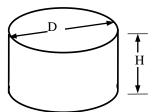
Problem 1 (50%)



Find the time for which $T_{\min} = 90^{\circ}\text{C}$

Given: $T_i = 40^{\circ}\text{C}$; $T_{\infty} = 110^{\circ}\text{C}$; $h = 470 \text{ W/m}^2 \text{-K}$

Vegetable properties approximate water D = 12 cm and H = 10 cm

Assumptions: Unsteady heat conduction (heating) with constant properties; Radiation may be considered negligible. No natural convection within the can (pure conduction)

Solution:

Check for LPA:

Guess average temperature of (40+110)/2=75 °C and read the thermophysical properties of water:

$$k = 0.671 \text{ W/m-°C}; \ \rho = 974.9 \text{ kg/m}^3; \ c_p = 4190 \text{ J/kg-°C}; \ \alpha = \frac{k}{\rho c_p} = \frac{0.671}{974.9 \times 4190} = 1.64 \times 10^{-7} \text{ m}^2/\text{s}$$

$$Bi = \frac{hL_c}{k}; \quad L_c = \frac{\text{volume}}{\text{Surf. total}} = \frac{\pi D^2 / 4 \times H}{2 \pi D^2 / 4 + \pi DH} = \frac{D / 4 \times H}{D / 2 + H} = \frac{0.12 / 4 \times 0.10}{0.12 / 2 + 0.10} = 0.01875 \text{ m}$$
exposed conv.

$$Bi = \frac{470 \ 0.01875}{0.671} = 13.13 > 0.1 \Rightarrow LPA \text{ not valid}$$

The $T_{\min} = 90$ °C is at the center of the can, i.e., farthest point from the hot thermal boundaries. The can geometry can be constructed by intersecting a long cylinder of diameter $D=2r_o$ and an infinite plate of thickness H. t is not known at this stage.

Assume: Plane wall: $t_1^* = \alpha t / H / 2^2 > 0.2$, LongCylinder: $t_2^* = \alpha t / r_o^2 > 0.2$

thus, 1-term approximation of infinite series solution is adequate

$$\varphi_{r,x,t} = \frac{T_{r,x,t} - T_{\infty}}{T_{i} - T_{\infty}} = C_{r,t} \times P_{x,t}; \quad \varphi_{0,0,t} = \frac{T_{0,0,t} - T_{\infty}}{T_{i} - T_{\infty}} = C_{0,t} \times P_{0,t}$$

$$CASE: A \Longrightarrow P_{0,t} = C_{B1} \exp -A_{B1}^2 t_1^* \quad CASE: B \Longrightarrow C_{0,t} = C_{B2} \exp -A_{B2}^2 t_2^*$$

$$\varphi_{0,0,t} = \frac{T_{0,0,t} - T_{\infty}}{T_{i} - T_{\infty}} = C_{0,t} \times P_{0,t} = C_{B1}C_{B2} \exp\left(-\left[\frac{A_{B1}^{2}}{H/2^{2}} + \frac{A_{B2}^{2}}{r_{o}^{2}}\right]\alpha t\right)$$
Quick check:
$$t_{1}^{*} = \alpha t / H/2^{2}$$

$$Bi_{M1} = \frac{h \ H/2}{k} = \frac{470 \ 0.05}{0.671} = 35 \xrightarrow{Table} A_{B1} = 1.5264; C_{B1} = 1.272$$

$$t_1^* = \frac{1.64 \times 10^{-7} \times 4865.2}{0.05^2} = 0.319$$

$$Bi_{M2} = \frac{hr_o}{k} = \frac{470 \ 0.06}{0.671} = 42 \xrightarrow{Table} A_{B2} = 2.3455; C_{B2} = 1.5993$$

$$\frac{90-110}{40-110} = 1.272 \times 1.5993 \times \exp\left(-\left[\frac{1.5264^{2}}{0.05^{2}} + \frac{2.3455^{2}}{0.06^{2}}\right]1.64 \times 10^{-7}t\right)$$

$$t_{2}^{*} = \frac{1.64 \times 10^{-7} \times 4865.2}{0.06^{2}} = 0.2216$$

$$0.1404 = \exp -0.000403459t$$

$$\Rightarrow t = 4865.2 \text{ s}$$

Quick check:

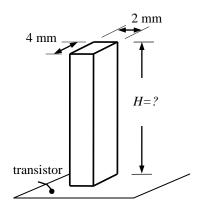
$$t_1^* = \alpha t / H / 2^2$$

$$t_1^* = \frac{1.64 \times 10^{-7} \times 4865.2}{0.05^2} = 0.319$$

$$t_2^* = \frac{\alpha t / r_o^2}{0.06^2}$$

$$t_2^* = \frac{1.64 \times 10^{-7} \times 4865.2}{0.06^2} = 0.2216$$

Problem 2 (50%)



a) Find *H*.

