

$$\begin{aligned}
 1) \text{ Bulk mean temperature: } \bar{T}_b &= \frac{1}{2} (T_{m,i} + T_{m,o}) \\
 &= \frac{1}{2} (5 + 60) \\
 &= 32.5^\circ\text{C}
 \end{aligned}$$

Water properties @ 32.5°C :

$$c_p = 4178 \text{ J kg}^{-1} \text{ K}^{-1}$$

$$\rho = 994.8 \text{ kg m}^{-3}$$

Constant surface temperature, internal convection:

$$\dot{Q} = h A_s \Delta T_{lm}$$

$$\dot{Q} = \dot{m}_w c_p (T_{m,o} - T_{m,i}) = \dot{m}_s h_{fg}$$

Steam condensation temperature: 68°C

$$\frac{2333 - 2345.4}{70 - 65} = \frac{h_{fg} - 2345.4}{68 - 65}$$

$$h_{fg} = 2337.96 \text{ kJ kg}^{-1}$$

$$\begin{aligned}
 \dot{Q} &= \dot{m}_s h_{fg} \\
 &= 0.6 (2337.96) \\
 &= 1402.776 \text{ kW}
 \end{aligned}$$

1) Log mean temperature difference:

$$\Delta T_{lm} = \frac{\Delta T_2 - \Delta T_1}{\ln \Delta T_2 - \ln \Delta T_1} = \frac{(68-60) - (68-5)}{\ln(68-60) - \ln(68-5)}$$
$$= 26.65124855^\circ\text{C}$$

$$h = \frac{\dot{Q}}{A_s \Delta T_{lm}} = \frac{\dot{Q}}{n \pi D_i L \Delta T_{lm}}$$
$$= \frac{1402.776}{7\pi(25 \times 10^{-3}) \times 5 \times 26.65124855}$$
$$= 19.13694146 \text{ kW m}^{-2} \text{K}^{-1}$$

$$\dot{m}_w = \frac{\dot{Q}}{c_p(T_{m,o} - T_{m,i})} = \frac{1402.776 \div 7}{4.178(60-5)}$$
$$= 0.8720856931 \text{ kg s}^{-1}$$
$$\approx 0.872 \text{ kg s}^{-1}$$

$$u_m = \frac{\dot{m}_w}{\rho A_c} = \frac{0.872}{994.8(\pi(\frac{25}{2} \times 10^{-3})^2)}$$
$$= 1.785884987 \text{ m s}^{-1}$$
$$\approx 1.79 \text{ m s}^{-1}$$

$$\begin{aligned}
 2) T_b &= \frac{1}{2} (T_{m,i} + T_{m,o}) \\
 &= \frac{1}{2} (10 + 80) \\
 &= 45^\circ\text{C}
 \end{aligned}$$

Water properties @ 45°C :

$$\rho = 990.1 \text{ kg m}^{-3}$$

$$k = 0.637 \text{ W m}^{-1} \text{ K}^{-1}$$

$$\nu = 0.602 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$$

$$c_p = 4180 \text{ J kg}^{-1} \text{ K}^{-1}$$

$$Pr = 3.91$$

Constant heat flux: $\dot{Q} = \dot{q} A$

$$\begin{aligned}
 \dot{Q} &= \dot{q} A = m_w c_p (T_{m,o} - T_{m,i}) \\
 &= \rho \dot{V} c_p (T_{m,o} - T_{m,i}) \\
 &= 990.1 \left(\frac{5 \times 10^{-3}}{60} \right) (4.18) (80 - 10) \\
 &= 24.14193833 \text{ kW} \\
 &\approx 24.1 \text{ kW}
 \end{aligned}$$

$$\begin{aligned}
 2) \text{Re}_D &= \frac{U_\infty D}{\nu} = \frac{\left(\frac{\dot{V}}{A_c}\right) D}{\nu} \\
 &= \frac{\frac{5 \times 10^{-3}}{60} \div \left(\pi \times \left(\frac{2}{2} \times 10^{-2}\right)^2\right) \times 2 \times 10^{-2}}{0.602 \times 10^{-6}} \\
 &= 8812.566063 > 2300 \text{ (Turbulent flow)}
 \end{aligned}$$

$$\begin{aligned}
 \frac{L}{D} &= \frac{13}{2 \times 10^{-2}} \\
 &= 650 > 10
 \end{aligned}$$

$$\begin{aligned}
 \bar{Nu}_D &= 0.023 \text{Re}_D^{\frac{4}{5}} \text{Pr}^{0.4} \\
 &= 0.023 (8812.57)^{\frac{4}{5}} (3.91)^{0.4} \\
 &= 56.84345246
 \end{aligned}$$

$$\begin{aligned}
 \bar{h} &= \frac{\bar{Nu}_D k}{D} \\
 &= 1810.463961 \text{ W m}^{-2} \text{ K}^{-1}
 \end{aligned}$$

