

MECH366: Modeling of Mechatronic Systems

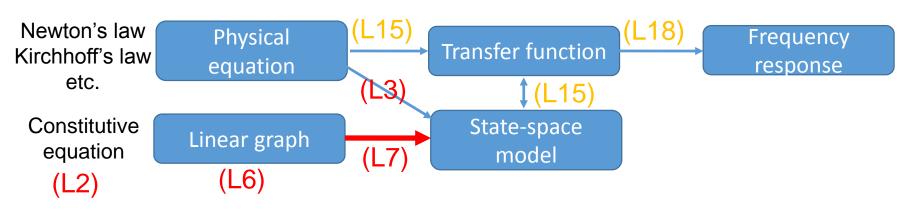
L7: Derivation of state-space models from linear graphs

Dr. Ryozo Nagamune
Department of Mechanical Engineering
University of British Columbia

Review and today's topic



- In the last class, we studied how to represent mechanical elements in linear graphs:
 - Single-port elements, including energy source elements
 - Two-port elements (transformer & gyrator)
- Today, we will study how to derive state-space models from linear graphs.



__ : State variable

Constitutive relation for

| | Energy storage element | | Energy dissipating element |
|------------------------|------------------------------------|----------------------------|----------------------------|
| System type | A-Type | T-Type | D-Type |
| Mechanical | Mass | Spring | Viscous Damper |
| (translational) | | | |
| v: velocity acros | ss var. $m\underline{\dot{v}} = f$ | $\underline{\dot{f}} = kv$ | f = bv |
| f: force through | var. m : mass | k: stiffness | b: damping const. |
| Electrical | Capacitor | Inductor | Resistor |
| v: voltage | $C\dot{v}=i$ | $L\dot{i}=v$ | v = Ri |
| i: current | C: capacitance | L: inductance | R: resistance |
| Thermal | Thermal capacitor | None | Thermal resistor |
| T: temperature | $C_t \dot{T} = Q$ | | $T = R_t Q$ |
| Q: heat transfer rate | C: thermal capacitance | | R_t : thermal resistance |
| Fluid | Fluid capacitor | Fluid inertor | Fluid resistor |
| P: pressure difference | $C_f \dot{P} = Q$ | $I_f \dot{Q} = P$ | $P = R_f Q$ |
| Q: volume flow rate | C_f : fluid capacitance | I_f : fluid inertance | R_f : fluid resistance |



power

$$\mathcal{P} = fv$$

How to derive state-space models from linear graphs

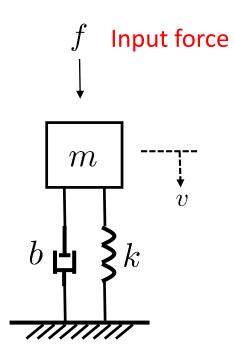


- Key steps
 - Draw a linear graph.
 - 2. Define state variables.
 - 3. Write a constitutive equation for each element.
 - 4. Write loop equations and node equations.
 - Loop equations are similar to Kirchhoff voltage law.
 - Node equations are similar to Kirchhoff current law.
 - Eliminate redundant variables.

Example 1 System description

a place of mind

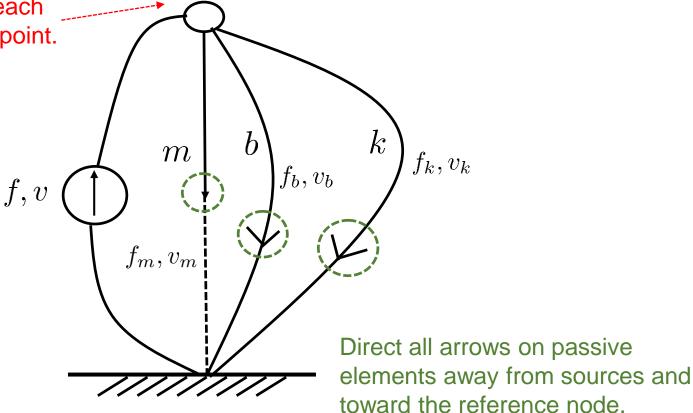
• 1-DOF mass-spring-damper



Example 1 Linear graph drawing



Take a node for each different velocity point.



