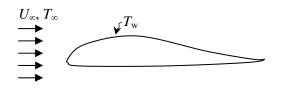
Solutions - Problem Set #7

Problem 1:



a)

$$\begin{aligned} q_{total} &= \overline{q}_{w}^{"} A_{s} = hA \left(T_{w} - T_{\infty} \right) \\ h_{1} &= \frac{q_{total-1} / A_{s}}{\left(T_{w} - T_{\infty} \right)} = \frac{200 / 0.02}{\left(75 - 25 \right)} = 200 \text{ W/m}^{2} - ^{\circ}\text{C} \\ h_{2} &= \frac{q_{total-2} / A_{s}}{\left(T_{w} - T_{\infty} \right)} = \frac{600 / 0.02}{\left(75 - 25 \right)} = 600 \text{ W/m}^{2} - ^{\circ}\text{C} \end{aligned}$$

b)

$$Nu = C \operatorname{Re}^m \operatorname{Pr}^n$$

$$\frac{hL_c}{k} = C \left(\frac{\rho U_{\infty} L_c}{\mu}\right)^m \left(\frac{\mu c_p}{k}\right)^n$$

In this problem:

 L_c, μ, ρ, c_p, k are all constant, so

$$h = \underbrace{\Upsilon}_{\text{constant}} U_{\infty}^{m}$$

Using the data provided,

the exponent m can be calculated:

$$\frac{h_1}{h_2} = \left(\frac{U_{\infty,1}}{U_{\infty,2}}\right)^m \Rightarrow m = \frac{\ln(h_1/h_2)}{\ln(U_{\infty,1}/U_{\infty,2})}$$

$$m = \frac{\ln(200/600)}{\ln(5/24.02)} = 0.7$$

and the constant $\Upsilon = \frac{h_1}{U_{\infty,1}^{m}} = 64.826 \frac{\text{W/m}^2 - ^{\circ}\text{C}}{(\text{m/s})^{0.7}}$

Thus, when U_{∞} , = 13.46 m/s:

$$h = \Upsilon U_{\infty}^{m} = 64.826 \times (13.46)^{0.7} = 400.02 \text{ W/m}^2 - ^{\circ}\text{C}$$

$$q = hA\Delta T = 400.02 \times 0.02 \times (75 - 25) = 400.02 \text{ W}$$

Given: $A_s = 0.02 \text{ m}^2$; $T_w = 75^{\circ}\text{C}$; $T_{\infty} = 25^{\circ}\text{C}$ $\rho = 1 \text{ kg/m}^3$; $c_p = 1000 \text{ J/kg-°C}$; k = 0.025 W/m-°C

Experimental results:

Run 1: $U_{\infty} = 5$ m/s; $q_{\text{total}} = 200$ W; $D_1 = 0.01$ N

Run 2: $U_{\infty} = 24.02 \text{ m/s}$; $q_{\text{total}} = 600 \text{ W}$

Assumptions: Steady-state flow;

Ec<<1 (negligible viscous dissipation);

 $Nu = C \operatorname{Re}^m \operatorname{Pr}^n$; Chilton-Colburn Analogy applies

c)

$$\rho = 1 \text{ kg/m}^3$$
; $c_p = 1000 \text{ J/kg-°C}$;

$$k = 0.025 \text{ W/m-}^{\circ}\text{C}$$
; and In Run 1:

Friction Drag Total = 0.01 N

$$\overline{c}_{f} = \frac{\overline{\tau}_{w}}{\frac{1}{2}\rho U_{\infty}^{2}} = \frac{Drag/A_{s}}{\frac{1}{2}\rho U_{\infty}^{2}} = \frac{0.01/0.02}{\frac{1}{2}\times 1\times 25} = 0.04$$

The Chilton-Colburn Analogy gives: $\frac{\overline{c}_f}{2} = \overline{S}t \operatorname{Pr}^{2/3}$;

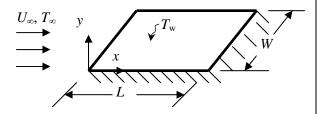
$$\overline{S}t = \frac{h}{\rho U_{c}c_{p}} = \frac{200}{1 \times 5 \times 1000} = 0.04$$

$$\Rightarrow Pr^{2/3} = \frac{0.5 \times 0.04}{0.04} = 0.5 \Rightarrow Pr = 0.3536$$

$$Pr = \frac{\mu c_p}{k} = 0.3536$$

$$\Rightarrow \mu = 0.3536 \times 0.025 / 1000 = 8.84 \times 10^{-6} \text{kg/m-s}$$

