MATH2089 Numerical Methods Lecture 11

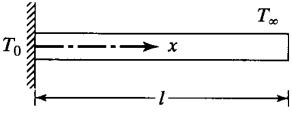
Boundary Value Problems
Parabolic Equations
Methods of Solutions

Boundary Value Problems

- Conditions for the equation are not all given at the initial point but are specified at two different values for the independent variable
- These values are usually at the endpoints (or boundaries) of some domain of interest
- Example
 - A cooling fin extends from a hot surface

$$kA\frac{d^2T}{dx^2} - hP(T - T_{\infty}) = 0$$

Boundary conditions: $T(x = 0) = T_0$ and $-k \frac{dT(x = l)}{dx} = h(T(x = l) - T_{\infty})$



Main Focus

- This lecture is concerned with solving boundary-value problems by replacing the derivatives with <u>finite</u> <u>difference</u> approximations
- When this is accomplished, the solution is obtained by solving a set of simultaneous equations

Finite Difference Methods

- FDA (finite difference approximation) of the differential equation is obtained at a number of mesh points in the interval of integration
- This leads to converting the differential equation to a set of simultaneous algebraic equations
- For example, consider

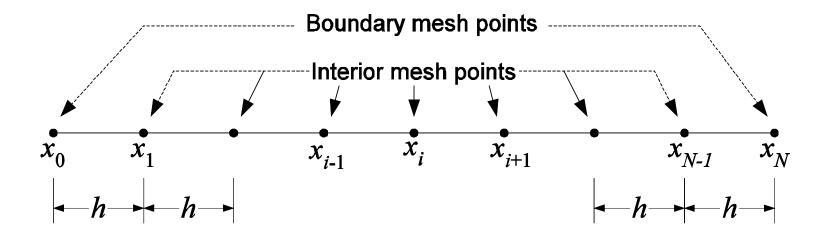
$$P(x)\frac{d^2y}{dx^2} + Q(x)\frac{dy}{dx} + R(x)y = S(x), \quad x_0 \le x \le x_N$$

subject to boundary conditions (end points)

$$y(x_0) = Y_0 \qquad y(x_N) = Y_N$$

Consider the problem as having discrete points along x, the interval of integration can be divided into N equal parts of width

$$h = (x_0 - x_N)/N \implies x_i = x_0 + ih$$



Employing central difference

$$\frac{dy}{dx} = \frac{y_{i+1} - y_{i-1}}{2h} + O(h^2), \quad \frac{d^2y}{dx^2} = \frac{y_{i+1} - 2y_i + y_{i-1}}{h^2} + O(h^2)$$

Hence, at the interior node I

$$P(x_i) \frac{y_{i+1} - 2y_i + y_{i-1}}{h^2} + Q(x_i) \frac{y_{i+1} - y_{i-1}}{2h} + R(x_i) y_i = S(x_i), \quad i = 1, 2, ..., N - 1$$

Let $P(x_i) = a_{2,i}$, $Q(x_i) = a_{1,i}$, $R(x_i) = a_{0,i}$, $S(x_i) = g_i$

$$\underbrace{\left(\frac{a_{2,i}}{h^2} - \frac{a_{1,i}}{2h}\right)}_{A_i} y_{i-1} + \underbrace{\left(a_{0,i} - \frac{2a_{2,i}}{h^2}\right)}_{B_i} y_i + \underbrace{\left(\frac{a_{2,i}}{h^2} + \frac{a_{1,i}}{2h}\right)}_{C_i} y_{i+1} = \underbrace{g_i}_{D_i}, \quad i = 1, 2, ..., N-1$$

Simplifying,

$$A_i y_{i-1} + B_i y_i + C_i y_{i+1} = D_i, \quad i = 1, 2, ..., N-1$$

> Applying the boundary conditions $y(x_0) = Y_0$ and $y(x_N) = Y_N$ we can write

$$\begin{cases} i = 1, & B_{1}y_{1} + C_{1}y_{2} = D_{1} - A_{1}Y_{0} \\ i = 2, & A_{2}y_{1} + B_{2}y_{2} + C_{2}y_{3} = D_{2} \\ i = 3, & A_{3}y_{2} + B_{3}y_{3} + C_{3}y_{4} = D_{3} \\ \vdots \\ i = N - 2, & A_{N-2}y_{N-3} + B_{N-2}y_{N-2} + C_{N-2}y_{N-1} = D_{N-2} \\ i = N - 1, & A_{N-1}y_{N-2} + B_{N-1}y_{N-1} = D_{N-1} - C_{N-1}Y_{N} \end{cases}$$

