

# HT Heat Pump WP5 report

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# 1 Introduction

## 1.1 Goal

The goals of WP5 are verifying whether the compressor can be used to build a functioning HT heat pump. These following steps are taken:

- Simulating the work of Heat Pump under reference cases.
- reserve...
- 
- 
- 
- 

# 2 Generalized setup of calculation model

## 2.1 Simulation methods

Building energy simulation is a vast field of research that started on the late 50's and that is still highly active nowadays. Building energy simulations are mainly used to help taking design decisions, to analyze current designs and to forecast future building energy use. Building energy modelling methods can mainly be divided into three categories:

- White box model (physics-base)
- Black box model (data-driven)
- Grey box (hybrid)

White box model is based on the equations related to the fundamental laws of energy and mass balance and heat transfer. White box models can be differentiated in two types, distributed parameter models and lumped parameter models. Lumped parameter models simplify the description of distributed physical systems into discrete entities that approximate the behavior of a distributed system. The advantage of using lumped models is the decrease on simulation time (Ramallo-González et al.). White box model is of special interest for the design phase as they are used to predict and analyses the performance of the building envelope and building systems.

Black box models are based on the statistical relation between input and output system values. The statistical relation between input and output is

based on actual data. The relation between the parameters can differ based on the amount of data and the method used to analyze the relation. Currently, there is a large and active field of research about statistical models that are used on black box models (Coacley et al.). Black box models are of special interest when there is a large amount of actual input and output data available.

Grey box model is a hybrid model form that aim to combine the advantages of both systems. In order to use them it is necessary to implement some equations and it is also required to have actual data of inputs and outputs.

## 2.2 White box lumped model: RC network

The apartment and office building load profile model for this project is to serve as test environment for a heat pump model, what means that the models is intended as a tool to help taking building systems design decisions. The heating needs calculation model implemented for this project is a white box lumped model. Specifically, it is a RC network model consisting of resistances (R) and capacities (C). The RC network model is based on electrical systems analogy. The simulation of thermodynamic systems characterizing building elements as resistances or capacities allows to simplify the model while maintaining a high simulation results accuracy (Bagheri et al., Bacher et al.).

There are several types of RC models, the most common being 3R4C models and 3R2C models which are applied on the outer and internal wall. For the simulation of simple buildings 3R2C models perform as accurate as more complex 3R4C models (Fraisie et al. ). Considering that one of the objectives for this project is to obtain a fast but accurate simulation of a simple 3R2C network model appeared as starting point. In the 3R2C model two indoor temperature nodes in the dwelling with capacities (usually an air and a wall temperature) and a well-known outdoor temperature are present. Between these 3 temperature nodes 3 heat transfer resistances are present. However, the direct heat transfer between the inner walls and the outdoor air is low. Moreover, uncertainties are present about heat transfer coefficients between walls and indoor air, different indoor temperatures in the house rooms and the ground temperature which deviates from the outdoor temperature. In addition, occupancy behaviour varies strongly. For that reason, we have made a further simplification to a 2R2C model.

Assume that the apartment/office building is a single zone, furniture and the surface part of the walls have the same temperature as the air and the wall mass is divided between the air and wall mass. Thus, the capacity of the air node consists of the air capacity, furniture capacity and capacity of a part of the walls. In the resistance  $R_{air,outdoor}$  the influence of heat transmission through

the outdoor walls and natural ventilation is considered.

### 2.2.1 Office building

The heating system layout for office building is shown in figure []:

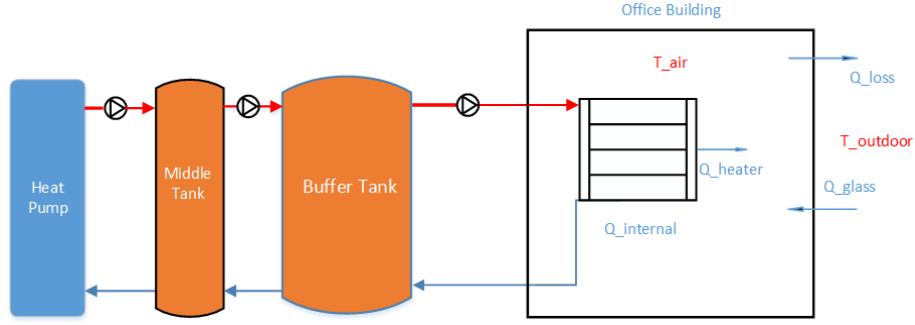


Figure 1: Heating system layout for office building

The room temperature can be calculated as:

$$C_{air} \frac{dT_{air}}{dt} = \frac{T_{outdoor} - T_{air}}{R_{air\_outdoor}} + \frac{T_{wall} - T_{air}}{R_{air\_wall}} + Q_{inst} + Q_{internal} + CF \cdot Q_{solar} \quad (1)$$

$$C_{wall} \frac{dT_{wall}}{dt} = \frac{T_{air} - T_{wall}}{R_{air\_wall}} + (1 - CF) \cdot Q_{solar} \quad (2)$$

- CF: convectional factor.
- $Q_{inst}$ : delivered heat from heating system (radiator) [W].
- $Q_{solar}$ : heat from solar irradiation [W].
- $T_{air}$ : indoor air temperature °C.
- $T_{outdoor}$ : outdoor temperature °C.
- $T_{wall}$ : wall temperature °C.
- $R_{air\_wall}$ : walls surface resistance.
- $R_{air\_outdoor}$ : outdoor surface resistance.
- $C_{air}$ : air capacity.
- $C_{wall}$ : wall capacity.

