A general property of exact differentials :

consider f(x, y) and df = gdx + hdy, where  $g \equiv g(x, y)$  and  $h \equiv h(x, y)$ 

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U(S, V), dU = TdS - pdV

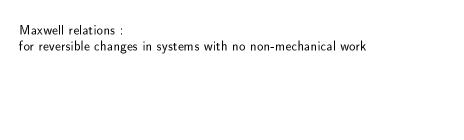
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$$U(S, V)$$
,  $dU = TdS - pdV$  when  $df$  is an exact differential, 
$$\left(\frac{\partial g}{\partial y}\right)_x = \frac{\partial^2 f}{\partial y \partial x} = \frac{\partial^2 f}{\partial x \partial y} = \left(\frac{\partial h}{\partial x}\right)_y$$

both x and y, vary



Maxwell relations : for reversible changes in systems with no non-mechanical work dU = TdS - pdV

$$\left(\frac{\partial T}{\partial V}\right)_{S} = -\left(\frac{\partial p}{\partial S}\right)_{V}$$

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$$\left(\frac{\partial T}{\partial \rho}\right)_{S} = \left(\frac{\partial V}{\partial S}\right)_{\rho}$$

$$dA = -SdT - pdV$$

$$\left(\frac{\partial p}{\partial T}\right) = \left(\frac{\partial S}{\partial V}\right)$$

$$\left(\frac{\partial p}{\partial T}\right)_{V} = \left(\frac{\partial S}{\partial V}\right)_{T}$$

Maxwell relations: for reversible changes in systems with no non-mechanical work dU = TdS - pdV

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$$\left(\frac{\partial T}{\partial p}\right)_{S} = \left(\frac{\partial V}{\partial S}\right)_{p}$$

 $\left(\frac{\partial V}{\partial T}\right)_{p} = -\left(\frac{\partial S}{\partial p}\right)_{T}$ 

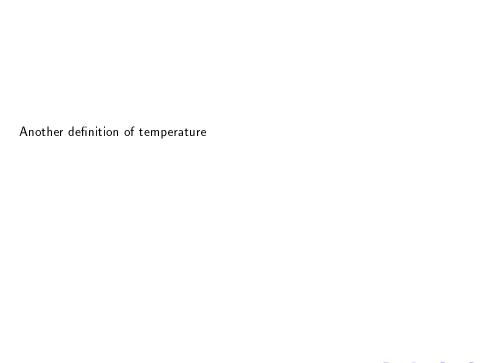
$$\left(\frac{\partial p}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T$$

$$\left(\frac{\partial p}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T$$
 
$$dG = Vdp - SdT$$

$$dA = -SdT - pdV$$

$$\left(\frac{\partial T}{\partial p}\right)_{S} = \left(\frac{\partial V}{\partial S}\right)_{p}$$

$$\left(\frac{\partial V}{\partial S}\right)_p$$



Another definition of temperature

$$dU = TdS - pdV \implies \boxed{\frac{1}{T} = \left(\frac{\partial S}{\partial U}\right)_V}$$

$$dU = TdS - pdV \implies \boxed{\frac{1}{T} = \left(\frac{\partial S}{\partial U}\right)_V}$$

 $dH = TdS + Vdp \implies \frac{1}{T} = \left(\frac{\partial S}{\partial H}\right)_p$ 

$$dU = TdS - pdV \implies \boxed{\frac{1}{T} = \left(\frac{\partial S}{\partial U}\right)}$$

Thermodynamic equation of state:

$$dU = TdS - pdV$$

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 $\left(\frac{\partial U}{\partial V}\right)_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$  or,  $\pi_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$ 





Thermodynamic equation of state:

$$dU = TdS - pdV$$

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 or,  $\pi_T = T\left(\frac{\partial S}{\partial V}\right)_T - \infty$   
xwell relation  $\left(\frac{\partial p}{\partial T}\right)_T = \left(\frac{\partial S}{\partial V}\right)_T$ 

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 or,  $\pi_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$   
Using Maxwell relation  $\left(\frac{\partial p}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T$ 

$$p$$
 or,  $\pi_T = T \left( rac{\partial S}{\partial V} 
ight)_T - 1$  or  $\left( rac{\partial p}{\partial T} 
ight)_V = \left( rac{\partial S}{\partial V} 
ight)_T$ 

