

# MICROWAVE CIRCUIT PROJECT REPORT

*Directional coupler microstrip line*

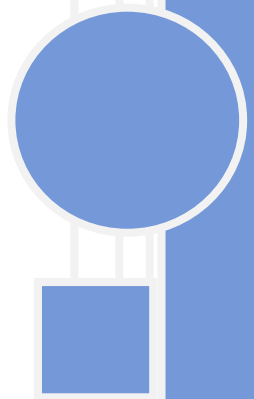
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Ngoc An Ha - 967813

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Date

January 20<sup>th</sup>, 2015



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## Directional coupler microstrip line

Design and implementation of directional coupler using microstrip line technique, Agilent's Advanced Design System application and optimization.

Center frequency	Coupling Coefficient
$F_0 = 2 \text{ GHz}$	$C = -10 \text{ dB}$

**Step 1:** Calculate odd mode and even mode characteristic impedance.

**Step 2:** Create and simulate circuit using ideal couple line CLIN

**Step 3:** Transform to circuit using microstrip couple line MCLIN and use momentum simulation.

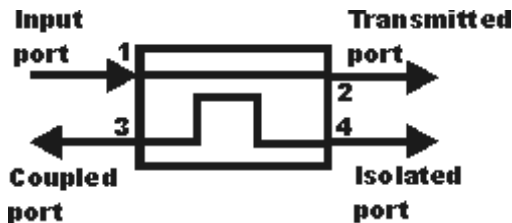
**Step 4:** Optimize circuit along with the discontinuities.

**Step 5:** Finish realizable circuit structure layout. Create the circuit.

**Step 6:** Using Network Analyzer to measure the result of the circuit. Compare the measurement result and simulation result.

## I. FORMULA AND DESIGN

### A. Circuit



$S_{11}$ : Reflection coefficient

$S_{21}$ : Transmission coefficient

$S_{31}$ : Coupling coefficient

$S_{41}$ : Isolation

$/S_{41}-S_{31} /$ : Directivity

### B. Formula

$$F_0 = 2 \text{ GHz} = 2 \cdot 10^9 \text{ Hz}$$

$$C = 10 \text{ dB} = 10^{\frac{10}{20}} = 0.316$$

$$\lambda = \frac{c_0}{F_0} = \frac{3 \cdot 10^8}{2 \cdot 10^9} = 0.15 \text{ m}$$

$$B = \frac{2 \cdot \pi}{\lambda} = 41.888$$

$$l = \frac{\lambda}{4} = \frac{0.15}{4} = 0.0375 \text{ m}$$

$$C = \frac{Z_{Ce} - Z_{Co}}{Z_{Ce} + Z_{Co}} = 0.316 \Rightarrow Z_{Ce} - Z_{Co} = 0.316 \cdot (Z_{Ce} + Z_{Co})$$

$$\Rightarrow 0.684 \cdot Z_{Ce} = 1.316 \cdot Z_{Co} \quad (1)$$

$$Z_0^2 = 50^2 = Z_{Ce} \cdot Z_{Co} \quad (2)$$

From (1) and (2), we have

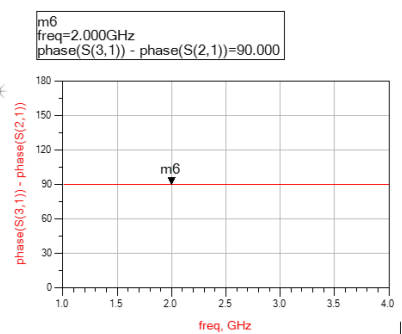
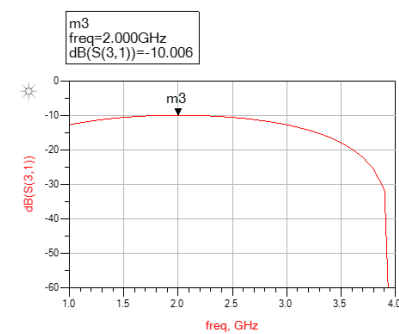
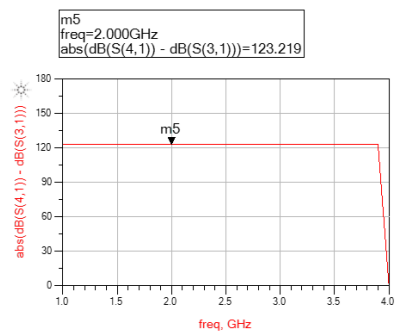
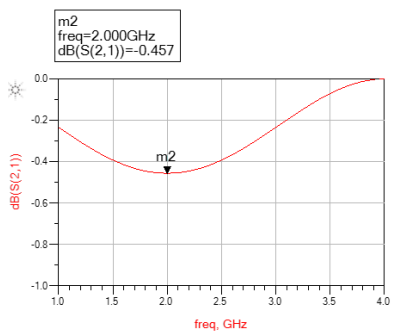
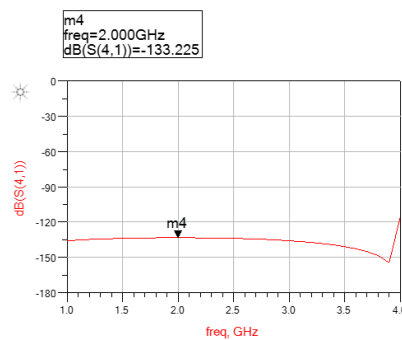
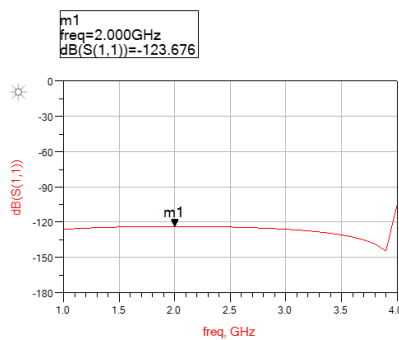
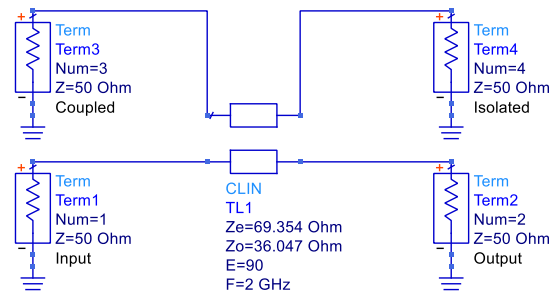
$$Z_{Co} = 36.047 \Omega$$

$$Z_{Ce} = 69.354 \Omega$$

## II. CREATE CIRCUIT USING IDEAL COUPLE LINE CLIN

### S-PARAMETERS

S\_Param  
SP1  
Start=1.0 GHz  
Stop=4.0 GHz  
Step=0.1 GHz



The simulation result show that at 2 GHz, we have coupling coefficient S31 at -10dB. This is a good result, since it show that our calculation results in  $Z_{ce}$  and  $Z_{co}$  are right.