$$A_{cs} = 4 \times 10^{-3} \times 2 \times 10^{-3} = 8 \times 10^{-6} \text{ m}^2$$

 $P_{cs} = 2 \times 4 \times 10^{-3} + 2 \times 10^{-3} = 12 \times 10^{-3} \text{ m}$

$$m = \sqrt{\frac{hP_{cs}}{k_{fin}A_{cs}}} = \sqrt{\frac{14 \times 12 \times 10^{-3}}{165 \times 8 \times 10^{-6}}} = 11.28 \quad \text{m}^{-1}$$

Given:
$$T_{base} = 80^{\circ}\text{C}$$
; $T_{\infty} = 25^{\circ}\text{C}$; $h = 14 \text{ W/m}^2\text{-K}$
 $k_{fin} = 165 \text{ W/m-K}$
Fin effectiveness $\varepsilon_{fin} = 20$, 12 identical fins Transistor area 30 mm \times 20 mm

Assumptions: Quasi 1D steady heat conduction in the fin. Using compensated length, Case 3 solution (insulated tip) approximation is adequate. Radiation may be considered negligible.

$$\mathcal{E}_{\mathit{Fin}} \; \Box \; \frac{\mathbf{q}_{\text{actual}}}{\mathsf{Area}_{\mathsf{Base}} h \; T_{\mathit{wall}} - T_{\infty}} \; \Rightarrow \\ \mathcal{E}_{\mathit{Fin}}^{\mathit{Fin}} \; = \; \frac{\sqrt{k_{\mathit{fin}} A_{\mathit{c.s.}} h P_{\mathit{c.s.}}} \; T_{\mathit{Base}} - T_{\infty} \; \; \tanh \; \mathit{mL}_{\mathit{c}}}{A_{\mathit{c.s.}} h \; T_{\mathit{Base}} - T_{\infty}} = \sqrt{\frac{k_{\mathit{fin}} P_{\mathit{c.s.}}}{A_{\mathit{c.s.}} h}} \\ \mathsf{tanh} \; \; \mathit{mL}_{\mathit{c}}$$

$$\varepsilon_{Fin} = 20 = \sqrt{\frac{165 \times 12 \times 10^{-3}}{8 \times 10^{-6} \times 14}}$$
tanh 11.28 $L_c \implies 0.15 = \text{tanh } 11.28L_c$

$$\Rightarrow$$
 11.28 $L_c = 0.151 \Rightarrow L_c = 0.0134 \text{ m}$ or 13.4 mm

$$L_c = H + \frac{A_{cs}}{P_{cs}} \Rightarrow H = 0.0134 - \frac{8 \times 10^{-6}}{12 \times 10^{-3}} = 0.0127 \text{ m or } 12.7 \text{ mm}$$

b)

$$q_{tot} = q_{unfinned} + q_{finned} = A_{tot} - A_{finned} \quad h \quad T_{Base} - T_{\infty} \quad + N \times q_{one-fin}$$

$$q_{tot} = A_{tot} - A_{finned} \ h \ T_{Base} - T_{\infty} \ + N \times \varepsilon_{fin} A_{cs} h \ T_{Base} - T_{\infty}$$

$$\frac{q_{\mathit{finned}}}{q_{\mathit{tot}}} = \frac{N \times \varepsilon_{\mathit{fin}} A_{\mathit{cs}} h \ T_{\mathit{Base}} - T_{\scriptscriptstyle{\infty}}}{A_{\mathit{tot}} - A_{\mathit{finned}} \ h \ T_{\mathit{Base}} - T_{\scriptscriptstyle{\infty}} \ + N \times \varepsilon_{\mathit{fin}} A_{\mathit{cs}} h \ T_{\mathit{Base}} - T_{\scriptscriptstyle{\infty}}}$$

$$\frac{q_{\mathit{finned}}}{q_{\mathit{tot}}} = \frac{N \times \varepsilon_{\mathit{fin}} A_{\mathit{cs}}}{\left(A_{\mathit{tot}} - N A_{\mathit{cs}}\right) + N \times \varepsilon_{\mathit{fin}} A_{\mathit{cs}}} = \frac{\varepsilon_{\mathit{fin}}}{\left(A_{\mathit{tot}} / N A_{\mathit{cs}} - 1\right) + \varepsilon_{\mathit{fin}}} = \frac{20}{\left[30 \times 20 / (2 \times 4 \times 2)\right] + 20} = 79.2\%$$