

# **Automatic Generation Control**

## **2.1 Introduction**

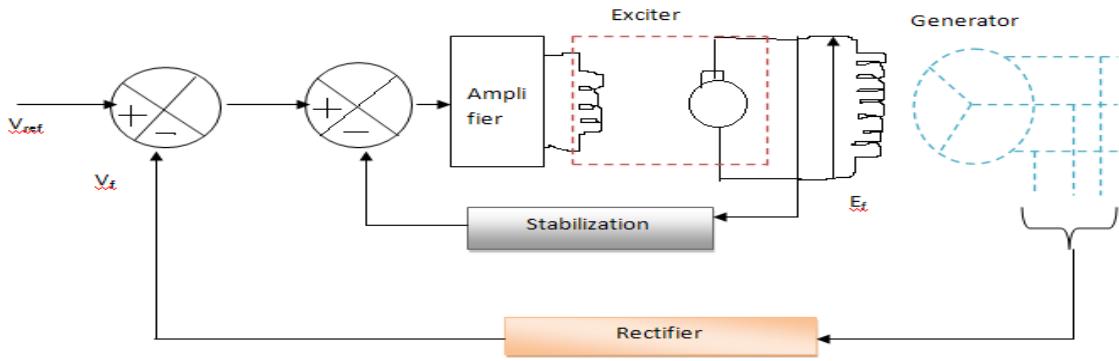
The main objective of power system operation and control is to maintain continuous supply of power with an acceptable quality, to all the consumers in the system. The system will be in equilibrium, when there is a balance between the power demand and the power generated. As the power in AC form has real and reactive components: the real power balance; as well as the reactive power balance is to be achieved.

There are two basic control mechanisms used to achieve reactive power balance (acceptable voltage profile) and real power balance (acceptable frequency values). The former is called the automatic voltage regulator (AVR) and the latter is called the automatic load frequency control (ALFC) or automatic generation control (AGC).

## **2.2 Generator Voltage Control System**

The voltage of the generator is proportional to the speed and excitation (flux) of the generator. The speed being constant, the excitation is used to control the voltage. Therefore, the voltage control system is also called as excitation control system or automatic voltage regulator (AVR).

For the alternators, the excitation is provided by a device (another machine or a static device) called exciter. For a large alternator the exciter may be required to supply a field current of as large as 6500A at 500V and hence the exciter is a fairly large machine. Depending on the way the dc supply is given to the field winding of the alternator (which is on the rotor), the exciters are classified as: i) DC Exciters; ii) AC Exciters; and iii) Static Exciters. Accordingly, several standard block diagrams are developed by the IEEE working group to represent the excitation system. A schematic of an excitation control system is shown in Fig2.1.



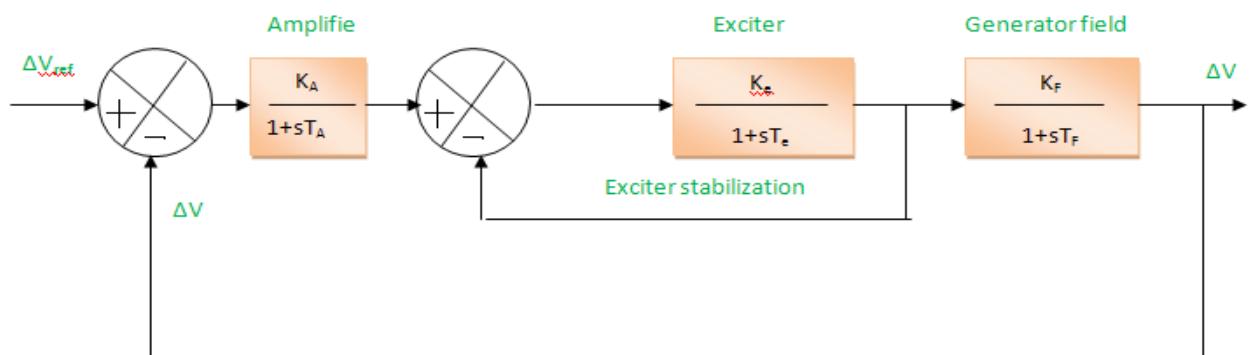
**A schematic of excitation (voltage) control system**