Total heat transfer of solar irradiation through the glass windows.

$$Q_{solar} = g \cdot \sum (A_{glass} \cdot q_{solar}) \quad (3)$$

- $q_{solar}$ : solar radiation on the outdoor walls [ $W/m^2$ ].
- $g$ : g value of the glass (=ZTA in dutch) [0..1]
- $A$ : glass surface [ $m^2$ ].

### 2.2.2 Apartment Building

The system layout for an Apartment building is shown in figure [...]. The configuration for space heating is similar with the office. The D.H.W is configured in parallel with space heating.

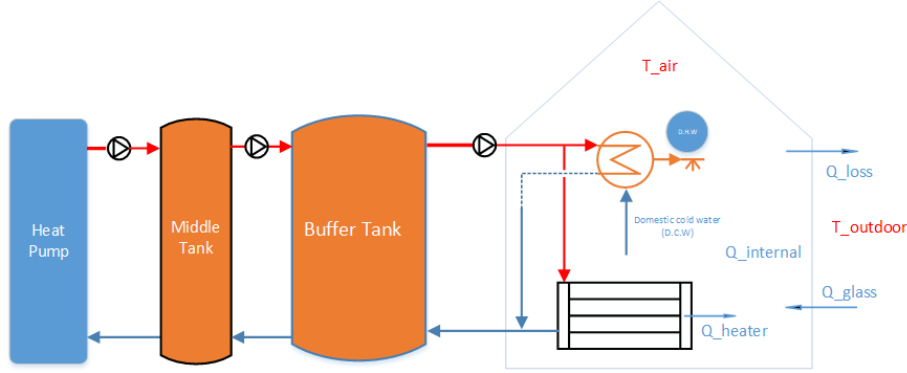


Figure 2: Heating system layout for Apartment building.

The energy balance equation for space heating of an apartment is similar with office building (equation [1],[2]) where a single zone will be considered.

$$C_{air} \frac{dT_{air}}{dt} = \frac{T_{outdoor} - T_{air}}{R_{air\_outdoor}} + \frac{T_{wall} - T_{air}}{R_{air\_wall}} + Q_{inst} + Q_{internal} + CF \cdot Q_{solar}$$

$$C_{wall} \frac{dT_{wall}}{dt} = \frac{T_{air} - T_{wall}}{R_{air\_wall}} + (1 - CF) \cdot Q_{solar}$$

The D.H.W consumption is base on D.H.W user profile and will be discussed in the next chapter.

The hot tap water temperature is calculated follow:

$$c\rho V_{HE} \frac{dT_{tap}}{dt} = \alpha_{HE} 2\pi r_{HE} \Delta x [T_{HE}(x + \Delta x, t) - T_{tap}] - Q_{D.H.W\_profile} \quad (4)$$

$$c\rho\pi r_{HE}^2\Delta x \frac{dT_{HE}(x+\Delta x)}{dt} = c\rho\dot{m}[T_{HE}(x,t) - T_{HE}(x+\Delta x,t)] - \alpha_{HE}2\pi r_{HE}\Delta x[T_{HE}(x+\Delta x,t) - T_{tap}] \quad (5)$$

Where  $T_{HE\_in} = T_{hot}$ ,  $T_{HE\_out}$  is the return water temperature from heat exchanger.

$T_{tap}$  is the hot tap water temperature  $^{\circ}C$ ,  $T_{HE}$  is the heat ex-changer temperature  $^{\circ}C$ , and  $Q_{D.H.W\_profile}$  is the hot tap water profile.

### 2.3 Radiators equation

Heat transfer from the radiators and the radiators outlet temperature is described as:

$$\frac{Q_{rad}}{dt} = Q_{in} - Q_{inst} - Q_{loss} \quad (6)$$

With  $Q_{inst}$  is the heat emission from a radiator. Its depends primarily on the temperature difference between the hot surface and the surrounding air (figure). The heat emission can be calculated [11]:

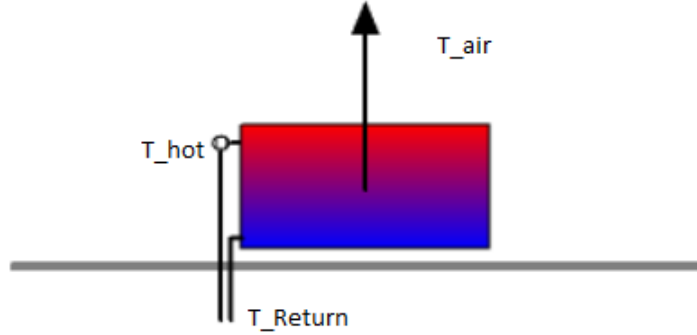


Figure 3: Heat emission from radiator [11].

$$C_{rad} \frac{dT_{rad}}{dt} = \dot{m}c\Delta T - Q_{50} \left( \frac{LMTD}{49.32} \right)^n \quad (7)$$

$$C_{rad} \frac{dT_{return}}{dt} = \dot{m}c(T_{hot} - T_{return}) - Q_{50} \left( \frac{T_{hot} - T_{return}}{\ln(T_{hot} - T_{air}) - \ln(T_{return} - T_{air})} \frac{1}{49.32} \right)^n \quad (8)$$

- LMTD: log mean Temperature Difference for the radiators.
- Crad: radiator constant.
- n: radiator exponent.
- $Q_{50}$ : heat emission from radiator with temperature difference  $50^{\circ}C$  [W]
- n: constant describing the type of radiator (1.33 for standard panel radiators, 1.3 - 1.6 for convectors).
- $T_{rad}$ : radiator temperature [ $^{\circ}C$ ].
- $T_{hot}$ : water temperature from buffer tank [ $^{\circ}C$ ].
- $T_{return}$ : water return temperature from radiator to the buffer tank [ $^{\circ}C$ ].
- $T_{air}$ : room temperature [ $^{\circ}C$ ].