$$\dot{q} = h (T_s - T_{f,m})$$

$$T_{s,o} = \frac{\dot{q}}{h} + T_{m,o}$$

$$= \frac{\dot{Q}}{h A_s} + T_{m,o}$$

$$= \frac{24.14193833}{1.810463961 (0.02 \pi \times 13)} + 80$$

$$= 96.32521958^\circ \text{C} \approx 96.3^\circ \text{C}$$

$$3a) \dot{m}c_p(T_m + dT_m) - \dot{m}c_p T_m = \delta \dot{Q}$$

$$\dot{m}c_p dT_m = \delta \dot{Q}$$

$$\delta \dot{Q} = \dot{q} dA$$

$$= \dot{q} \pi D dx$$

$$= a \kappa \pi D dx$$

$$\dot{m}c_p dT_m = a \kappa \pi D dx$$

$$dT_m = \frac{a \pi D}{\dot{m}c_p} \kappa dx$$

$$\int_{T_{m,i}}^{T_m} dT_m = \frac{a \pi D}{\dot{m}c_p} \int_0^{\kappa} x dx$$

$$T_m - T_{m,i} = \frac{a \pi D}{2 \dot{m}c_p} \kappa^2$$

$$T_m = \frac{a \pi D}{2 \dot{m}c_p} \kappa^2 + T_{m,i}$$

when $T_{m,i} = 25$, $a = 400$, $\dot{m} = 0.1$, $c_p = 4178 \text{ J kg}^{-1} \text{ K}^{-1}$
 $D = 25 \times 10^{-3}$

$$T_m = \frac{400 \pi (25 \times 10^{-3})}{2(0.1)(4178)} \kappa^2 + 25$$

$$T_m = \frac{25}{2089} \pi \kappa^2 + 25$$

b) when $\kappa = 3$

$$T_{m,o} = \frac{25}{2089} \pi (23)^2 + 25$$

$$= 44.88873281 \approx 44.9^\circ \text{C}$$

$$3c) \dot{Q} = \dot{q} A_s = \dot{m} c_p (T_{m,o} - T_{m,i})$$

$$\dot{q} (25 \times 10^{-3}) (23) \pi = 0.1 (4178) (44.9 - 25)$$

$$\dot{q} = 4600 \text{ W m}^{-2}$$

4) Properties of air @ 25°C, 100 kPa:

$$\rho = 1.184 \text{ kg m}^{-3}$$

$$k = 0.02551 \text{ W m}^{-1} \text{ K}^{-1}$$

$$\nu = 1.562 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$$

$$c_p = 1007 \text{ J kg}^{-1} \text{ K}^{-1}$$

$$Pr = 0.7296$$

$$D_h = \frac{4A_c}{P}$$

$$= \frac{4(0.2 \times 14)}{2(0.2 + 14)}$$

$$= \frac{28}{71} \text{ cm}$$

$$Re_D = \frac{V_{avg} D_h}{\nu} = \frac{4\left(\frac{28}{71} \times 10^{-2}\right)}{1.562 \times 10^{-5}}$$

$$= 1009.900633 < 2300 \text{ (laminar flow)}$$

$$\frac{a}{b} = \frac{14}{0.2} = 70$$

$$Nu = 8.24 = \frac{\bar{h} D}{k} \text{ from table}$$

$$\bar{h} = \frac{Nu k}{D} = \frac{8.24 \times 0.02551}{\frac{28}{71} \times 10^{-2}}$$

$$= 53.30132286 \text{ W m}^{-2} \text{ K}^{-1}$$

$$\begin{aligned}
 4) \quad \dot{m} &= \rho U_m A_c \\
 &= 1.184(4)(0.2 \times 14 \times 10^{-4}) \\
 &= 1.32608 \times 10^{-3} \text{ kg s}^{-1}
 \end{aligned}$$

$$\dot{Q} = \dot{m} c_p (T_{m,o} - T_{m,i}) = \bar{h} A (T_{s,o} - T_{m,o})$$

$$1.32608 \times 10^{-3} (1007) (T_{m,o} - 15) = 53.3 (50 - T_{m,o}) \times (15 \times 20 \times 10^{-4})$$

$$1.33536256 T_{m,o} - 20.0304384 = -1.599039686 T_{m,o} + 79.95198429$$

$$T_{m,o} = 34.07250074^\circ\text{C}$$

$$\begin{aligned}
 \dot{Q} &= \dot{m} c_p (T_{m,o} - T_{m,i}) \\
 &= 1.32608 \times 10^{-3} (1007) (34.07 - 15) \\
 &= 25.46870341
 \end{aligned}$$

$$\begin{aligned}
 \text{Actual } T_b &= \frac{1}{2} (34.07 + 15) \\
 &= 24.53625037^\circ\text{C}
 \end{aligned}$$

\therefore The assumption is acceptable.