

# ENEE 303 Recitation 08

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# Week Notes

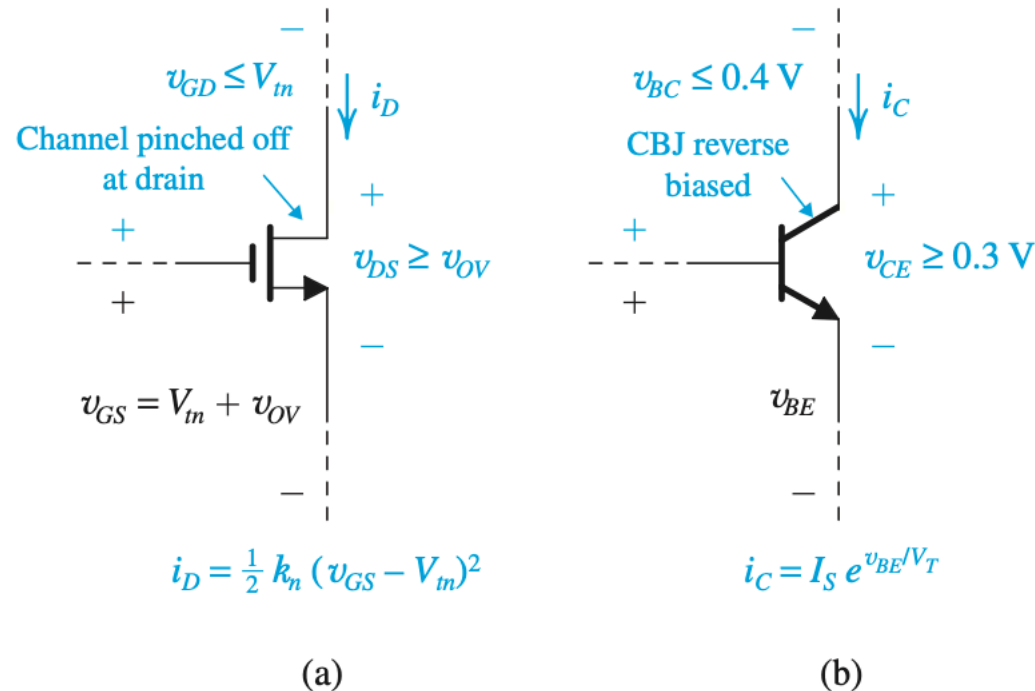
- Transistor amplifiers
  - Review for MOSFET and BJT
- Voltage transfer characteristics
- Small signal voltage gain
- Small signal operation and models
- 3 example problems

# Week Notes

- To build a voltage amplifier with the transistor, MOSFET or BJT
- To obtain a linear amplifier from the nonlinear transistors
- To model the transistor operation so that we can analyze and design transistor amplifiers

# Basic principles

- Recall the current equations for MOSFET and BJT



$$\text{MOSFET: } i_D = \frac{1}{2} k_n (v_{GS} - V_m)^2$$

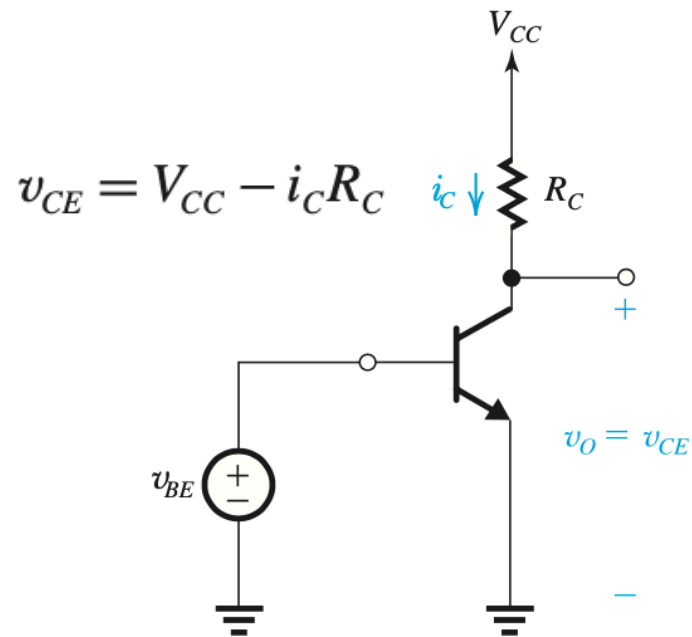
$$\text{BJT: } i_C = I_S e^{v_{BE}/V_T}$$