*Fig2.1: A schematic of Excitation (Voltage) Control System.*

A simplified block diagram of the generator voltage control system is shown in Fig2.2. The generator terminal voltage  $V_t$  is compared with a voltage reference  $V_{ref}$  to obtain a voltage error signal  $\Delta V$ . This signal is applied to the voltage regulator shown as a block with transfer function  $K_A/(1+T_A)$ . The output of the regulator is then applied to exciter shown with a block of transfer function  $K_e/(1+T_e)$ . The output of the exciter  $E_{fd}$  is then applied to the field winding which adjusts the generator terminal voltage. The generator field can be represented by a block with a transfer function  $K_F/(1+sT_F)$ . The total transfer

$$\frac{\Delta V}{\Delta V_{ref}} = \frac{G(s)}{1 + G(s)} \text{ where, } G(s) = \frac{K_A K_e K_F}{(1 + sT_A)(1 + sT_e)(1 + sT_F)}$$

The stabilizing compensator shown in the diagram is used to improve the dynamic response of the exciter. The input to this block is the exciter voltage and the output is a stabilizing feedback signal to reduce the excessive overshoot.



**A simplified block diagram of voltage (excitation) control system**

*Fig2.2: A simplified block diagram of Voltage (Excitation) Control System.*

## Performance of AVR Loop

The purpose of the AVR loop is to maintain the generator terminal voltage within acceptable values. A static accuracy limit in percentage is specified for the AVR, so that the terminal voltage is maintained within that value. For example, if the accuracy limit is 4%, then the terminal voltage must be maintained within 4% of the base voltage.

The performance of the AVR loop is measured by its ability to regulate the terminal voltage of the generator within prescribed static accuracy limit with an acceptable speed of response. Suppose the static accuracy limit is denoted by  $A_c$  in percentage with reference to the nominal value. The error voltage is to be less than  $(A_c/100)\Delta|V|_{ref}$ .

From the block diagram, for a steady state error voltage  $\Delta e$ ;

$$\begin{aligned}\Delta e &= \Delta|V|_{ref} - \Delta|V|_t < \frac{A_c}{100} \Delta|V|_{ref} \\ \Delta e &= \Delta|V|_{ref} - \Delta|V|_t = \Delta|V|_{ref} - \frac{G(s)}{1+G(s)} \Delta|V|_{ref} \\ &= \left\{ 1 - \frac{G(s)}{1+G(s)} \right\} \Delta|V|_{ref}\end{aligned}$$

For constant input condition, ( $s \rightarrow 0$ )

$$\begin{aligned}\Delta e &= \left\{ 1 - \frac{G(s)}{1+G(s)} \right\} \Delta|V|_{ref} = \left\{ 1 - \frac{G(0)}{1+G(0)} \right\} \Delta|V|_{ref} \\ &= \frac{1}{1+G(0)} \Delta|V|_{ref} = \frac{1}{1+K} \Delta|V|_{ref}\end{aligned}$$

where,  $K = G(0)$  is the open loop gain of the AVR. Hence,

$$\frac{1}{1+K} \Delta|V|_{ref} < \frac{A_c}{100} \Delta|V|_{ref} \quad \text{or} \quad K > \left\{ \frac{100}{A_c} - 1 \right\}$$

*Example 1:* Find the open loop gain of an AVR loop if the static accuracy required is 3%.

*Solution:* Given  $A_c = 3\%$ .  $K > \left\{ \frac{100}{A_c} - 1 \right\} = K > \left\{ \frac{100}{3} - 1 \right\} = 32.33$ . Thus, if the open loop gain of the AVR loop is greater than 32.33, then the terminal voltage will be within 3% of the base voltage.