Radiators are in general designed for middle panel temperature  $70^{\circ}C$  - and surrounding air temperature  $20^{\circ}C$  (difference  $50^{\circ}C$ )

## 2.4 Water buffer

In figure [ ] to minimize the effect of water variation which can lead to the significant reduce in heat pump performance. The middle tank with a smaller size is placed in between Heat Pump and the main buffer.

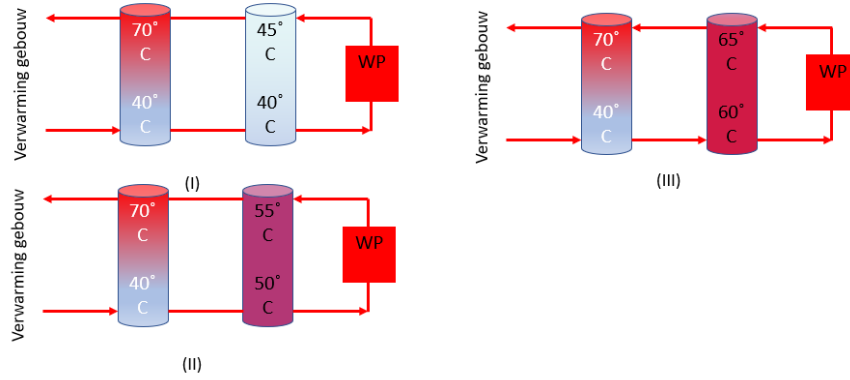


Figure 4: An illustration of heat flow.

The energy balance in the buffer tank can be determined:

$$c\rho V_{buffer} \frac{dT_{hot}}{dt} = c\rho \dot{m}(T_{mid\_tank} - T_{hot}) - c\rho \dot{m}(T_{hot} - T_{return}) \quad (9)$$

Where  $V_{buffer}$  is the volume of the tank in  $m^3$  and  $T_{mid\_tank}$  is the temperature of the middle tank  $^{\circ}C$ .

The energy balance in the middle tank:

$$c \cdot \rho V_{mid\_tank} \frac{dT_{mid\_tank}}{dt} = Q_{HP} - c \rho \dot{m} (T_{mid\_tank} - T_{hot}) \quad (10)$$

Where:

- $V_{mid\_tank}$  is the volume of the middle tank [ $m^3$ ]
- $T_{mid\_tank}$  water temperature inside the middle tank [ $^{\circ}C$ ].
- $Q_{HP}$  Heat output from Heat Pump [W]

## 2.5 Heat Pump model from WP2

## 3 Office building load profile

For nearly energy-neutral buildings (bijna energieneutrale kantoorgebouwen 'BENG') specific requirements for energy consumption will apply from 2021. The maximum energy requirement for heating, cooling and lighting for utility buildings, is  $50 \text{ kWh}/m^2$  per year. The number is increased to  $65 \text{ kWh}/m^2$  per year for healthcare buildings. This excludes the energy consumption for office equipment [1].

The average gas consumption for office building is around  $17 \text{ m}^3/m^2$  (figure 1) for the building with the construction year between 1977 and 1989. The report from ECN has calculated the buildings with an office function cover a total of 87 million  $m^2$ . This concerns 68,000 buildings in the Netherlands. Gas consumption amounts to 955 million  $m^3$  (30 PJ) and electricity to 7800 million kWh (28 PJ). These values are the most accurate available at the moment. [2],[3].

#	Branche en/of rubriek	Gebouwtype	Gas-intensiteit $m^3/m^2$	Elek-intensiteit $kWh/m^2$	Totaal $kWh/m^2$
01	kantoor	kantoor	17	60	223

Figure 5: Energy Consumption

The reference building has been selected:

- Construction year: 1977-1989.
- Surface  $m^2$ : 500
- Gas consumption:  $17 \text{ m}^3/m^2$



- T\_outside : out door temperature from NEN5060\_2018 with 1 hour sampling rate for 1 year long.

Add plot of load profile .... and validate

## 4 Apartment Building load profile

### 4.1 Heating profile

The apartment building (Flatwoningen (overig) Gebouwd) build in the period 1965-1974 which represent 1.8 % of the dutch housing stock [5] (highest number in the flatwoningen category) will be selected. Houses in this category often have 2 to 4 rooms. The average gas consumption for this type of apartment (energy label C) is  $829 \text{ m}^3/\text{year}$  with the average usage area is  $77 \text{ m}^2$  and 2.8 people in the house. Label C has been selected because the focus of heat pump heating will be on the renovated house with good insulation. The property features are showing in figure [ ... ].

