

Task 02: Analysis of Temperature Distribution within a Printed Wall

Yating Wei
Hakim Dalim
Yahya Badine

Agenda

Task	Subtask	
Camera Mount Design	Design Description	 hakimdalim
	Thermal Camera Calibration	 YaHya BaDine
	Camera Setup Procedure	 YaHya BaDine
Temperature Measurement		
	Printing Speed Affect the Temperature Distribution	 hakimdalim
	Temperature Difference on Printing Wall Size	 hakimdalim
Simulation	Simulation Model and Method	 Wei
	Printing Speed on Temperature Distribution	 Wei
	Results and Analysis	 Wei

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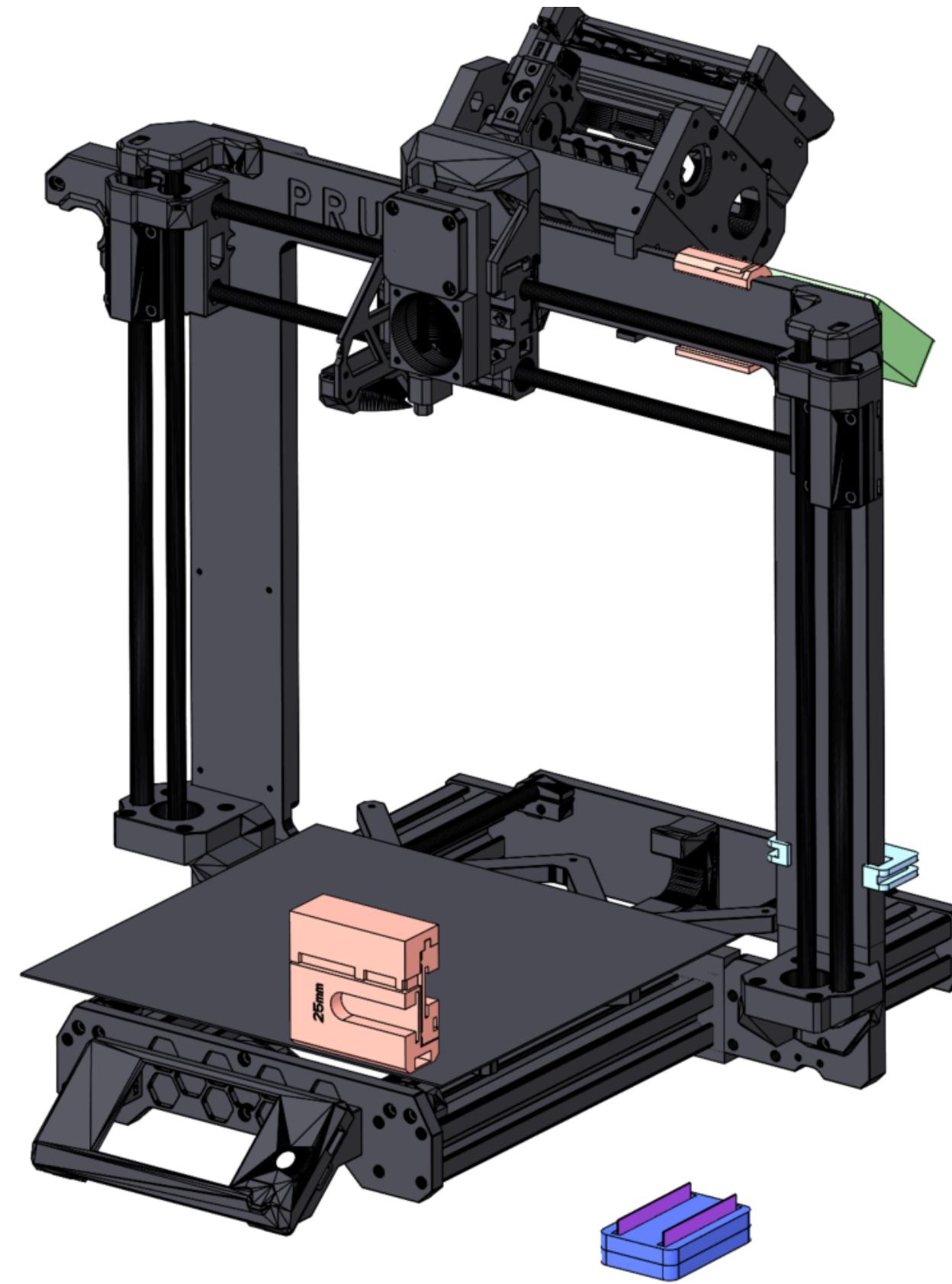
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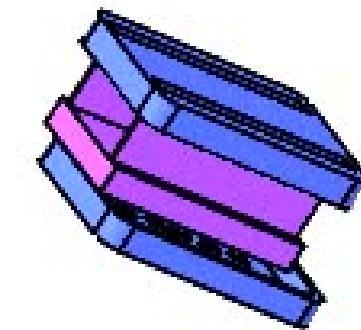
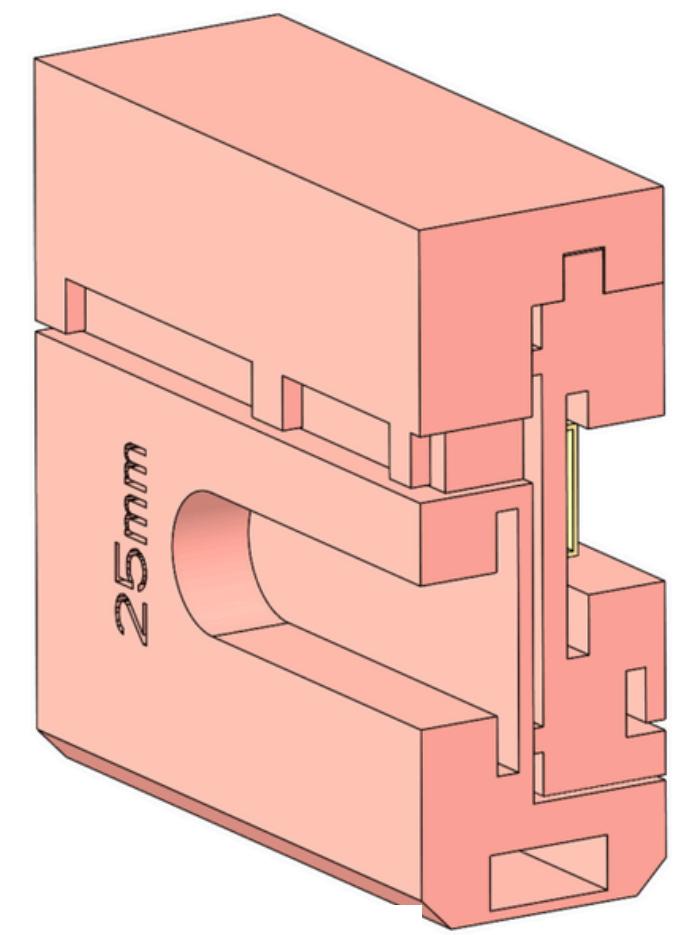
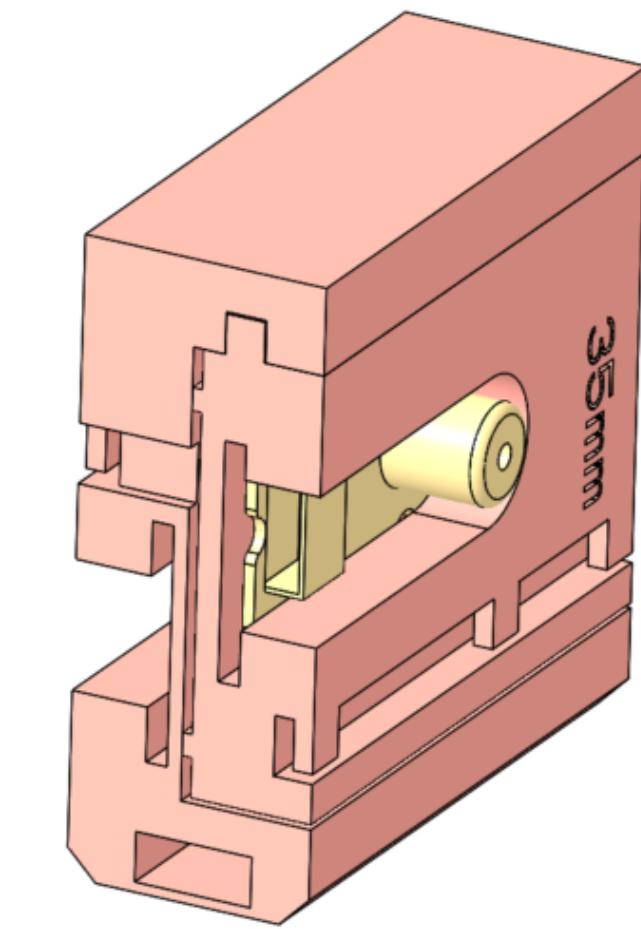
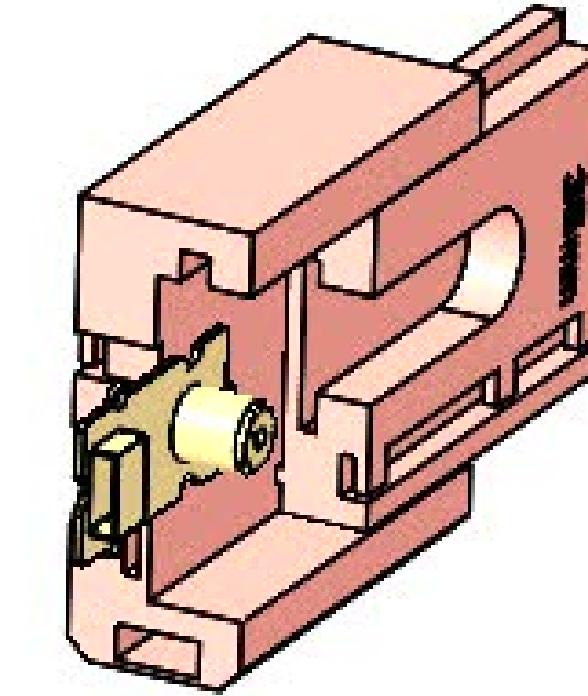
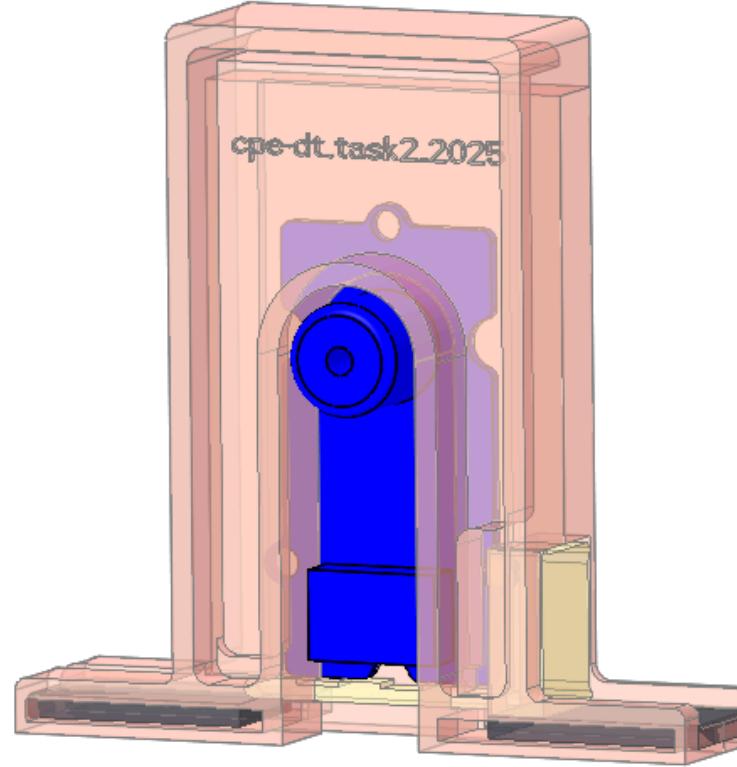
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Camera Mount Design