### III. TRANSFORMATION TO A STRUCTURE WITH MICROSTRIP LINE COMPONENT MCLIN

The screenshot shows the LineCalc software interface with the following parameters:

Substrate Parameters	
ID	MSub1
H	0.762 mm
Er	3.480
Mur	1.000
Cond	5.8E+7
Hu	3.9e+034 mil
T	17.500 um
TanD	0.000

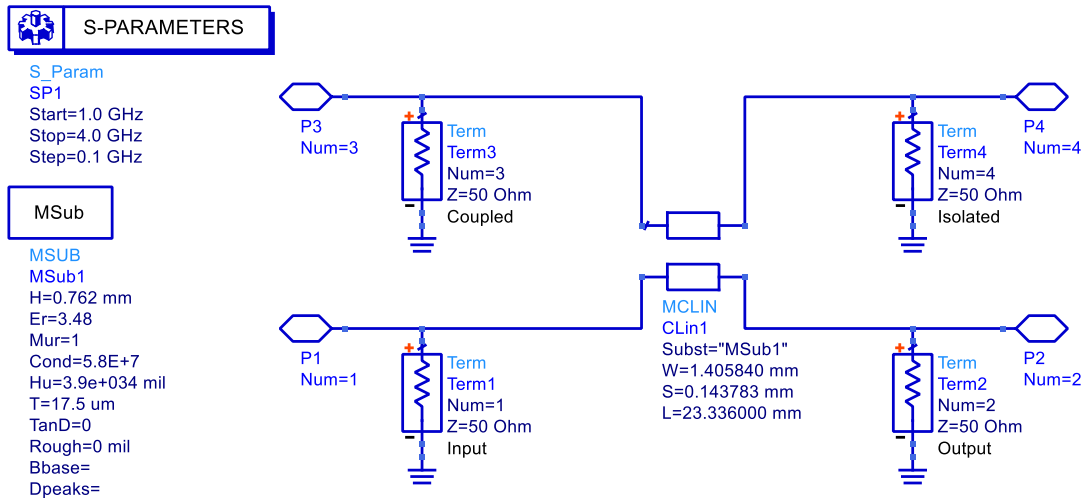
Physical	
W	1.405840 mm
S	0.143783 mm
L	23.336000 mm

Electrical	
ZE	69.354 Ohm
ZO	36.047 Ohm
Z0	50.000036 Ohm
C_DB	-10.006184
E_Eff	90.000 deg

Calculated Results:

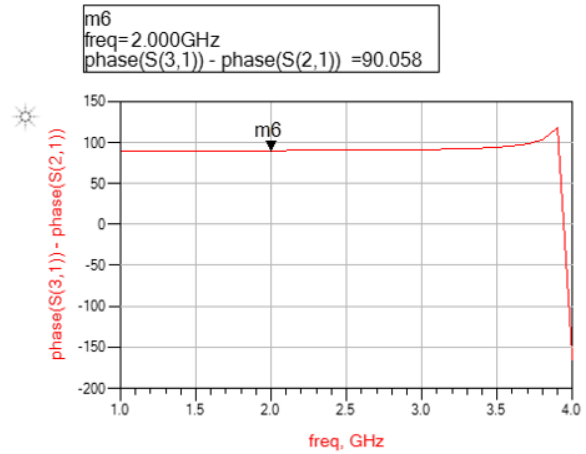
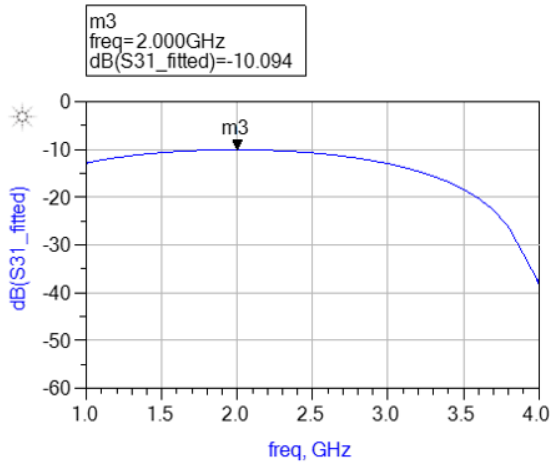
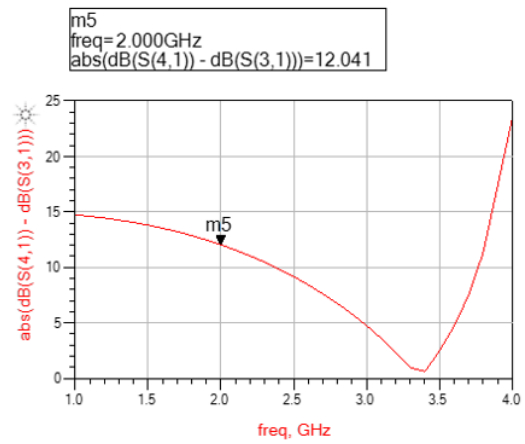
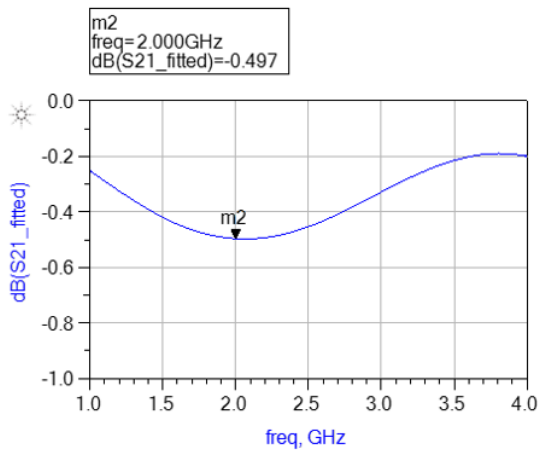
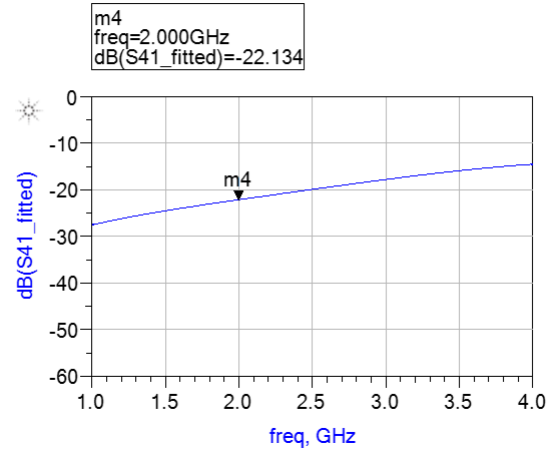
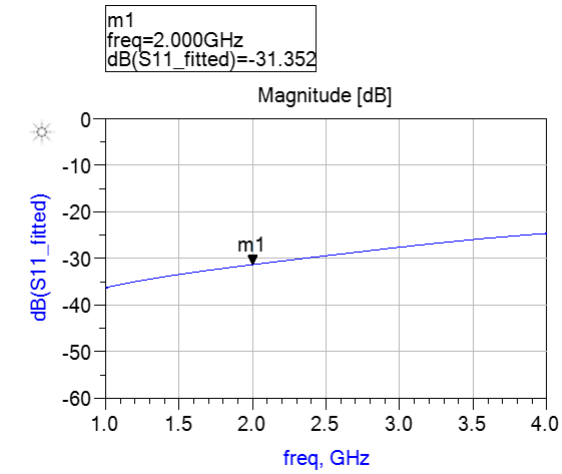
- KE = 2.875
- KO = 2.297
- AE\_DB = 0.010
- AO\_DB = 0.020
- SkinDepth = 0.058

Diagram: A 3D perspective view of a microstrip line on a substrate, showing dimensions W, S, and L.