- System of (N-1) equations with (N-1) unknowns y_i
- Set of simultaneous algebraic equations which can be expressed in the matrix form

$$[A]\vec{y} = \vec{b}$$

$$\begin{bmatrix} B_1 & C_1 & 0 & 0 & 0 & 0 & 0 \\ A_2 & B_2 & C_2 & 0 & 0 & 0 & 0 & 0 \\ 0 & A_3 & B_3 & C_3 & 0 & 0 & 0 & 0 \\ \vdots & \vdots & \ddots & \ddots & \ddots & \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & A_{N-3} & B_{N-3} & C_{N-3} & 0 & y_{N-3} \\ 0 & 0 & 0 & 0 & A_{N-2} & B_{N-2} & C_{N-2} \\ 0 & 0 & 0 & 0 & 0 & A_{N-1} & B_{N-1} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ \vdots \\ y_{N-3} \\ y_{N-2} \\ y_{N-1} \end{bmatrix} = \begin{bmatrix} D_1 - A_1 Y_0 \\ D_2 \\ D_3 \\ \vdots \\ D_{N-3} \\ D_{N-2} \\ D_{N-1} - C_{N-1} Y_N \end{bmatrix}$$

- What type of matrix is it?
- Tri-Diagonal matrix which can be solved using the TDMA (Tri-Diagonal Matrix Algorithm)
- Can be resolved via two steps
- > Step 1, eliminate A_i $B_1^{(1)} = B_1$, $B_i^{(1)} = B_i \frac{A_i}{B_{i-1}^{(1)}} C_{i-1}$, $D_i^{(1)} = D_i \frac{A_i}{B_{i-1}^{(1)}} D_{i-1}^{(1)}$

$$\begin{bmatrix} B_1 & C_1 & & & & D_1^{(1)} \\ 0 & B_2^{(1)} & C_2 & & & D_2^{(1)} \\ & 0 & B_3^{(1)} & C_3 & & & D_3^{(1)} \\ & & \ddots & \ddots & \ddots & & \vdots \\ & & 0 & B_{N-3}^{(1)} & C_{N-3} & & D_{N-3}^{(1)} \\ & & 0 & B_{N-2}^{(1)} & C_{N-2} & D_{N-2}^{(1)} \\ & & 0 & B_{N-1}^{(1)} & D_{N-1}^{(1)} \end{bmatrix}$$

$$i = 2, 3, \dots, N-1$$

$$i = 2, 3, ..., N-1$$

Step 2, backward substitution

$$y_{N-1} = \frac{D_{N-1}^{(1)}}{B_{N-1}^{(1)}},$$

$$y_{i} = \frac{D_{i}^{(1)} - C_{i} y_{i+1}}{B_{i}^{(1)}}, i = N-2, N-3, ..., 2, 1$$

Example

Formulate the boundary-value problem for an infinitely long hollow cylinder whose inner surface (r = 5") is maintained at 200°F, while the outer surface (r = 10") is maintained at 65°F. The radial heat transfer in a thick hollow cylinder is given by

$$\frac{d^2T}{dr^2} + \frac{1}{r}\frac{dT}{dr} = 0$$

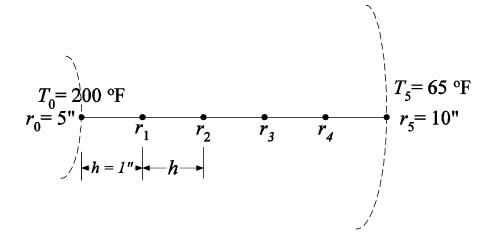
Solution

Using h = 1", interval 5" $\leq x \leq 10$ " can be divided into N = 5

Employ the central difference formulae

$$\frac{d^2T}{dr^2} + \frac{1}{r}\frac{dT}{dr} = 0$$

$$\frac{T_{i+1} - 2T_i + T_{i-1}}{h^2} + \frac{1}{r_i} \frac{T_{i+1} - T_{i-1}}{2h} = 0$$