Transistors are basically transconductance amplifiers

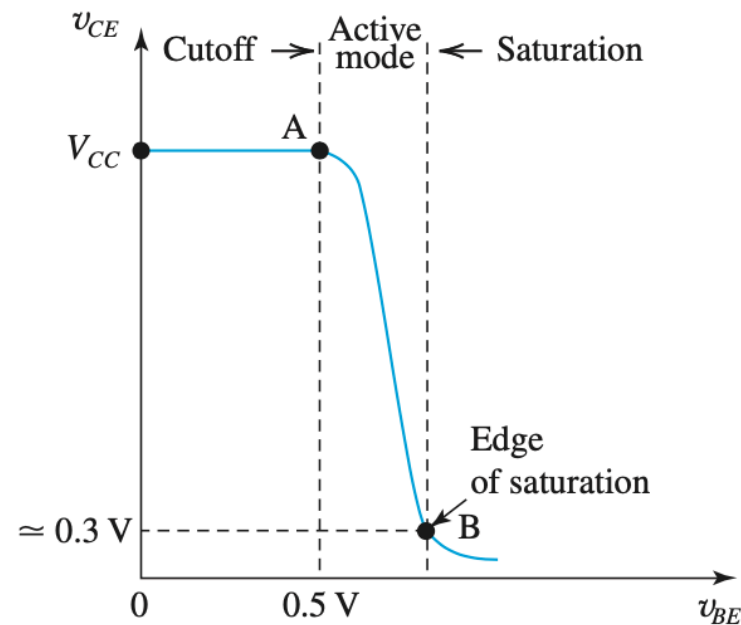
**Figure 7.1** Operating (a) an NMOS transistor and (b) an npn transistor in the active mode. Note that  $v_{GS} = V_m + v_{OV}$  and  $v_{DS} \geq v_{OV}$ ; thus  $v_{GD} \leq V_m$ , which ensures channel pinch-off at the drain end. Similarly,  $v_{BE} \simeq 0.7 \text{ V}$ , and  $v_{CE} \geq 0.3 \text{ V}$  results in  $v_{BC} \leq 0.4 \text{ V}$ , which is sufficient to keep the CBJ from conducting.

# Voltage transfer characteristics

- To use transistor to build a voltage amplifier, we need a load resistance



(c)

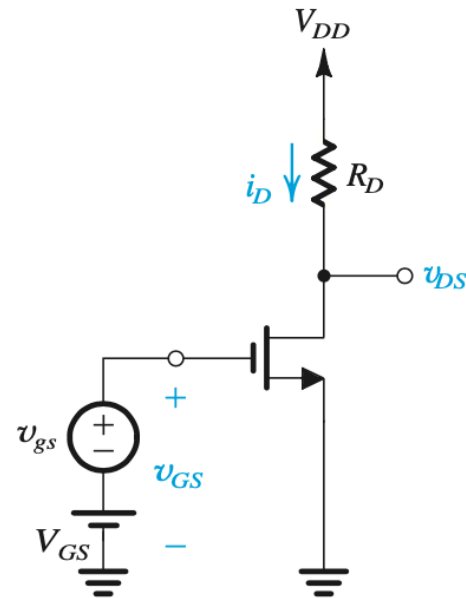


(d)

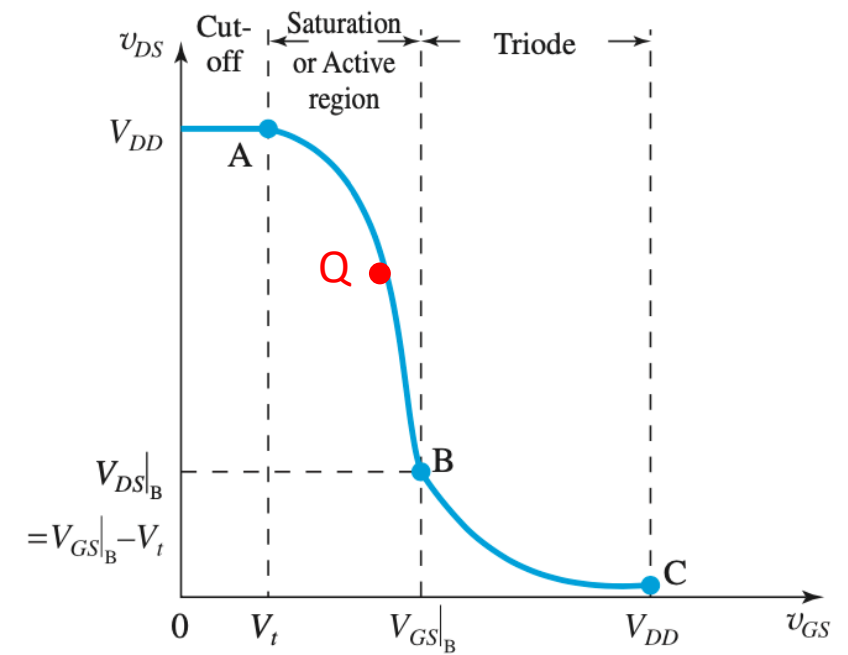
# Voltage transfer characteristics

Linear amp by biasing MOSFET to operate in the active region and by keeping the input signal small

$$V_{GS}|_B = V_t + \frac{\sqrt{2k_n R_D V_{DD}} + 1 - 1}{k_n R_D}$$



$$v_{DS} = V_{DD} - i_D R_D$$



(b)