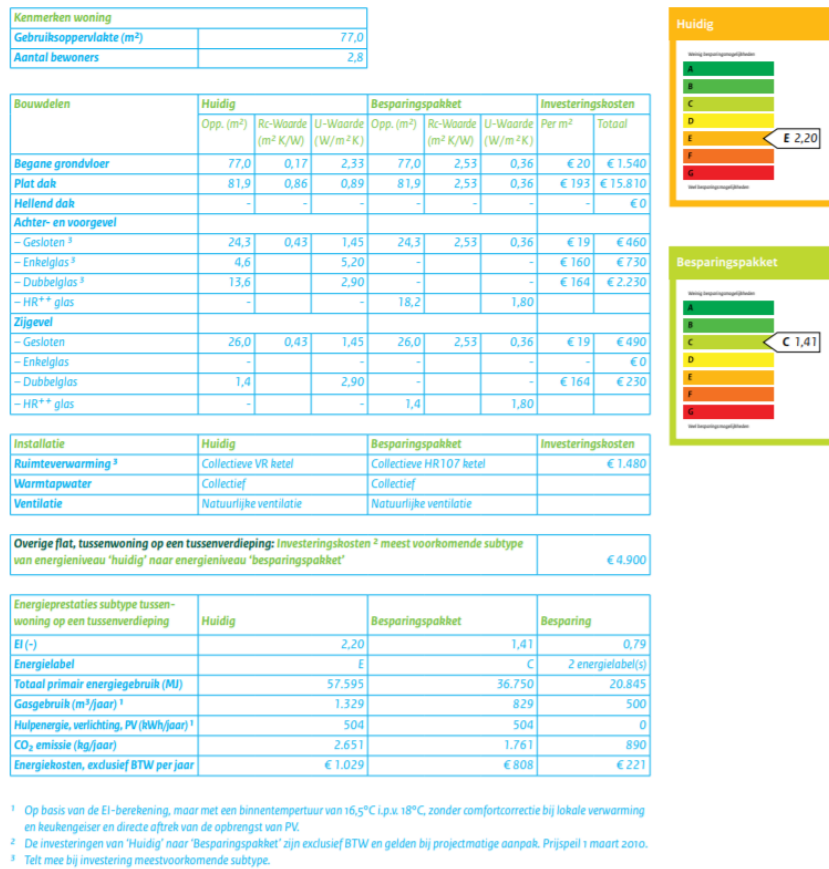


Figure 6: property features [5].

From statista.com (figure 4) one person use approximately 120 liters of water per day therein one third of the water is used for showering and bathing. The rest for washing, toilet and cooking.

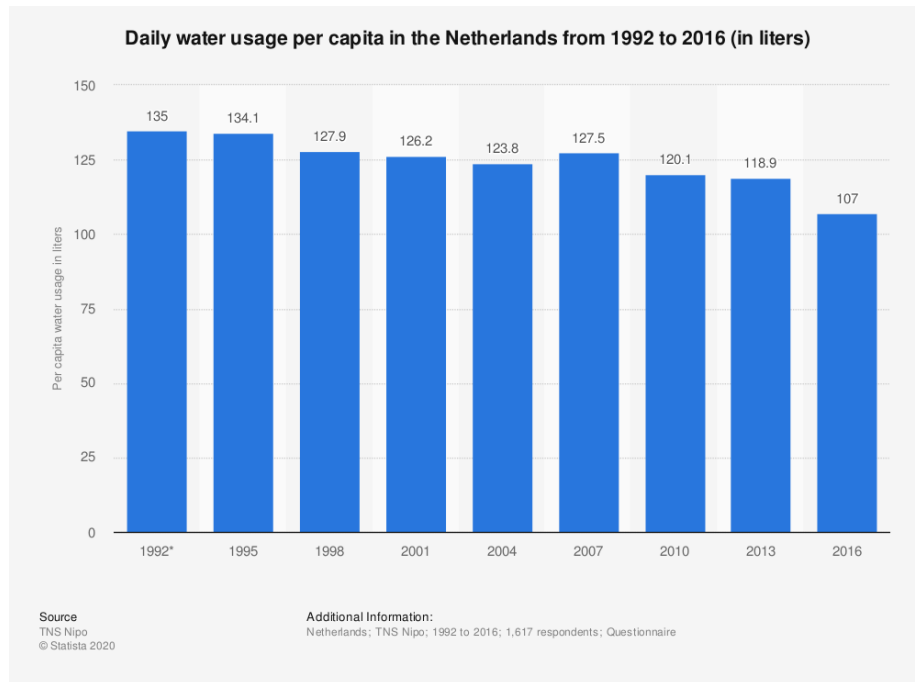


Figure 7: daily water usage by capital.

According to "VERORDENING (EU) Nr. 814/2013 VAN DE COMMISSIE van 2 augustus 2013". The hot water capacity M profile (will be discussed in next chapter) has a sum of energy use for tap water per day 5,845 kwh.

h	M				L				XL			
	$Q_{tap}$	$f$	$T_m$	$T_p$	$Q_{tap}$	$f$	$T_m$	$T_p$	$Q_{tap}$	$f$	$T_m$	$T_p$
	kWh	l/min	°C	°C	kWh	l/min	°C	°C	kWh	l/min	°C	°C
19:00	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
19:30												
20:00												
20:30	<b>0,735</b>	4	10	55	<b>0,735</b>	4	10	55	<b>0,735</b>	4	10	55
20:45												
20:46									<b>4,42</b>	10	10	40
21:00					<b>3,605</b>	10	10	40				
21:15	<b>0,105</b>	3	25						<b>0,105</b>	3	25	
21:30	<b>1,4</b>	6	40		<b>0,105</b>	3	25		<b>4,42</b>	10	10	40
21:35												
21:45												
$Q_{ref}$	<b>5,845</b>				<b>11,655</b>				<b>19,07</b>			

Figure 8: example hot tap water profile.

## 4.2 Hot tap water profile

A normal dutch house using CW label 3 or 4 (Appendix A). Therefore capacity profile M will be selected as a reference.