## 2.3 Automatic Load Frequency Control

The ALFC is to control the frequency deviation by maintaining the real power balance in the system. The main functions of the ALFC are to i) to maintain the steady frequency; ii) control the tie-line flows; and iii) distribute the load among the participating generating units. The control (input) signals are the tie-line deviation  $\Delta P_{tie}$  (measured from the tie-line flows), and the frequency deviation  $\Delta f$  (obtained by measuring the angle deviation  $\Delta\delta$ ). These error signals  $\Delta f$  and  $\Delta P_{tie}$  are amplified, mixed and transformed to a real power signal, which then controls the valve position. Depending on the valve position, the turbine (prime mover) changes its output power to establish the real power balance. The complete control schematic is shown in Fig2.3

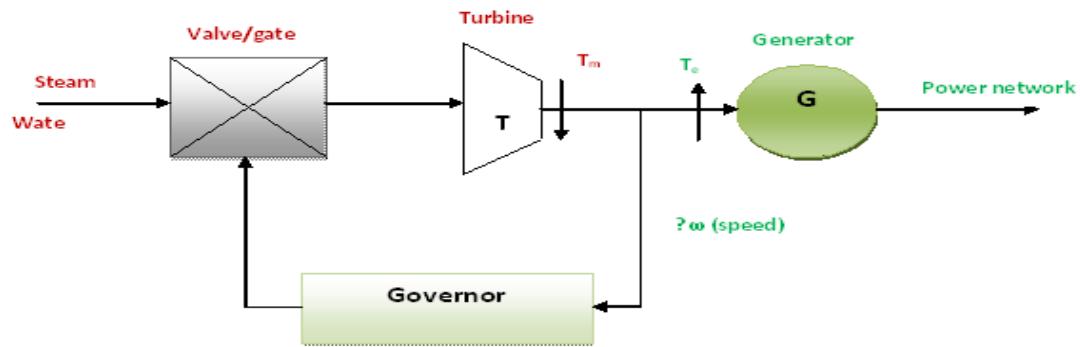


Fig2.3: The Schematic representation of ALFC system

For the analysis, the models for each of the blocks in Fig2 are required. The generator and the electrical load constitute the power system. The valve and the hydraulic amplifier represent the speed governing system. Using the swing equation, the generator can be

modeled by  $\frac{2Hd^2\Delta\delta}{\omega_s dt^2} = \Delta P_m - \Delta P_e$ . Expressing the speed deviation in pu,

$$\frac{d\Delta\omega}{dt} = \frac{1}{2H}(\Delta P_m - \Delta P_e)$$

This relation can be represented as shown in Fig2.4.

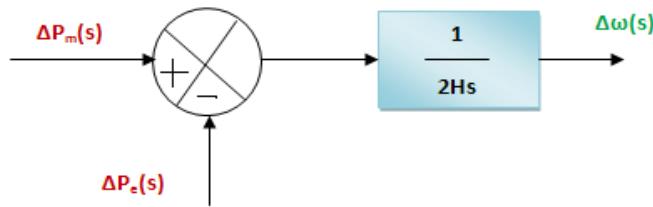


Fig2.4. The block diagram representation of the Generator

The load on the system is composite consisting of a frequency independent component and a frequency dependent component. The load can be written as  $\Delta P_e = \Delta P_0 + \Delta P_f$  where,  $\Delta P_e$  is the change in the load;  $\Delta P_0$  is the frequency independent load component;  $\Delta P_f$  is the frequency dependent load component.  $\Delta P_f = D\Delta\omega$  where,  $D$  is called frequency characteristic of the load (also called as damping constant) expressed in percent change in load for 1% change in frequency. If  $D=1.5\%$ , then a 1% change in frequency causes 1.5% change in load. The combined generator and the load (constituting the power system) can then be represented as shown in Fig2.5