# Small signal voltage gain

- MOSFET case

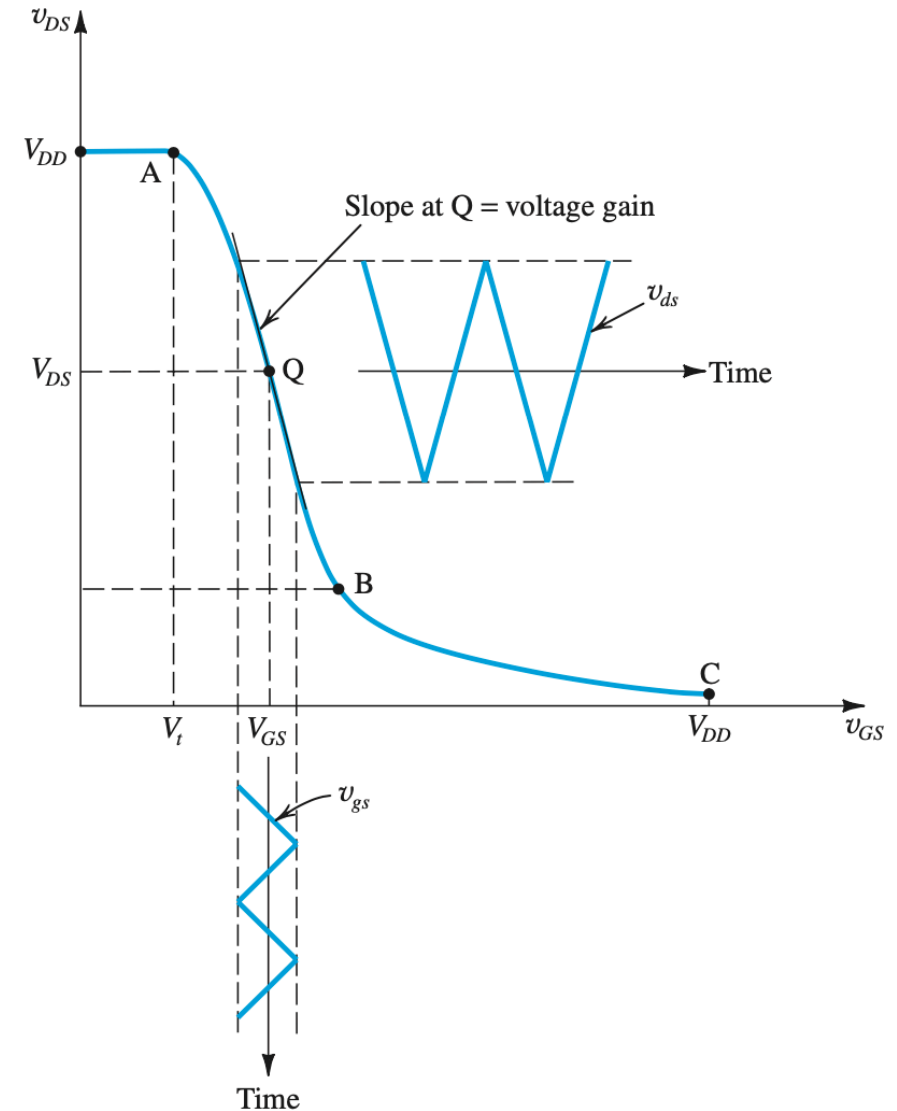
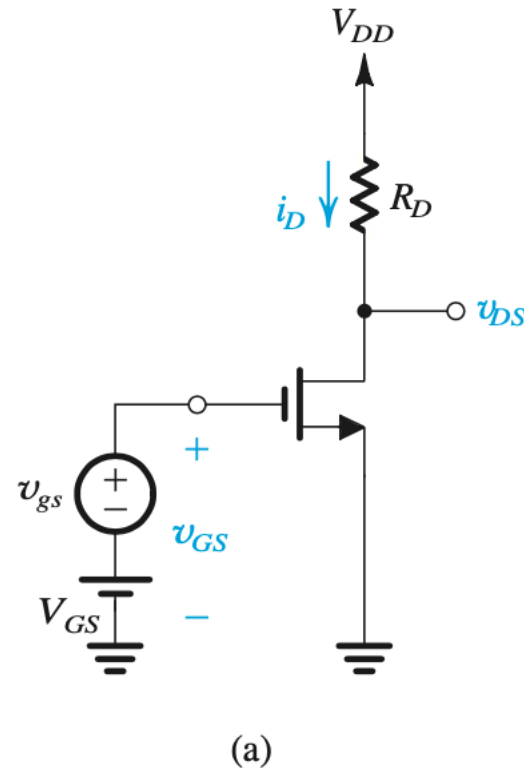
$$v_{DS} = V_{DD} - \frac{1}{2} k_n R_D (v_{GS} - V_t)^2$$