Problem 2:



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$$q_{total} = hA(T_w - T_\infty);$$
 Drag= $\overline{\tau}_w A;$ and $A = 1 \text{ m}^2$

$$h_1 = 168/(1 \times 40) = 4.2 \text{ W/m}^2 - \text{°C}; \quad \overline{\tau}_{w1} = 8.4 \times 10^{-3} \text{ N/m}^2$$

$$h_2 = 1170.8/(1 \times 40) = 29.27 \text{ W/m}^2 - ^{\circ}\text{C}; \quad \overline{\tau}_{w,2} = 0.5854 \text{ N/m}^2$$

The Chilton-Colburn Analogy gives: $\frac{\overline{c}_f}{2} = \overline{S}t \operatorname{Pr}^{2/3}; \quad \overline{S}t = \frac{\overline{h}}{\rho U_{\infty} c_n}$

Run 1:
$$\frac{1}{2} \left[\frac{\overline{\tau}_{w,1}}{0.5 \rho U_{\infty,1}^{2}} \right] = \frac{\overline{h}_{1}}{\rho U_{\infty,1} c_{p}} Pr^{2/3}$$
Run 2:
$$\frac{1}{2} \left[\frac{\overline{\tau}_{w,2}}{0.5 \rho U_{\infty,2}^{2}} \right] = \frac{\overline{h}_{2}}{\rho U_{\infty,2} c_{p}} Pr^{2/3}$$

$$\Rightarrow \frac{U_{\infty,2}}{U_{\infty,1}} = \frac{\overline{h}_{1}}{\overline{h}_{2}} \frac{\overline{\tau}_{w,2}}{\overline{\tau}_{w,1}} \Rightarrow U_{\infty,2} = 2 \times \frac{4.2}{29.27} \times \frac{0.5854}{8.4 \times 10^{-3}} = 20 \text{ m/s}$$

b)

Assume in Run 1, Re $< 5 \times 10^5$

using the exact solution (Blasius similarity sol.):

$$c_{f,x} = \frac{\tau_{w,x}}{\frac{1}{2}\rho U_{\infty}^2} = 0.664(Re_x)^{-1/2}$$
 and

$$c_{f,av} = \frac{1}{L} \int_{0}^{L} c_{f,x} dx = 1.328 (Re_L)^{-1/2}$$

$$c_{f,av\atop 0 \le x \le L} = \frac{\tau_{w,av}}{\frac{1}{2}\rho U_{\infty}^{2}}; \text{ and } Re_{L} = \frac{\rho U_{\infty} L}{\mu}$$

$$\Rightarrow c_{f,av} = \frac{\tau_{w,av}}{\frac{0 \le x \le L}{0 \le x \le L}} = 1.328 \left(\frac{\rho U_{\infty} L}{\mu}\right)^{-1/2}$$

Using data from Run 1:

$$\mu = \left[\frac{\tau_{w,av}}{\frac{1.328}{2}\rho U_{\infty}^{2}}\right]^{2} \rho U_{\infty} L = \left[\frac{8.4 \times 10^{-3}}{\frac{1.328}{2} \times 1 \times 2^{2}}\right]^{2} 1 \times 2 \times 1$$

$$\mu = 2 \times 10^{-5} \text{ kg/m-s}$$

Given: L = 1 m, W = 1 m. $T_w = 50^{\circ}\text{C}$

Experimental data show the followings:

Run 1: Laminar flow throughout:

$$U_{\infty, 1} = 2 \text{ m/s}; T_{\infty, 1} = 10^{\circ}\text{C}; \text{Drag}_1 = 8.4 \times 10^{-3} \text{ N};$$

and
$$q_{\text{total, 1}} = 168 \text{ W}$$

Run 2:
$$U_{\infty, 2} = ?$$
 m/s; $T_{\infty, 2} = 10$ °C; Drag₁ = 0.5854 N;

and
$$q_{\text{total, 2}} = 1170.8 \text{ W}$$

$$\rho = 1 \text{ kg/m}^3$$
; $c_p = 1000 \text{ J/kg-°C}$

Assumptions: Steady-state flow; Ec<<1 (negligible viscous dissipation); Chilton-Colburn Analogy applies