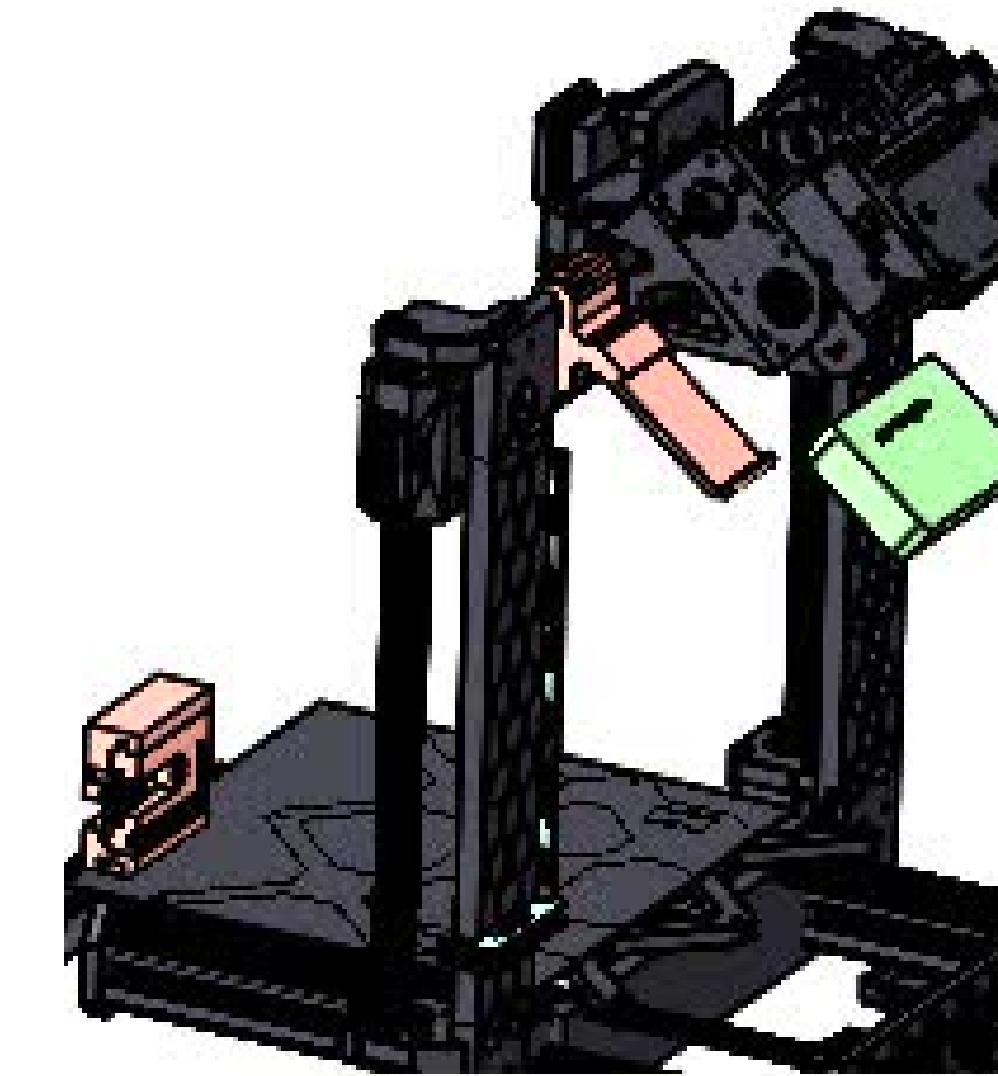
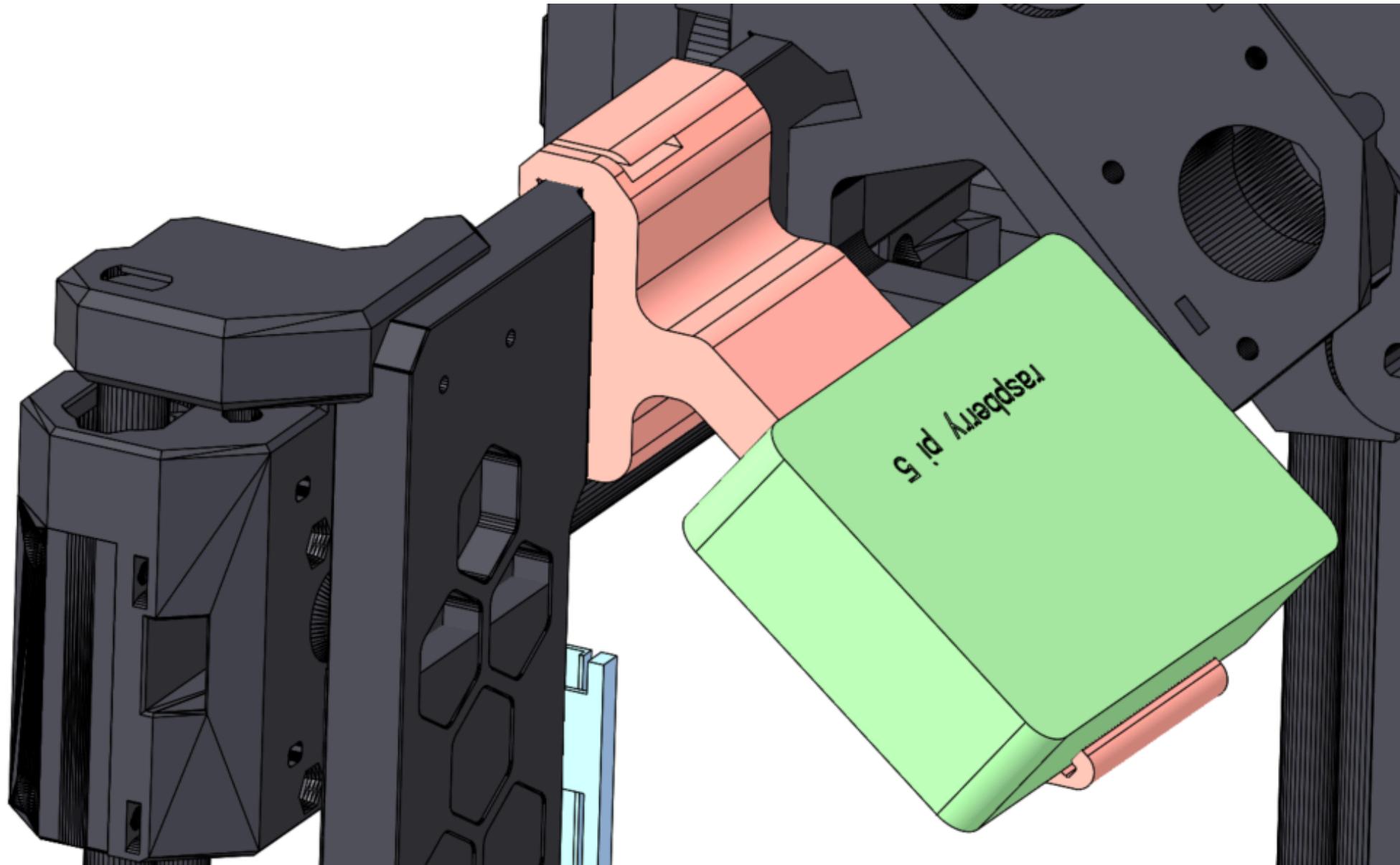
- Requirements and Constraints
 - Easy attachment and detachment
 - Full field of view
 - Stable



Camera Mount Design: ESP32 Wroom

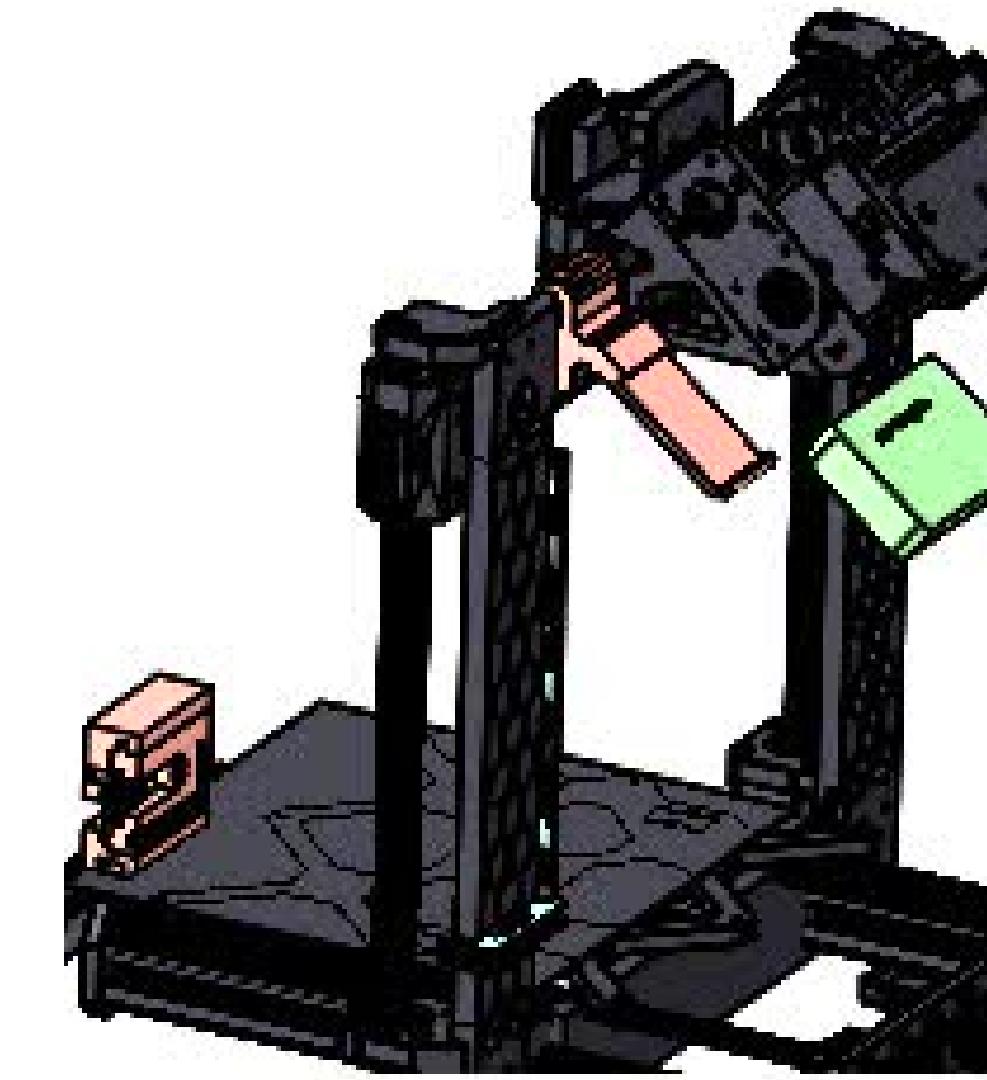
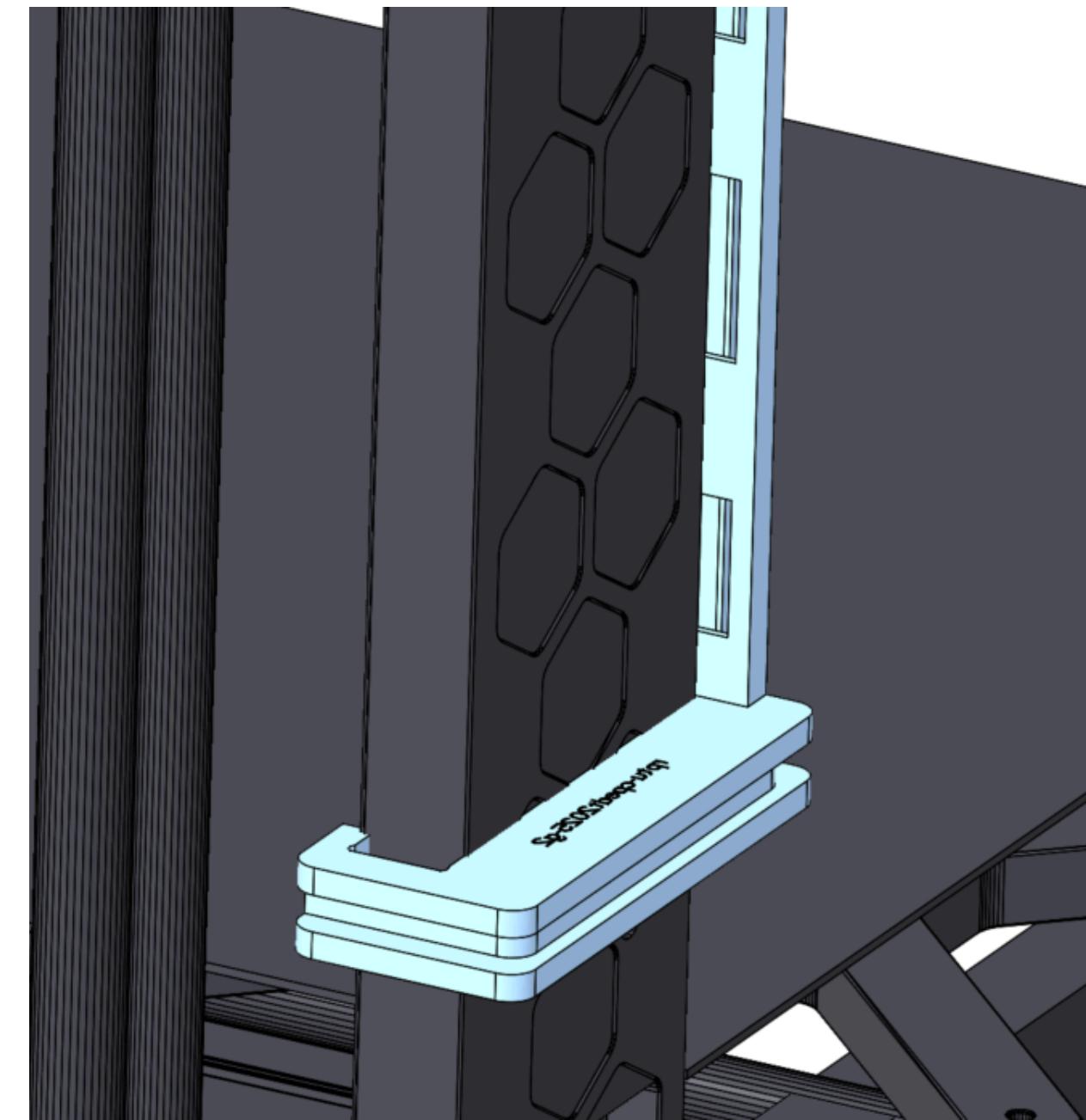
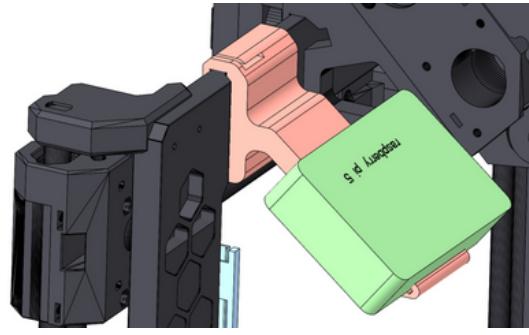