$$A_v = \left. \frac{dv_{DS}}{dv_{GS}} \right|_{v_{GS}=V_{GS}} = -k_n V_{OV} R_D$$

$$I_D = \frac{1}{2} k_n V_{OV}^2$$

$$A_v = -\frac{I_D R_D}{V_{OV}/2} = -\frac{V_{DD} - V_{DS}}{V_{OV}/2}$$

$$|A_{v\max}| = \frac{V_{DD} - V_{DS}|_B}{V_{OV}|_B/2} = \frac{V_{DD} - V_{OV}|_B}{V_{OV}|_B/2}$$



# Small signal voltage gain

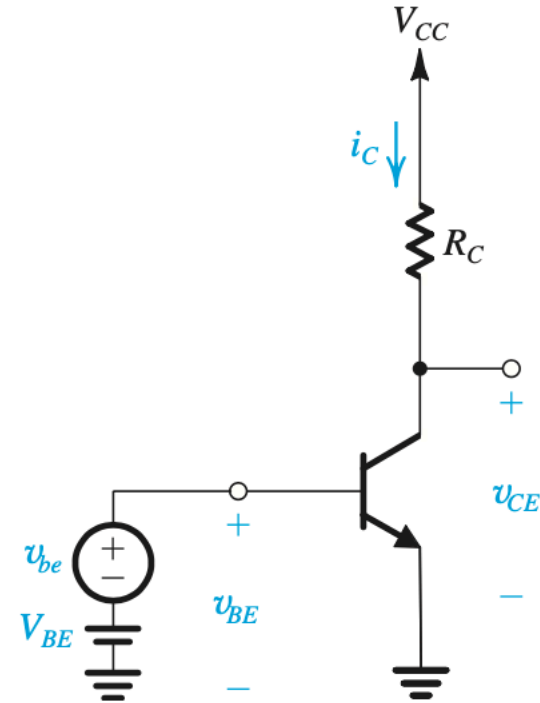
- BJT case

$$v_{CE} = V_{CC} - I_C R_C = V_{CC} - I_S e^{\frac{v_{BE}}{V_T}} R_C$$

$$A_v = \left. \frac{dv_{CE}}{dv_{BE}} \right|_{v_{BE}=V_{BE}} = - \left( \frac{I_C}{V_T} \right) R_C$$