Capacity profile definition: Annex III of the EU regulation[3] describes a capacity profile for a 24-hour measurement cycle intended for checking compliance with the requirements.

This capacity profile is as follows:

- No hot water consumption from 9:35 PM to 7 AM.
- From 07:00 to 21:30 hot water consumption according to a precisely defined tap profile.

An example calculation is shown below:

h	<b>M</b>			
	$Q_{tap}$	$f$	$T_m$	$T_p$
	kWh	l/min	°C	°C
07:00	<b>0,105</b>	3	25	
07:05	<b>1,4</b>	6	40	

Figure 9: Tap water example [4].

At 7.00  $Q_{tap}$  is 0.105 kwh with the flow rate at 3 liters per minutes and temperature added is 25 degree.

$$m = \frac{3600.Q}{c.\Delta T}$$

m = 6 liters(kg), c=4.19 kj/kg.K. Therefore 2 minutes of tap water has been used at 7.00 AM

The hot tap water profile M for 1 day is showing in figure 10:

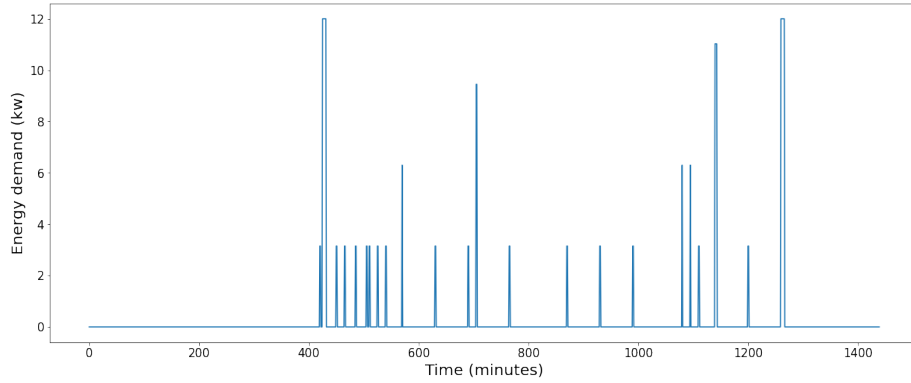


Figure 10: hot tap water profile M.

### 4.3 Simulation profile for the entire building

The simulation is base on the assumption of the apartment building with 24 residential apartments. The hot tap water demand for 24 apartments will be calculated base on the calculation rules public in kennisbank isso 55.

Type		$q_{v, tap; kw}$	$q_{v, tap; v}$	$V_{ww; 10}$	$V_{ww; 60}$	$V_{ww; 120}$	$V_{v, day}$
Single and double household	Studio	$0.227 + 0.109\sqrt{n} + 0.00366n$	$0.272 + 0.0373\sqrt{n} + 0.00359n$	$78.8 + 6.99\sqrt{n} + 1.59n$	$71.3 + 33.6\sqrt{n} + 6.2n$	$61.5 + 48.2\sqrt{n} + 10.7n$	$100 + 63.4\sqrt{n} + 47n$
	Luxury two-room apartment (100 m <sup>2</sup> )	$0.578 + 0.146\sqrt{n} + 0.01n$	$0.270 + 0.107\sqrt{n} + 0.00325n$	$127 + 39.7\sqrt{n} + 1.62n$	$243 + 67.9\sqrt{n} + 12.8n$	$203 + 88.3\sqrt{n} + 23.8n$	$104 + 168\sqrt{n} + 94.6n$
	Apartment for seniors (120 m <sup>2</sup> )	$0.331 + 0.064\sqrt{n} + 0.007n$	$0.225 + 0.052\sqrt{n} + 0.00259n$	$60.6 + 10.7\sqrt{n} + 1.10n$	$5.29 + 54.4\sqrt{n} + 3.88n$	$-0.389 + 68.9\sqrt{n} + 7.92n$	$43.3 + 69.9\sqrt{n} + 47.6n$
Multi-person household	Three-room apartment (120 m <sup>2</sup> )	$0.348 + 0.0902\sqrt{n} + 0.00803n$	$0.246 + 0.0523\sqrt{n} + 0.00341n$	$75.2 + 8.81\sqrt{n} + 2.46n$	$20.4 + 59.6\sqrt{n} + 7.70n$	$63.7 + 58.8\sqrt{n} + 15.2n$	$96.3 + 74.4\sqrt{n} + 80.1n$
	Three-room apartment luxury (160 m <sup>2</sup> )	$0.563 + 0.171\sqrt{n} + 0.013n$	$0.323 + 0.0924\sqrt{n} + 0.00637n$	$162 + 27.9\sqrt{n} + 3.58n$	$307 + 55.8\sqrt{n} + 18.4n$	$287 + 76.2\sqrt{n} + 31.9n$	$211 + 165\sqrt{n} + 145n$
	Luxury four-room apartment (250-300 m <sup>2</sup> )	$0.449 + 0.191\sqrt{n} + 0.0118n$	$0.359 + 0.0795\sqrt{n} + 0.0068n$	$162 + 24.6\sqrt{n} + 3.79n$	$288 + 69.8\sqrt{n} + 18.6n$	$177 + 142\sqrt{n} + 29.2n$	$490 + 110\sqrt{n} + 163n$

Figure 11: Calculation rules for hot tap water demand for apartment buildings[6].

