

Parts and assemblies engineering

Lab-2

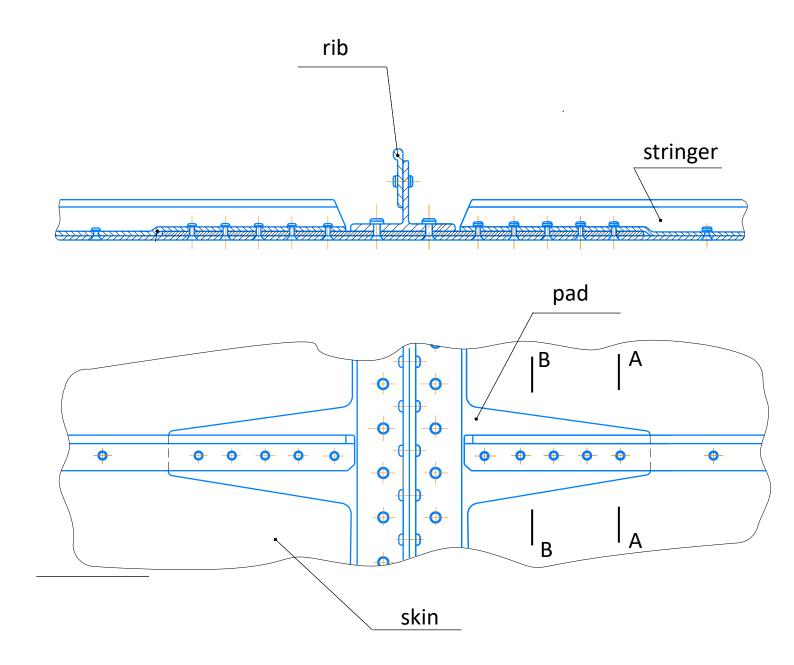


The task

Design the overlap joint (rivet) between two stringers and the rib

The goals of task:

- Determine the number of rivets
- Calculate the diameter of rivet
- And determine the overlap joint position between two stringers and rib with pad
- Determine the thickness and dimensions of pad





1. Choose the task variant and obtain maximum tensile load for stringer:

$$P_{\text{max_str}} = A_{str} \cdot \sigma_{B_str} \text{ or } P_{\text{max_str}} = P \cdot 1.3$$

| Type of stringer | | Dimer | Cross-section area, $[mm^2]$ | | |
|------------------|----|-------|------------------------------|---|----|
| 710012 | Н | В | S=S1 | а | 6E |
| | 20 | 15 | 1.5 | 2 | 65 |

| | Variants | | | |
|-------------------|----------|--------|--------|--------|
| Variants | 1 | 2 | 3 | 4 |
| Type of stringers | 710010 | 710003 | 710020 | 710012 |
| P, N | 13500 | 10000 | 190000 | 24000 |

2. Choose the materials of stringers, pad and skin



Table – Variants of Task

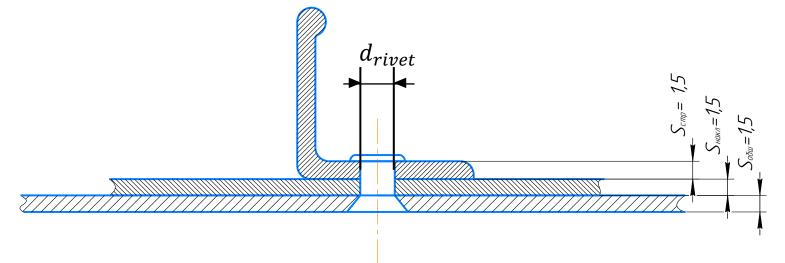
| | Variants | | | | | | | | |
|-------------------|----------|--------|--------|--------|--------|--------|--------|--|--|
| Variants | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | |
| Type of stringers | 710010 | 710003 | 710020 | 710012 | 420069 | 420075 | 710017 | | |
| P, N | 13500 | 10000 | 19000 | 24000 | 27000 | 38000 | 23000 | | |



3. Preliminary diameter of rivet calculate by equation:

$$d_{\text{rivet}} = 2\sqrt{t_{total}}$$
, where $t_{total} = t_{str} + t_{skin} + t_{pad}$

 t_{str} = S or S1 - thickness of stringer, t_{skin} - thickness of skin, t_{pad} - thickness of pad