Check the Re₁ (Run 1)

$$Re_{L} = \frac{\rho U_{\infty} L}{\mu} = \frac{1 \times 2 \times 1}{2 \times 10^{-5}} = 10^{5} < 5 \times 10^{5}$$

$$Nu_{av,L} \triangleq \frac{(h_{av})L}{k_{guid}} = 0.664(Re_L)^{1/2} Pr^{1/3}$$

$$Pr = \frac{\mu c_p}{1c}$$
;

$$\Rightarrow \frac{h_{av} L}{k_{fluid}} = 0.664 (Re_L)^{1/2} \left(\frac{\mu c_p}{k}\right)^{1/3}$$

$$\Rightarrow k^{-2/3} = \frac{0.664(Re_L)^{1/2}}{h_{av}} \left(\mu c_p\right)^{1/3}$$

$$k = \frac{0.664 \times (10^5)^{1/2}}{4.2 \times 1} (2 \times 10^{-5} \times 1000)^{1/3}$$

$$k = 0.02 \text{ W/m}\text{-}^{\circ}\text{C}$$

c) Run 2

$$\begin{aligned} q_{0.1m \leq x \leq 1m} &= q_{0 \leq x \leq 1m} - q_{0 \leq x \leq 0.1m} \\ &\text{in Run 2, } q_{0 \leq x \leq 1m} = 1170.8 \text{ W} \\ &\text{at } x = 0.1m, \text{Re}_{x=0.1} = \frac{\rho U_{\infty,2} 0.1}{\mu} = \frac{1 \times 20 \times 0.1}{2 \times 10^{-5}} \\ &\text{Re}_{x=0.1} = 10^{5} < 5 \times 10^{5}; \text{Pr} = \frac{\mu c_{p}}{k} = 1 \\ Ν_{av} &\triangleq \frac{(h_{av}) 0.1}{b_{sluid}} = 0.664 (Re_{0.1})^{1/2} Pr^{1/3} \end{aligned}$$

$h_{av} = \frac{0.02}{0.1} = \frac{0.02}{0.1} = \frac{0.0664 \times (10^5)^{1/2} \times 1^{1/3}}{0.1} = 41.995 \text{ W/m}^2 - \text{°C}$ $q_{0 \leq x \leq 0.1m} = h_{av \atop 0 \leq x \leq 0.1} \left(A_{0 \leq x \leq 0.1} \right) \left(T_w - T_\infty \right)$ $q_{0 \le x \le 0.1m} = 41.995 \times (0.1 \times 1)(40) = 167.98 \text{ W}$ $q_{0.1m \le x \le 1m} = 1170.8 - 167.98$ $\Rightarrow q_{0.1m \le x \le 1m} = 1002.82 \text{ W}$

Problem 3:



Governing diff. eq.:

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$$\rho_{solid}c_{p,solid}V\frac{dT}{dt} = -hA(T - T_{\infty});$$

$$t = 0s, \quad T_{t=0} = T_{i} = 420^{\circ}\text{C}$$

$$dT / dt = -5.4^{\circ}\text{C/s}$$

$$t = 60s, \quad T_{t=60s} = 188.9^{\circ}\text{C}$$

$$dT / dt = -2.6^{\circ}\text{C/s}$$

$$thus, h_{t=0} = \frac{-\rho_{solid}c_{p,solid}V}{A(T_{t=0} - T_{\infty})} \left(\frac{dT}{dt}\right)_{t=0}$$

$$h_{t=0} = \frac{-2000 \times 500 \times 8 \times 10^{-6}}{2 \times 10^{-3} (420 - 20)} \times -5.4$$

$$h_{t=0} = 54 \text{ W/m}^{2} - ^{\circ}\text{C}$$

$$h_{t=60} = \frac{-\rho_{solid}c_{p,solid}V}{A(T_{t=60} - T_{\infty})} \left(\frac{dT}{dt}\right)_{t=60}$$