Camera Mount Design: Raspberry Pi 5

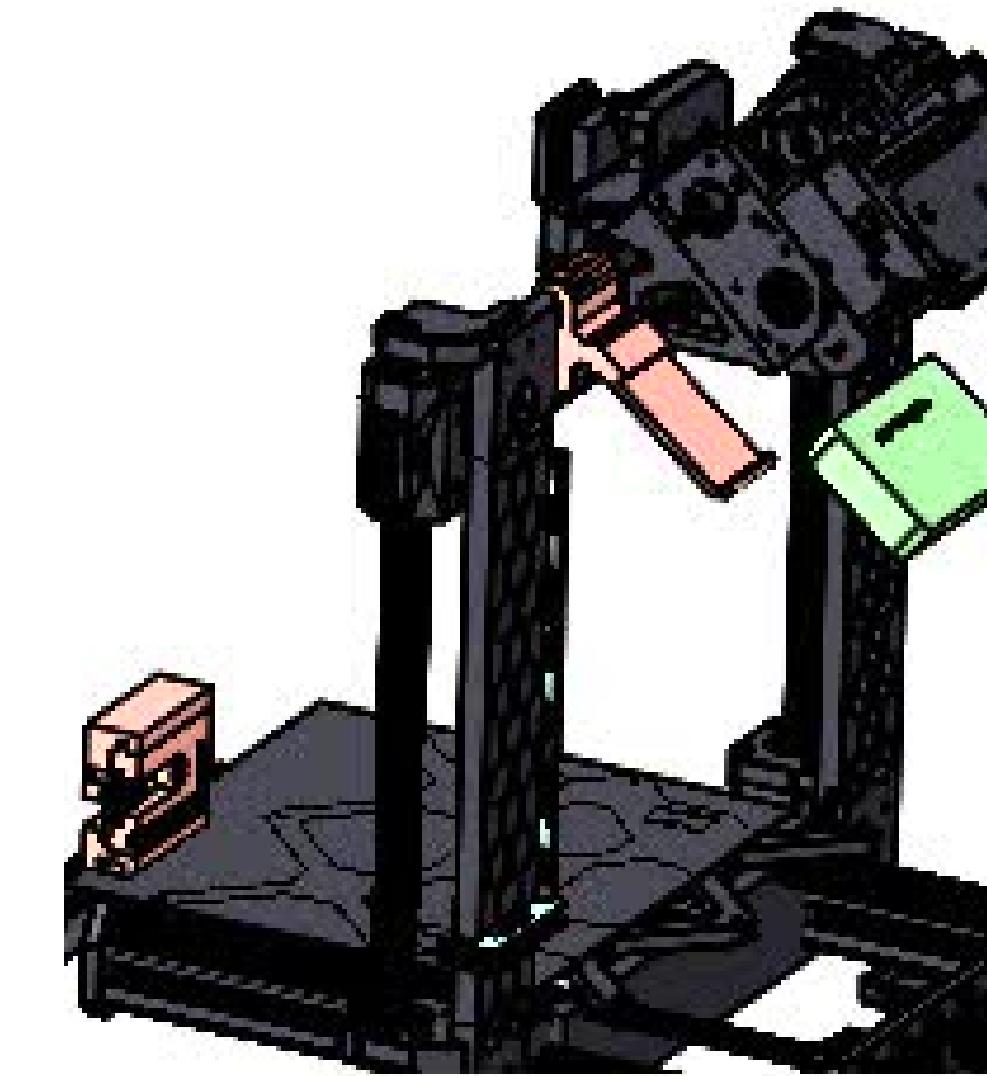
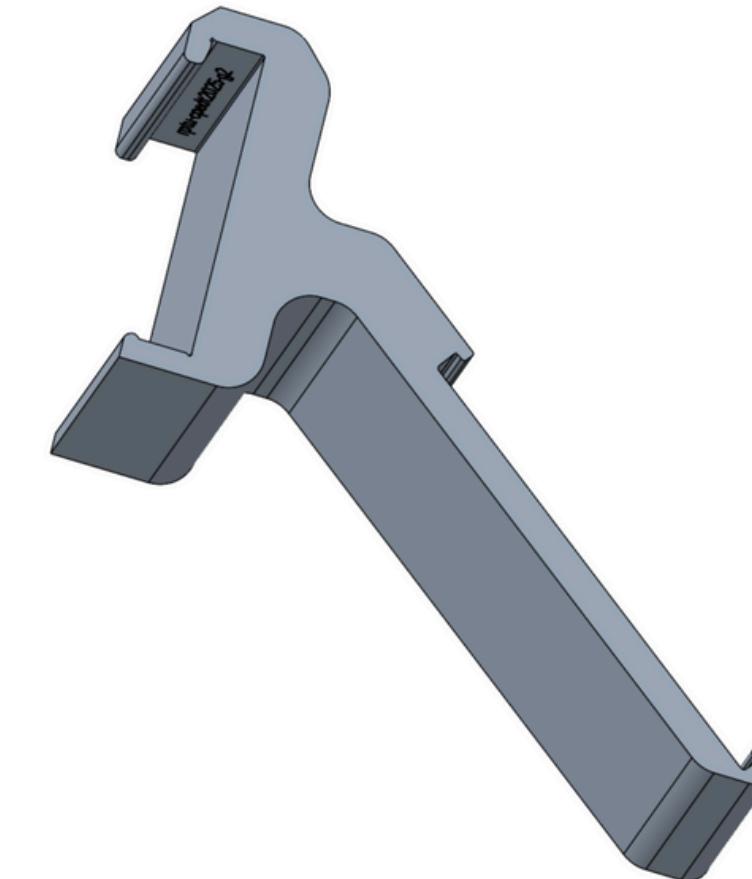
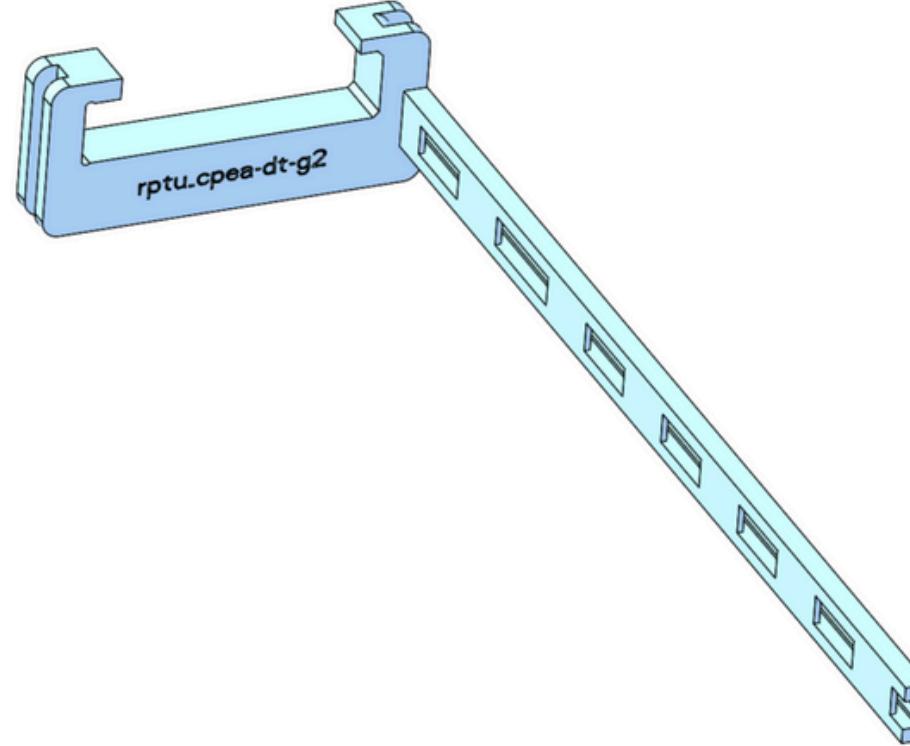


[2] PRUSA M4 printer

Camera Mount Design: Raspberry Pi 5



Camera Mount Design: Raspberry Pi 5



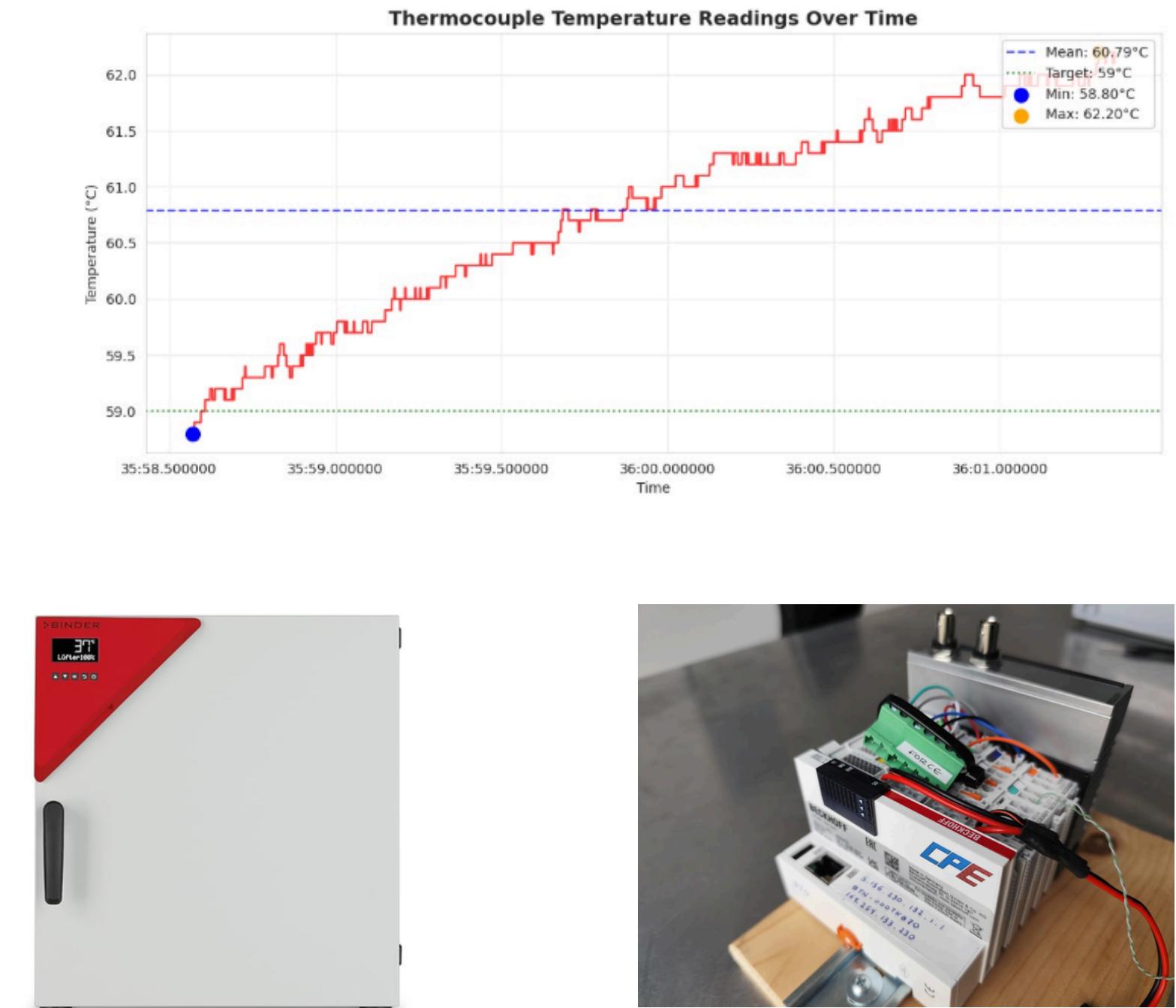
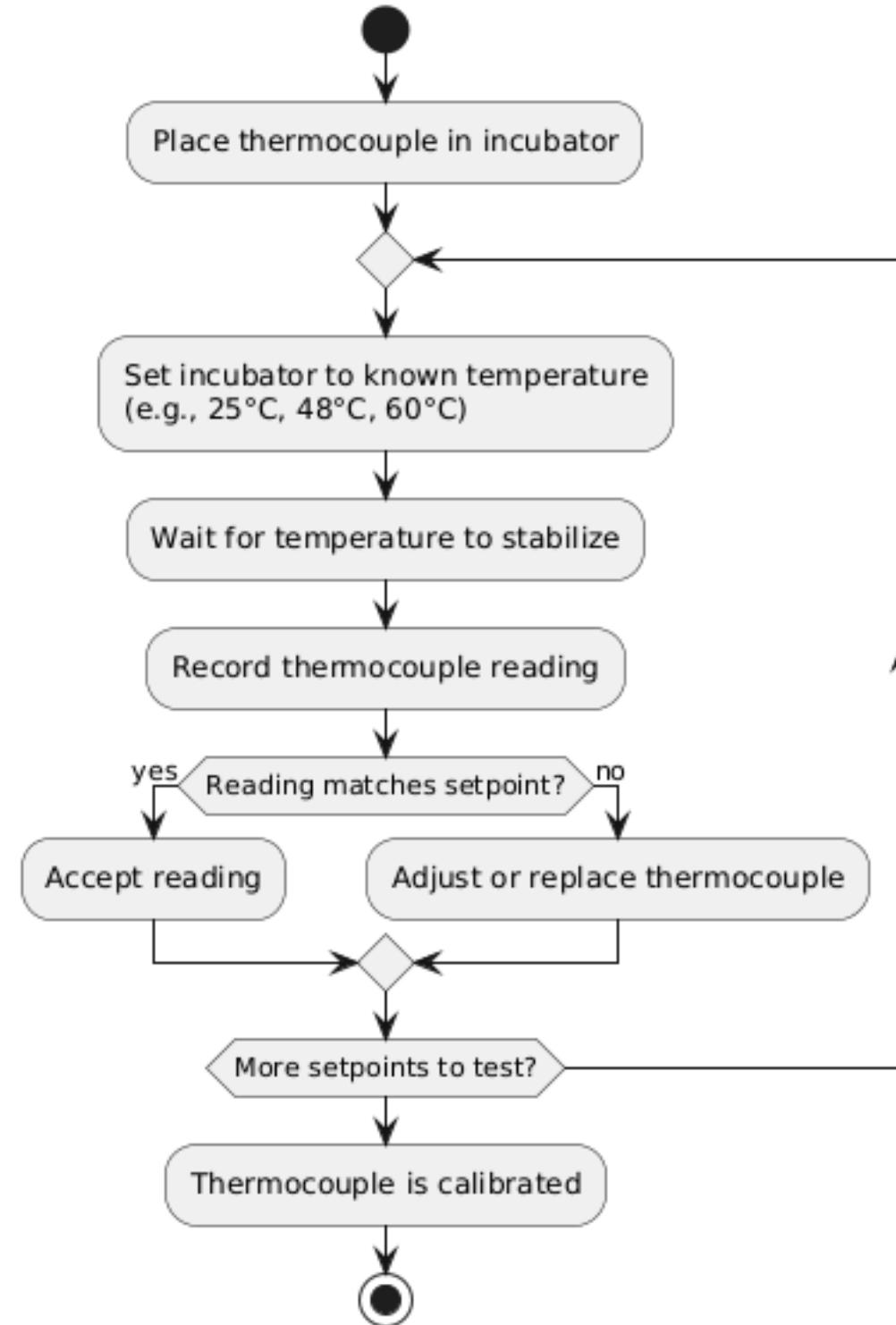
Camera Mount Design

Mount aspect				
Task	Status	Priority	Notes	
cable management	✓ Completed	High		
cable protection	✓ Completed	High	hot nozzle	
vibration isolation	✓ Completed	Medium	magnet; zero interference between bed and nozzle motor	
distance-adaptive	✓ Completed	Medium	range between obj and cam	

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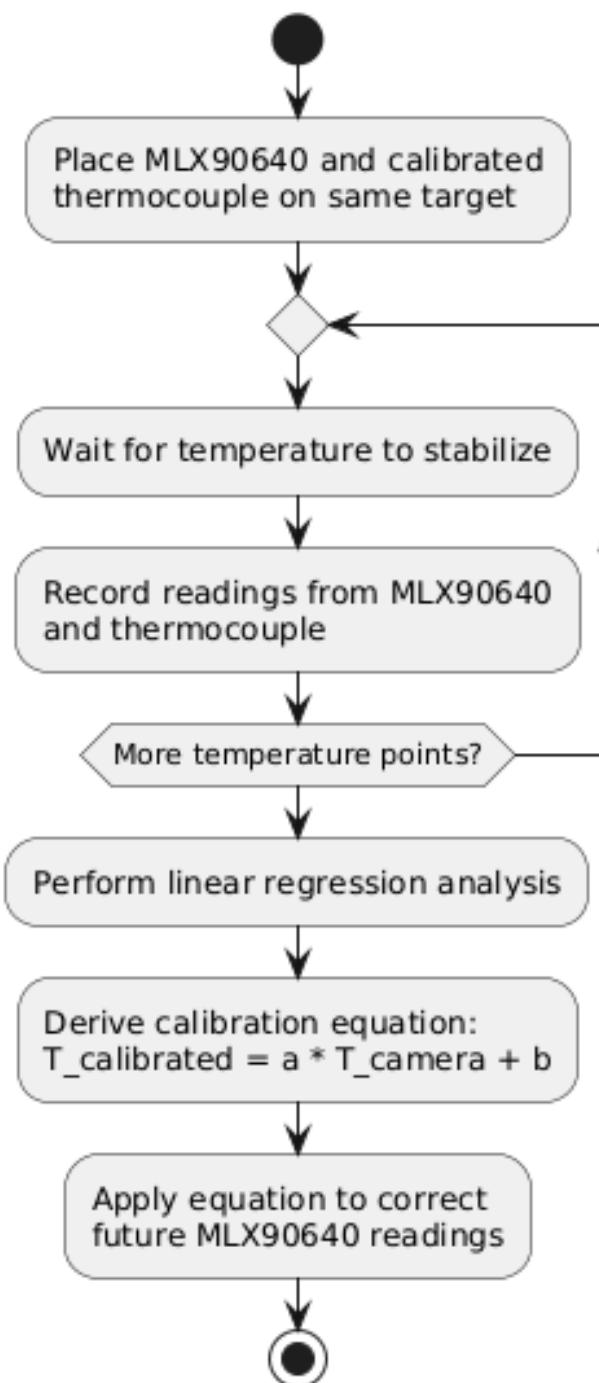
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Thermalcouple Calibration