For preliminary calculation thickness of skin and pad equal 1.5 mm



4. Checking of tensile stress:

$$\sigma \leq [\sigma]$$
, where $\sigma = \frac{P_{\text{max_str}}}{A_{str} - d_{\text{rivet}} \cdot t_{str}}$

The value of $[\sigma]$ is equal to $[\sigma] = 0.8 \cdot \sigma_{B,srt}$;

5. Calculate the coefficient of safety η :

$$\eta = \frac{\lfloor \sigma \rfloor}{\sigma}$$
, ideally $\eta = [1...1.5]$



6. After assuming the material and diameter of the rivet we can calculate the requirable number of rivets :

$$n_{rivet} = \frac{P_{\text{max_str}}}{P_{rivet}};$$

where P_{rivet} - determine the cutting force of rivet with GOST 134104-80 data and the maximum number of rivets in a row along stringers axis a 5...6;

For different diameter of rivet find the minimum cutting force for rivet from the table (in the next slide)



Cutting force of rivet P_{rivet}, kN (1000*N)

Name of material

| Мерке | Минимельные разрушающие нагрузки на одинарный сроз, $\frac{\kappa H}{\kappa rc}$ Диаметр заклепки d , мм | | | | | | | | | | | | | | |
|-----------|--|--------------|---------------|---------------|------|---------------|---------------|---------------|---------------|---------------|-----------------|----------------------|-----------------|-----------------|-------|
| чатериала | | 2 | 2 | ,6 | | 3 | | ,5 | | 4 | T | 5 | | 6 | |
| -10 | 2,0 | 2,1 | 2,6 | 2,7 | 3,0 | 3,1 | 3,5 | 3,6 | 4,0 | 4,1 | 5,0 | 5,1 | 6,0 | 6,15 | 1 |
| 10 | 1,05 | 1,15 | 1,77 180,4 | 1,91 194,6 | 2,35 | 2,51 256,5 | 3,16 | 3,39 345,9 | 4.18 | 4,40 | 6,54 667,2 | 6,80 694,2 | 9,42 | 9,89 1009,5 | |
| 20Г2 | - | - | - | - | - | - | 4,65 | 4,98 508,7 | 6,15 628,0 | 6,47 659,8 | 9,62 | 10.00 | 13,85 | 14,55 1484,6 | |
| 2X18H9T | 1,35 | 1,49 | 2,29 | 2,47 251,8 | 3,05 | 3,25 | 4,09 | 4,39 | 5,42 552,6 | 5,69 580,6 | 8,46 863,5 | 8,80 | 12,18 | 12,80 1306,4 | |
| ХН78Т | - | - | - | - | 3,12 | 3,33 | 4,19 | 4,49 457,8 | 5,54 565,2 | 5,82 593,8 | 883,1 | 9,00 | - | - | |
| хнеовт | - | - | - | - | 3,46 | 3,70 | 4,65 | 4,98 508.7 | 6,15 628,0 | 6,47 659,8 | 9,62 | 10,00 | - | - | |
| B65 | - | - | 1,30 | 1,40 | 1,73 | 1,85 | 2,33 | 2,49 254,4 | 3,08 | 3,23 | 4,81 | 5,00 510,4 | 6,92 706,5 | 742,5 | 1 |
| IRS-IMA | 0,50 | 0,54 55,4 | 0,83 | 0.90 | 1,11 | 1,19 | 1,49 151,9 | 1,60 162,8 | 1,97 | 2,07 | 3,08 | 3,20 | 4,43 | 4,66 475,0 | |
| дів | 0,60 | 0,64 | 0,99 | 1,06 108,7 | 1,32 | 1,40 | 1,77 180,4 | 1,89 | 2,34 238,6 | 2,46 250,7 | 3,65 | 3,80 | 5,26 536,9 | 5,53 564,1 | 14.00 |
| дзеп | - | - | 1,46 | 1,57 | 1,94 | 2,07 211,2 | 2,60 265,8 | 2,79 284,9 | 3,45 351,7 | 3.62 369,5 | 5,38 549,5 | <u>5,60</u> 571,7 | 7,75 | 8,15 | |
| BT16 | _ | - | 2,86 | 3,08 | 3,81 | 4,07 | 5,18 | 5,48 559,6 | 6,77 690,8 | 7,11 | 10.58 1079,4 | 11,00 1123,0 | 15,23 1554,3 | 16,00 1633,0 | ١١٥ |