Rearrange

$$\left(\frac{1}{h^2} - \frac{1}{2hr_i}\right)T_{i-1} - \left(\frac{2}{h^2}\right)T_i + \left(\frac{1}{h^2} + \frac{1}{2hr_i}\right)T_{i+1} = 0$$

$$A_i \qquad B_i \qquad C_i \qquad D_i$$

$$i = 1, A_1 = 0, B_1 = -2/h^2,$$

$$C_1 = \left(\frac{1}{h^2} + \frac{1}{2hr_1}\right) \qquad D_1 = -\left(\frac{1}{h^2} - \frac{1}{2hr_i}\right) * T_0$$

Discrete form of equation

$$\left(\frac{1}{h^2} - \frac{1}{2hr_i}\right)T_{i-1} - \left(\frac{2}{h^2}\right)T_i + \left(\frac{1}{h^2} + \frac{1}{2hr_i}\right)T_{i+1} = 0$$

$$A_i \qquad B_i \qquad C_i \qquad D_i$$

$$\rightarrow$$
 $i = 2,3$

$$A_i = \left(\frac{1}{h^2} - \frac{1}{2hr_i}\right) \qquad C_i = \left(\frac{1}{h^2} + \frac{1}{2hr_i}\right)$$

$$B_i = -\left(\frac{2}{h^2}\right) \qquad D_i = 0$$

Discrete form of equation

$$\left(\frac{1}{h^2} - \frac{1}{2hr_i}\right)T_{i-1} - \left(\frac{2}{h^2}\right)T_i + \left(\frac{1}{h^2} + \frac{1}{2hr_i}\right)T_{i+1} = 0$$

$$A_i \qquad B_i \qquad C_i \qquad D_i$$

$$i = 4$$
, $B_4 = -2/h^2$, $C_4 = 0$,

$$A_4 = \left(\frac{1}{h^2} - \frac{1}{2hr_4}\right) \qquad D_4 = -\left(\frac{1}{h^2} + \frac{1}{2hr_i}\right) * T_5$$

Finite difference approximation at the interior node points i = 1, 2, 3 and 4 are

$$i = 1, \quad 11T_0 - 24T_1 + 13T_2 = 0 \qquad -24T_1 + 13T_2 = -11(200)$$
 $i = 2, \quad 13T_1 - 28T_2 + 15T_3 = 0$
 $i = 3, \quad 15T_2 - 32T_3 + 17T_4 = 0$
 $\Rightarrow \quad 13T_1 - 28T_2 + 15T_3 = 0$
 $\Rightarrow \quad 15T_2 - 32T_3 + 17T_4 = 0$
 $\Rightarrow \quad 15T_2 - 32T_3 + 17T_4 = 0$
 $\Rightarrow \quad 17T_3 - 36T_4 + 19T_5 = 0$
 $\Rightarrow \quad 17T_3 - 36T_4 = -19(65)$

- Solved by TDMA
- Step 1, eliminate A_i

$$\begin{bmatrix} -24 & 13 & 0 & 0 \\ 0 & -20.958 & 15 & 0 \\ 0 & 0 & -21.264 & 17 \\ 0 & 0 & 0 & -22.409 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \begin{bmatrix} -2200 \\ -1191.7 \\ -852.88 \\ -1916.84 \end{bmatrix}$$

Step 2, backward substitution

$$\begin{vmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{vmatrix} = \begin{cases} 164.53 \\ 134.51 \\ 108.49 \\ 85.538 \end{cases}$$