$$A_v = - \frac{V_{CC} - V_{CE}}{V_T}$$

$$|A_{v\max}| = \frac{V_{CC} - 0.3}{V_T}$$

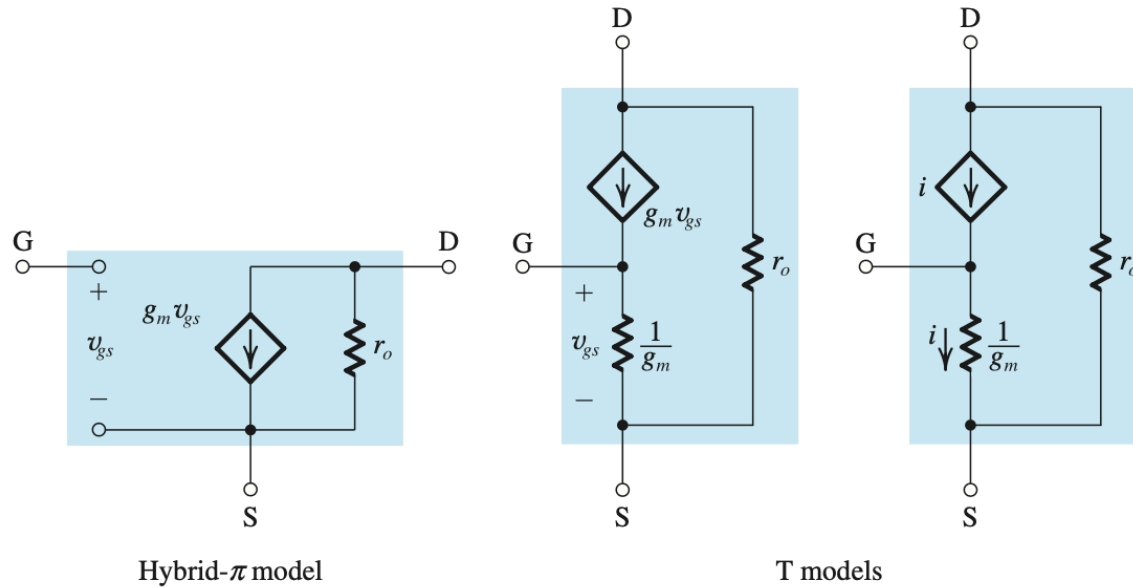




# Small signal models

## MOSFET

Small-Signal, Equivalent-Circuit Models



Small signal condition:  $v_{gs} \ll 2(V_{GS} - V_t)$

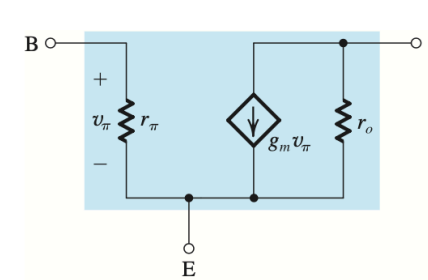
$$g_m \equiv \left. \frac{\partial i_D}{\partial v_{GS}} \right|_{v_{GS}=V_{GS}} = k_n (V_{GS} - V_t)$$

$$A_v \equiv \frac{v_{ds}}{v_{gs}} = -g_m R_D$$

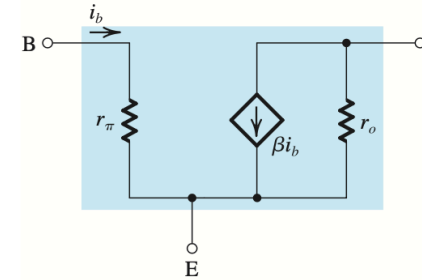
## BJT

Hybrid- $\pi$  Model

■  $(g_m v_\pi)$  Version

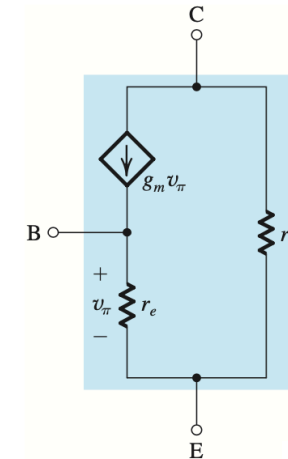


■  $(\beta i_b)$  Version

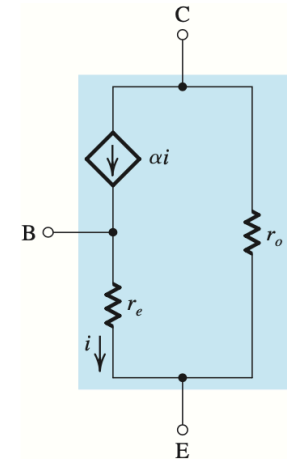


T Model

■  $(g_m v_\pi)$  Version



■  $(\alpha i)$  Version



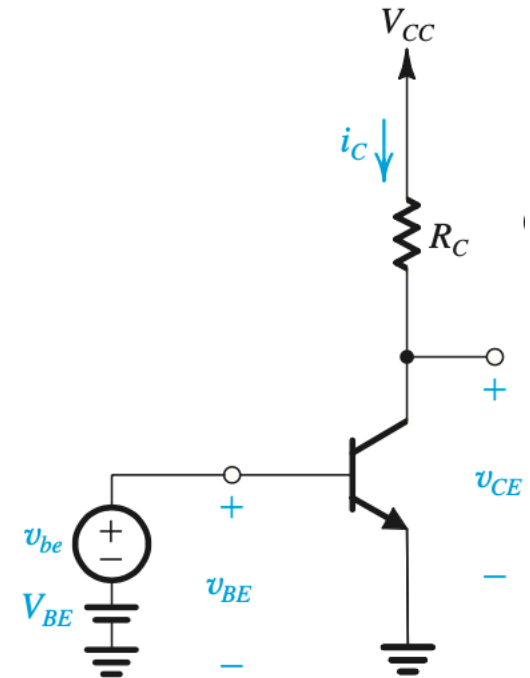
$v_{be} \ll V_T$

$$g_m = \left. \frac{\partial i_C}{\partial v_{BE}} \right|_{i_C=I_C} = \frac{I_C}{V_T} \quad r_\pi = \frac{\beta}{g_m}$$