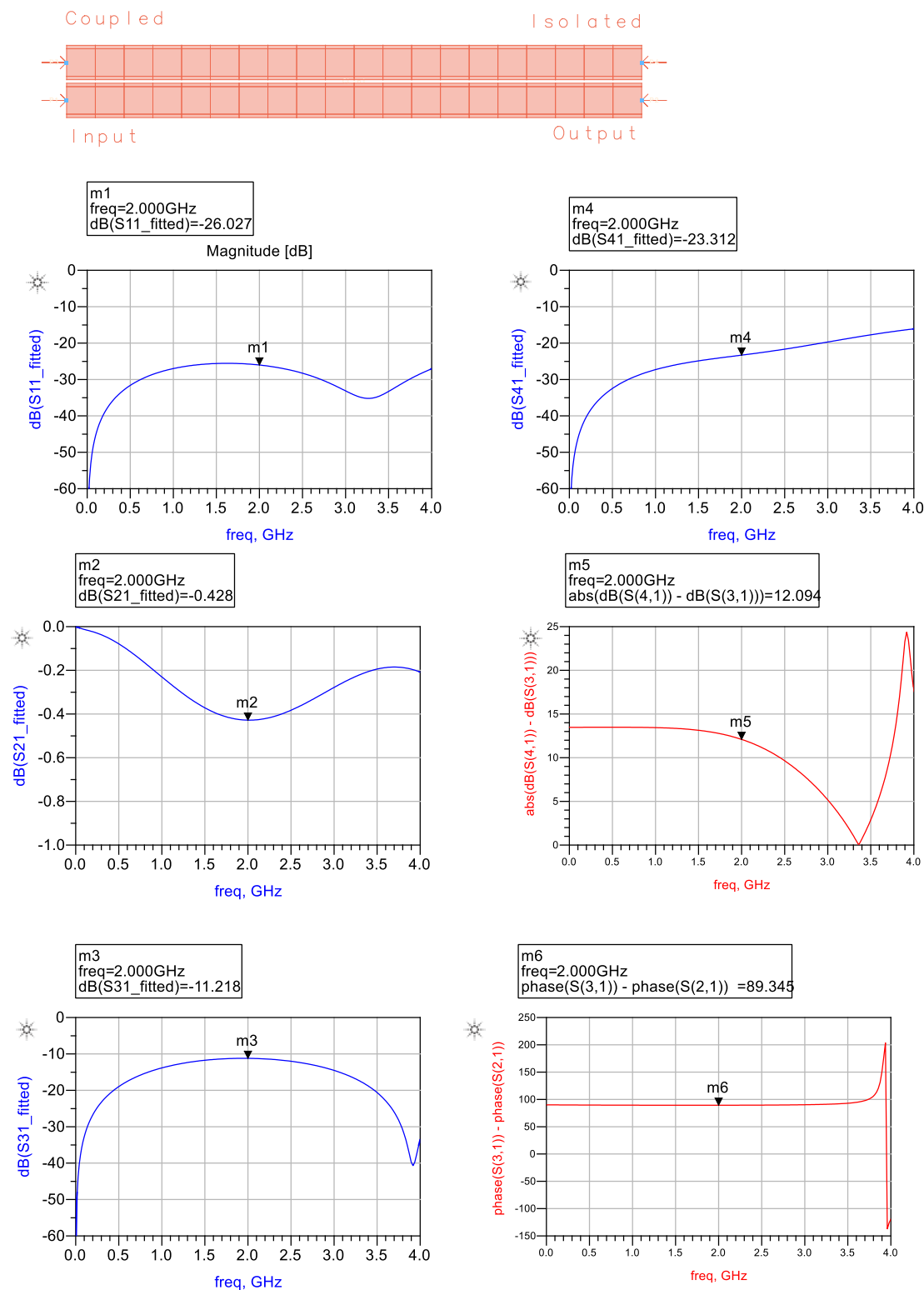
We would like to realize our circuit by using microstrip couple line elements. Therefore, we replaced CLIN by MCLIN.

Using the tool LineCal of ADS, with the Effective Electrical Length E\_Eff of coupled section at 90 degree and center frequency at 2 GHz, we obtained the variable data for the Microstrip Couple Line. The reason we choose the E\_Eff at 90 degree because from the design of the couple line method, each couple line must have  $\frac{\lambda}{4}$  electrical length. In addition, for direction coupler, the phase between port 1 and port 4, as well as port 2 and port 3 is 90 degree.