Boundary Conditions

- There are different types of boundary conditions that can be imposed
- Dirichlet condition

$$y(x_0) = f(x)$$
 or $y(x_0) = \text{constant}$

Neumann condition: derivative in the n direction

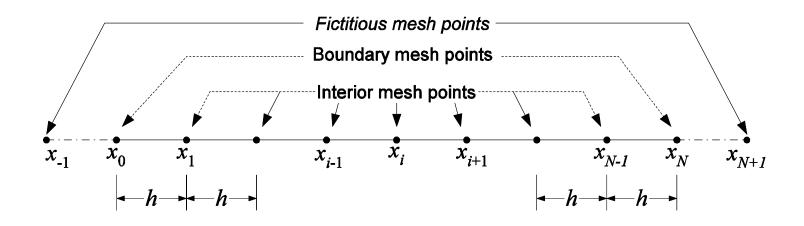
$$\left. \frac{dy}{dn} \right|_{x_0} = f(x)$$
 or $\left. \frac{dy}{dn} \right|_{x_0} = \text{constant}$

Mixed condition

$$\left. \frac{dy}{dn} \right|_{x_0} + cy(x_0) = f(x)$$
 or $\left. \frac{dy}{dn} \right|_{x_0} + cy(x_0) = \text{constant}$

FDA of Boundary Conditions

- Leads to an additional equation at x₀, hence the system consists of N simultaneous equations in tri-diagonal form in the N unknowns
- How to employ central difference formulae at endpoints? Use fictitious points as seen below



Example

A cooling fin extends from a hot furnace wall as shown below. Assuming that heat flows only in the *x*-direction, the thermal equilibrium relation leads to the following governing equation

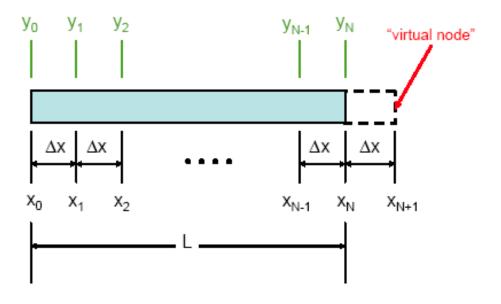
$$kA\frac{d^{2}T}{dx^{2}} - hP(T - T_{\infty}) = 0$$

$$\begin{cases} \begin{cases} \begin{cases} T_{\infty} \\ \end{cases} \end{cases} \end{cases} \begin{cases} \begin{cases} T(0) = T_{0} \\ -k\frac{dT(L)}{dx} = h(T(L) - T_{\infty}) \end{cases} \end{cases}$$

Let $Y = T - T_{\infty}$, k/h = A/P, $T_0 - T_{\infty} = 10$, the boundary conditions are

$$\frac{d^{2}Y}{dx^{2}} - Y = 0, \quad Y(0) = T_{0} - T_{\infty} = 10, \quad -\frac{dY}{dx} = Y(1)$$

Consider a finite difference solution



- ▶ Divide the fin into N equal segments of length $\Delta x = L/N$
- Temperature difference at each node is denoted at y_i, i
 = 1, 2, ... N
- > First and second-derivative at each node can be expressed to order $O(\Delta x^2)$ using centered difference expressions

$$y'_{i} = \frac{y_{i+1} - y_{i-1}}{2\Delta x}, \quad y''_{i} = \frac{y_{i+1} - 2y_{i} + y_{i-1}}{\Delta x^{2}}$$

• At node 1 (Note $y_0 = 10$)

$$y_1'' = y_1 \Rightarrow \frac{y_0 - 2y_1 + y_2}{\Delta x^2} = y_1 \Rightarrow (2 + \Delta x^2) y_1 - y_2 = y_0$$

Similarly, at nodes 2, 3, ..., N-1, we get

$$y_{i}'' = y_{i} \Rightarrow \frac{y_{i-1} - 2y_{i} + y_{i+1}}{\Delta x^{2}} = y_{i} \Rightarrow -y_{i-1} + (2 + \Delta x^{2})y_{i} - y_{i+1} = 0$$

► End point requires *special* treatment because of the convective boundary condition at x = L