Diameter of rivet d, mm

The cutting force P_{rivet}, [kN] for rivet with d=4 mm using 12X18H9T material



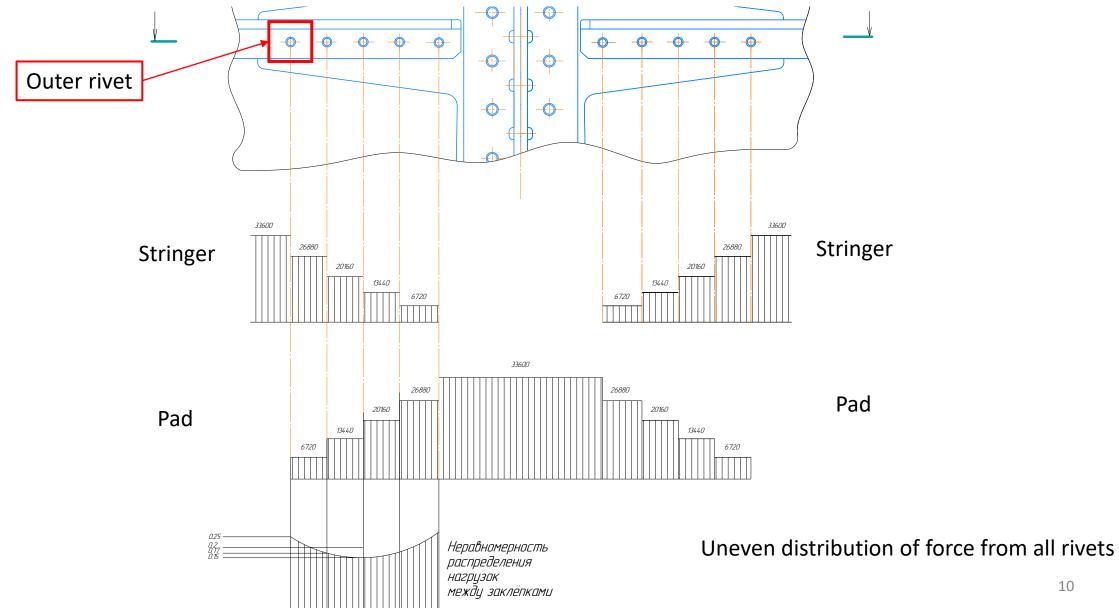
7. Check for crumbling of stringer under rivet:

$$\sigma_{crumbling} = \frac{P_{rivet}}{d_{rivet} \cdot t_{str}} \le 1.3 \dots 1.5 \cdot \sigma_{B,str};$$

8. And calculate the coefficient of safety η :

$$\eta = \frac{[\sigma]}{\sigma_{crumbling}}$$
, ideally $\eta = [1.2 \dots 1.6]$, $[\sigma] = 1.3 \cdot \sigma_{B,srt}$;







7. Check the coefficient of safety η for unevenly distributed force.

How we can see from last slide, the outer rivet has a maximum value from distributed force, so:

$$P_{rivet,outer} = 0.25 \cdot P_{\text{max_str}}$$

8. And calculate the coefficient of safety η :

$$\eta = \frac{P_{rivet}}{P_{rivet,outer}}$$
, ideally $\eta = [1.2 ... 1.6]$



9. Checking the edge distance m for cutting failure:

$$2 \cdot d_{\text{rivet}} \leq m \leq 2 \cdot d_{\text{rivet}} + 2$$
;

10. Calculate the actual shear stresses from cutting force:

$$\tau_{act} = \frac{P_{\text{max_riv}}}{2 \cdot m \cdot t_{str}} < \tau_B;$$

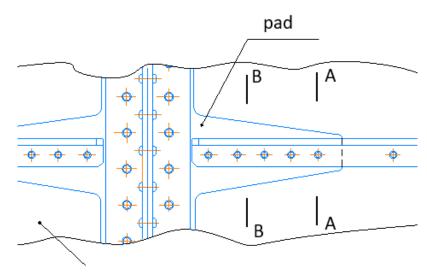
Where $\tau_B = (0.6 ... 065) \cdot \sigma_{B,str}$;