$$A_v \equiv \frac{v_{ce}}{v_{be}} = -g_m R_C$$

# Example Problem 1

- Consider a BJT amplifier circuit having  $I_S = 10^{-15} \text{ A}$ , a collector resistance  $R_C = 6.8 \text{ k}\Omega$ , and a power supply  $V_{CC} = 10 \text{ V}$ .
  - (a) what is  $I_C$  and  $V_{BE}$  when  $V_{CE} = 3.2 \text{ V}$ ?
  - (b) what is voltage gain  $A_V$ ?
  - (c) keeping  $I_C$  unchanged, find  $R_C$  that results in a voltage gain of  $-320 \text{ V/V}$
  - (d) What is the largest negative signal swing allowed at the output? Assuming  $v_{CE} \geq 0.3 \text{ V}$
  - (e) what is the corresponding  $v_{BE}$ ?



# Example problem 1 continued

(a)  $V_{CC} - I_C R_C = V_{CE}$

$$I_C = 1 \text{ mA}$$

$$I_C = I_S e^{\frac{V_{BE}}{V_T}}$$

$$V_{BE} = 690 \text{ mV}$$

(b)

$$A_V = -\frac{I_C R_C}{V_T} = -272 \text{ V/V}$$

(c) To keep  $I_C$  unchanged and  $A_V = -\frac{I_C R_C}{V_T}$

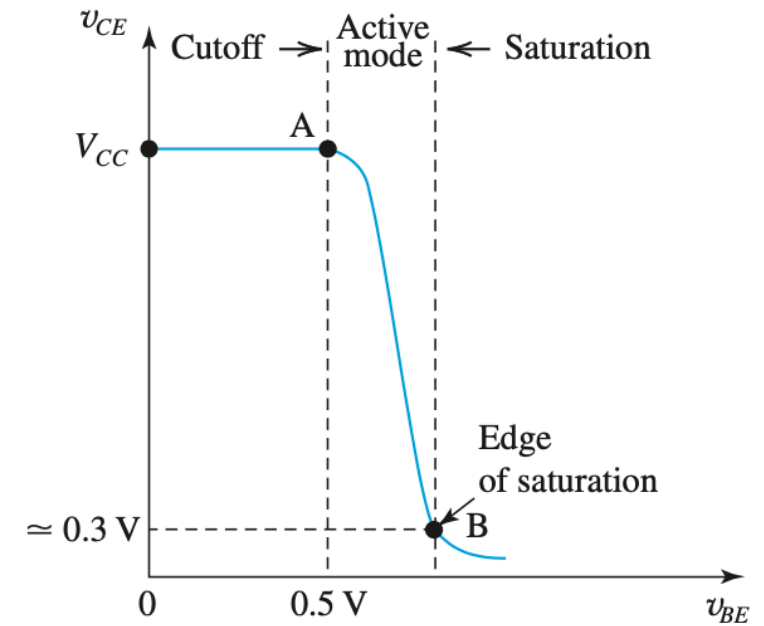
$$R_C = -\frac{A_V V_T}{I_C} = 8.28 \text{ k}\Omega$$

(d)  $V_{CE} = V_{CC} - I_C R_C = 1.72 \text{ V}$

Since  $v_{CE} \geq 0.3 \text{ V}$ , the largest allowable negative signal is  $1.72 - 0.3 = 1.42 \text{ V}$

(e)  $A_V = -320 \text{ V/V}$

$$v_{BE} = \frac{v_{CE}}{A_V} = 4.4 \text{ mV}$$



(d)

# Example problem 2

Design the circuit of Fig. 5.52(e) to operate at a dc drain current of 0.5 mA and  $V_D = +2$  V. Let  $V_t = 1$  V,  $k'_n W/L = 1$  mA/V<sup>2</sup>,  $\lambda = 0$ ,  $V_{DD} = V_{SS} = 5$  V. Use standard 5% resistor values (see Appendix G), and give the resulting values of  $I_D$ ,  $V_D$ , and  $V_S$ .

$$I_D = \frac{1}{2} (k'_n W/L) V_{OV}^2 \quad V_{OV} = V_{GS} - V_t = 1 \text{ V}$$