By introducing a fictitious node at N+1, with temperature y_{N+1}, leads to an approximation at node N

$$y_{N}'' = y_{N} \Rightarrow \frac{y_{N-1} - 2y_{N} + y_{N+1}}{\Delta x^{2}} = y_{N} \Rightarrow -y_{N-1} + (2 + \Delta x^{2})y_{N} - y_{N+1} = 0$$

To obtain the relationship for y_{N+1} , we employ the natural boundary condition at x = L. Together with the central difference expression

$$-y'_{N} = y_{N} \Rightarrow -\frac{y_{N+1} - y_{N-1}}{2\Delta x} = y_{N} \Rightarrow y_{N+1} = y_{N-1} - 2\Delta x y_{N}$$

$$-\frac{dY}{dx} = Y(1)$$

Eliminating y_{N+1} using

$$-y'_{N} = y_{N} \Rightarrow -\frac{y_{N-1} - y_{N+1}}{2\Delta x} = y_{N} \Rightarrow y_{N+1} = y_{N-1} - 2\Delta xy_{N}$$

we get

$$-2y_{N-1} + (2 + 2\Delta x + \Delta x^2)y_N = 0$$

Equations for N unknowns can be summarized as

$$(2 + \Delta x^{2}) y_{1} - y_{2} = y_{0}$$

$$-y_{i-1} + (2 + \Delta x^{2}) y_{i} - y_{i+1} = 0 \quad i = 2, 3, ..., N - 1$$

$$-2y_{N-1} + (2 + 2\Delta x + \Delta x^{2}) y_{N} = 0$$

Shooting Method

- An alternative procedure for solving a two-point boundary value problem involves its conversion to an *Initial value problem* (IVP) by the determination of sufficient additional conditions at one boundary
- (IVP): values of the dependent variables or their derivatives are known at the initial value of the independent variable
- Missing initial conditions are determined in a way which causes the given conditions at the other boundary to be satisfied

Procedure

- The steps involved are:
 - split the second (or higher) order equation into two (or more) equivalent first order equations
 - estimate values for the missing initial conditions
 - integrate the equations as an initial value problem
 - compare the solution at the final boundary with the given final boundary condition(s); if they don't agree, then
 - adjust the estimated values of the missing initial condition(s)
 - repeat the integration until the process converges

Non-linear Boundary Value Problems

Consider the equation

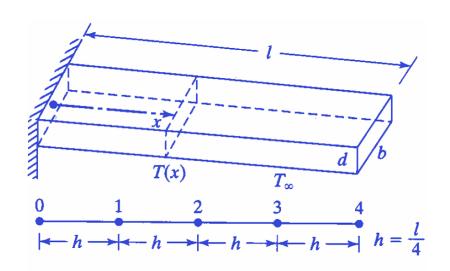
$$\frac{d^2T}{dx^2} = \frac{\sigma \varepsilon P}{kA} \left(T^4 - T_{\infty}^4 \right)$$

- What is the physical significance?
- Employing an energy balance, conduction balances with the radiation at the surface of the material
- How do you solve it?

Example

Find the temperature distribution in a rectangular fin given by

$$\frac{d^2T}{dx^2} = \frac{\sigma\varepsilon P}{kA} \left(T^4 - T_{\infty}^4\right)$$



$$c = \frac{\sigma \varepsilon P}{kA} = 1.9 \times 10^{-9}$$

$$T(0) = 1000K$$

$$T(l) = 350K \quad l = 2m$$

$$T_{\infty} = 500K$$

- Divide the fin into equal segments of h
- Second-derivative at each node can be expressed to order $O(\Delta x^2)$ using centered difference expressions

$$T_{i}'' = \frac{T_{i+1} - 2T_{i} + T_{i-1}}{h^{2}}$$

 \rightarrow The set of equations to be solved for i = 1,2,3

$$i = 1, \quad \frac{T_0 - 2T_1 + T_2}{h^2} - cT_1^4 + cT_\infty^4 = 0$$

$$i = 2, \quad \frac{T_1 - 2T_2 + T_3}{h^2} - cT_2^4 + cT_\infty^4 = 0$$

$$i = 3, \quad \frac{T_2 - 2T_3 + T_4}{h^2} - cT_3^4 + cT_\infty^4 = 0$$

- Non-linear equations must be solved through the iterative Newton-Rhapson method
- Rearranging,