 $\pi_T = T \left( \frac{\partial p}{\partial T} \right)_V - p$ 

Thermodynamic equation of state: dU = TdS - pdV

$$\begin{pmatrix} \frac{\partial U}{\partial V} \end{pmatrix}_T = T \begin{pmatrix} \frac{\partial S}{\partial V} \end{pmatrix}_T - p \quad \text{or, } \pi_T = T \begin{pmatrix} \frac{\partial S}{\partial V} \end{pmatrix}_T - p$$
 Using Maxwell relation 
$$\begin{pmatrix} \frac{\partial p}{\partial T} \end{pmatrix}_V = \begin{pmatrix} \frac{\partial S}{\partial V} \end{pmatrix}_T$$

 $\pi_T = T \left( \frac{\partial p}{\partial T} \right)_V - p$ 

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For perfect gas, show that this leads to  $\pi_T = 0$ 

Thermodynamic equation of state: dU = TdS - pdV

$$-pdV$$

 $\left(\frac{\partial U}{\partial V}\right)_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$  or,  $\pi_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$ 

$$\left(\frac{\partial \mathcal{O}}{\partial \mathcal{V}}\right)_T = I\left(\frac{\partial \mathcal{S}}{\partial \mathcal{V}}\right)_T - \rho$$
 or,  $\pi_T = I\left(\frac{\partial \mathcal{S}}{\partial \mathcal{V}}\right)_T - V$   
Using Maxwell relation  $\left(\frac{\partial \mathcal{P}}{\partial \mathcal{T}}\right)_V = \left(\frac{\partial \mathcal{S}}{\partial \mathcal{V}}\right)_T$ 

$$\pi_T = T \left( \frac{\partial p}{\partial T} \right)_V - p$$

For perfect gas, show that this leads to 
$$\pi_{\mathcal{T}}=0$$

Find for van der Waals gas.,  $\pi_T = a \frac{n^2}{V^2}$ 

Thermodynamic equation of state:

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 $\left(\frac{\partial U}{\partial V}\right)_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$  or,  $\pi_T = T\left(\frac{\partial S}{\partial V}\right)_T - p$ 

Using Maxwell relation 
$$\left(\frac{\partial p}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T$$

$$\pi_T = T \left( \frac{\partial p}{\partial T} \right)_V - p$$

For perfect gas, show that this leads to 
$$\pi_{\mathcal{T}}=0$$

Find for van der Waals gas.,  $\pi_T = a \frac{n^2}{V^2} > 0 \implies \left(\frac{\partial U}{\partial V}\right)_T > 0$ 

Gibbs' Free energy and entropy

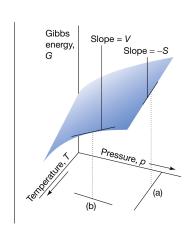
Gibbs' Free energy and entropy

$$\left(\frac{\partial G}{\partial T}\right)_p = -S < 0$$

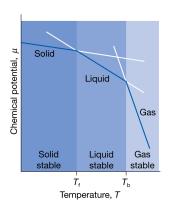
## Gibbs' Free energy and entropy

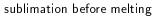
$$\left(\frac{\partial G}{\partial T}\right)_{p} = -S < 0$$

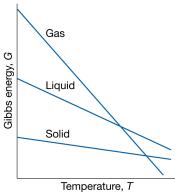
$$\left(\frac{\partial G}{\partial p}\right)_{T} = V > 0$$

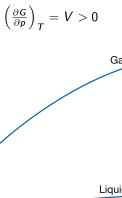


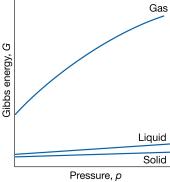
## chemical potential and phase equilibrium : $\left( rac{\partial \mu}{\partial T} ight)_p = -S_m$











$$\left(\frac{\partial G}{\partial T}\right)_p = \frac{G - H}{T}$$

$$\left(\frac{\partial G}{\partial T}\right)_p = \frac{G - H}{T}$$

Use this to show : 
$$\left(\frac{\partial \left[\frac{c}{T}\right]}{\partial T}\right)_p = -\frac{H}{T^2}$$

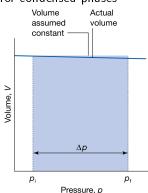
$$\left(\frac{\partial \left[\frac{G}{T}\right]}{\partial T}\right) =$$