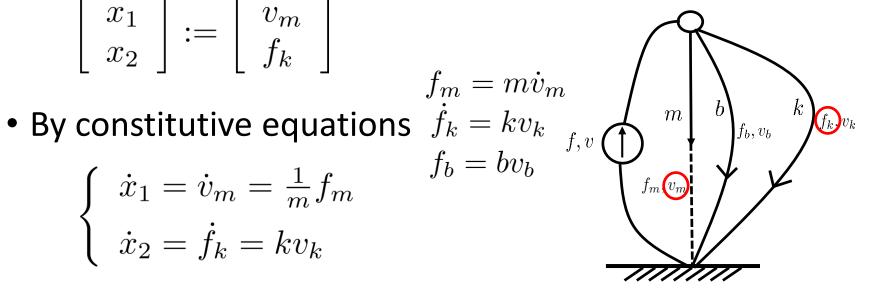
Example 1 State-variable selection



- Select the following as state variables:
 - Across variable (v) for A-type element (m)
 - Through variable (f) for T-type element (k)

$$\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right] := \left[\begin{array}{c} v_m \\ f_k \end{array}\right]$$

$$\begin{cases} \dot{x}_1 = \dot{v}_m = \frac{1}{m} f_m \\ \dot{x}_2 = \dot{f}_k = k v_k \end{cases}$$



Example 1 Loop and node equations



States

$$\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right] := \left[\begin{array}{c} v_m \\ f_k \end{array}\right]$$

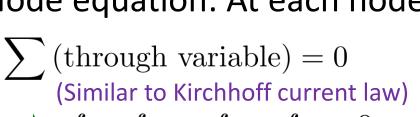
• Loop equation: In each loop,

$$\sum (across variable) = 0$$
(Similar to Kirchhoff voltage law)

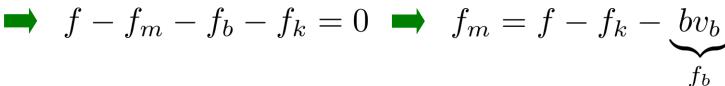
$$\begin{array}{c} \bullet \quad \begin{cases} v - v_m = 0 \\ v_m - v_b = 0 \\ v_b - v_k = 0 \end{cases}$$

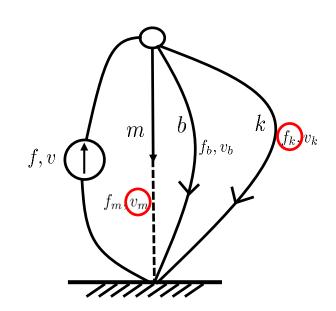
$$\rightarrow v_m = v_b = v_k = v$$

Node equation: At each node,









Example 1 State-space model



States

$$\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right] := \left[\begin{array}{c} v_m \\ f_k \end{array}\right]$$

State equation

$$\begin{cases} \dot{x}_1 = \frac{1}{m} f_m = \frac{1}{m} (f - f_k - bv_b) = \frac{1}{m} (u - x_2 - bx_1) \\ \dot{x}_2 = kv_k = kv_m = kx_1 \end{cases}$$

Output equation

• If
$$y = v_m$$
 then $y = \begin{bmatrix} 1 & 0 \end{bmatrix} x$

• If
$$y=z_m$$
 then $y=\begin{bmatrix}0&1/k\end{bmatrix}x$ $(f_k=kz_k=kz_m)$

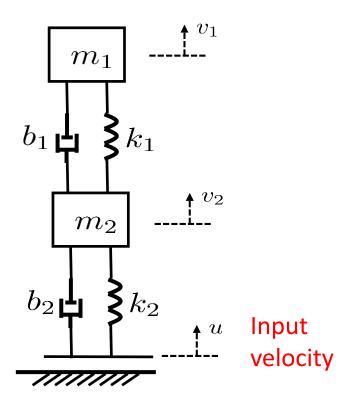
(zm: displacement)

(See Lecture 3, Slide 10.)

Example 2 System description

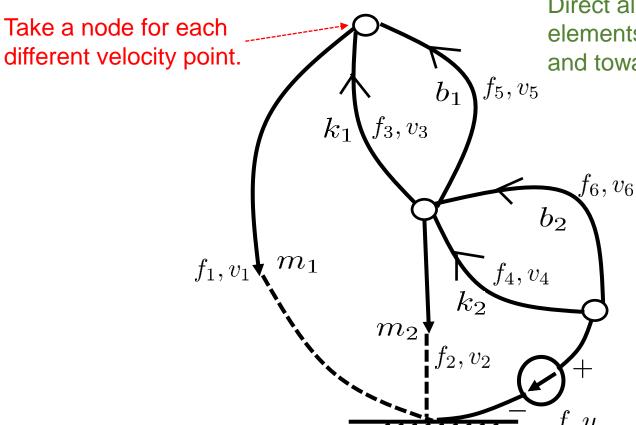
a place of mind

2-DOF mass-spring-damper



Example 2 Linear graph drawing





Direct all arrows on passive elements away from sources and toward the reference node.