$$f_{1}(T_{1}, T_{2}, T_{3}) = \frac{T_{0} - 2T_{1} + T_{2}}{h^{2}} - cT_{1}^{4} + cT_{\infty}^{4} = 0$$

$$f_{2}(T_{1}, T_{2}, T_{3}) = \frac{T_{1} - 2T_{2} + T_{3}}{h^{2}} - cT_{2}^{4} + cT_{\infty}^{4} = 0$$

$$f_{3}(T_{1}, T_{2}, T_{3}) = \frac{T_{2} - 2T_{3} + T_{4}}{h^{2}} - cT_{3}^{4} + cT_{\infty}^{4} = 0$$

- Step 1: start with an initial guess $T_1^{(1)}, T_2^{(1)}, T_3^{(1)}$
- Step 2: evaluate the function values

$$f_1^{(1)} = f_1(T_1^{(1)}, T_2^{(1)}, T_3^{(1)})$$
 $f_2^{(1)} = f_2(T_1^{(1)}, T_2^{(1)}, T_3^{(1)})$
 $f_3^{(1)} = f_3(T_1^{(1)}, T_2^{(1)}, T_3^{(1)})$

Step 3: find the partial derivatives of the function f_i and solve the equations as $\lceil \partial f^{(1)} - \partial f^{(1)} \rceil$

$$\begin{bmatrix} \frac{\partial f_{1}^{(1)}}{\partial T_{1}} & \frac{\partial f_{1}^{(1)}}{\partial T_{2}} & \frac{\partial f_{1}^{(1)}}{\partial T_{3}} \\ \frac{\partial f_{2}^{(1)}}{\partial T_{1}} & \frac{\partial f_{2}^{(1)}}{\partial T_{2}} & \frac{\partial f_{2}^{(1)}}{\partial T_{3}} \\ \frac{\partial f_{3}^{(1)}}{\partial T_{1}} & \frac{\partial f_{3}^{(1)}}{\partial T_{2}} & \frac{\partial f_{3}^{(1)}}{\partial T_{3}} \end{bmatrix} \begin{bmatrix} \Delta T_{1}^{(1)} \\ \Delta T_{2}^{(1)} \\ \Delta T_{3}^{(1)} \end{bmatrix} = \begin{bmatrix} -f_{1}^{(1)} \\ -f_{2}^{(1)} \\ -f_{3}^{(1)} \end{bmatrix}$$

Step 4: find the new solution as

$$T_{1}^{(i+1)} = T_{1}^{(i)} + \Delta T_{1}^{(i)}$$

$$T_{2}^{(i+1)} = T_{2}^{(i)} + \Delta T_{2}^{(i)}$$

$$T_{3}^{(i+1)} = T_{3}^{(i)} + \Delta T_{3}^{(i)}$$

Step 5: check the convergence by evaluating the function values

$$f_{1}^{(i+1)} = f_{1}(T_{1}^{(i+1)}, T_{2}^{(i+1)}, T_{3}^{(i+1)}); \quad \left| f_{1}^{(i+1)} \right| \leq \varepsilon$$

$$f_{2}^{(i+1)} = f_{2}(T_{1}^{(i+1)}, T_{2}^{(i+1)}, T_{3}^{(i+1)}); \quad \left| f_{2}^{(i+1)} \right| \leq \varepsilon$$

$$f_{3}^{(i+1)} = f_{3}(T_{1}^{(i+1)}, T_{2}^{(i+1)}, T_{3}^{(i+1)}); \quad \left| f_{3}^{(i+1)} \right| \leq \varepsilon$$