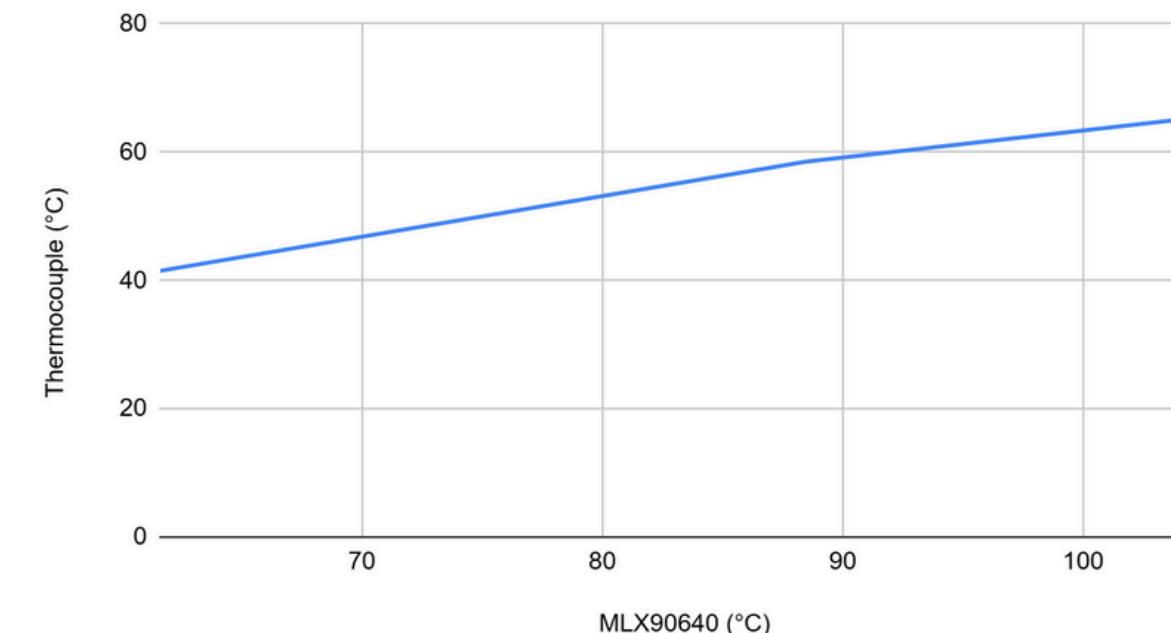


Thermal Camera Calibration

Thermal Camera (MLX90640) Calibration Workflow



Thermocouple (°C) vs MLX90640 (°C)



MLX90640 (°C)	Thermocouple (°C)
61.58	41.5
88.46	58.53
105.26	65.6

$$T_{calibrated} = 0.559 \cdot T_{camera} + 7.61$$

Thermal Camera Calibration

Solution : Piecewise Linear Calibration

- Why?

The relationship between thermal camera and actual temperature is nonlinear.

- Approach:

Split the data into two temperature ranges and apply a separate linear fit to each.

- Benefits:

Simple to implement

More accurate than one global linear model

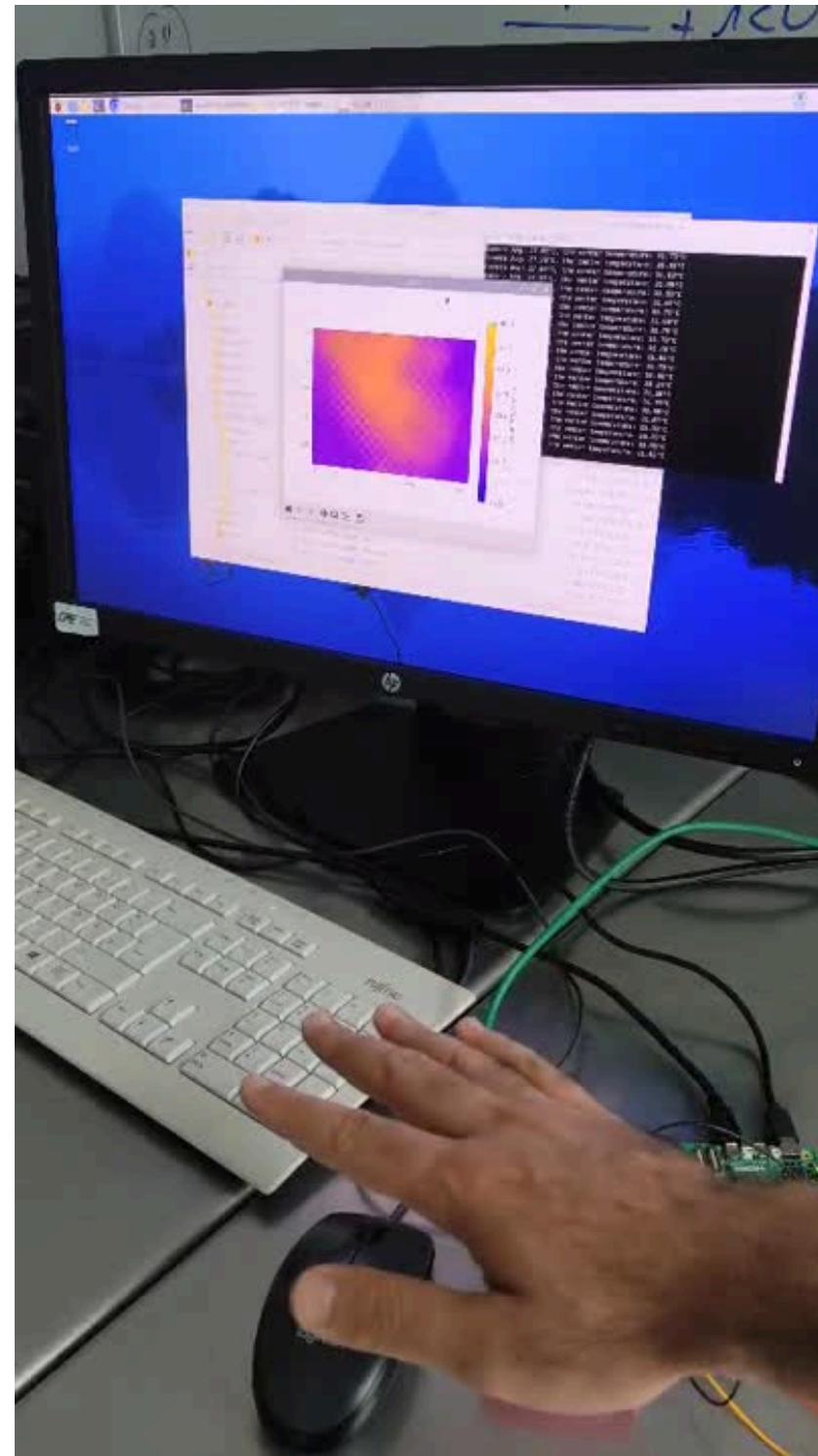
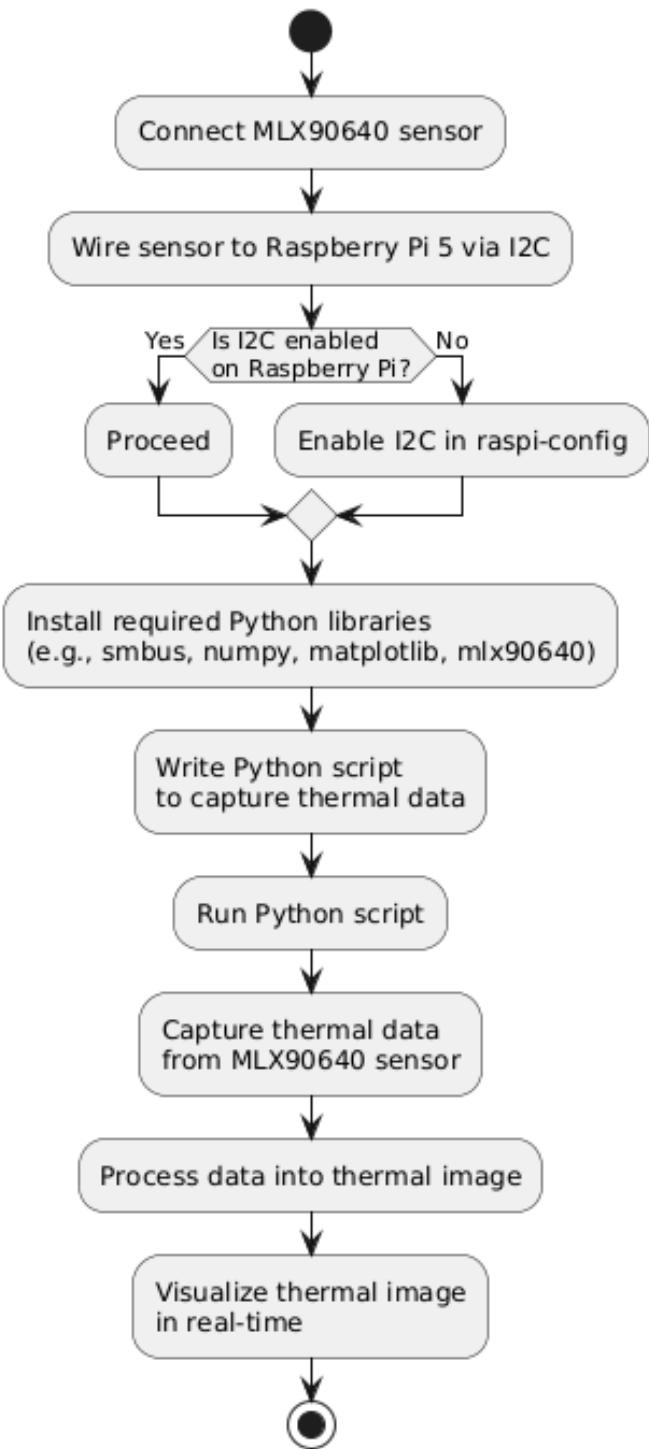
Works well for small dataset

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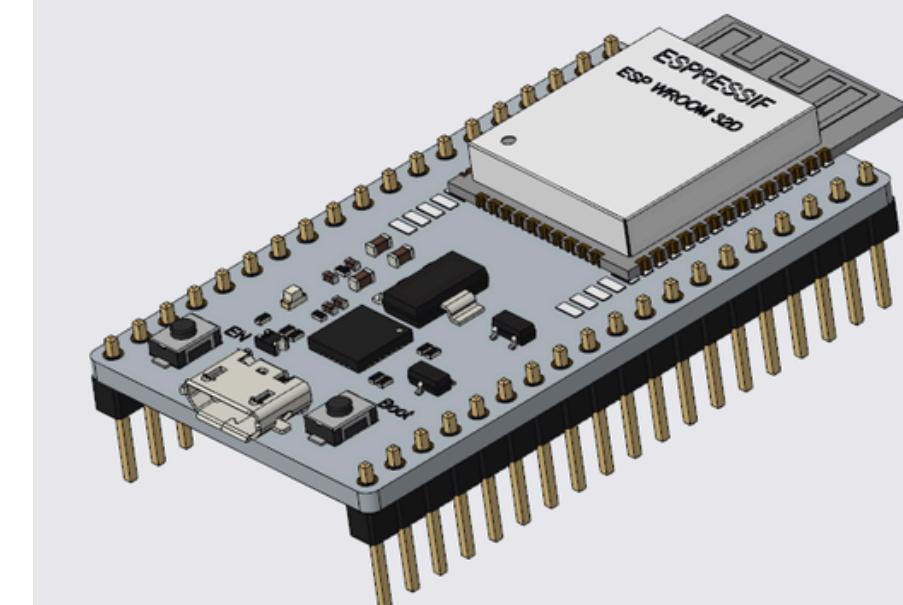
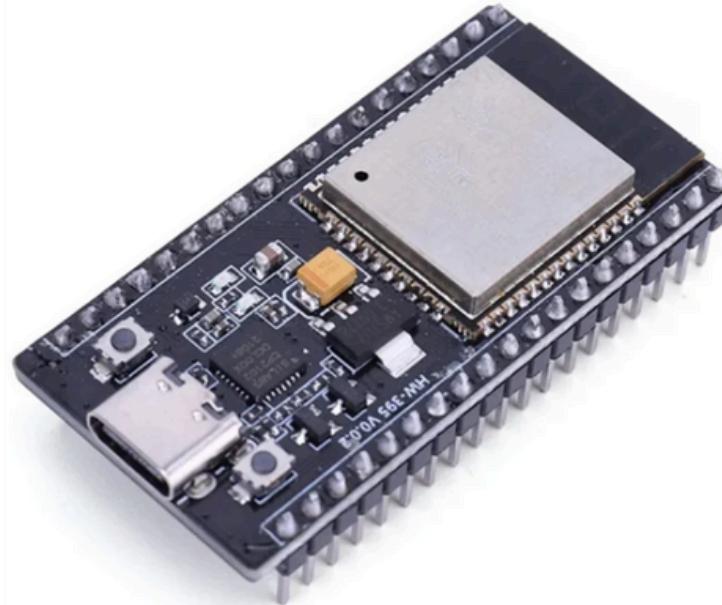
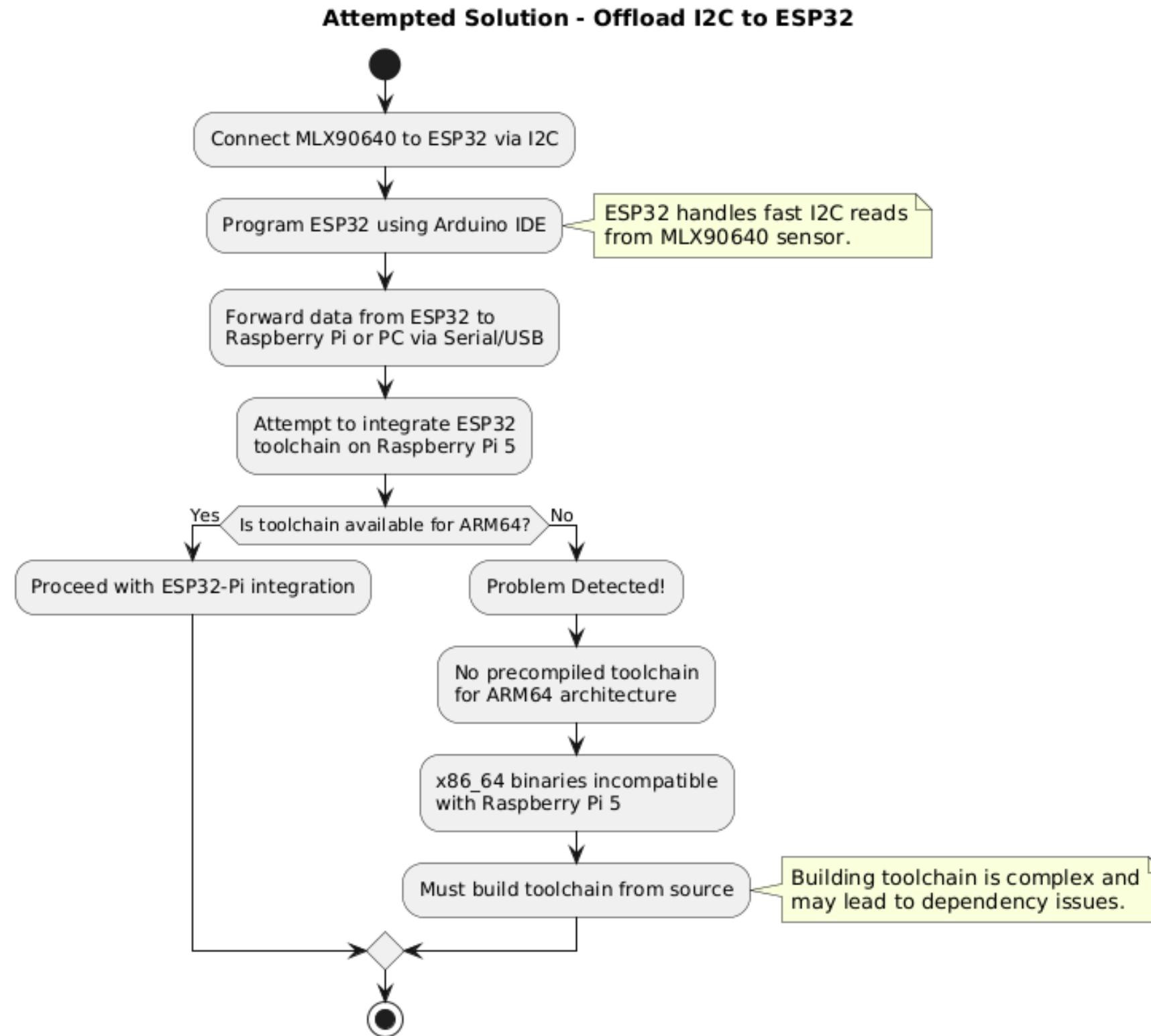
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Camera Setup Procedure