11. Analysis of pad:

Check the crumbling in A-A section, assuming the thickness and material of the pad:

$$\sigma_{crumbling,pad} = \frac{P_{\text{max_riv}}}{d_{\text{rivet}} \cdot t_{str}} \leq [\sigma]_{crumbling} = 1.3 \dots 1.5 \sigma_{B,pad};$$



One should use $\sigma_{B,riv}$ if $[\sigma]_{B,riv} \leq [\sigma]_{B,pad}$ in the upper expression;



12. Tension failure in A-A and B-B sections:

Calculating the stress:

$$\sigma_{A-A} = \frac{P_{\text{str}}}{A_{pad}}$$

$$\sigma_{A-A} = \frac{P_{\text{str}}}{t_{\text{pad}} \cdot (b_{min} - n_{rivet A-A} \cdot d_{rivet})} \le [\sigma]_{bear} = 1.3 \dots 1.5 \cdot \sigma_{B,pad};$$

where: k≈1,15...1,2 stress concentration factor



The minimum width b_{\min} of the pad in a section is obtained due to tension in section:

$$b_{\min A-A} = \frac{k \cdot P_{\max_riv}}{t_{\text{pad}} \cdot \sigma_{B_pad}} + n_{rivet\ A-A} \cdot d_{\text{rivet}}$$

where
$$n_{rivet A-A} = 1$$

 $n_{rivet\ A-A}$ -number of rivets in the section A-A (equal to 1) $\sigma_{B,pad}$ -strength of material of the pad



14. Calculate the length of the rivet:

For rivet joint the skin and stringers:

$$t_{stringer_skin} = t_{str} + t_{skin}$$

Check the length with GOST 1 10642-72

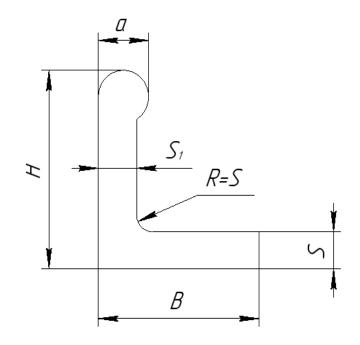
For rivet joint the skin, stringers and pad:

$$t_{total} = t_{str} + t_{skin} + t_{pad}$$

Check the length with GOST 1 10642-72

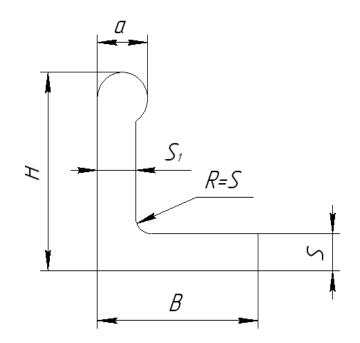
15. Sketch the joint and prepare the report of lab





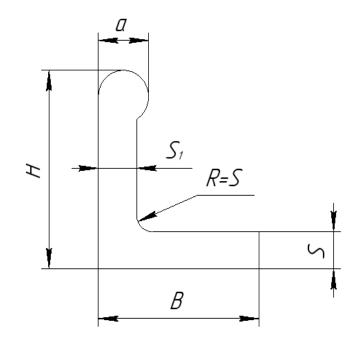
| Туре | | Dime | Cross-section area, $[mm^2]$ | | |
|--------|----|------|------------------------------|---|----|
| 710010 | Н | В | S=S1 | а | 37 |
| 710010 | 20 | 13 | 1.0 | 3 | 37 |