Step 1: start with an initial guess

$$T_{0} = 1000K$$

$$T_1^{(1)} = 800K, T_2^{(1)} = 700K, T_3^{(1)} = 600K$$

$$T_{_4}=350K$$

 $T_{\tilde{x}} = 500K$

Step 2: evaluate the function values

$$f_{1}^{(1)}(T_{1}^{(1)},T_{2}^{(1)},T_{3}^{(1)}) = \frac{T_{0} - 2T_{1}^{(1)} + T_{2}^{(1)}}{h^{2}} - c\left(T_{1}^{(1)}\right)^{4} + cT_{\infty}^{4} = 0$$

$$f_{2}^{(1)}(T_{1}^{(1)},T_{2}^{(1)},T_{3}^{(1)}) = \frac{T_{1}^{(1)} - 2T_{2}^{(1)} + T_{3}^{(1)}}{h^{2}} - c\left(T_{2}^{(1)}\right)^{4} + cT_{\infty}^{4} = 0$$

$$f_{3}^{(1)}(T_{1}^{(1)},T_{2}^{(1)},T_{3}^{(1)}) = \frac{T_{2}^{(1)} - 2T_{3}^{(1)} + T_{4}}{h^{2}} - c\left(T_{3}^{(1)}\right)^{4} + cT_{\infty}^{4} = 0$$

Step 3: find the partial derivatives of the function f_i , for example,

$$\frac{\partial f_1^{(1)}}{\partial T_1} = -\frac{2}{h^2} - 4c \left(T_1^{(1)}\right)^3 \qquad \frac{\partial f_1^{(1)}}{\partial T_2} = \frac{1}{h^2} \qquad \frac{\partial f_1^{(1)}}{\partial T_3} = 0$$

and so forth for other partial derivatives, Use Gaussian elimination to evaluate the matrix

$$\begin{bmatrix} \frac{\partial f_1^{(1)}}{\partial T_1} & \frac{\partial f_1^{(1)}}{\partial T_2} & \frac{\partial f_1^{(1)}}{\partial T_3} \\ \frac{\partial f_2^{(1)}}{\partial T_1} & \frac{\partial f_2^{(1)}}{\partial T_2} & \frac{\partial f_2^{(1)}}{\partial T_3} \\ \frac{\partial f_3^{(1)}}{\partial T_1} & \frac{\partial f_3^{(1)}}{\partial T_2} & \frac{\partial f_3^{(1)}}{\partial T_3} \end{bmatrix} \begin{bmatrix} \Delta T_1^{(1)} \\ \Delta T_2^{(1)} \\ \Delta T_3^{(1)} \end{bmatrix} = \begin{bmatrix} -f_1^{(1)} \\ -f_2^{(1)} \\ -f_3^{(1)} \end{bmatrix}$$

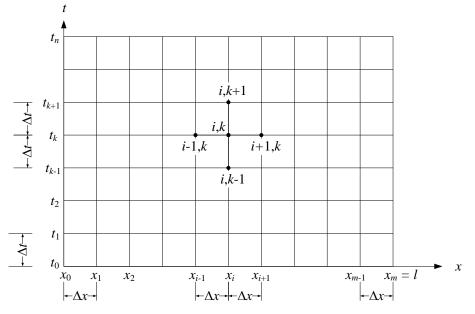
Parabolic Equations

The one-dimensional time varying heat conduction equation is an example of a parabolic equation

$$\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial x^2}$$

To derive the finite difference equation, the grid shown

below is considered



Parabolic Equations (continue)

This problem can be solved finite difference approximations in two approaches: explicit and implicit methods

Explicit Method

Forward Time Centred Space (FTCS) scheme

$$\frac{T_i^{k+1} - T_i^k}{\Delta t} = \alpha \frac{T_{i+1}^k - 2T_i^k + T_{i-1}^k}{(\Delta x)^2}$$
forward difference central difference

Rearranging,

$$T_{i}^{k+1} = \left(\frac{\alpha \Delta t}{(\Delta x)^{2}}\right) T_{i+1}^{k} + \left(1 - \frac{2\alpha \Delta t}{(\Delta x)^{2}}\right) T_{i}^{k} + \left(\frac{\alpha \Delta t}{(\Delta x)^{2}}\right) T_{i-1}^{k}$$

Let $s = \alpha \Delta t / (\Delta x)^2$

$$T_{i}^{k+1} = sT_{i+1}^{k} + (1-2s)T_{i}^{k} + sT_{i-1}^{k}$$

Explicit Method (continue)