Change in G with  $p: G(p_f) = G(p_i) + \int\limits_{p_i}^{p_f} Vdp$ 

## Change in G with $p: G(p_f) = G(p_i) + \int\limits_{p_i}^{p_f} Vdp$

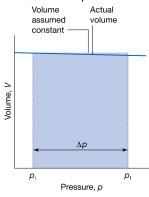
for condensed phases

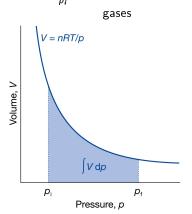
gases



## Change in G with $p: G(p_f) = G(p_i) + \int_{n}^{p_f} Vdp$

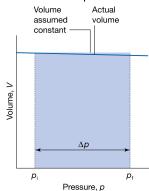
for condensed phases





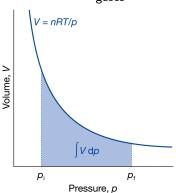
Change in G with 
$$p: G(p_f) = G(p_i) + \int_{p_i}^{p_f} V dp$$

for condensed phases



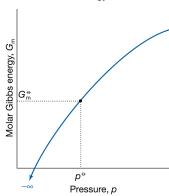
$$G_m(p_f) = G_m(p_i) + V_m(p_f - p_i)$$





$$G_m(p_f) = G_m(p_i) + V_m(p_f - p_i)$$
  $G_m(p_f) = G_m(p_i) + RT \int_{p_i}^{p_f} \frac{dp}{p} = G_m(p_i) + RT \ln \frac{p_f}{p_i}$ 

molar Gibbs energy vs p :  $G_m(p) = G_m^\circleddash + RT \ln rac{p}{p^\circleddash}$ 



molar Gibbs energy vs p :  $G_m(p) = G_m^{\odot} + RT \ln \frac{f}{p^{\odot}}$ ; f (fugacity) =  $\underbrace{\phi}_{\text{fugacity coeff}}$ .p

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 $\int\limits_{p'}^{p} V_m dp = G_m(p) - G_m(p') = \left\{ G_m^{\odot} + RT \ln \frac{f}{p^{\odot}} \right\} - \left\{ G_m^{\odot} + RT \ln \frac{f'}{p^{\odot}} \right\}$ 

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;  $f$  (fugacity) =  $\underbrace{\phi}_{\text{fugacity coeff}}$ .  $\underbrace{f}_{\text{fugacity coeff}}$   $\underbrace{f}_{\text{fugacity coeff}}$   $\underbrace{f}_{\text{fugacity coeff}}$   $\underbrace{f}_{\text{fugacity coeff}}$   $\underbrace{f}_{\text{fugacity coeff}}$   $\underbrace{f}_{\text{fugacity coeff}}$ 

$$\int_{p'}^{p} V_{\text{perfect}, m} dp = RT \int_{p'}^{p} \frac{dp}{p} = RT \ln \frac{p}{p'}$$

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molar Gibbs energy vs p: 
$$G_m(p) = G_m^{\ominus} + RT \ln \frac{r}{p^{\ominus}}$$
;  $f$  (fugacity)  $= \underbrace{\phi}_{\text{fugacity coeff}}$ .  $f$ 

$$\int_{-\infty}^{p} V_m dp = G_m(p) - G_m(p') = \left\{ G_m^{\ominus} + RT \ln \frac{f}{p^{\ominus}} \right\} - \left\{ G_m^{\ominus} + RT \ln \frac{f'}{p^{\ominus}} \right\}$$

$$\int\limits_{p'}^{p} V_{\mathsf{perfect},\,m} dp = RT \int\limits_{p'}^{p} \frac{dp}{p} = RT \ln \frac{p}{p'}$$

$$\int\limits_{p'}^{p} \left( V_m - V_{\mathsf{perfect},\,m} \right) dp = RT \left( \ln \frac{f}{f'} - \ln \frac{p}{p'} \right)$$

molar Gibbs energy vs p :  $G_m(p) = G_m^{\odot} + RT \ln \frac{f}{p^{\odot}}; \quad f \text{ (fugacity)} = \underbrace{\phi} .p$ 

fugacity coeff 
$$\int_{-\infty}^{p} V_m dp = G_m(p) - G_m(p') = \left\{ G_m^{\odot} + RT \ln \frac{f}{p^{\odot}} \right\} - \left\{ G_m^{\odot} + RT \ln \frac{f'}{p^{\odot}} \right\}$$

$$\begin{split} &\int\limits_{p'}^{p} V_{\mathsf{perfect},\,m} dp = RT \int\limits_{p'}^{p} \frac{dp}{p} = RT \ln \frac{p}{p'} \\ &\int\limits_{p'}^{p} \left( V_m - V_{\mathsf{perfect},\,m} \right) dp = RT \left( \ln \frac{f}{f'} - \ln \frac{p}{p'} \right) \\ &\mathsf{or,} \ln \frac{f}{p} - \ln \frac{f'}{p'} = \frac{1}{RT} \int\limits_{p'}^{p} \left( V_m - V_{\mathsf{perfect},\,m} \right) dp \end{split}$$