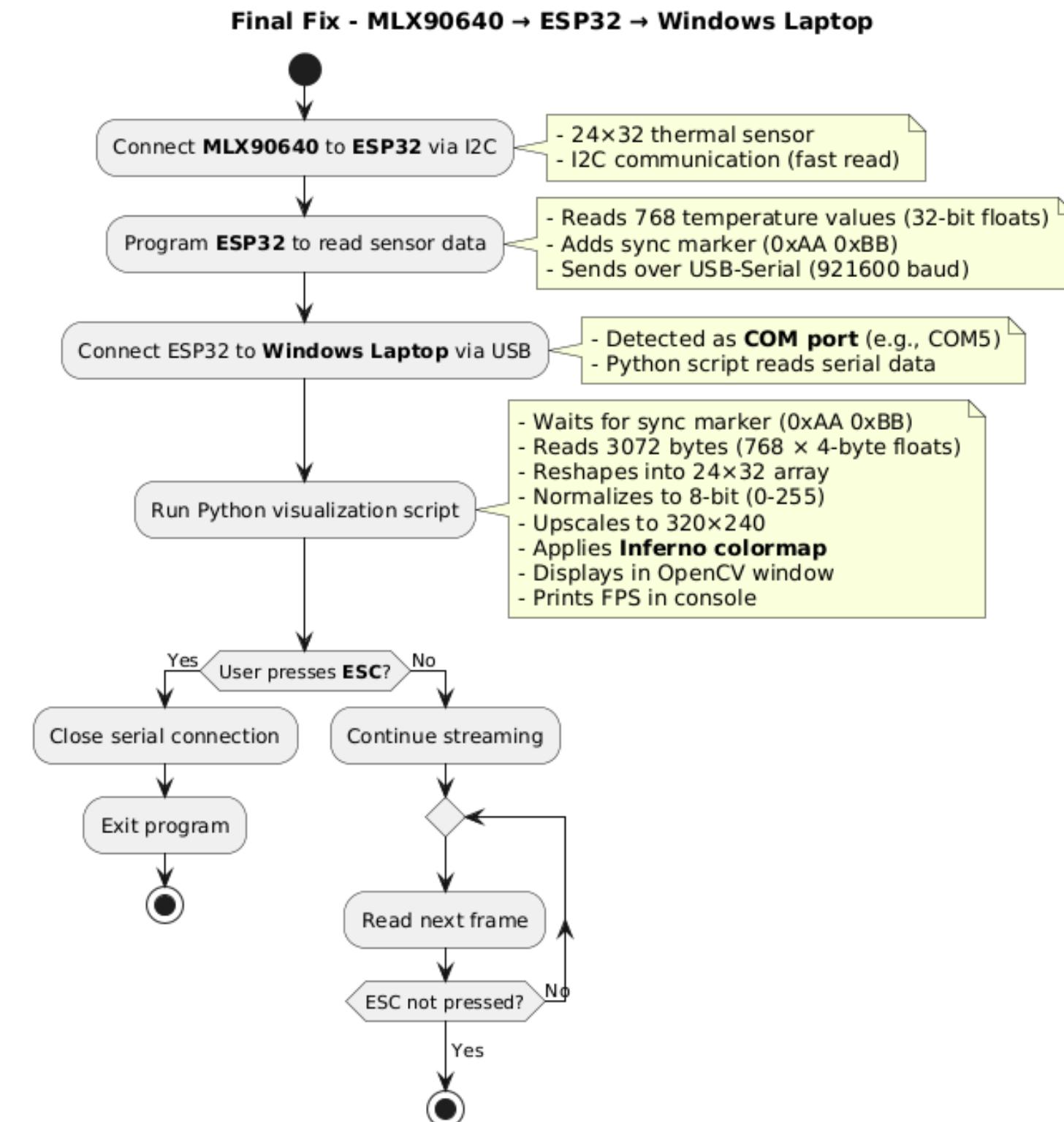
Initial Setup - MLX90640 + Raspberry Pi 5



Camera Setup Procedure



Camera Setup Procedure



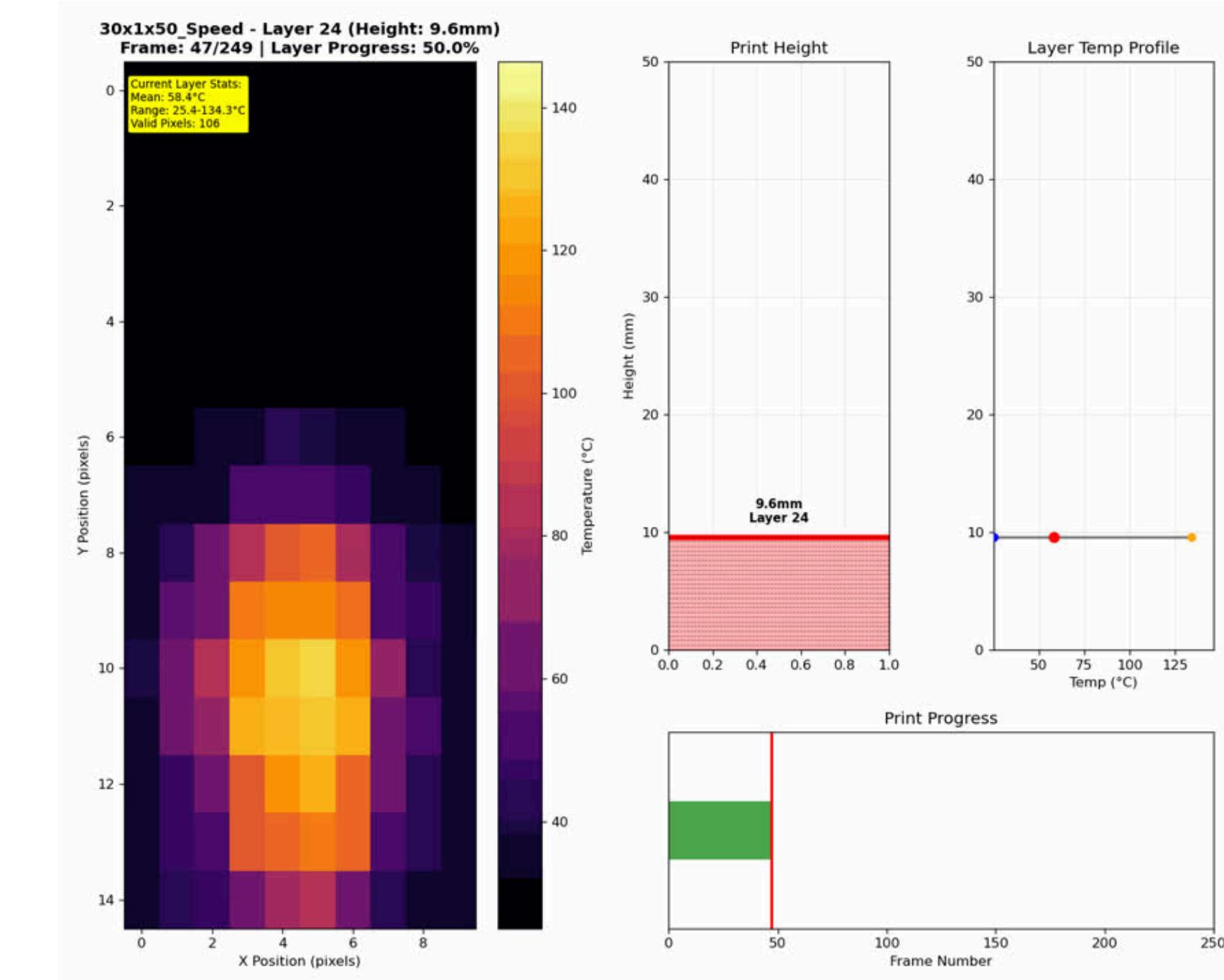
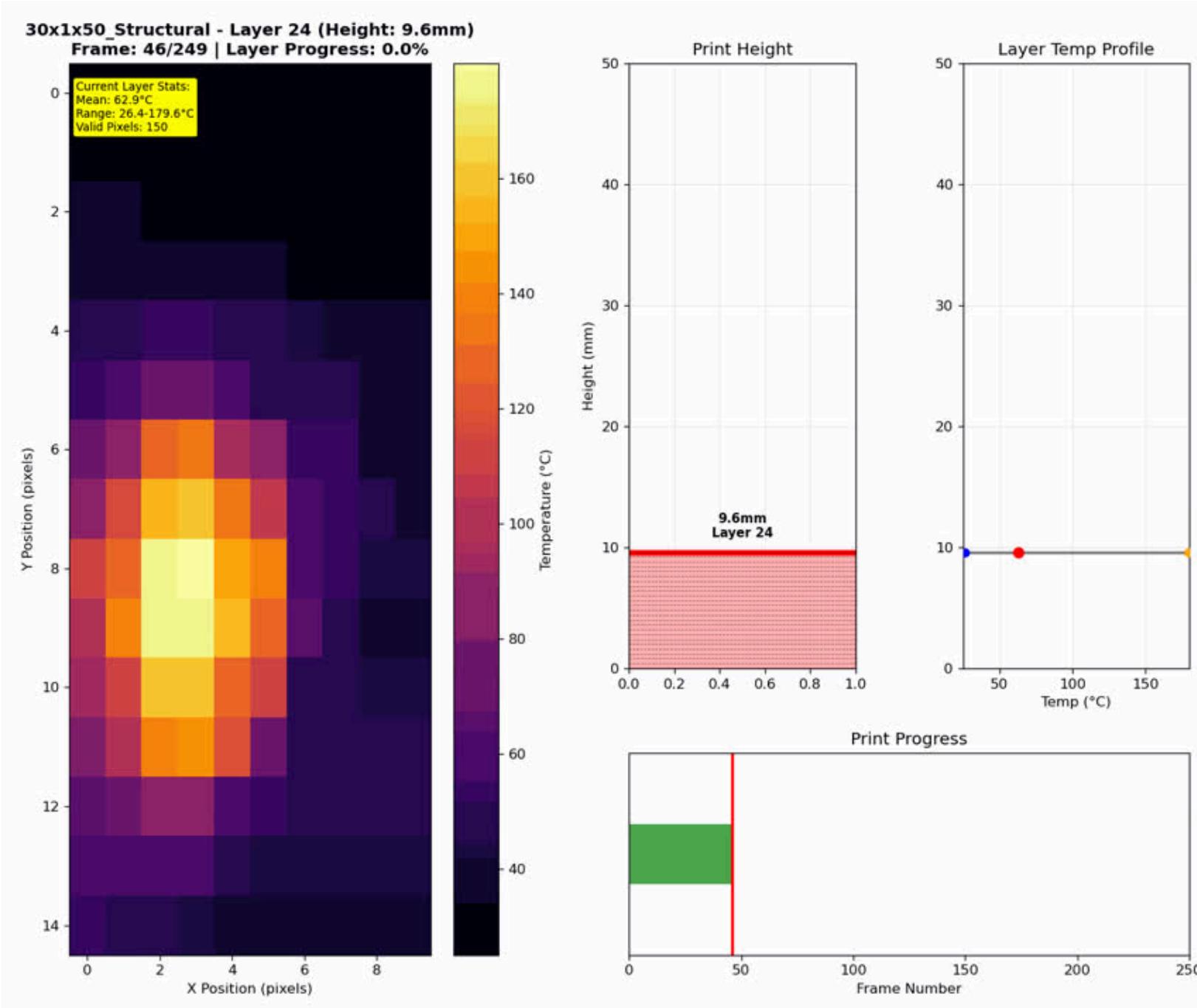
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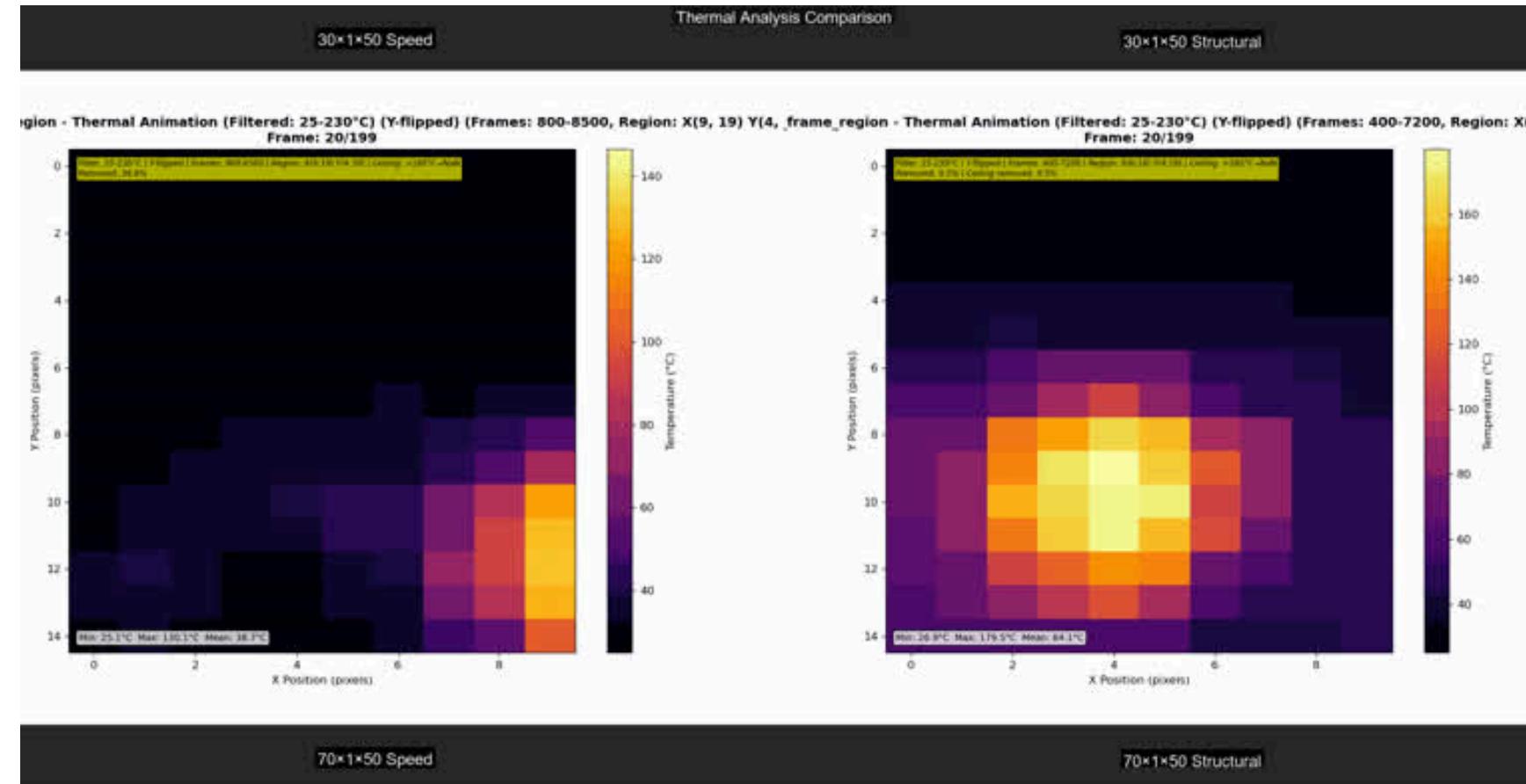
Printing Height Speed