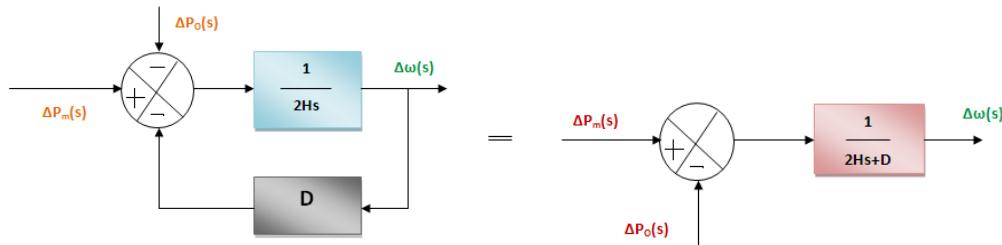


Fig2.5. The block diagram representation of the Generator and load

The turbine can be modeled as a first order lag as shown in the Fig2.6

$$\frac{\Delta P_v(s)}{1+sT_t} \rightarrow G_t(s) = \frac{\Delta P_m(s)}{\Delta P_v(s)} = \frac{K_t}{1+sT_t}$$

$G_t(s)$  is the TF of the turbine;  $\Delta P_v(s)$  is the change in valve output (due to action).

$\Delta P_m(s)$  is the change in the turbine output

Fig2.6. The turbine model.

The governor can similarly modeled as shown in Fig2.7. The output of the governor is by

$$\Delta P_g = \Delta P_{ref} - \frac{\Delta\omega}{R} \text{ where } \Delta P_{ref} \text{ is the reference set power, and } \Delta\omega/R \text{ is the power given}$$

by governor speed characteristic. The hydraulic amplifier transforms this signal  $\Delta P_g$  into valve/gate position corresponding to a power  $\Delta P_v$ . Thus  $\Delta P_v(s) = (K_g/(1+sT_g))\Delta P_g(s)$ .

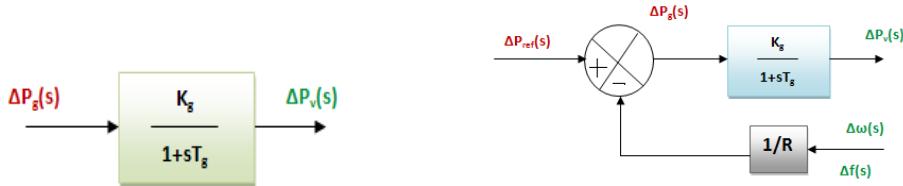


Fig2.7: The block diagram representation of the Governor

All the individual blocks can now be connected to represent the complete ALFC loop as shown in Fig2.8

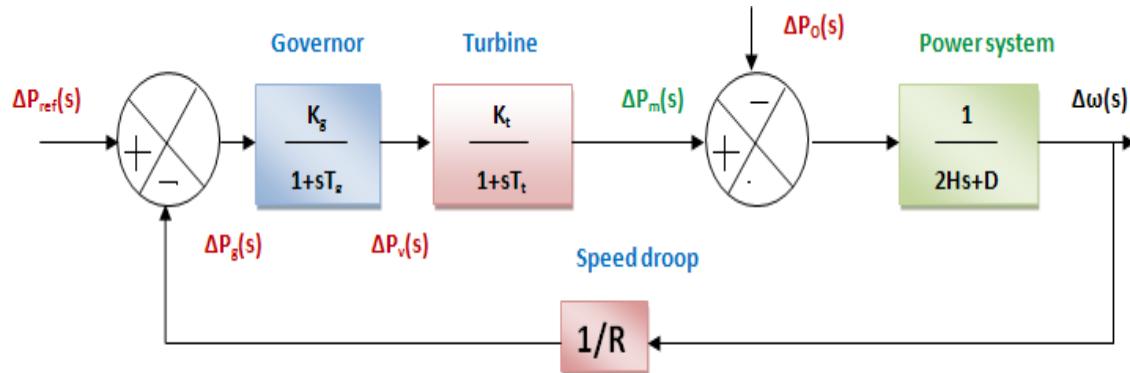


Fig2.8: The block diagram representation of the ALFC

## 2.4 Steady State Performance of the ALFC Loop

In the steady state, the ALFC is in ‘open’ state, and the output is obtained by substituting  $s \rightarrow 0$  in the TF.