The instantaneous hot water requirement for an hour is:

	Peak duration [s]	Formula
$q_{v, tap; v}$	1	$0.270 + 0.107\sqrt{n} + 0.00325n$
$V_{ww; 10}$	600	$127 + 39.7\sqrt{n} + 1.62n$
$V_{ww; 60}$	3,600	$243 + 67.9\sqrt{n} + 12.8n$
$V_{ww; 120}$	7,200	$203 + 88.3\sqrt{n} + 23.8n$
$V_{v, day}$	43,200	$104 + 168\sqrt{n} + 94.6n$

Figure 12: Calculation rules for hot tap water demand for an hour[6].

$$V_{WW;60} = 243 + 67.9\sqrt{n} + 12.8n \quad (11)$$

$V_{WW;60}$ : volume flow of hot water in 60 minutes n: number of apartments

The hot tap water profile for building apartment are shown below:

1 day hot tap water usage	
Time	$Q_{tap}$ (kwh)
07:00	38.64
08:00	10.08
09:00	5.04
10:00	2.52
11:00	5.04
12:00	7.56
13:00	0
14:00	2.52
15:00	2.52
16:00	2.52
17:00	0
18:00	7.56
19:00	2.52
20:00	17.64 7
21:00	36.12
22:00	0

Table 1: Hot water profile

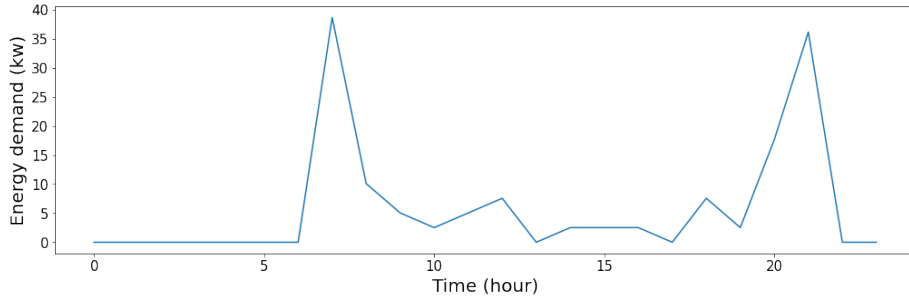


Figure 13: Hot tap water use of entire apartment.

#### 4.4 BENG and load profile correction

Total energy consumption for D.H.W with profile M [4] (Appendix A) is 5,845 kwh per day. The annual consumption is therefore approximately 2134 kwh. The value is much higher than the indicated value ( approximately 1600 kwh) for 77m2 apartments from NTA8800 [7], figure 13.

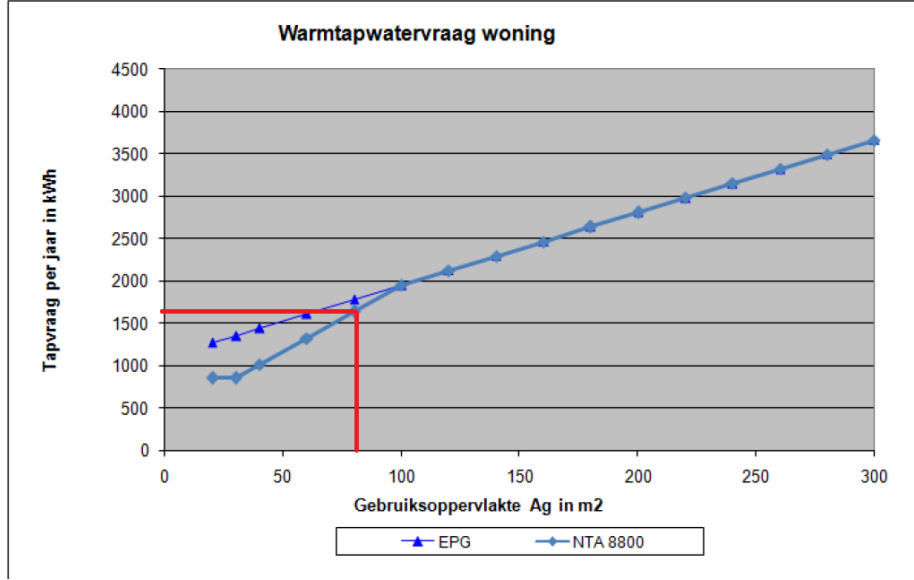


Figure 14: Hot tap water use per year (kWh/m²) [7].

According to NEN 12831-3 [10], Method for calculation of the design heat load - Part 3: Domestic hot water systems heat load and characterisation of needs. The value of volume of hot water per day ( $V_{W;P;day}$ ) can be calculated based on the number of equivalent persons (adults)  $n_{P,eq}$ .

#### Apartment dwellings.

The area is used to calculate  $n_{P,eq,max}$  as follow:

$$n_{P,eq,max} = 1.75 - \begin{cases} 1, & \text{if } A_h < 10m^2 \\ 0.01875 \cdot (50 - A_h), & \text{if } 10m^2 < A_h < 50m^2 \\ 0.035 \cdot A_h, & \text{if } A_h > 50m^2 \end{cases} \quad (12)$$

The total number of equivalent persons is defined by formula:

$$n_{P,eq} = 1.75 + \begin{cases} 0.3 \cdot n_{P,eq,max}, & \text{if } n_{P,eq,max} < 1.75 \\ 0.3 \cdot (n_{P,eq,max} - 1.75), & \text{if } n_{P,eq,max} \geq 1.75 \end{cases} \quad (13)$$

For the residential case and at the level of one dwelling, requirements can be expressed by formula:

$$V_{W,P,day} = \min\left(x; \left(y \cdot \frac{A_h}{n_{P,eq}}\right)\right) \quad (14)$$



Where:

$A_h$ : habitable area.