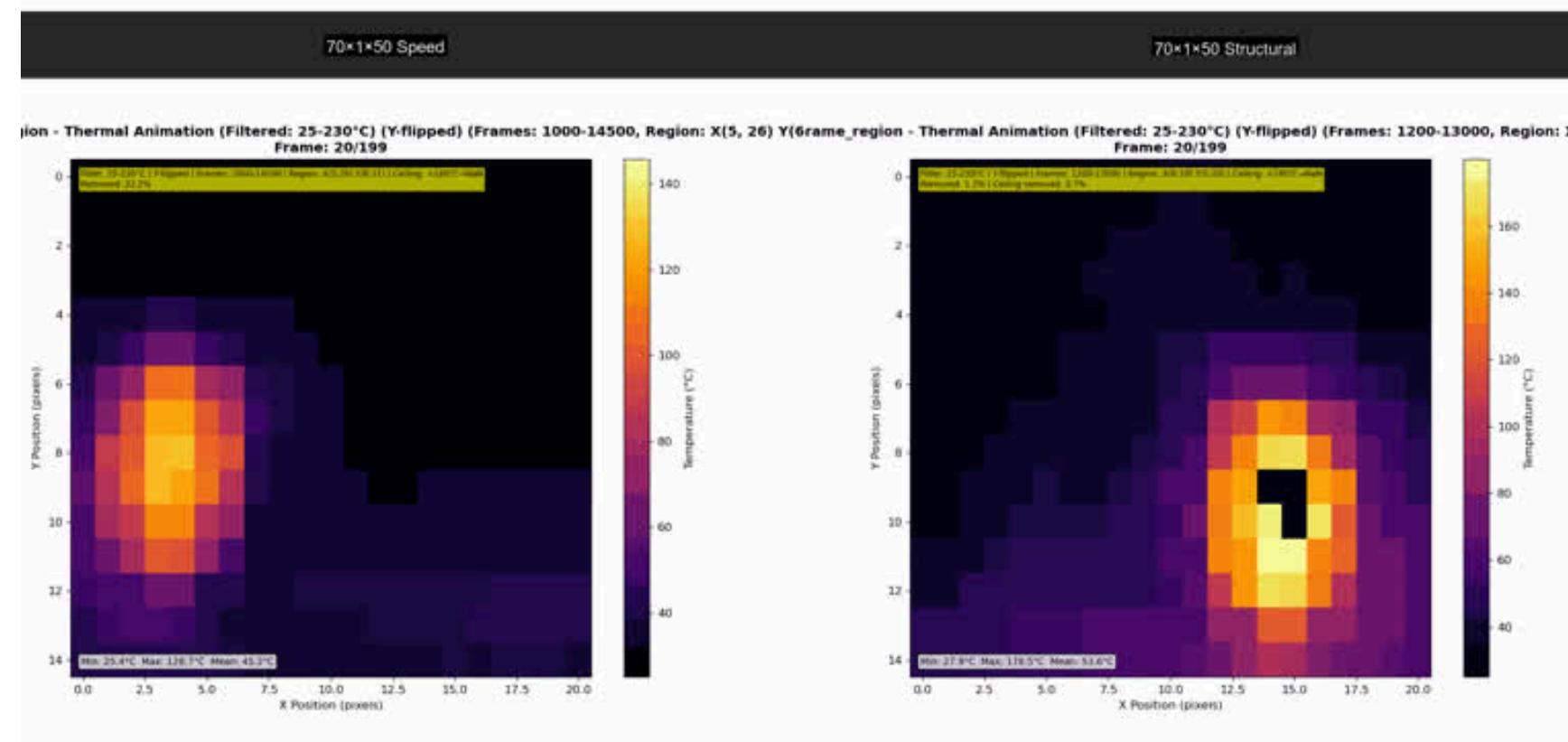
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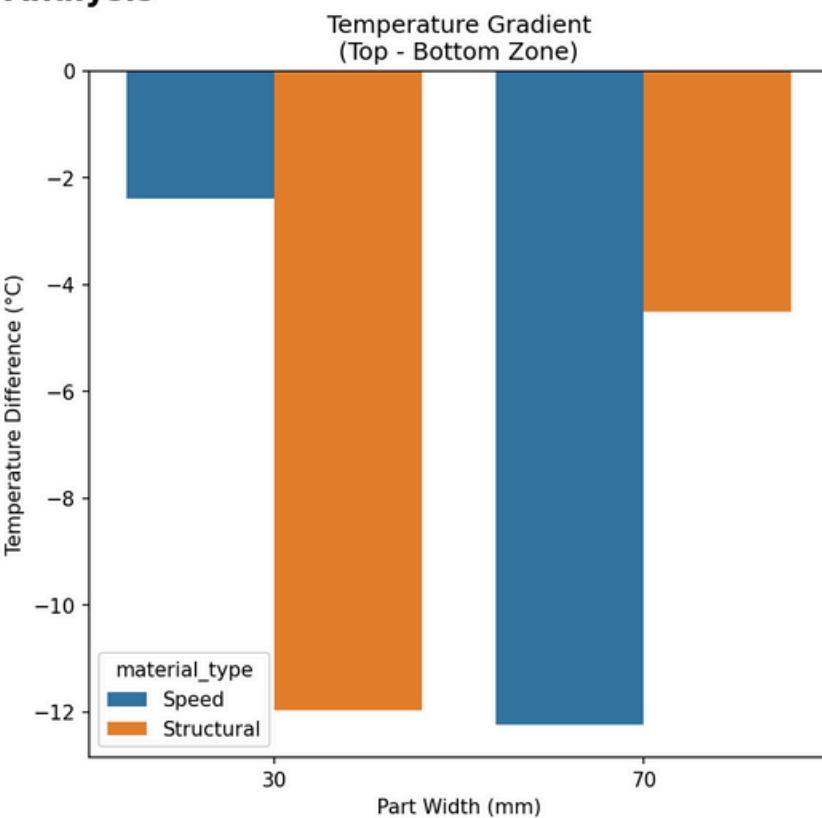
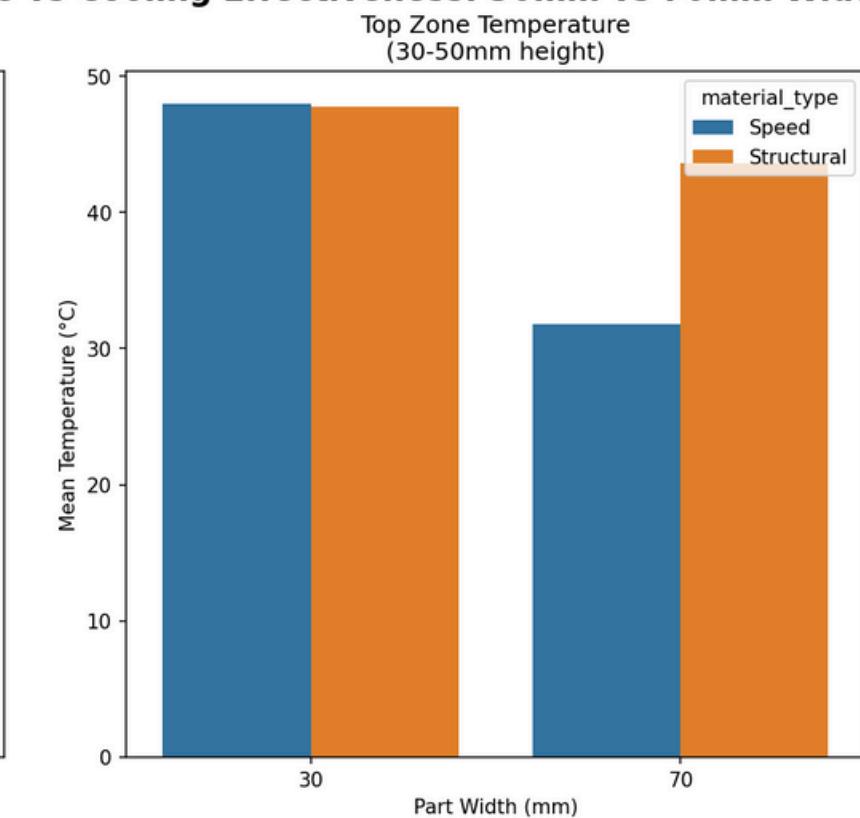
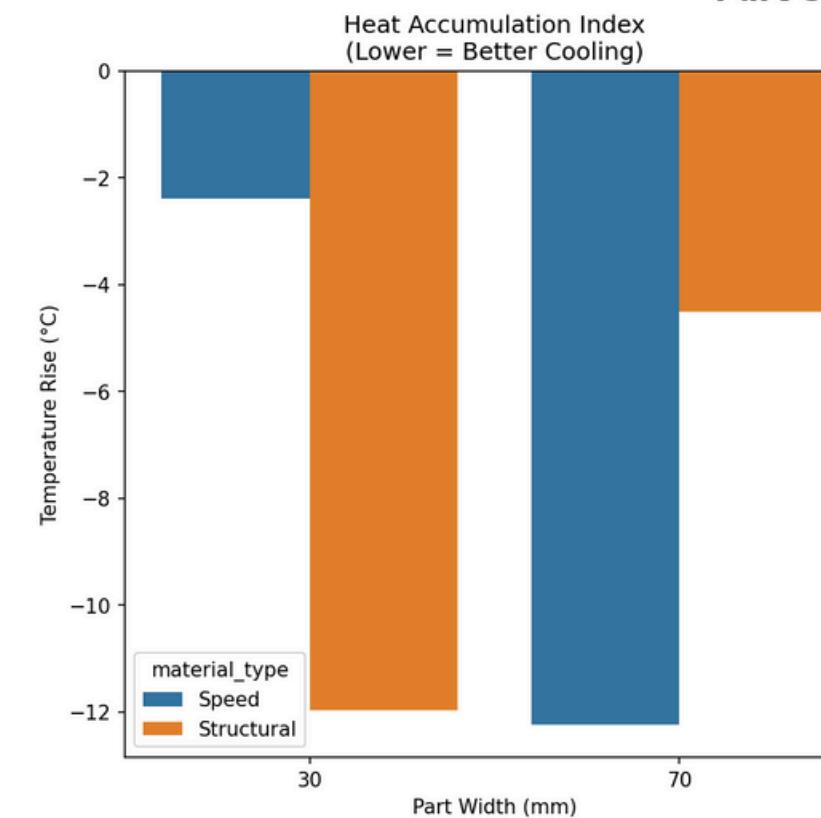
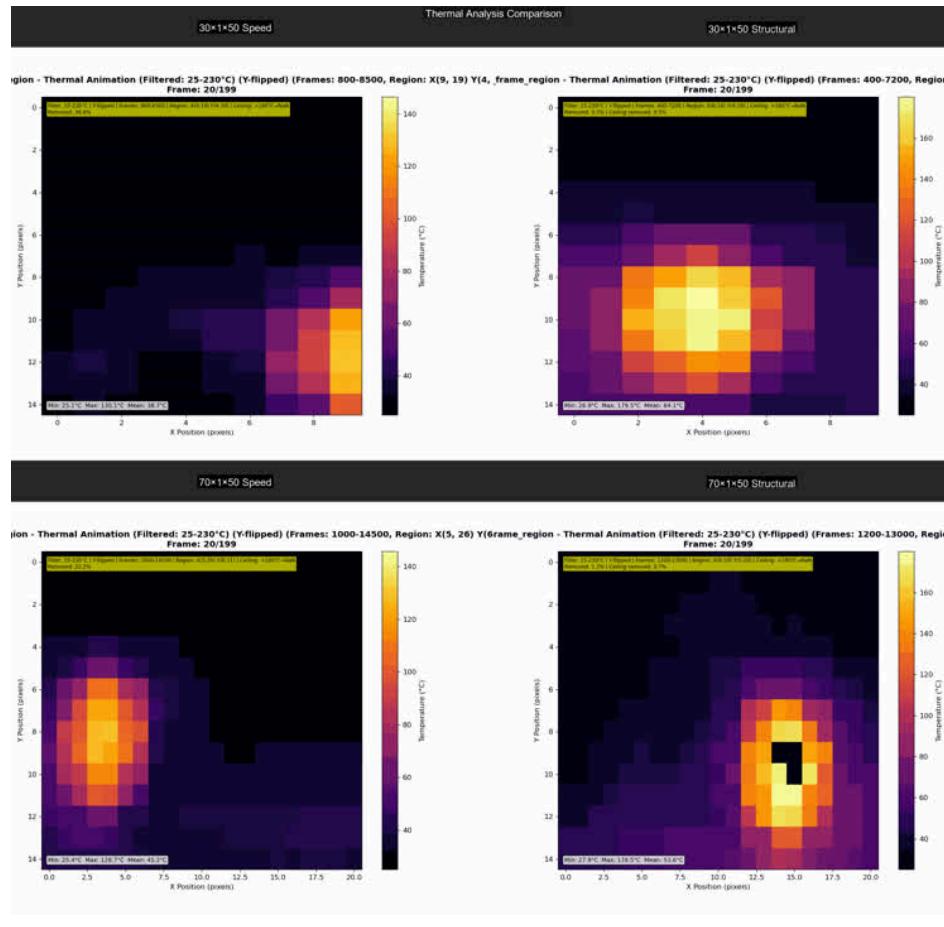
Temperature Difference Detection on Difference Wall Size