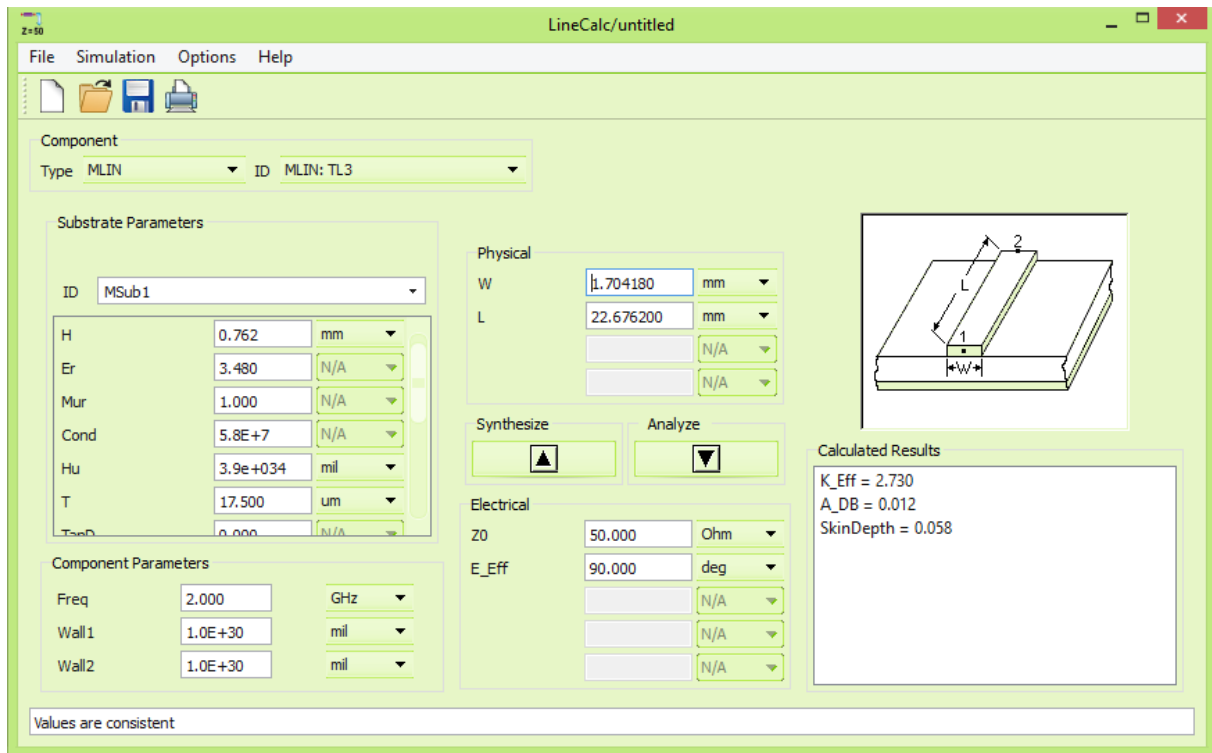
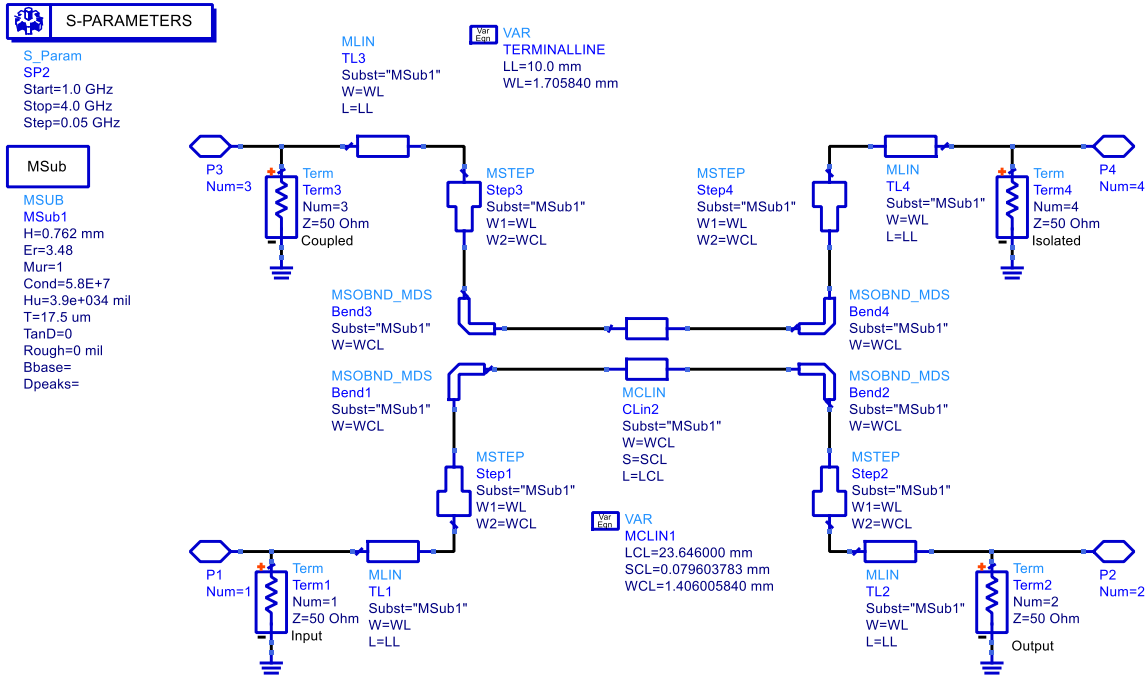
Judging from the simulation result, we can see that at 2GHz, we can still have coupling coefficient at -10dB.

## Momentum simulation



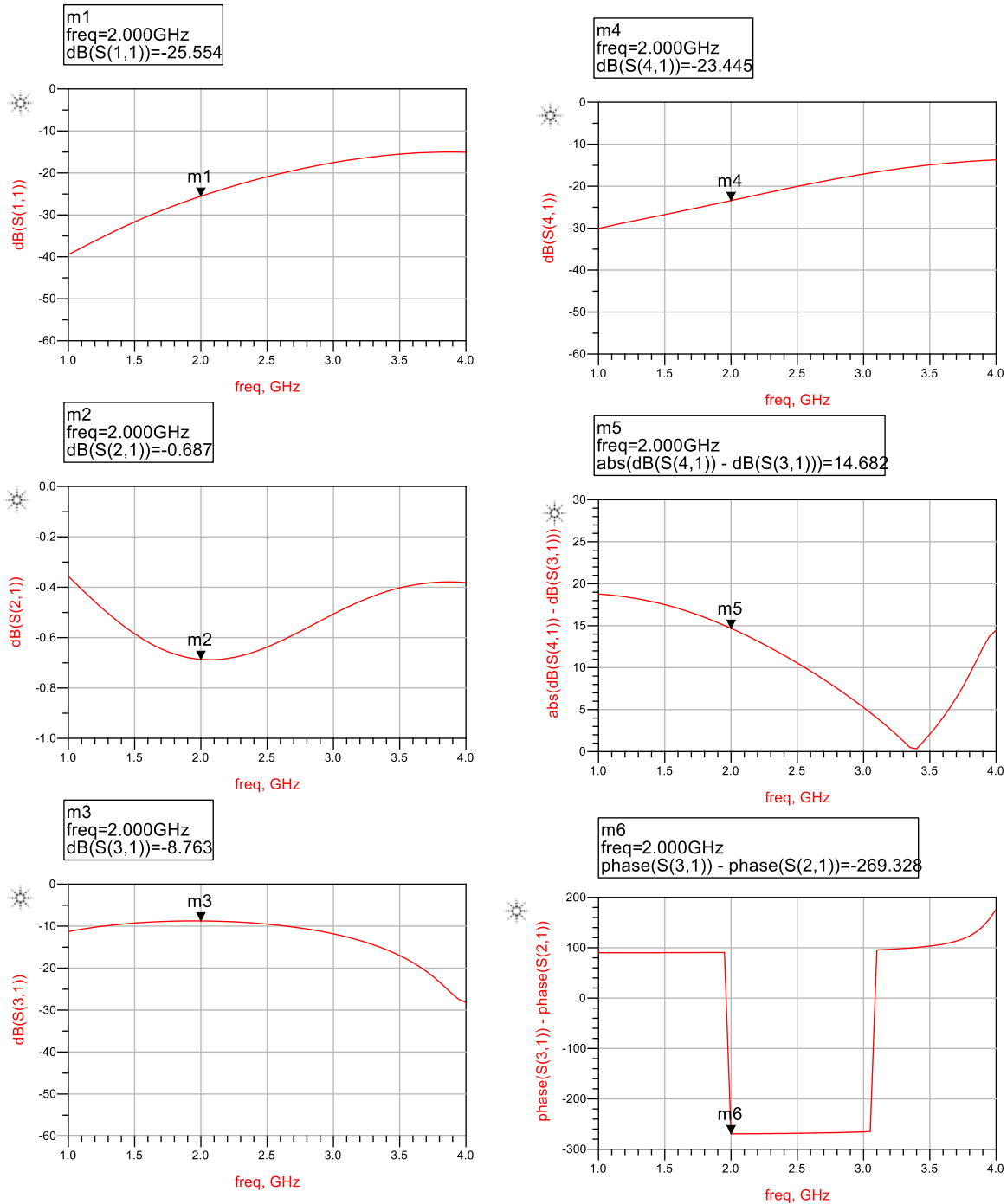
From the momentum simulation, we can see the coupling coefficient decreased to nearly -11/5 dB. In addition, from the result of  $S_{11}$ , we can see that our center frequency was shifted to 3.3 GHz. Moreover, we also have to consider the discontinuity of the circuit. So, in the next step, we have to include all the discontinuities, and then optimize the circuit to achieve the best result we can get.