Example 2 State-variable selection

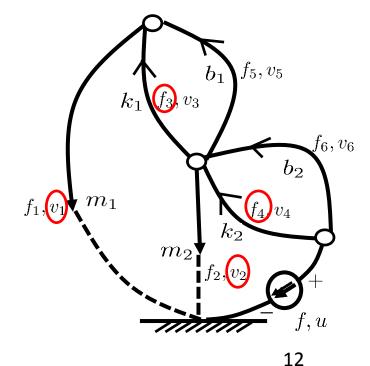


- Select the following as state variables:
 - Across variable (v) for A-type element (m)
 - Through variable (f) for T-type element (k)

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} := \begin{bmatrix} v_1 \\ v_2 \\ f_3 \\ f_4 \end{bmatrix}$$

Constitutive equations

$$\dot{v}_1 = \frac{1}{m_1} f_1, \quad \dot{v}_2 = \frac{1}{m_2} f_2$$
 $\dot{f}_3 = k_1 v_3, \quad \dot{f}_4 = k_2 v_4$
 $f_5 = b_1 v_5, \quad f_6 = b_2 v_6$



MECH 366

Example 2 Loop and node equations



$$\begin{cases} v_1 - v_2 + v_3 = 0 \\ v_2 - u + v_4 = 0 \\ -v_4 + v_6 = 0 \\ -v_3 + v_5 = 0 \end{cases}$$

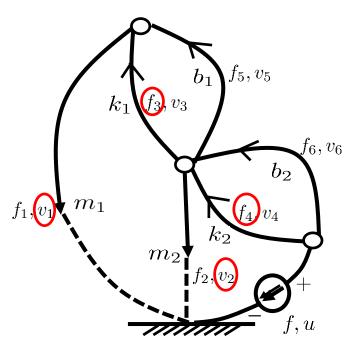
Node equations

$$\begin{cases}
-f_1 + f_3 + f_5 = 0 \\
-f_3 - f_5 - f_2 + f_4 + f_6 = 0 \\
-f_4 - f_6 + f = 0
\end{cases}$$



States

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} := \begin{bmatrix} v_1 \\ v_2 \\ f_3 \\ f_4 \end{bmatrix}$$



13

Example 2 State equation

States

$$\left[\begin{array}{c} x_1 \\ x_2 \\ x_3 \\ x_4 \end{array}\right] := \left[\begin{array}{c} v_1 \\ v_2 \\ f_3 \\ f_4 \end{array}\right]$$



$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} -b_1/m_1 & b_1/m_1 & 1/m_1 & 0 \\ b_1/m_2 & -(b_1+b_2)/m_2 & -1/m_2 & 1/m_2 \\ -k_1 & k_1 & 0 & 0 \\ 0 & -k_2 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 \\ b_2/m_2 \\ 0 \\ k_2 \end{bmatrix} u$$

$$\dot{v}_1 = \frac{1}{m_1} f_1 = \frac{1}{m_1} (f_3 + f_5) = \frac{1}{m_1} (f_3 + b_1 v_5) = \frac{1}{m_1} (f_3 + b_1 v_3) = \frac{1}{m_1} (f_3 + b_1 (-v_1 + v_2))$$

$$\dot{v}_2 = \frac{1}{m_2} f_2 = \frac{1}{m_2} (f_4 + f_6 - f_3 - f_5) = \frac{1}{m_2} (f_4 + b_2 v_6 - f_3 - b_1 v_5)$$

$$= \frac{1}{m_2} (f_4 + b_2 v_4 - f_3 - b_1 v_3) = \frac{1}{m_2} (f_4 + b_2 (u - v_2) - f_3 - b_1 (v_2 - v_1))$$

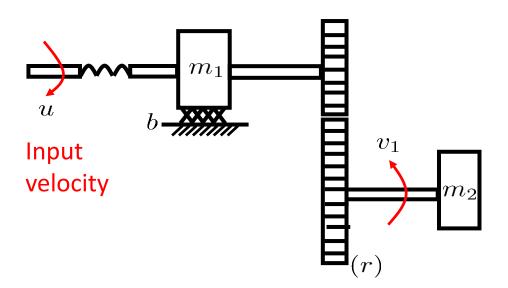
$$\dot{f}_3 = k_1 v_3 = k_1 (v_2 - v_1)$$