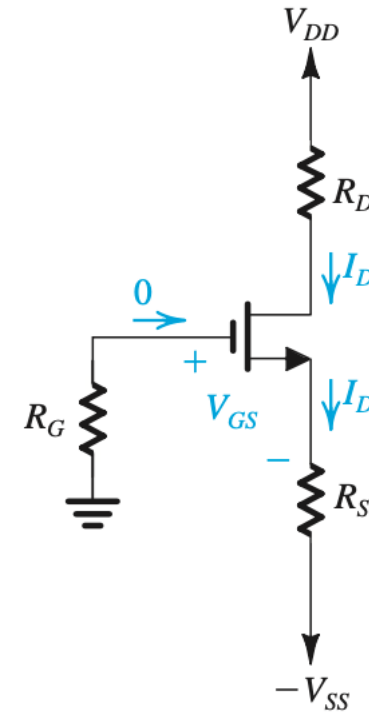
$$V_G - V_S = V_{OV} + V_t$$

$$V_S = -2 \text{ V}$$

$$I_D = \frac{V_S - V_{SS}}{R_S} \quad R_S = 6 \text{ k}\Omega$$

$$I_D = \frac{V_{DD} - V_D}{R_D} \quad R_D = 6 \text{ k}\Omega$$

Because of the standard resistor, there only exists  $R = 6.2 \text{ k}\Omega$



# Example problem 2 continued

If we choose  $R_S = R_D = 6.2k\Omega$

$$V_{GS} = V_G - V_S = -V_S = V_{SS} - I_D R_S$$

$$I_D = \frac{1}{2}(k'_n W/L)(V_{GS} - V_t)^2 = \frac{1}{2}(V_{SS} - I_D R_S - V_t)^2$$

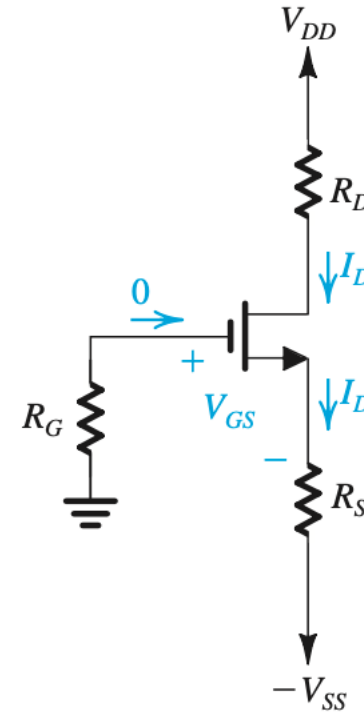
$$R_S^2 I_D^2 - (2 + R_S(V_{SS} - V_t))I_D + (V_{SS} - V_t)^2 = 0$$

$$I_D = 0.49 \text{ mA or } \cancel{0.86 \text{ mA}}$$

$$V_S > 0$$

$$V_S = -1.96 \text{ V}$$

$$V_D = 1.96 \text{ V}$$



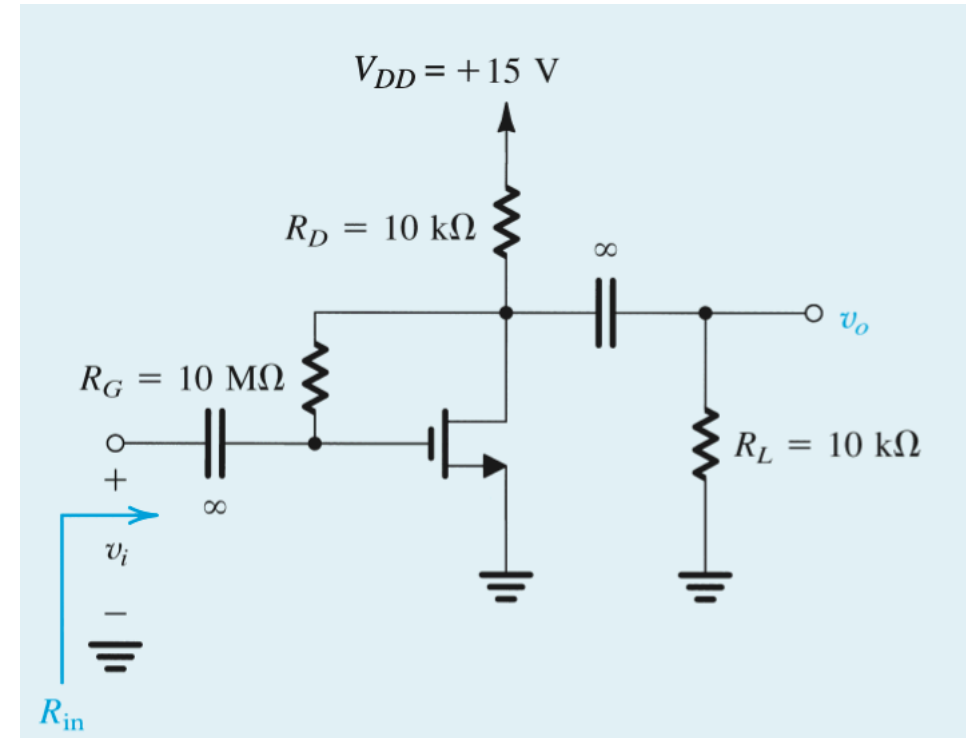
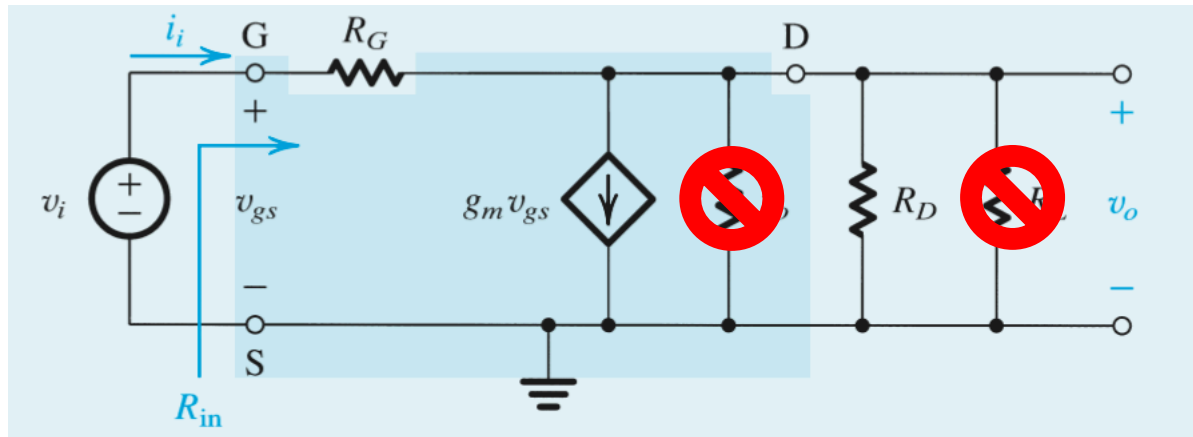
# Example problem 3