## IV. OPTIMIZATION CIRCUIT



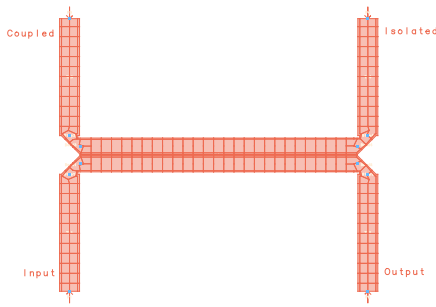
Since we want to measure our circuit using network analyzer, SMA ports are required, but with the SMA port size issue, we need to integrate some transmission line part to our circuit. The participated transmission line must have the characteristic impedance  $Z_0$  equal 50 Ohm, which means that its width should be 1.705 mm.

Here we use the MSTEP components to have a better simulation, where the differences in width between 2 part of a microstrip line are counted in. This different in dimension is considered as the discontinuities. After that, by using layout generation function of ADS, we were able to get the layout of the filter circuit. Then, we can use ADS EM simulation function which include the electrical magnetic affections to get the result that the circuit may possibly behave in reality.

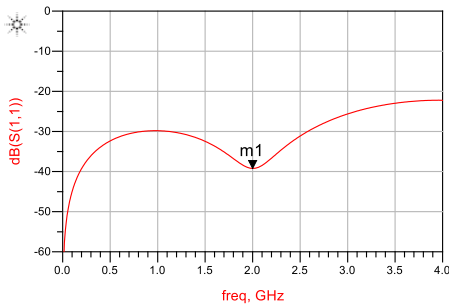




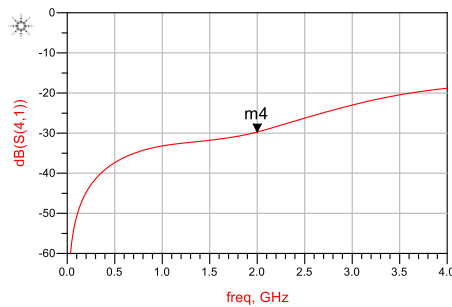
## Optimized Circuit Momentum Simulation



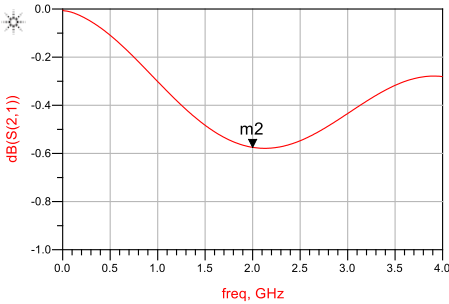
m1  
freq=2.000GHz  
dB(S(1,1))=-39.224



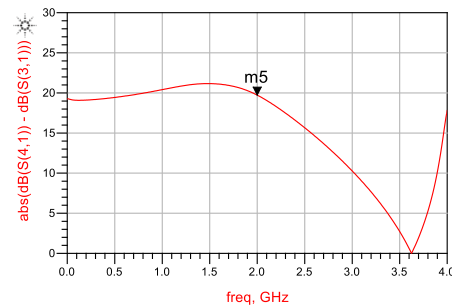
m4  
freq=2.000GHz  
dB(S(4,1))=-29.724



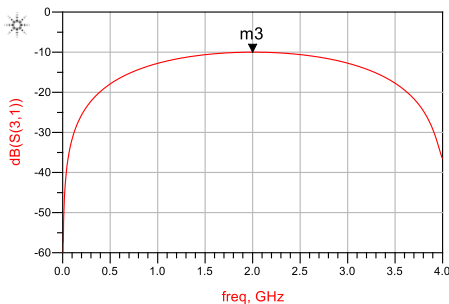
m2  
freq=2.000GHz  
dB(S(2,1))=-0.575



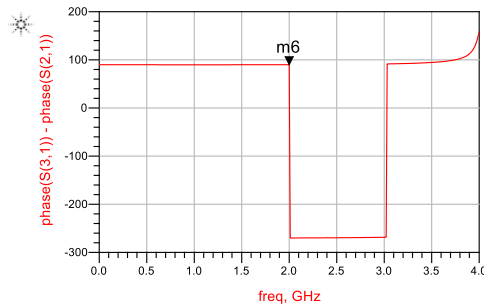
m5  
freq=2.000GHz  
abs(dB(S(4,1)) - dB(S(3,1)))=19.725



m3  
freq=2.000GHz  
dB(S(3,1))=-10.000

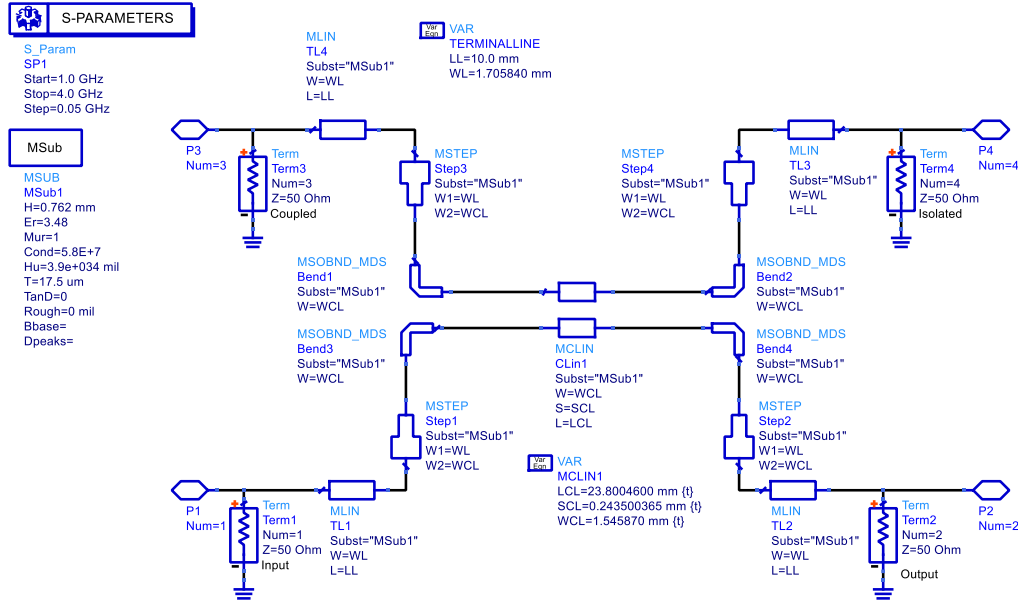


m6  
freq=2.000GHz  
phase(S(3,1)) - phase(S(2,1))=89.952

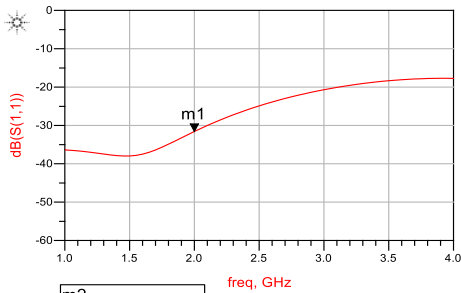


Now that we were able to get a better result from our momentum, we could proceed to create the circuit. Unfortunately, we were not able to exactly create the circuit. In this case, all we could try is to change the design of the circuit so that it can be realizable. Because we had to increase the distance between two lines of the microstrip couple line component, the coupling coefficient would decrease as well. So our new design coupling coefficient S31 would be -13 dB, which is the nearest to the goal -10 dB.