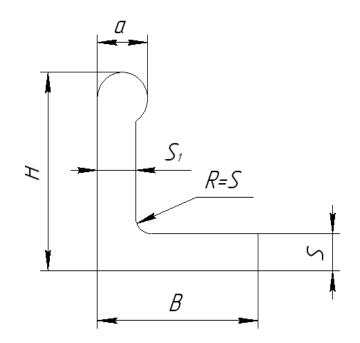
| Туре | | Dime | Cross-section area, $[mm^2]$ | | |
|--------|----|------|------------------------------|---|----|
| 710003 | Н | В | S=S1 | а | 37 |
| 710003 | 15 | 18 | 1.0 | 3 | 37 |





| Туре | | Dime | Cross-section area, $[mm^2]$ | | |
|--------|----|------|------------------------------|---|----|
| 710020 | Н | В | S=S1 | а | 52 |
| 710020 | 23 | 13 | 1.5 | 4 | 32 |

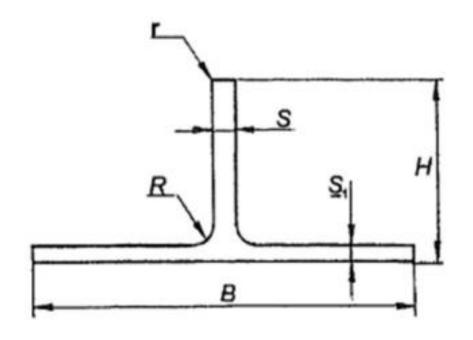




| Туре | | Dime | Cross-section area, $[mm^2]$ | | |
|--------|----|------|------------------------------|---|----|
| 710012 | Н | В | S=S1 | а | 65 |
| 710012 | 20 | 15 | 1.5 | 2 | 03 |



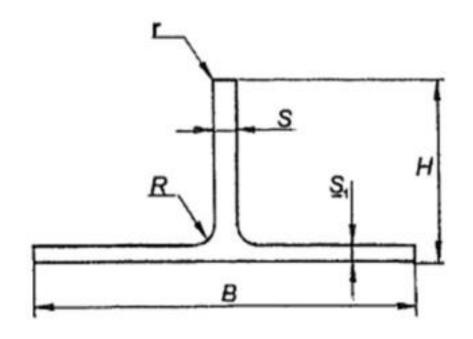
Table – Variants-5



| Туре | | Din | Cross- section area, $[mm^2]$ | | | |
|--------|----|-----|-------------------------------|-----|-----|----|
| 420060 | Η | В | S | S1 | R | 82 |
| 420069 | 20 | 30 | 1.5 | 2.0 | 2.0 | 62 |

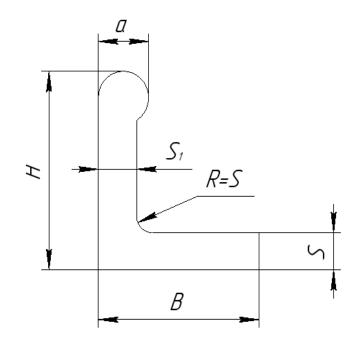


Table – Variants-6



| Туре | | Din | Cross- section area, $[mm^2]$ | | | |
|--------|----|-----|-------------------------------|-----|-----|-----|
| 420075 | Н | В | S | S1 | R | 105 |
| 420075 | 20 | 38 | 2.0 | 1.5 | 2.0 | 105 |





| Туре | | Dime | Cross-section area, $[mm^2]$ | | |
|--------|----|------|------------------------------|-----|----|
| 710017 | Н | В | S=S1 | а | 98 |
| 710017 | 20 | 20 | 1.5 | 3.5 | 30 |



Table – Material Properties

| Material | Ultimate tensile | Proof strength | Shear strength* | Modulus of | Shear modulus | Density, |
|----------|------------------------|---------------------|-------------------------------------|---------------|------------------|-----------------|
| | strength | σ_{02} , MPa | $\tau_{\rm B}, \tau_{\rm 02}$ (% of | elasticity | G,GPa | ρ g/cm^3 |
| | $\sigma_{\rm B}$, MPa | | tensile strength) | E, GPa | | |
| | | | Sur Fingury | | | |
| | | | | | | |
| 30ХГСА | 1100 | 850 | 63 | 210 | 78 | 7,85 |
| Д16Т | 450 | 300 | 50 | 72 | 28 | 2,8 |
| BT20 | 1000 | 910 | 50 | 110 | 44 | 4,5 |

^{* -} ultimate shear strength and proof strength are approximated by taking the denoted percentage of tensile ultimate and proof strength respectively



Link for section data, variants and PPT