$$\dot{f}_4 = k_2 v_4 = k_2 (u - v_2)$$

Example 3 System description

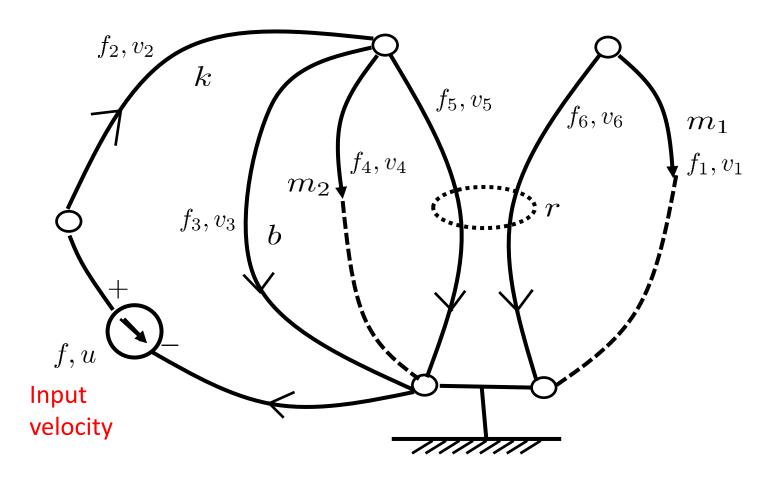


Rotary motion control with a gearbox



Example 3 Linear graph drawing





Example 3 State-variable selection

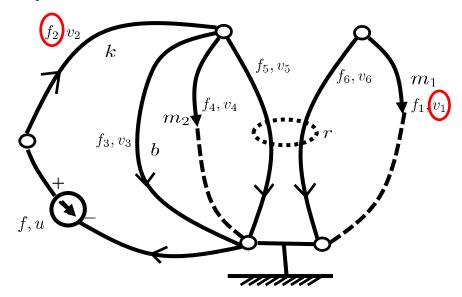


- Select the following as state variables:
 - Across variable (v) for A-type element (Inertia m)
 - Through variable (f) for T-type element (Rot. Spring k)
- Two masses are not independent.

$$\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right] := \left[\begin{array}{c} v_1 \\ f_2 \end{array}\right]$$

$$\dot{x}_1 = \dot{v}_1 = \frac{1}{m_1} f_1$$

$$\dot{x}_2 = \dot{f}_2 = k v_2$$



Example 3 Constitutive equations



Remaining constitutive equations

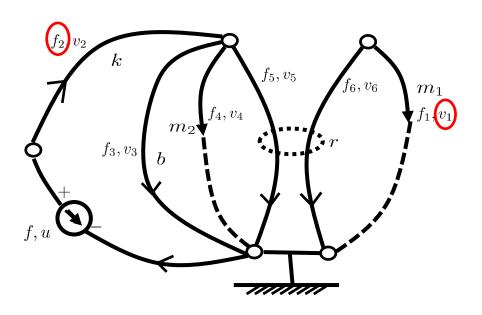
• Damper: $f_3 = bv_3$

• Mass 2:
$$\dot{v}_4 = \frac{1}{m_2} f_4$$

Transformer

$$v_6 = rv_5$$

$$f_6 = -\frac{1}{r}f_5$$



Example 3 Loop and node equations



States

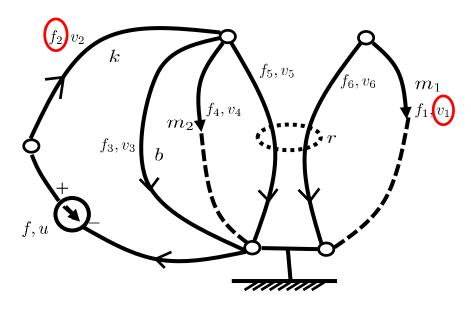
$$\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right] := \left[\begin{array}{c} v_1 \\ f_2 \end{array}\right]$$

Loop equations

$$\begin{cases} v_6 - v_1 = 0 \\ v_4 - v_5 = 0 \\ v_3 - v_4 = 0 \\ -v_2 + u - v_3 = 0 \end{cases}$$

Node equations

$$\begin{cases}
-f_1 - f_6 = 0 \\
f_2 - f_3 - f_4 - f_5 = 0 \\
f - f_2 = 0
\end{cases}$$



Example 3 State equation

States

$$\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right] := \left[\begin{array}{c} v_1 \\ f_2 \end{array}\right]$$



$$\dot{v}_1 = \frac{1}{m_1} f_1 = \frac{1}{m_1} (-f_6) = \frac{1}{m_1} \left(\frac{1}{r} f_5 \right)
= \frac{1}{m_1 r} (f_2 - f_3 - f_4) = \frac{1}{m_1 r} (f_2 - bv_3 - m_2 \dot{v}_4)
= \frac{1}{m_1 r} \left(f_2 - b \frac{1}{r} v_6 - m_2 \frac{1}{r} \dot{v}_1 \right) = \frac{1}{m_1 r} \left(f_2 - b \frac{1}{r} v_1 - m_2 \frac{1}{r} \dot{v}_1 \right)$$

Summary



- Derivation of state-space models from linear graphs
- Three examples
 - 1-DOF mass spring damper
 - 2-DOF mass spring damper
 - Rotary motion control with a gearbox
- Next, two more examples
- Homework 2: Due Sep 30 (Monday), 3pm