With  $s \rightarrow 0$ ,  $G_g(s)$  and  $G_t(s)$  become unity, then, (note that  $\Delta P_m = \Delta P_T = \Delta P_G = \Delta P_e = \Delta P_D$  ; That is turbine output = generator/electrical output = load demand)

$$\Delta P_m = \Delta P_{ref} - (1/R)\Delta\omega \quad \text{or} \quad \Delta P_m = \Delta P_{ref} - (1/R)\Delta f$$

When the generator is connected to infinite bus ( $\Delta f = 0$ , and  $\Delta V = 0$ ), then  $\Delta P_m = \Delta P_{ref}$ .

If the network is finite, for a fixed speed changer setting ( $\Delta P_{ref} = 0$ ), then

$$\Delta P_m = -(1/R)\Delta f \quad \text{or} \quad \Delta f = -R \Delta P_m$$

If the frequency dependent load is present, then

$$\Delta P_m = \Delta P_{ref} - (1/R + D)\Delta f \quad \text{or} \quad \Delta f = \frac{-\Delta P_m}{D + 1/R}$$

If there are more than one generator present in the system, then

$$\Delta P_{m, eq} = \Delta P_{ref, eq} - (D + 1/R_{eq})\Delta f$$

where,  $\Delta P_{m, eq} = \Delta P_{m1} + \Delta P_{m2} + \Delta P_{m,3} + \dots$

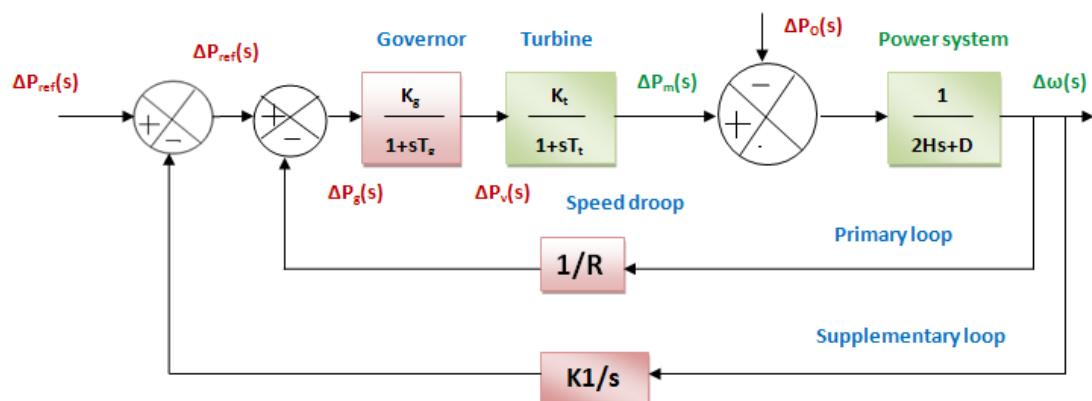
$$\Delta P_{\text{ref, eq}} = \Delta P_{\text{ref1}} + \Delta P_{\text{ref2}} + \Delta P_{\text{ref3}} + \dots$$

$$1/R_{\text{eq}} = (1/R_1 + 1/R_2 + 1/R_3 + \dots)$$

The quantity  $\beta = (D + 1/R_{eq})$  is called the area frequency (bias) characteristic (response) or simply the stiffness of the system.

## 2.5 Concept of AGC (Supplementary ALFC Loop)

The ALFC loop shown in Fig2.8, is called the primary ALFC loop. It achieves the primary goal of real power balance by adjusting the turbine output  $\Delta P_m$  to match the change in load demand  $\Delta P_D$ . All the participating generating units contribute to the change in generation. But a change in load results in a steady state frequency deviation  $\Delta f$ . The restoration of the frequency to the nominal value requires an additional control loop called the supplementary loop. This objective is met by using integral controller which makes the frequency deviation zero. The ALFC with the supplementary loop is generally called the AGC. The block diagram of an AGC is shown in Fig2.9. The main objectives of AGC are i) to regulate the frequency (using both primary and supplementary controls); ii) and to maintain the scheduled tie-line flows. A secondary objective of the AGC is to distribute the required change in generation among the connected generating units economically (to obtain least operating costs).