**D7.4** Consider the amplifier circuit of Fig. 7.15(a) without the load resistance  $R_L$  and with channel-length modulation neglected. Let  $V_{DD} = 5$  V,  $V_t = 0.7$  V, and  $k_n = 1$  mA/V<sup>2</sup>. Find  $V_{OV}$ ,  $I_D$ ,  $R_D$ , and  $R_G$  to obtain a voltage gain of  $-25$  V/V and an input resistance of  $0.5$  M $\Omega$ . What is the maximum allowable input signal,  $\hat{v}_i$ ?

We want  $A_v = -25$  V/V and  $R_{in} = 0.5$  M $\Omega$

By KVL

$$R_{in} = \frac{v_i}{i_i} = \frac{v_i}{v_i - v_o} R_G = \frac{R_G}{26} \quad \boxed{R_G = 26R_{in} = 13 \text{ M}\Omega}$$



# Example problem 3 continued

$$A_v = -g_m R_D, \text{ we have } g_m R_D = 25 = k_n V_{OV} R_D$$

$$I_D R_D = \frac{1}{2} k_n V_{OV}^2 R_D = \frac{1}{2} g_m V_{OV} R_D = 12.5 V_{OV}$$

$$V_{OV} = V_{DD} - I_D R_D - V_t = 5 - 12.5 V_{OV} - 0.7$$

$$V_{OV} = 0.319 \text{ V}$$

$$g_m = k_n V_{OV} = 319 \mu\text{A/V}$$

$$R_D = 78.5 \text{ k}\Omega$$

To obtain max allowable input signal, we need to keep the MOSFET in saturation. In other words,

$$v_{DS} \geq v_{GS} - V_t$$

For the equality condition,  $v_{DS} = v_{GS} - V_t$      $V_{DS} - |A_v| \hat{v}_i = V_{GS} + \hat{v}_i - V_t$

$$\hat{v}_i = \frac{V_t}{|A_v| + 1} = \frac{0.7\text{V}}{26} = 26.9 \text{ mV}$$

**Table J.1** Standard Resistance Values

5% Resistor Values (k $\Omega$ )	1% Resistor Values (k $\Omega$ )			
	100–174	178–309	316–549	562–976
10	100	178	316	562
11	102	182	324	576
12	105	187	332	590
13	107	191	340	604
15	110	196	348	619
16	113	200	357	634
18	115	205	365	649
20	118	210	374	665
22	121	215	383	681
24	124	221	392	698
27	127	226	402	715
30	130	232	412	732
33	133	237	422	750
36	137	243	432	768
39	140	249	442	787
43	143	255	453	806
47	147	261	464	825
51	150	267	475	845
56	154	274	487	866
62	158	280	499	887
68	162	287	511	909
75	165	294	523	931
82	169	301	536	953
91	174	309	549	976