$n_P, e_q$ : number of equivalent persons used for calculating the D.H.W requirements.

$n_P, e_{q,max}$ : maximum number of equivalent persons corresponding to the part of the group supplied by the same D.H.W transmitter (individual or attached house and collective housing).

The default values for x, and y are:  $x = 40,71$   $y = 3,26$  [10]

Applied equations (13) and (14) for the 77m<sup>2</sup> apartment dwelling.  $n_P, e_q = 1.4665$ .

Compare the assumption of define cases with 2.8 people in 77 m<sup>2</sup> there are more likely that the EU-M capacity profile was define for more than 1.4 people,

Check\_\_\_\_\_

According to NEN NTA2020 - 13.3.2.1 / 856kwh/jaar/person = 856\*2.8= 2396.8

## 5 Associated operating conditions compressor

## 6 Package of requirements and compressor test plan

## 7 Overview of components with substantiation

## References

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- [11] [https://www.engineeringtoolbox.com/heat-emission-radiators-d\\_272.html](https://www.engineeringtoolbox.com/heat-emission-radiators-d_272.html)

## A Hot tap water profile

Since september 26, 2015, the Ecodesign [8] and energy labeling guidelines, also apply to appliances for the production of domestic hot water. Devices that do not comply with these guidelines may no longer be sold. In figure 5 the tap water profile label has been highlighted with red square.

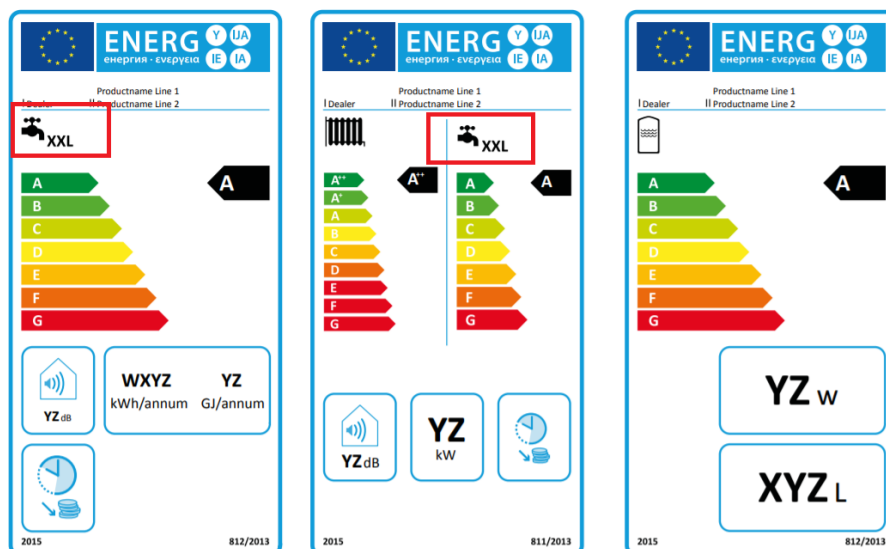


Figure 15: Energy label[8]

The hot water classes are defined in the EU regulation with different category label. For example hot water class with label "XL" must be able to supply 18 kWh of hot water per day (1 kWh corresponds to 64.8 MJ heat). This EU regulation also stipulates what conditions hot tap water class must be met. Figure 8 show that tap water profile for showering can only be selected from label S to XXL.

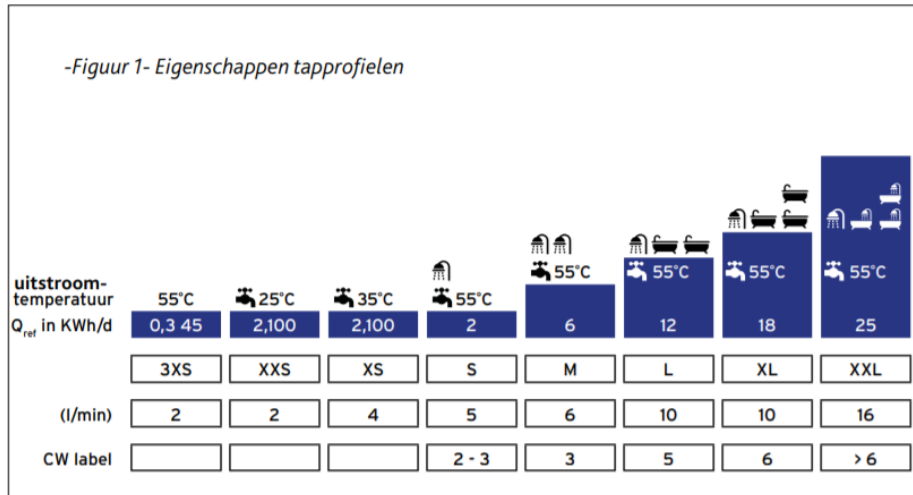


Figure 16: hot water profile labels[8].

h	M				L				XL			
	$Q_{sup}$	$f$	$T_m$	$T_p$	$Q_{sup}$	$f$	$T_m$	$T_p$	$Q_{sup}$	$f$	$T_m$	$T_p$
	kWh	l/min	°C	°C	kWh	l/min	°C	°C	kWh	l/min	°C	°C
07:00	0,105	3	25		0,105	3	25		0,105	3	25	
07:05	1,4	6	40		1,4	6	40					
07:15									1,82	6	40	
07:26									0,105	3	25	
07:30	0,105	3	25		0,105	3	25					
07:45					0,105	3	25		4,42	10	10	40
08:01	0,105	3	25						0,105	3	25	
08:05					3,605	10	10	40				
08:15	0,105	3	25						0,105	3	25	
08:25					0,105	3	25					
08:30	0,105	3	25		0,105	3	25		0,105	3	25	
08:45	0,105	3	25		0,105	3	25		0,105	3	25	
09:00	0,105	3	25		0,105	3	25		0,105	3	25	
09:30	0,105	3	25		0,105	3	25		0,105	3	25	
10:00									0,105	3	25	

Figure 17: Capaciteitsprofielen van waterverwarmingstoestellen.