Temperature Measurement



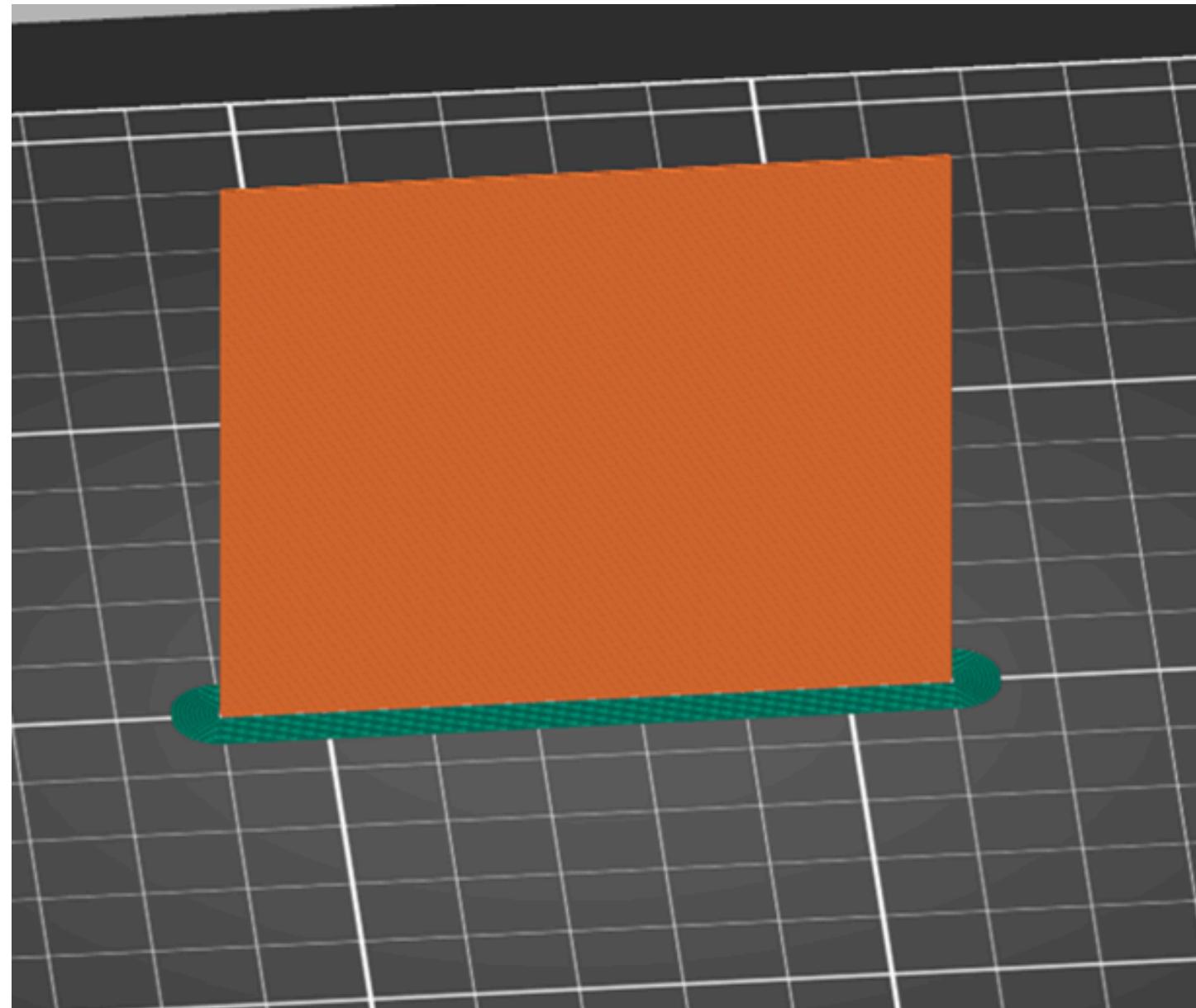
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Task 3 : Simulation of the temperature distribution in the wall



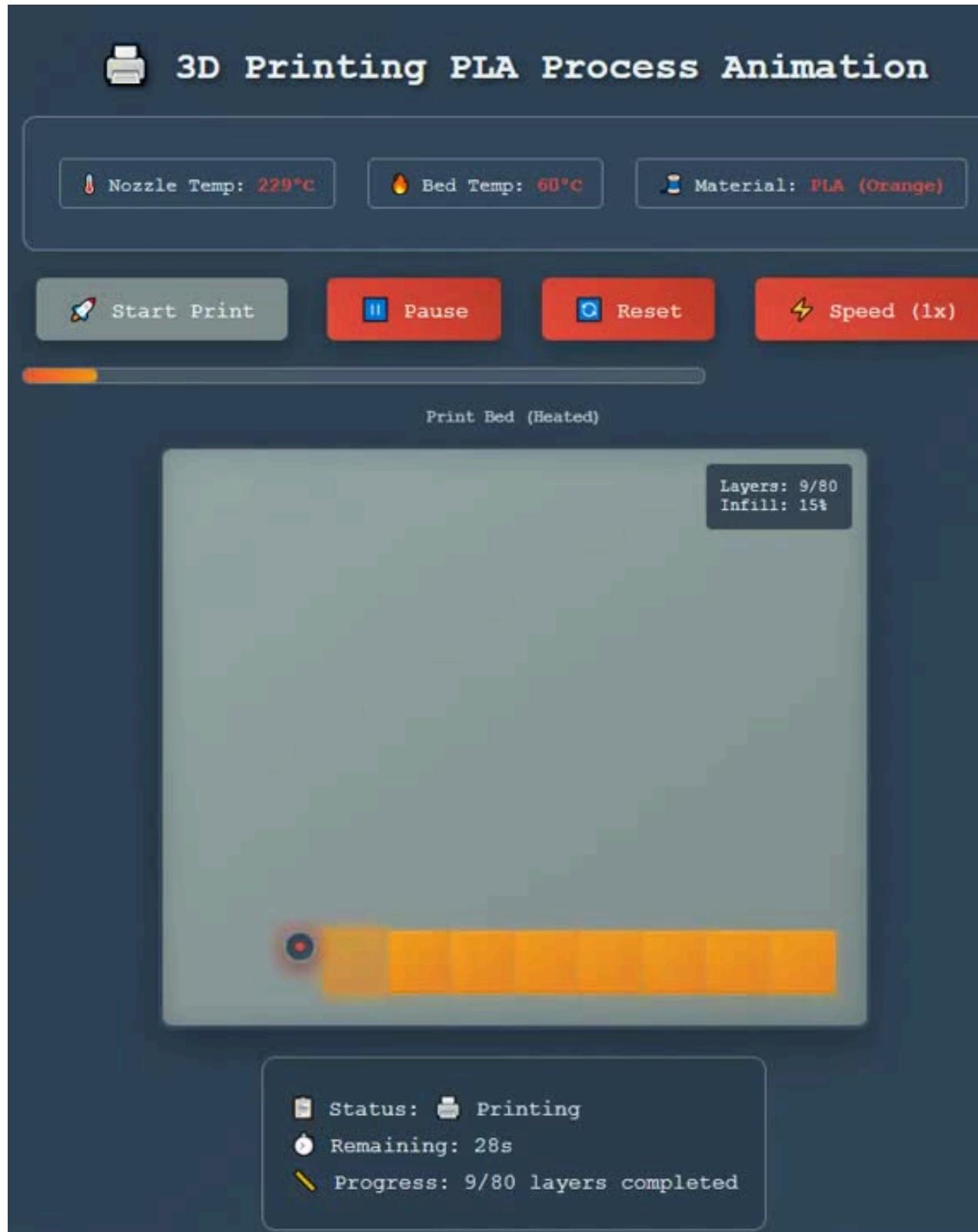
Printing Parameter:

layer height:	0.2 mm
speed for print move:	45/170 mm/s
size: length	30/70 mm
thickness	1 mm
height	50 mm

PLA material properties:

density ρ :	1250 kg/m ³
specific heat capacity c_p :	1800 J/ (kg K)
thermal conductivity K_0 :	0.13 W/(m K)

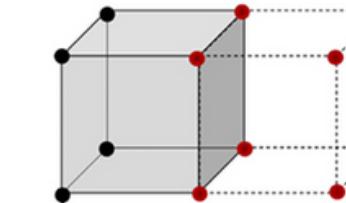
Simulation Setting: Model + Method



Problem: transient 2D Heat transfer [Ramos et al.]

$$\rho c_p \frac{\partial T(\mathbf{x},t)}{\partial t} = \nabla \cdot (K_0 \nabla T(\mathbf{x},t)) + Q$$

$$\mathbf{q} = K_0 \nabla T(\mathbf{x},t)$$



Boundary Conditions:

$$K_0 \nabla T(\mathbf{x},t) \cdot \mathbf{n} + h(T - T_\infty) = 0 \quad \mathbf{x} \in \Gamma_c$$

$$T(\mathbf{x},t) = T_b \quad \mathbf{x} \in \Gamma_b$$

Initial Condition:

$$T(\mathbf{x},0) = T_a \quad \mathbf{x} \in \Omega_q$$

$$T^i(\mathbf{x},0) = T^{i-1}(\mathbf{x},t_e) \quad \mathbf{x} \in \Omega_q$$

Q : heat source [W/m^3]

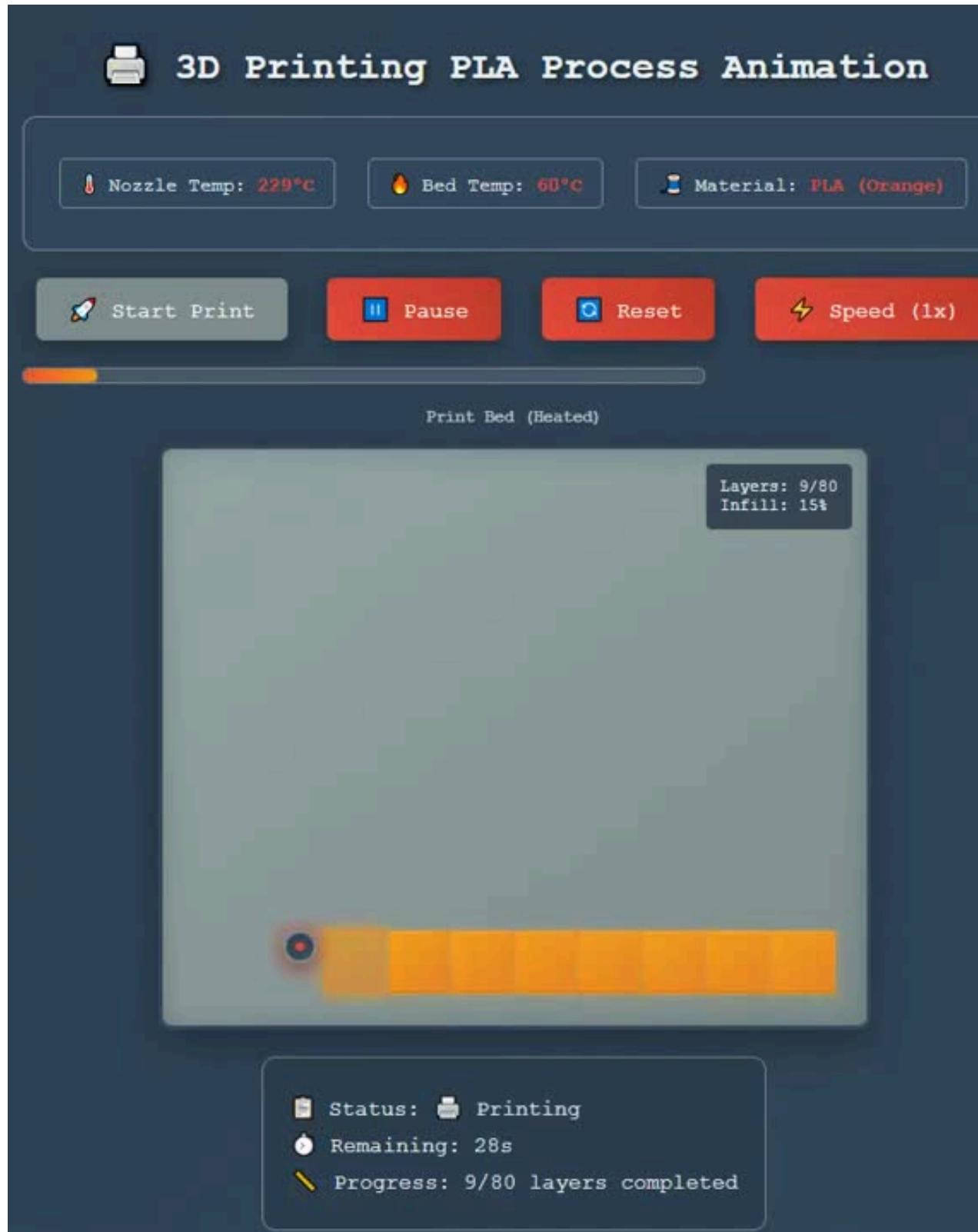
\mathbf{q} : heat flux vector [W/m^2]

h : heat transfer coefficient = $25 \text{ W}/(\text{m}^2 \text{ K})$

T_b : bed temperature = 60°C

T_a : ambient temperature = 25°C

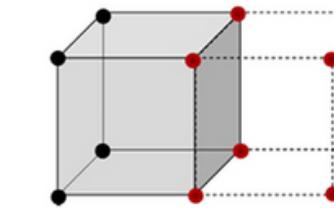
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Problem: transient 2D Heat transfer [Ramos et al.]

$$\rho c_p \frac{\partial T(\mathbf{x},t)}{\partial t} = \nabla \cdot (K_0 \nabla T(\mathbf{x},t)) + Q$$

$$\mathbf{q} = K_0 \nabla T(\mathbf{x},t)$$



Method:

Numerical:

Time discretization: θ – method

$$\frac{T^{n+1} - T^n}{\Delta t} = \theta \cdot f(T^{n+1}) + (1-\theta) \cdot f(T^n)$$

$\theta = 0 \rightarrow$ explicit

$\theta = 1 \rightarrow$ implicit

$\theta = 0.5 \rightarrow$ Crank-Nicolson

Space discretization: FDM

Analytical: $Q \rightarrow$ moving heat source \rightarrow complex

Boundary Conditions:

$$K_0 \nabla T(\mathbf{x},t) \cdot \mathbf{n} + h(T - T_\infty) = 0 \quad \mathbf{x} \in \Gamma_c$$

$$T(\mathbf{x},t) = T_b \quad \mathbf{x} \in \Gamma_b$$

Initial Condition:

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Q : heat source $[W/m^3]$

\mathbf{q} : heat flux vector $[W/m^2]$

h : heat transfer coefficient $= 25 W/(m^2 K)$

T_b : bed temperature $= 60 ^\circ C$

T_a : ambient temperature $= 25 ^\circ C$

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Printing Speed on Temperature Distribution [Tomáš et al.]