*Fig2.9: The block diagram representation of the AGC*

## 2.6 AGC in a Single Area System

In a single area system, there is no tie-line schedule to be maintained. Thus the function of the AGC is only to bring the frequency to the nominal value. This will be achieved using the supplementary loop (as shown in Fig.2.9) which uses the integral controller to change the reference power setting so as to change the speed set point. The integral controller gain  $K_I$  needs to be adjusted for satisfactory response (in terms of overshoot, settling time) of the system. Although each generator will have a separate speed governor, all the generators in the control area are replaced by a single equivalent generator, and the ALFC for the area corresponds to this equivalent generator.

## 2.7 AGC in a Multi Area System

In an interconnected (multi area) system, there will be one ALFC loop for each control area (located at the ECC of that area). They are combined as shown in Fig2.10 for the interconnected system operation. For a total change in load of  $\Delta P_D$ , the steady state

deviation in frequency in the two areas is given by  $\Delta f = \Delta\omega_1 = \Delta\omega_2 = \frac{-\Delta P_D}{\beta_1 + \beta_2}$  where,

$$\beta_1 = (D_1 + 1/R_1); \text{ and } \beta_2 = (D_2 + 1/R_2).$$

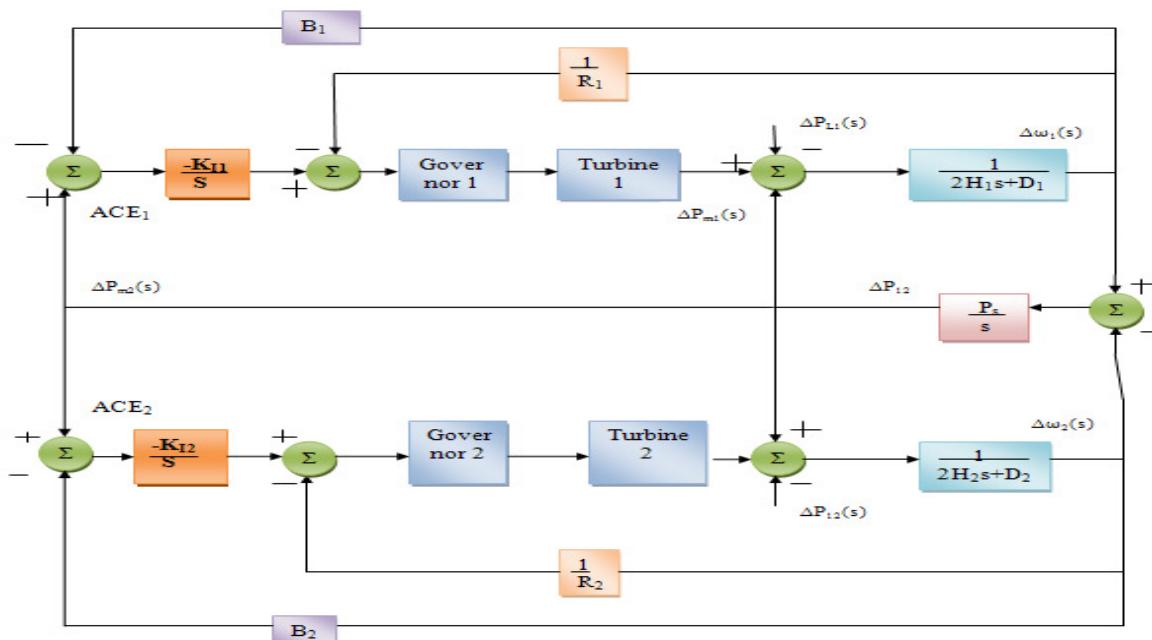


Fig.2.10. AGC for a multi-area operation.