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$$\int_{-p}^{p} V_m dp = G_m(p) - G_m(p') = \left\{ G_m^{\odot} + RT \ln \frac{f}{p^{\odot}} \right\} - \left\{ G_m^{\odot} + RT \ln \frac{f'}{p^{\odot}} \right\}$$

$$\begin{split} &\int\limits_{p'}^{p} V_{\mathrm{perfect},\,m} dp = RT \int\limits_{p'}^{p} \frac{dp}{p} = RT \ln \frac{p}{p'} \\ &\int\limits_{p'}^{p} \left( V_{m} - V_{\mathrm{perfect},\,m} \right) dp = RT \left( \ln \frac{f}{f'} - \ln \frac{p}{p'} \right) \\ &\text{or, } \ln \frac{f}{p} - \ln \frac{f'}{p'} = \frac{1}{RT} \int\limits_{p'}^{p} \left( V_{m} - V_{\mathrm{perfect},\,m} \right) dp \end{split}$$

 $\underset{p\to 0}{\mathcal{L}t} f \to p$ 

molar Gibbs energy vs p :  $G_m(p) = G_m^{\odot} + RT \ln \frac{f}{p^{\odot}}$ ; f (fugacity) =  $\phi$  .p

 $\int\limits_{-r}^{p} V_{m} dp = G_{m}(p) - G_{m}(p') = \left\{ G_{m}^{\odot} + RT \ln \frac{f}{p^{\odot}} \right\} - \left\{ G_{m}^{\odot} + RT \ln \frac{f'}{p^{\odot}} \right\}$ 

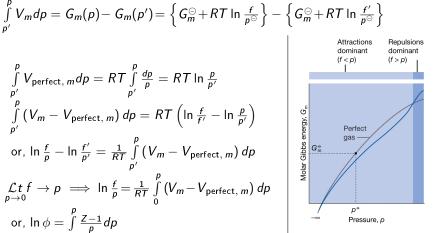
$$\int_{p'}^{p} V_{\text{perfect}, m} dp = RT \int_{p'}^{p} \frac{dp}{p} = RT \ln \frac{p}{p'}$$

$$\int_{p'}^{p} (V_m - V_{\text{perfect}, m}) dp = RT \left( \ln \frac{f}{f'} - \ln \frac{p}{p'} \right)$$
or,  $\ln \frac{f}{p} - \ln \frac{f'}{p'} = \frac{1}{RT} \int_{p'}^{p} (V_m - V_{\text{perfect}, m}) dp$ 

$$\mathcal{L}t f \to p \implies \ln \frac{f}{p} = \frac{1}{RT} \int_{0}^{p} (V_m - V_{\text{perfect}, m}) dp$$

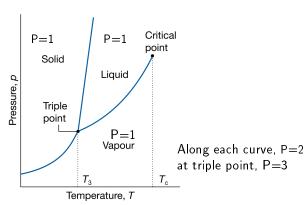
molar Gibbs energy vs p :  $G_m(p) = G_m^{\odot} + RT \ln \frac{f}{p^{\odot}}$ ; f (fugacity) =  $\phi$ fugacity coeff

$$\begin{split} &\int\limits_{p'}^{p} V_{\mathrm{perfect},\,m} dp = RT \int\limits_{p'}^{p} \frac{dp}{p} = RT \ln \frac{p}{p'} \\ &\int\limits_{p'}^{p} \left( V_{m} - V_{\mathrm{perfect},\,m} \right) dp = RT \left( \ln \frac{f}{f'} - \ln \frac{p}{p'} \right) \\ &\text{or, } \ln \frac{f}{p} - \ln \frac{f'}{p'} = \frac{1}{RT} \int\limits_{p'}^{p} \left( V_{m} - V_{\mathrm{perfect},\,m} \right) dp \\ &\mathcal{L}t \, f \to p \implies \ln \frac{f}{p} = \frac{1}{RT} \int\limits_{0}^{p} \left( V_{m} - V_{\mathrm{perfect},\,m} \right) dp \\ &\text{or, } \ln \phi = \int\limits_{0}^{p} \frac{Z - 1}{p} dp \end{split}$$



