_2)^2 + M)) / l_1$$

pendulum 2 acceleration, $\ddot{\theta}_2 =$

$$-(g \sin(\theta_2) + (\cos(\theta_2) (l_1 m_1 \sin(\theta_1) \dot{\theta}_1^2 + l_2 m_2 \sin(\theta_2) \dot{\theta}_2^2 - F + g m_1 \cos(\theta_1) \sin(\theta_1) - g m_2 \cos(\theta_2) \sin(\theta_2))) / (m_1 \sin(\theta_1)^2 + m_2 \sin(\theta_2)^2 + M)) / l_2$$

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Q1 b) State Space representation of our Linearized system:

A Matrix:

$$\begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & -(g m_1) / M & 0 & (g m_2) / M & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & -(g + (g m_1) / M) / l_1 & 0 & (g m_2) / (M l_1) & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & -(g m_1) / (M l_2) & 0 & -(g - (g m_2) / M) / l_2 & 0 \end{bmatrix}$$

B Matrix:

$$\begin{bmatrix} 0 \\ 1/M \\ 0 \\ 1/(M l_1) \\ 0 \\ 1/(M l_2) \end{bmatrix}$$

C Matrix:

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

D Matrix:

$$0$$

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Q1 c) Checking conditions on controllability :

$$-(g^6 \cdot l_1^2 - 2 \cdot g^6 \cdot l_1 \cdot l_2 + g^6 \cdot l_2^2) / (M^6 \cdot l_1^6 \cdot l_2^6)$$

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Q1 d) Substitute the values in the matrices, obtain LQR controller, simulate response and certify local/global stability: ↙

Substituting M =1000 Kg, m1=m2=100 Kg, l1=20m, l2=10m, g=9.8m/s

A matrix:

0	1.0000	0	0	0	0
0	0	-0.9800	0	0.9800	0
0	0	0	1.0000	0	0
0	0	-0.5390	0	0.0490	0
0	0	0	0	0	1.0000
0	0	-0.0980	0	-0.8820	0

B matrix:

1.0e-03 *

0
1.0000
0
0.0500
0
0.1000

Rank of the controllability matrix :

6

It is full rank matrix, so the system at equilibrium is controllable.

The Open loop poles are:

0.0000 + 0.9313i
 0.0000 - 0.9313i
 -0.0000 + 0.7441i
 -0.0000 - 0.7441i
 0.0000 + 0.0000i
 0.0000 + 0.0000i

Designing Linear Quadratic Regulator...

Q matrix :

2000	0	0	0	0	0
0	10	0	0	0	0
0	0	1500000	0	0	0
0	0	0	10	0	0
0	0	0	0	2000000	0
0	0	0	0	0	10

R matrix :

1.0000e-04

LQR optimal gain matrix :

1.0e+05 *

0.0447 0.1426 1.1610 0.5137 0.9684 -1.0504

Closed Loop System Matrix (Ac):

Closed Loop poles:

-2.7678 + 2.8972i

-2.7678 - 2.8972i

-0.1197 + 0.7599i

-0.1197 - 0.7599i

-0.2757 + 0.3873i

-0.2757 - 0.3873i

all poles have real negative components, closed loop the system is stable by the Lyapunov's indirect method.

***** end of Question 1 *****

***** Question 2 *****

Q2 e) Check observability conditions:

Checking Observability condition ..

Rank with only x(t) 6

Rank with theta1, theta2: 4

Rank with x, theta2: 6

Rank with x, theta1, theta2: 6

Qn f) Designing Luenberger Observer..

For the Linearized System :

The real part of leftmost pole in the LQR closed loop system is

-2.7678

Lets choose the desired observer poles to be lesser than that

-3.8500 -4.7500 -3.5000 -3.4000 -3.1500 -2.9000

Qn g) Designing LQG Controller..

Kalman Observer Gain:

0.1448

0.0105

0.0063

0.0008

-0.0066

-0.0011

Warning: Simulation will start at a nonzero initial time.

> In DynamicSystem.checkLsimInputs (line 92)

In DynamicSystem/lsim (line 67)

In controller (line 305)

****End****

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