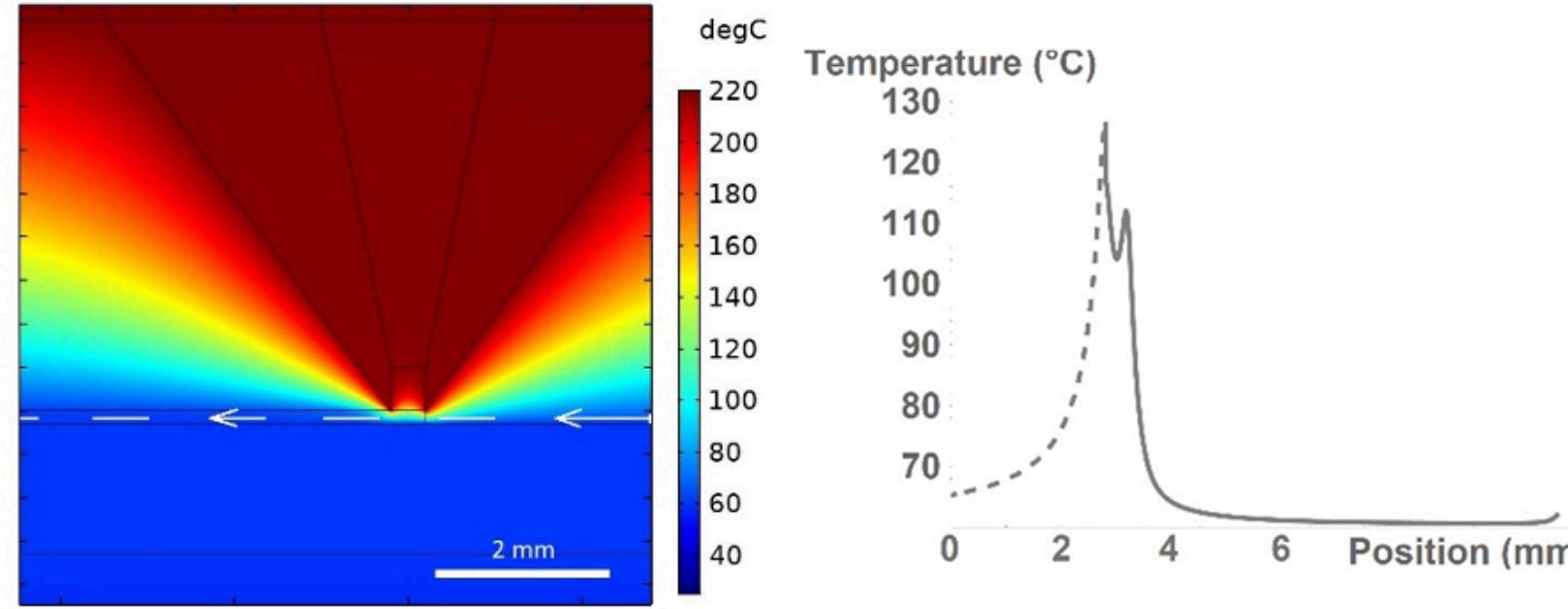


Figure 5. Detail of the printer nozzle/bed interface (left). Temperature distribution along the white line, where the white arrow denotes the direction of the x -axis (right). Printhead moves in the right direction.

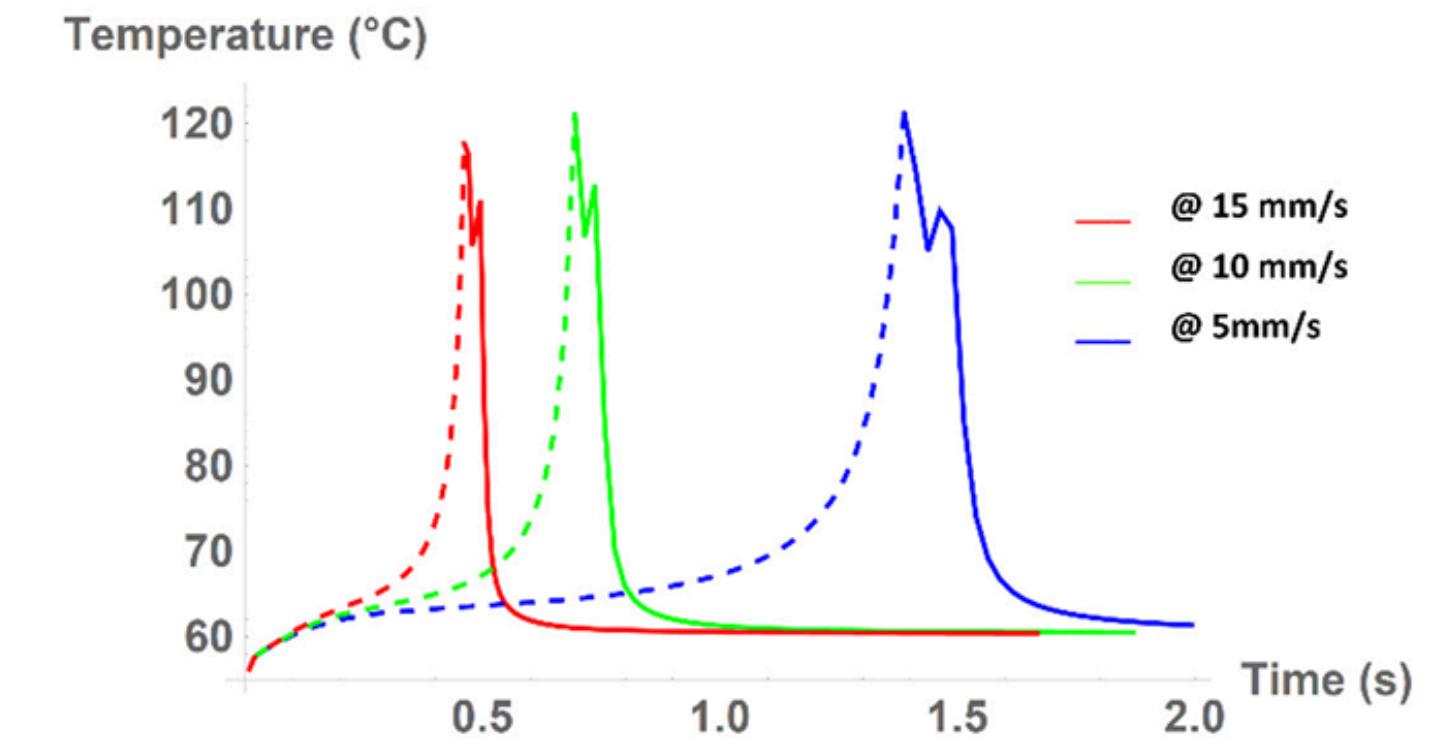


Figure 8. Temperature of the fixed-point during printing.

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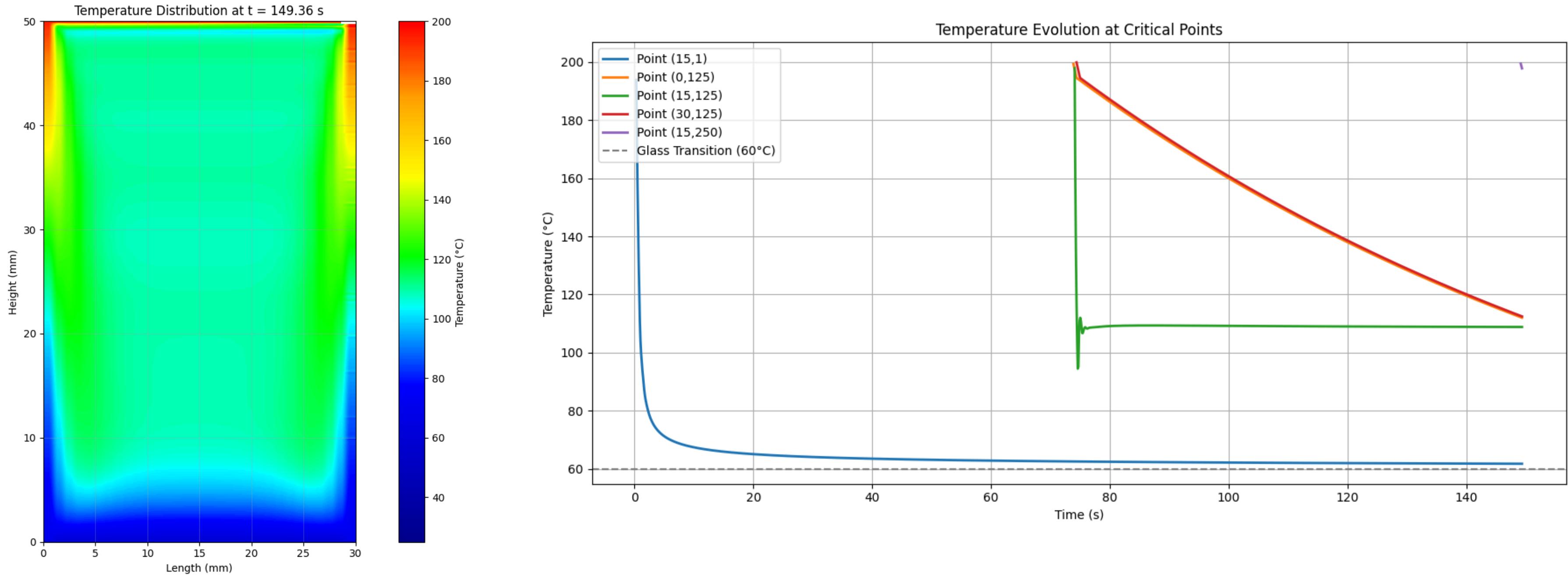
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Result

Camera Mount Design

Temperature Measurement

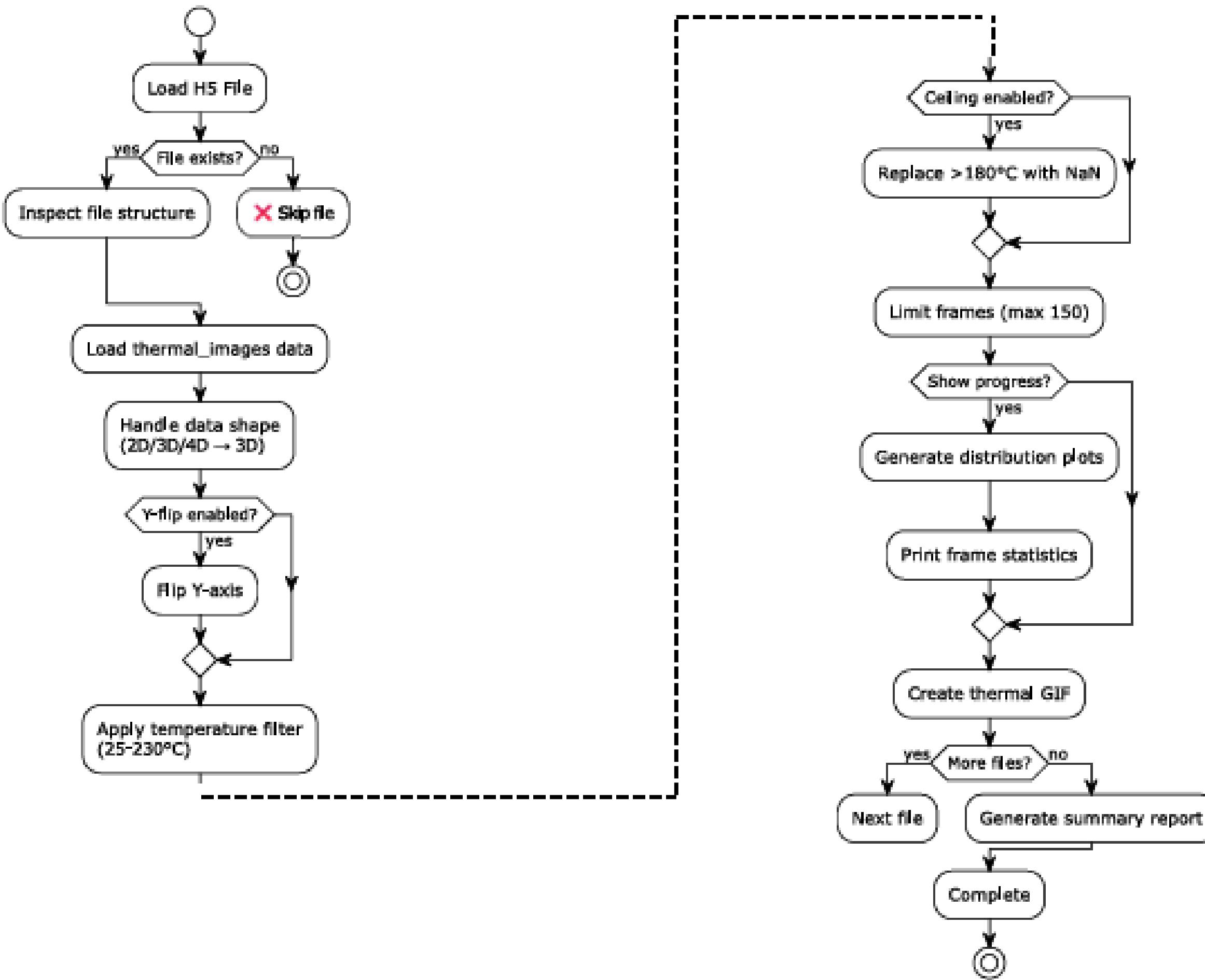
Simulation Model



Danke

Appendix

Thermal Data Preprocessing Pipeline



Appendix