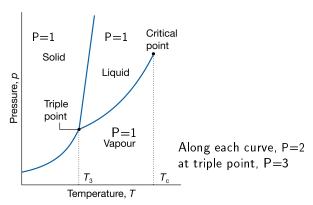
phase : form of matter that is uniform throughout in chemical composition and physical state P=# phases in a system

Phase equilibria - triple point  $(T_3)$  and critical point  $(T_C)$ 



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Phase equilibria - triple point  $(T_3)$  and critical point  $(T_C)$ 



For water :  $T_3 = 273.16$  K and 611 Pa (6.11 mbar)

- Triple point marks the lowest pressure at which a liquid phase can exist
- ▶ If the slope of the solid—liquid phase boundary is positive
- then triple point also marks the lowest temperature at which the liquid

can exist

the critical temperature is the upper limit

F=# degrees of freedom, C=# components, P=# phases

F = #degrees of freedom, C = #components, P = #phases

single-component, single-phase

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single-component, single-phase

$$F = 1 - 1 + 2 = 2$$

F = #degrees of freedom, C = #components, P = #phases

 $single-component,\ single-phase$ 

$$F = 1 - 1 + 2 = 2$$
 single-component, two-phases

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single-component, single-phase

$$F = 1 - 1 + 2 = 2$$
  
single-component, two-phases  
 $F = 1 - 2 + 2 = 1$ 

F = #degrees of freedom, C = #components, P = #phases

single-component, single-phase

$$F=1-1+2=2$$
 single-component, two-phases  $F=1-2+2=1$  phases  $\alpha$  and  $\beta$  in equilibr. at given  $p,\ T$   $\mu_{\alpha}\left(p,\ T\right)\!=\!\mu_{\beta}\left(p,\ T\right)$  eqn. relates  $p$  and  $T$ ,

so only one variable is independent

F = #degrees of freedom, C = #components, P = #phases

single-component, single-phase

$$F=1-1+2=2$$
 single-component, two-phases  $F=1-2+2=1$  phases  $\alpha$  and  $\beta$  in equilibr. at given  $p,\ T$   $\mu_{\alpha}\left(p,\ T\right)=\mu_{\beta}\left(p,\ T\right)$  eqn. relates  $p$  and  $T$ , so only one variable is independent

single-component

F = # degrees of freedom, C = # components, P = # phases

 $single-component,\ single-phase$ 

F = 1 - 1 + 2 = 2

single-component, two-phases 
$$F=1-2+2=1$$
 phases  $\alpha$  and  $\beta$  in equilibr. at given  $p,\ T$   $\mu_{\alpha}\left(p,\ T\right)\!=\!\mu_{\beta}\left(p,\ T\right)$  eqn. relates  $p$  and  $T$ ,

so only one variable is independent

single-component three-phases

F = # degrees of freedom, C = # components, P = # phases

single-component, single-phase

F = 1 - 1 + 2 = 2

single-component, two-phases 
$$F=1-2+2=1$$
 phases  $\alpha$  and  $\beta$  in equilibr. at given  $p,\ T$   $\mu_{\alpha}\left(p,\ T\right)\!=\!\mu_{\beta}\left(p,\ T\right)$  eqn. relates  $p$  and  $T$ ,

so only one variable is independent

 $\begin{aligned} & \text{single-component} \\ & \text{three-phases} \\ & \textit{F} = 1 - 3 + 2 = 0 \end{aligned}$ 

F = # degrees of freedom, C = # components, P = # phases

 $single-component,\ single-phase$ 

F = 1 - 1 + 2 = 2

single-component, two-phases 
$$F=1-2+2=1$$
 phases  $\alpha$  and  $\beta$  in equilibr. at given  $p,\ T$   $\mu_{\alpha}\left(p,\ T\right)\!=\!\mu_{\beta}\left(p,\ T\right)$  eqn. relates  $p$  and  $T$ , so only one variable is independent

single-component three-phases F=1-3+2=0 phases  $\alpha$ ,  $\beta$  and  $\gamma$  in equilibr. at given p, T,  $\mu(\alpha, p, T)=\mu(\beta, p, T)$   $=\mu(\gamma, p, T)$ 