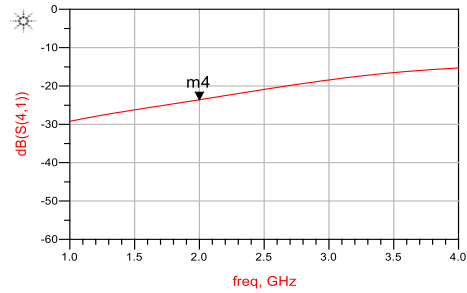
## V. REALIZING CIRCUIT DESIGN FOR 13 dB



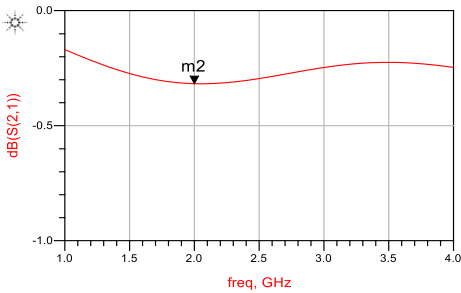
m1  
freq=2.000GHz  
dB(S(1,1))=-31.583



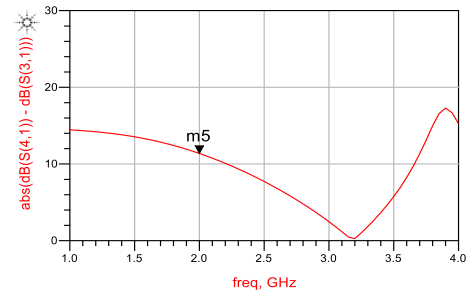
m4  
freq=2.000GHz  
dB(S(4,1))=-23.595



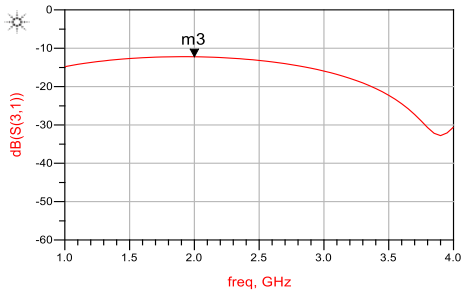
m2  
freq=2.000GHz  
dB(S(2,1))=-0.318



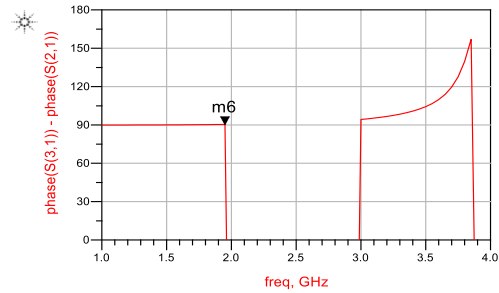
m5  
freq=2.000GHz  
abs(dB(S(4,1)) - dB(S(3,1)))=11.367



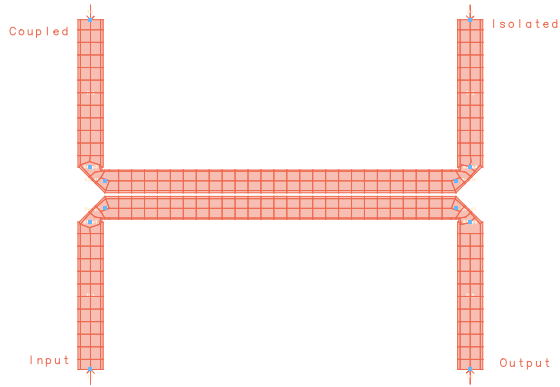
m3  
freq=2.000GHz  
dB(S(3,1))=-12.229



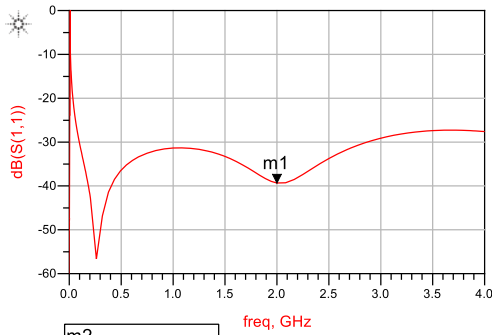
m6  
freq=1.950GHz  
phase(S(3,1)) - phase(S(2,1))=90.37



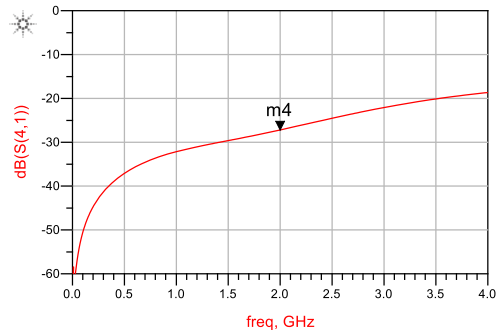
## Realizable Circuit Momentum Simulation



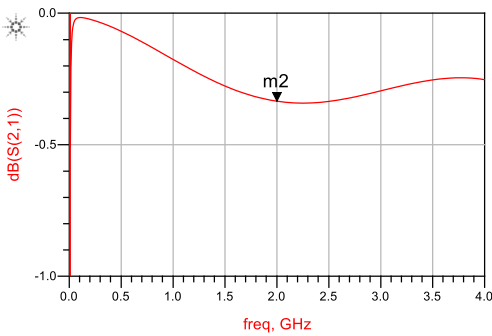
m1  
freq=2.000GHz  
dB(S(1,1))=-39.347



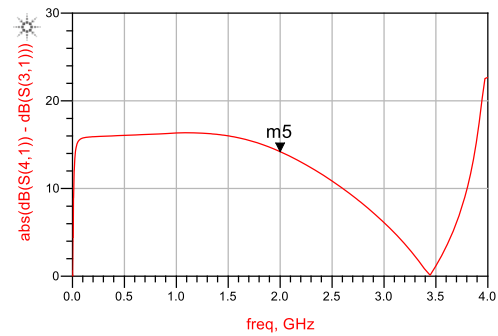
m4  
freq=2.000GHz  
dB(S(4,1))=-27.196



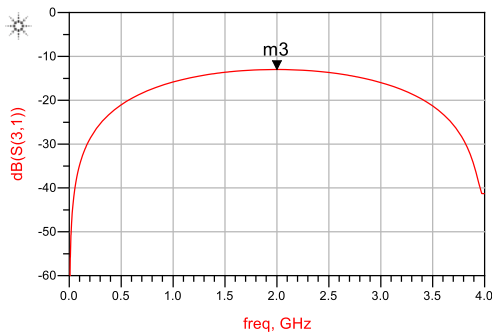
m2  
freq=2.000GHz  
dB(S(2,1))=-0.335



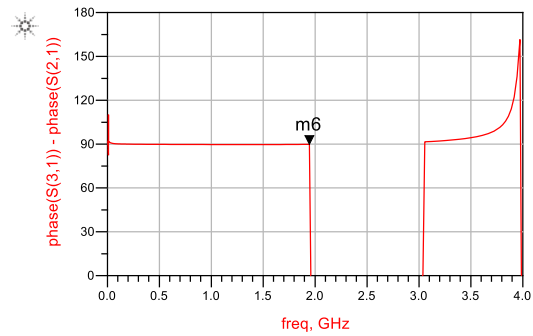
m5  
freq=2.000GHz  
abs(dB(S(4,1)) - dB(S(3,1)))=14.199