## 2.8 Expression for tie-line flow in a two-area interconnected system

Consider a change in load  $\Delta P_{D1}$  in area1. The steady state frequency deviation  $\Delta f$  is the same for both the areas. That is  $\Delta f = \Delta f_1 = \Delta f_2$ . Thus, for area1, we have

$$\Delta P_{m1} - \Delta P_{D1} - \Delta P_{12} = D_1 \Delta f$$

where,  $\Delta P_{12}$  is the tie line power flow from Area1 to Area 2; and for Area 2

$$\Delta P_{m2} + \Delta P_{12} = D_2 \Delta f$$

The mechanical power depends on regulation. Hence

$$\Delta P_{m1} = -\frac{\Delta f}{R_1} \quad \text{and} \quad \Delta P_{m2} = -\frac{\Delta f}{R_2}$$

Substituting these equations, yields

$$\left(\frac{1}{R_1} + D_1\right) \Delta f = -\Delta P_{12} - \Delta P_{D1} \quad \text{and} \quad \left(\frac{1}{R_2} + D_2\right) \Delta f = \Delta P_{12}$$

Solving for  $\Delta f$ , we get

$$\Delta f = \frac{-\Delta P_{D1}}{\left(1/R_1 + D_1\right) + \left(1/R_2 + D_2\right)} = \frac{-\Delta P_{D1}}{\beta_1 + \beta_2}$$

and  $\Delta P_{12} = \frac{-\Delta P_{D1}\beta_2}{\beta_1 + \beta_2}$

where,  $\beta_1$  and  $\beta_2$  are the composite frequency response characteristic of Area1 and Area 2 respectively. An increase of load in area1 by  $\Delta P_{D1}$  results in a frequency reduction in both areas and a tie-line flow of  $\Delta P_{12}$ . A positive  $\Delta P_{12}$  is indicative of flow from Area1 to Area 2 while a negative  $\Delta P_{12}$  means flow from Area 2 to Area1. Similarly, for a change in Area

2 load by  $\Delta P_{D2}$ , we have  $\Delta f = \frac{-\Delta P_{D2}}{\beta_1 + \beta_2}$

and  $\Delta P_{12} = -\Delta P_{D2} = \frac{-\Delta P_{D2}\beta_1}{\beta_1 + \beta_2}$

### Frequency bias tie line control

The tie line deviation reflects the contribution of regulation characteristic of one area to another. The basic objective of supplementary control is to restore balance between each area load generation. This objective is met when the control action maintains

- Frequency at the scheduled value

- Net interchange power (tie line flow) with neighboring areas at the scheduled values

The supplementary control should ideally correct only for changes in that area. In other words, if there is a change in Area1 load, there should be supplementary control only in Area1 and not in Area 2. For this purpose the area control error (ACE) is used (Fig2.9).

The ACE of the two areas are given by

$$\text{For area 1: } \text{ACE}_1 = \Delta P_{12} + \beta_1 \Delta f$$

$$\text{For area 2: } \text{ACE}_2 = \Delta P_{21} + \beta_2 \Delta f$$

## 2.9 Economic Allocation of Generation

An important secondary function of the AGC is to allocate generation so that each generating unit is loaded economically. That is, each generating unit is to generate that amount to meet the present demand in such a way that the operating cost is the minimum. This function is called Economic Load Dispatch (ELD).

## 2.10 Systems with more than two areas

The method described for the frequency bias control for two area system is applicable to multiarea system also.

Note:

*The regulation constant R is negative of the slope of the  $\Delta f$  verses  $\Delta p_m$  curve of the turbine-governor control. The unit of R is Hz/MW when  $\Delta f$  is in Hz and  $\Delta p_m$  is in MW. When  $\Delta f$  and  $\Delta p_m$  are in per-unit, R is also in per-unit.*

*The area frequency characteristic is defined as  $\beta = \{1/(D+1/R)\}$ , where D is the frequency damping factor of the load. The unit of  $\beta$  is MW/Hz when  $\Delta f$  is in Hz and  $\Delta p_m$  is in MW. If  $\Delta f$  and  $\Delta p_m$  are in per unit, then  $\beta$  is also in per unit.*

Examples:

Ex 1. A 500 MVA, 50 Hz, generating unit has a regulation constant R of 0.05 p.u. on its own rating. If the frequency of the system increases by 0.01 Hz in the steady state, what is the decrease in the turbine output? Assume fixed reference power setting.