F = #degrees of freedom, C = #components, P = #phases

 $single-component,\ single-phase$ 

$$F=1-1+2=2$$
 single-component, two-phases  $F=1-2+2=1$  phases  $\alpha$  and  $\beta$  in equilibr. at given  $p,\ T$   $\mu_{\alpha}\left(p,\ T\right)=\mu_{\beta}\left(p,\ T\right)$  eqn. relates  $p$  and  $T$ , so only one variable is independent

single-component three-phases F=1-3+2=0 phases  $\alpha$ ,  $\beta$  and  $\gamma$  in equilibr. at given p, T,  $\mu(\alpha, p, T)=\mu(\beta, p, T)$   $=\mu(\gamma, p, T)$ 

two eqns. for two unknowns  $\it p$  and  $\it T$ 

F = #degrees of freedom, C = #components, P = #phases

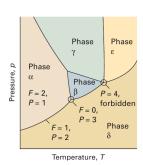
single-component, single-phase

$$F=1-1+2=2$$
 single-component, two-phases  $F=1-2+2=1$  phases  $\alpha$  and  $\beta$  in equilibr. at given  $p, T$   $\mu_{\alpha}\left(p, T\right) = \mu_{\beta}\left(p, T\right)$  eqn. relates  $p$  and  $T$ , so only one variable is independent

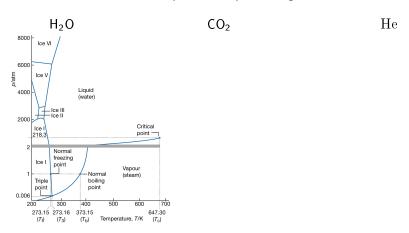
single-component three-phases F=1-3+2=0 phases  $\alpha$ ,  $\beta$  and  $\gamma$  in equilibr. at given p, T,  $\mu\left(\alpha,\,p,\,T\right)=\mu\left(\beta,\,p,\,T\right)=\mu\left(\gamma,\,p,\,T\right)$  two eqns. for two unknowns p and T fixed soln.

so no variation possible

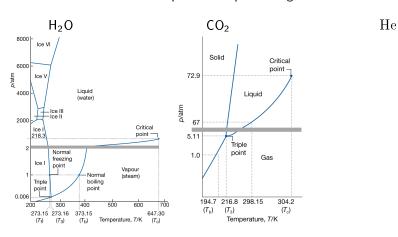
# Typical phase diagram



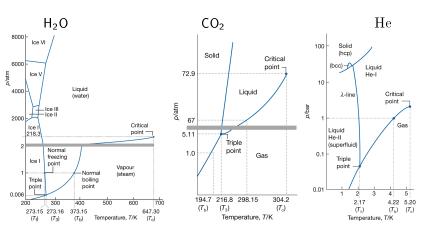
# Experimental phase diagrams



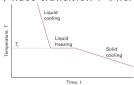
# Experimental phase diagrams



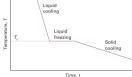
### Experimental phase diagrams



# ${\color{blue} Phase \ transition: Thermal \ analysis \ and \ Cooling \ curve}$



 $\begin{array}{c} \textbf{P}_{\textbf{h}} \textbf{ase}_{\textbf{transition}}: \textbf{Thermal analysis and Cooling curve} \\ \end{array}$ 



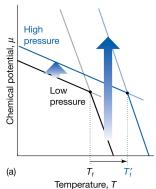
metastable phases: Kinetic barriers

Response of melting to applied pressure

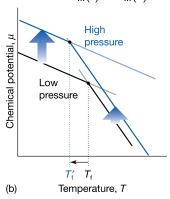
Response of melting to applied pressure

pressure-dependence of chemical potential :  $\left(rac{\partial \mu}{\partial 
ho}
ight)_T = V_m$ 

usual liquids :
$$V_m(I) > V_m(s)$$



water:  $V_m(I) < V_m(s)$ 



$$G_m(p) = G_m^{\odot} + RT \ln rac{p}{p^{\odot}}$$

$$G_m(p) - G_m + KT \prod$$

 $\implies \mu(p) = \mu^{\odot} + RT \ln \frac{p}{p^{\odot}} \stackrel{p^{\odot}=1}{=} \mu^{\odot} + RT \ln p$ 

location of phase boundaries :  $\left(\frac{\partial p}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T = \frac{\Delta_{\mathrm{trs}}S}{\Delta_{\mathrm{trs}}V}$ 

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solid/liq.:  $\frac{dp}{dT} = \frac{\Delta_{\text{fus}}H}{T\Delta_{\text{fus}}V}$ 

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, moving state of system to b

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relation between dp and dT ensures that system remains in equilibrium as either variable is changed