The solution will be stable if all the coefficients are positive

$$1 - 2s = \left(1 - \frac{2\alpha\Delta t}{(\Delta x)^2}\right) \ge 0 \quad \text{or} \quad s = \frac{\alpha\Delta t}{(\Delta x)^2} \le \frac{1}{2}$$

- Disadvantages:
 - □ The stability condition imposes a restriction on the step size Δx and Δt
 - Expression of T_i^{k+1} depends only on T_{i-1}^k , T_i^k and T_{i+1}^k . It should depend on all values of T^k

Implicit Method

Using central difference formula

$$\left. \frac{\partial T}{\partial t} \right|_{i,k+\frac{1}{2}} = \frac{T_i^{k+1} - T_i^k}{\Delta t}$$

Using a weighted average of the central difference values

$$\left. \frac{\partial^2 T}{\partial x^2} \right|_{i,k+\frac{1}{2}} = \theta \left. \frac{\partial^2 T}{\partial x^2} \right|_{i,k+1} + (1-\theta) \left. \frac{\partial^2 T}{\partial x^2} \right|_{i,k}$$

where θ = weighting factor and

$$\left. \frac{\partial^2 T}{\partial x^2} \right|_{i,k+1} = \frac{\left(T_{i+1}^{k+1} - 2T_i^{k+1} + T_{i-1}^{k+1} \right)}{\left(\Delta x \right)^2} \qquad \left. \frac{\partial^2 T}{\partial x^2} \right|_{i,k} = \frac{\left(T_{i+1}^{k} - 2T_i^{k} + T_{i-1}^{k} \right)}{\left(\Delta x \right)^2}$$

Implicit Method (continue)

We get

$$\frac{T_{i}^{k+1} - T_{i}^{k}}{\Delta t} = \theta \alpha \left(\frac{T_{i+1}^{k+1} - 2T_{i}^{k+1} + T_{i-1}^{k+1}}{(\Delta x)^{2}} \right) + (1 - \theta) \alpha \left(\frac{T_{i+1}^{k} - 2T_{i}^{k} + T_{i-1}^{k}}{(\Delta x)^{2}} \right)$$

Rearranging,

$$T_{i}^{k+1} - T_{i}^{k} = \theta \frac{\alpha \Delta t}{\left(\Delta x\right)^{2}} \left(T_{i+1}^{k+1} - 2T_{i}^{k+1} + T_{i-1}^{k+1}\right) + (1 - \theta) \frac{\alpha \Delta t}{\left(\Delta x\right)^{2}} \left(T_{i+1}^{k} - 2T_{i}^{k} + T_{i-1}^{k}\right)$$

► Let $s = \alpha \Delta t / (\Delta x)^2$

$$T_{i}^{k+1} - T_{i}^{k} = \theta s \left(T_{i+1}^{k+1} - 2T_{i}^{k+1} + T_{i-1}^{k+1} \right) + (1 - \theta) s \left(T_{i+1}^{k} - 2T_{i}^{k} + T_{i-1}^{k} \right)$$

Implicit Method (continue)

$$-\theta s T_{i+1}^{k+1} + (1+2\theta s) T_{i}^{k+1} - \theta s T_{i-1}^{k+1} = (1-\theta) s T_{i+1}^{k} + (1-2(1-\theta)s) T_{i}^{k} + (1-\theta) s T_{i-1}^{k}$$

Fully-implicit ($\theta = 1$)

$$-sT_{i+1}^{k+1} + (1+2s)T_{i}^{k+1} - sT_{i-1}^{k+1} = T_{i}^{k}$$

Semi-implicit ($\theta = 0.5$) – Crank-Nicolson Method

$$-0.5sT_{i+1}^{k+1} + (1+s)T_{i}^{k+1} - 0.5sT_{i-1}^{k+1} = 0.5sT_{i+1}^{k} + (1-s)T_{i}^{k} + 0.5sT_{i-1}^{k}$$

 \rightarrow Explicit ($\theta = 0$)

$$T_{i}^{k+1} = sT_{i+1}^{k} + (1-2s)T_{i}^{k} + sT_{i-1}^{k}$$