10:00									<b>0,105</b>	3	25	
10:30	<b>0,105</b>	3	10	40	<b>0,105</b>	3	10	40	<b>0,105</b>	3	10	40
11:00									<b>0,105</b>	3	25	
11:30	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
11:45	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
12:00												
12:30												
12:45	<b>0,315</b>	4	10	55	<b>0,315</b>	4	10	55	<b>0,735</b>	4	10	55
14:30	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
15:00									<b>0,105</b>	3	25	
15:30	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
16:00									<b>0,105</b>	3	25	
16:30	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
17:00									<b>0,105</b>	3	25	
18:00	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
18:15	<b>0,105</b>	3	40		<b>0,105</b>	3	40		<b>0,105</b>	3	40	
18:30	<b>0,105</b>	3	40		<b>0,105</b>	3	40		<b>0,105</b>	3	40	

Figure 18: Capaciteitsprofielen van waterverwarmingstoestellen.

h	M				L				XL			
	$Q_{tap}$	$f$	$T_m$	$T_p$	$Q_{tap}$	$f$	$T_m$	$T_p$	$Q_{tap}$	$f$	$T_m$	$T_p$
	kWh	l/min	°C	°C	kWh	l/min	°C	°C	kWh	l/min	°C	°C
19:00	<b>0,105</b>	3	25		<b>0,105</b>	3	25		<b>0,105</b>	3	25	
19:30												
20:00												
20:30	<b>0,735</b>	4	10	55	<b>0,735</b>	4	10	55	<b>0,735</b>	4	10	55
20:45												
20:46									<b>4,42</b>	10	10	40
21:00					<b>3,605</b>	10	10	40				
21:15	<b>0,105</b>	3	25						<b>0,105</b>	3	25	
21:30	<b>1,4</b>	6	40		<b>0,105</b>	3	25		<b>4,42</b>	10	10	40
21:35												
21:45												
$Q_{ref}$	<b>5,845</b>				<b>11,655</b>				<b>19,07</b>			

Figure 19: Capaciteitsprofielen van waterverwarmingstoestellen.

## B Calculation methods

Hot tap water profile for apartments building with 24 residential houses. From equation (4):

$$V_{WW;60} = 243 + 67.9\sqrt{n} + 12.8n$$

Applied for  $n = 4$  and  $n = 24$

$$ratio = \frac{V_{WW;60;24}}{V_{WW;60;1}}$$

$$f_{new} = f \cdot ratio$$

$f_{new}$ : new water flow rate.

Look at figure 9 for an example. The amount of water use (litter)

$$m = \frac{3600 \cdot Q_{tap}}{c \cdot \Delta T}$$

The time period that water has been used (hour)

$$water_{usetime} = \frac{m \cdot 24}{f_{new} \cdot 60}$$

Energy use per hour for 24 apartments:

$$Q_{tap/perhour} = 24.Q_{tap.water_{usetime}}$$

$$Q_{building} = Q_{hotwater} + Q_{heating}$$

with  $Q_{tap/perhour} = Q_{hotwater}$

## C Office building Construction

Volume floor and internal walls construction:

$$V_{internal\_mass} = A_{internal\_mass}.th_{internal\_mass} \quad (15)$$

$V_{internal\_mass}$ : volume floor and internal walls [ $m^3$ ].

$A_{internal\_mass}$ : floor and internal walls surface [ $m^2$ ].

$th_{internal\_mass}$ : construction thickness [m].

Ventilation volume air flow [ $m^3/s$ ]:

$$q_V = \frac{n.V_{dwelling}}{3600} \quad (16)$$

n: ventilation air change per hour.

$V_{dwelling}$ : internal volume  $m^3$ .

Ventilation, mass air flow [kg/s]

$$q_m = q_V.\rho_{air} \quad (17)$$

$\rho_{air}$ : air density [ $kg/m^3$ ].

Resistance indoor air<sub>wall</sub>:

$$R_{air\_wall} = \frac{1}{A_{internal\_mass}.\alpha_{internal\_mass}} \quad (18)$$

Thermal transmittance indoor air-facade [ $W/m^2$ ]:

$$U = \frac{1}{A_{alpha_{i-facade}} + Rc_{facade} + \frac{1}{\alpha_{e-facade}}} \quad (19)$$

Resistance indoor air-outdoor air:

$$R_{air\_outdoor} = \frac{1}{A_{facade}.U + A_{glass}.U_{glass} + qm.c_{air}} \quad (20)$$

Indoor air and walls capacity:

$$C_{air} = \frac{\rho_{internal\_mass}.c_{internal\_mass}.V_{internal\_mass}}{2 + \rho_{air}.c_{air}.V_{dwelling}} \quad (21)$$

$$C_{wall} = \frac{\rho_{internal\_mass}.c_{internal\_mass}.V_{internal\_mass}}{2} \quad (22)$$