m3  
freq=2.000GHz  
dB(S(3,1))=-12.997



m6  
freq=1.944GHz  
phase(S(3,1)) - phase(S(2,1))=89.81



## VI. COMPARING THE MEASURING RESULT OF THE NETWORK ANALYZER WITH THE MOMENTUM SIMULATION RESULT

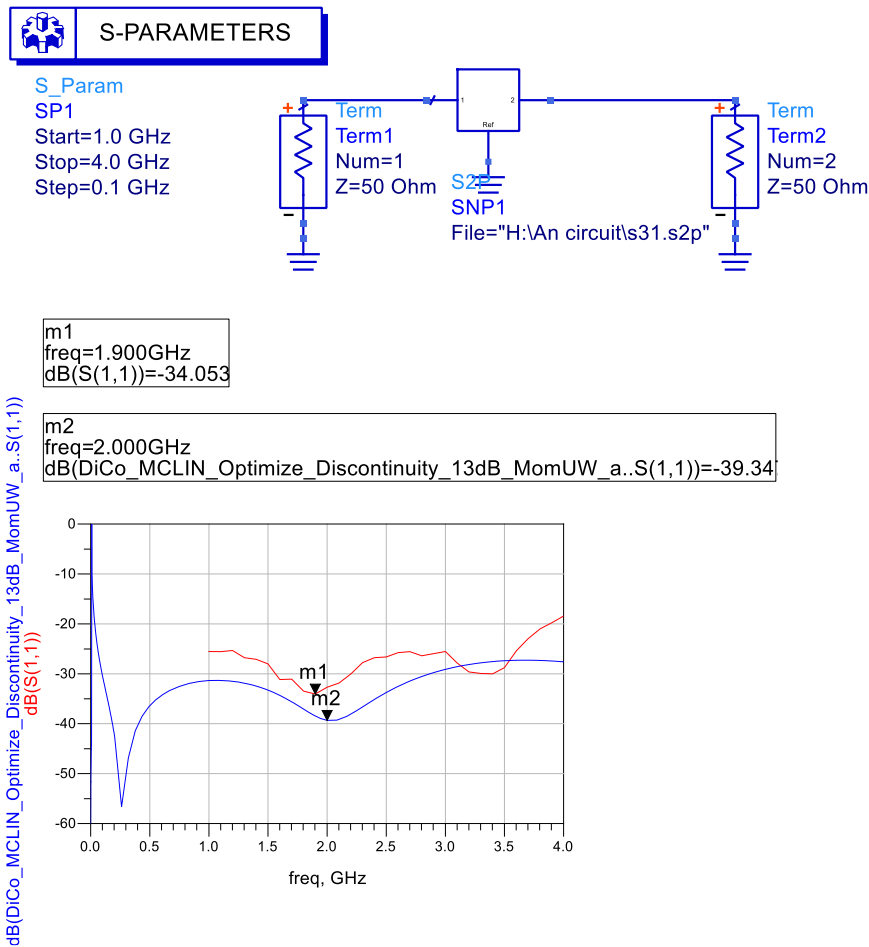


Figure 1 Comparison of reflection coefficient S11

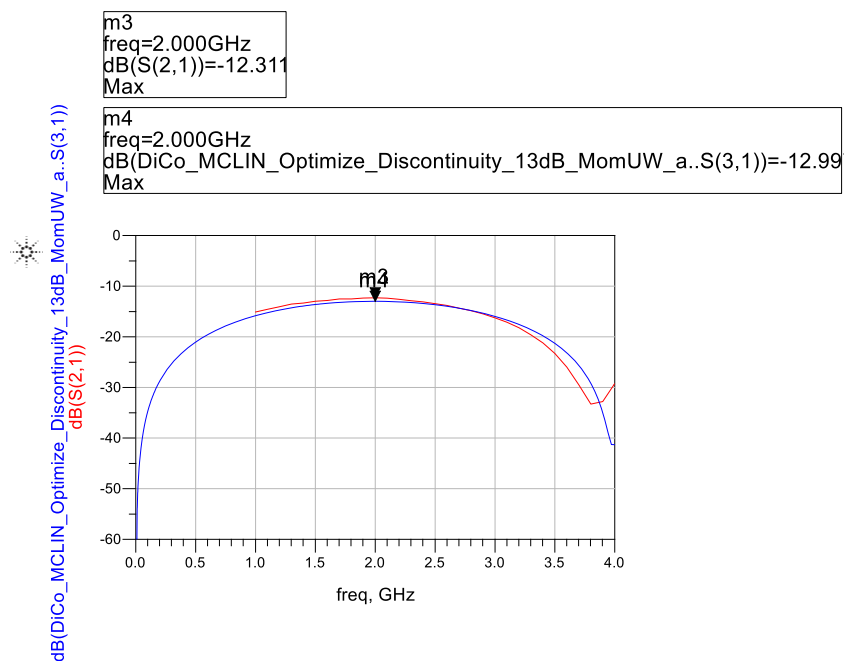


Figure 2 Comparison of coupling coefficient S31

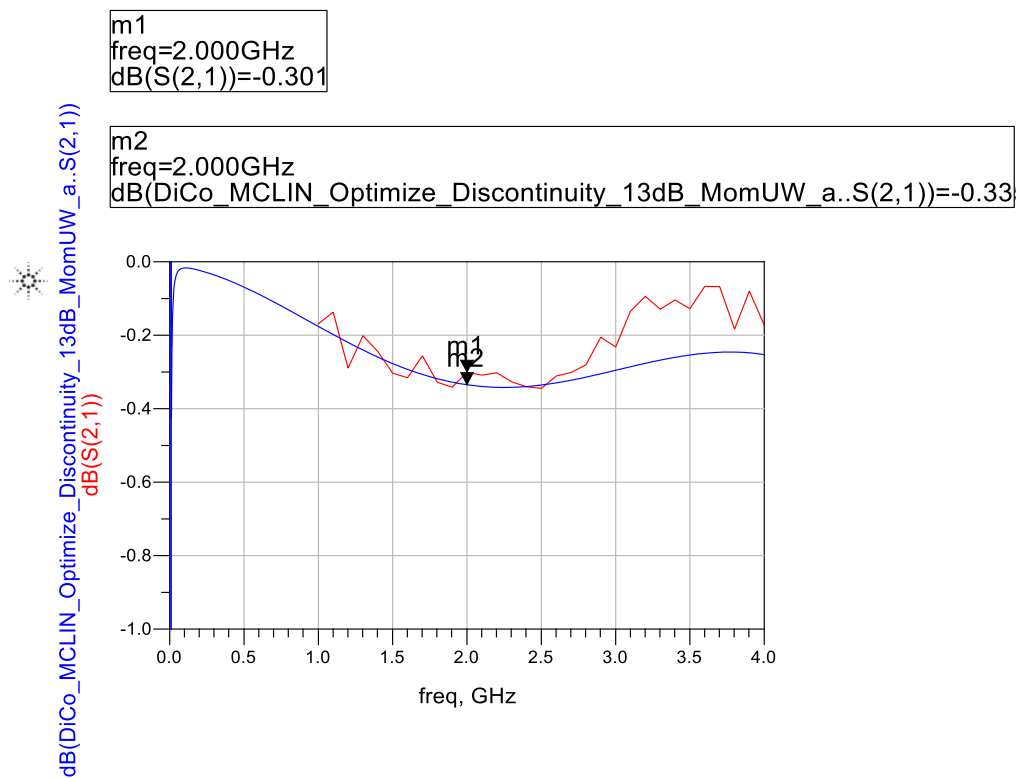


Figure 3 Comparison of transmission coefficient S21

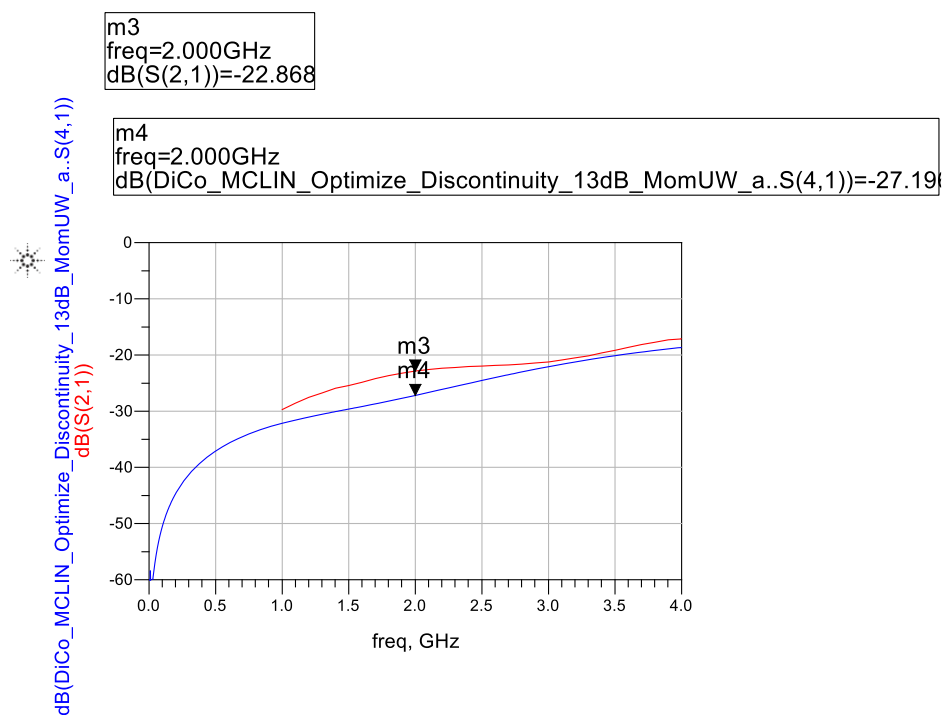


Figure 4 Comparison of isolation S41

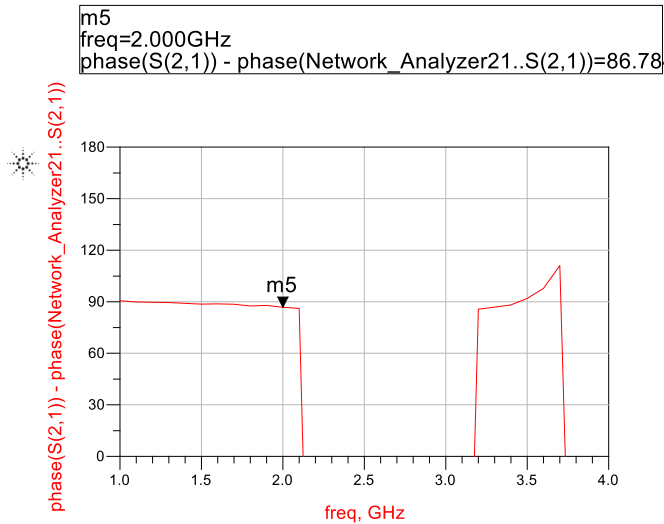


Figure 5 Measurement result of the phase shift between port 3 and port 2 of the circuit.