Solution: In p.u.  $\Delta f = 0.01/50 = 0.0002$  p.u.

$$\text{With } \Delta p_{\text{ref}} = 0, \quad \Delta p_m = -1/R(\Delta f) = -0.004 \text{ p.u.}$$

$$\text{Hence, } \Delta p_m = -0.004 S_{\text{base}} = -2 \text{ MW.}$$

Ex. 2. An interconnected 60 Hz power system consists of one area with three generating units rated 500, 750, and 1000 MVA respectively. The regulation constant of each unit is  $R = 0.05$  per unit on its own rating. Each unit is initially operating at one half of its rating, when the system load suddenly increases by 200MW. Determine (i) the area frequency response characteristic on a 1000 MVA system base, (ii) the steady state frequency deviation of the area, and (iii) the increase in turbine power output.

Regulation constants on common system base are ( $R_{\text{pu new}} = R_{\text{pu old}} (S_{\text{base new}}/S_{\text{base old}})$ ):

$$R_1 = 0.1; R_2 = 0.0667; \text{ and } R_3 = 0.05.$$

$$\text{Hence } \beta = (1/R_1 + 1/R_2 + 1/R_3) = 45 \text{ per unit.}$$

Neglecting losses and frequency dependence of the load, the steady state frequency deviation is  $\Delta f = (-1/\beta)\Delta p_m = -4.444 \times 10^{-3}$  per unit  $= (-4.444 \times 10^{-3})60 = -0.2667$  Hz.

$$\Delta p_{m1} = (-1/R_1)(\Delta f) = 0.04444 \text{ per unit} = 44.44 \text{ MW}$$

$$\Delta p_{m2} = (-1/R_2)(\Delta f) = 0.06666 \text{ per unit} = 66.66 \text{ MW}$$

$$\Delta p_{m3} = (-1/R_3)(\Delta f) = 0.08888 \text{ per unit} = 88.88 \text{ MW}$$

Ex.3. A 60 Hz, interconnected power system has two areas. Area1 has 2000 MW generation and area frequency response of 700 MW/Hz. Area 2 has 4000 MW generation and area frequency response of 1400 MW/Hz. Each area is initially generating half of its rated generation, and the tie-line deviation is zero at 60 Hz when load in Area1 is

suddenly increases by 100 MW. Find the steady state frequency error and tie line error of the two areas. What is the effect of using AGC in this system?

In the steady state,  $\Delta f = (-1/\beta) \Delta p_m = \{\Delta p_m / -(\beta_1 + \beta_2)\} = (-100/2100) = -0.0476$  Hz.

Assuming  $\Delta p_{ref} = 0$ ,

$$\Delta p_{m1} = -\beta_1 \Delta f = 33.33 \text{ MW}; \text{ and } \Delta p_{m2} = -\beta_2 \Delta f = 66.67 \text{ MW}.$$

Thus in response to 100 MW change in Area1, both areas will change their generation. The increase in Area 2 generation will now flow through tie line to Area1.

Hence  $\Delta p_{tie1} = -66.67 \text{ MW}$ ; and  $\Delta p_{tie2} = +66.67 \text{ MW}$ .

With AGC, the Area control error is determined as follows.

ACE 1 =  $\Delta p_{tie1} + B_1 \Delta f$  where  $B_1$  is the frequency bias constant.

ACE 2 =  $\Delta p_{tie2} (= -\Delta p_{tie1}) + B_2 \Delta f$  where  $B_2$  is the frequency bias constant.

The control will actuate such that in the steady state the frequency and tie line deviations are zero. Thus till ACE1= ACE2 = 0, the control signal will be present.