$$h_{t=60} = \frac{-2000 \times 500 \times 8 \times 10^{-6}}{2 \times 10^{-3} (188.9 - 20)} \times -2.6$$

$$h_{t=60} = 61.575 \text{ W/m}^{2} - ^{\circ}\text{C}$$

Given: $U_{\infty} = (10+0.05 \text{ t}) \text{ m/s}; \text{ Vol.}_{\text{solid}} = 8 \times 10^{-6} \text{ m}^3;$ $A_{\text{solid}} = 2 \times 10^{-3} \text{ m}^2$; $T_i = 420^{\circ}\text{C}$; $T_{\infty} = 20^{\circ}\text{C}$. Fluid properties: $\rho = 1 \text{ kg/m}^3$; $c_p = 1000 \text{ J/kg-°C}$; $\mu = 2 \times 10^{-5} \text{ kg/m-s}; k = 0.02 \text{ W/m-}^{\circ}\text{C}$ Solid properties: $\rho = 2000 \text{ kg/m}^3$; $c_p = 500 \text{ J/kg-°C}$; $k = 400 \text{ W/m-}^{\circ}\text{C}$

Measurements:

- inside the solid: T = T(t); (i)
- (ii) at t = 0 s, $T = T_i = 420$ °C and dT/dt = -5.4°C/s;
- at t = 60 s, $T = 188.9 \text{ }^{\circ}\text{C}$ (iii) and dT/dt = -2.6 °C/s.

Assumptions: Transient fluid flow and heat transfer; LPA is valid; $Nu = C \operatorname{Re}^m \operatorname{Pr}^n$; All given properties remain constant

$$Nu = C \operatorname{Re}^{m} \operatorname{Pr}^{n}$$

$$\frac{hL_{c}}{k_{fluid}} = C \left(\frac{\rho_{fluid}U_{\infty}L_{c}}{\mu_{fluid}}\right)^{m} \left(\frac{\mu_{fluid}c_{p,fluid}}{k_{fluid}}\right)^{n}$$

$$\Rightarrow h = \psi \left(U_{\infty}\right)^{m} \text{ where } \psi \text{ is a constant}$$
as was given $U_{\infty} = (10 + 0.05 \ t)$; thus,
$$t = 0s, \quad U_{\infty,0} = 10 \text{ m/s}; h_{t=0} = 54 \text{ W/m}^{2} \text{-°C}$$

$$t = 60s, \quad U_{\infty,60} = 13 \text{ m/s}; h_{t=60} = 61.575 \text{ W/m}^{2} \text{-°C}$$

$$thus, \quad 54 = \psi \left(10\right)^{m}$$

$$61.575 = \psi \left(13\right)^{m}$$

$$\Rightarrow m = 0.5$$

$$\psi = 17.08 \left(U_{\infty}\right)^{0.5}$$

b) Governing diff. eq.:
$$\ln\left(\frac{(T-T_{\infty})}{(T_{i}-T_{\infty})}\right) = -4.27 \times 10^{-3} \frac{1}{0.05} \left[\frac{2}{3} (10+0.05 \ t)^{3/2}\right]_{0}^{t}$$

$$\rho_{solid} c_{p_{solid}} V \frac{dT}{dt} = -hA(T-T_{\infty}); \qquad \ln\left(\frac{T_{t=100s}-20}{420-20}\right) = -56.933 \times 10^{-3} \times \left[(10+0.05 \ t)^{3/2}\right]_{0}^{100s}$$

$$h = 17.08 (U_{\infty})^{0.5}; \text{ and } U_{\infty} = (10+0.05 \ t) \text{ thus,} \qquad \ln\left(\frac{T_{t=100s}-20}{400}\right) = -56.933 \times 10^{-3} \times \left[(15)^{3/2}-(10)^{3/2}\right] = -1.507$$

$$h = 17.08 (10+0.05 \ t)^{0.5} \text{ or } \qquad T_{t=100s} = 20+400 \exp(-1.507) = 20+88.63$$

$$\frac{dT}{(T-T_{\infty})} = -\frac{17.08 \times A}{\rho_{solid} c_{p_{solid}} V} (10+0.05 \ t)^{0.5} dt$$

$$T_{t=100s} = 108.63^{\circ}\text{C}$$

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