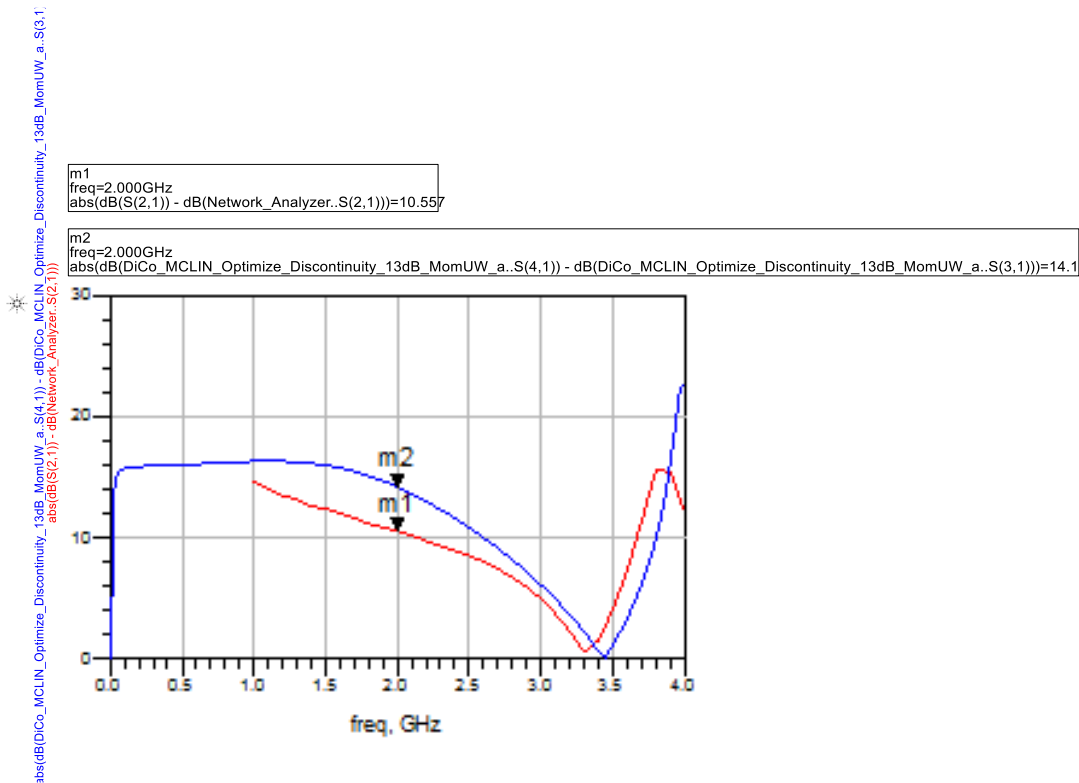


Figure 6 Comparison of the directivity of the circuit

## CONCLUSION

From the comparison figures, we can see that: in overall, the shape of the measurement results are pretty much the same looking as the simulation result. Although compare to the simulation, the value of the circuit is slightly higher than the simulation. However, this might be explained due to the substrate material and the circuit making process, those errors that we cannot avoid regarding to the material. In the end, our result is acceptable since it is not much different from the initial condition. We can confirm the succession of the project.