

Appendix 8

Computation of the inertia matrix of tree structured robots

In this appendix, we develop a method to compute efficiently the inertia matrix of tree structured robots. Note that a serial robot is a special case of the tree structured robot. This method is based on the utilization of a simplified special case of Newton-Euler algorithm and on the concept of composite links [Khalil 90b].

A8.1. Inertial parameters of a composite link

The composite link j^+ is composed of link j and of the links supported by link j (Figure A8.1). The inertial parameters of the composite link j^+ can be calculated in terms of the standard parameters (or base parameters) of its links using the following recursive algorithm:

i) initialization. For $j = 1, \dots, n$:

$${}^jJ_j^+ = {}^jJ_j, {}^jMS_j^+ = {}^jMS_j, M_j^+ = M_j$$

We recall that $a(j)$ indicates the link that is antecedent to link j ;

ii) for $j = n, \dots, 2$ and $a(j) \neq 0$:

$${}^{a(j)}J_{a(j)}^+ = {}^{a(j)}J_{a(j)}^+ + {}^{a(j)}A_j {}^jJ_j^+ {}^jA_{a(j)} - \{ {}^{a(j)}\hat{P}_j {}^{a(j)}MS_j^+ + ({}^{a(j)}\hat{P}_j {}^{a(j)}MS_j^+)^T \} + {}^{a(j)}\hat{P}_j {}^{a(j)}\hat{P}_j^T M_j^+ \quad [A8.1a]$$

$${}^{a(j)}MS_{a(j)}^+ = {}^{a(j)}MS_{a(j)}^+ + {}^{a(j)}MS_j^+ + {}^{a(j)}P_j M_j^+ \quad [A8.1b]$$

$$M_{a(j)}^+ = M_{a(j)}^+ + M_j^+ \quad [A8.1c]$$

with:

- ${}^a(j)\mathbf{MS}_j^+ = {}^a(j)\mathbf{A}_j \mathbf{jMS}_j^+$;
- $\hat{\mathbf{v}}$: (3x3) skew-symmetric matrix of the components of the vector \mathbf{v} ;
- ${}^a(j)\mathbf{T}_j = \begin{bmatrix} {}^a(j)\mathbf{A}_j & {}^a(j)\mathbf{p}_j \\ \mathbf{0}_{3,1} & 1 \end{bmatrix}$;
- \mathbf{jJ}_j^+ : inertia tensor of the composite link j^+ referred to frame R_j ;
- \mathbf{jMS}_j^+ : first moments of the composite link j^+ referred to frame R_j ;
- M_j^+ : mass of the composite link j^+ .

We note that equations [A8.1] are equivalent to the following:

$${}^a(j)\mathbf{K}_{a(j)}^+ = {}^a(j)\mathbf{K}_{a(j)}^+ + {}^a(j)\lambda_j \mathbf{jK}_j^+ \quad [\text{A8.2}]$$

where ${}^a(j)\lambda_j$ and \mathbf{jK}_j are defined in Chapters 9 and 10 and Appendix 7.

NOTE.— The relationship between the concept of composite link parameters and base inertial parameters is considered in [Khalil 90a].

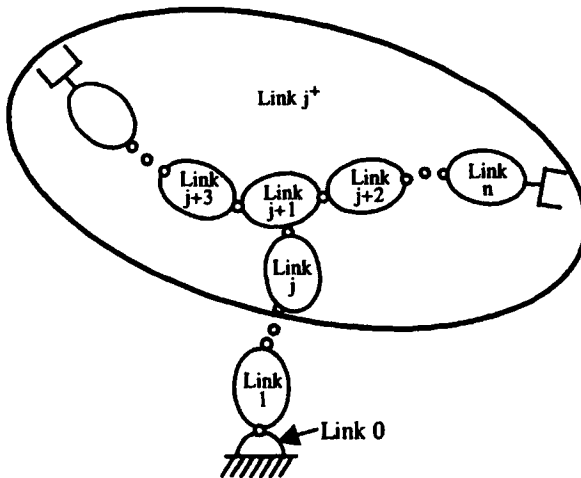


Figure A8.1. Composite link j^+

A8.2. Computation of the inertia matrix

We have seen in § 9.7.1 that the j^{th} column of the inertia matrix A can be computed by the Newton-Euler inverse dynamic algorithm by setting:

$$\ddot{\mathbf{q}} = \mathbf{u}_j, \dot{\mathbf{q}} = \mathbf{0}, \mathbf{g} = \mathbf{0}, \mathbf{F}_c = \mathbf{0} \quad (\mathbf{f}_{ei} = \mathbf{0}, \mathbf{m}_{ei} = \mathbf{0} \quad \text{for } i = 1, \dots, n)$$

where \mathbf{u}_j is an $(n \times 1)$ vector with a 1 in the j^{th} row and zeros elsewhere.

Under these conditions, the forward recursive equations of the Newton-Euler inverse dynamic (Chapter 9) are only applied to link j^+ :

$${}^k\omega_k = 0, {}^k\dot{\omega}_k = 0, {}^k\dot{V}_k = 0, {}^kF_k = 0, {}^kM_k = 0 \quad \text{for } k < j \quad [\text{A8.3}]$$

$${}^j\omega_j = 0 \quad [\text{A8.4}]$$

$${}^j\dot{\omega}_j = {}^0\sigma_j {}^j\mathbf{a}_j \quad [\text{A8.5}]$$

$${}^j\dot{V}_j = \sigma_j {}^j\mathbf{a}_j \quad [\text{A8.6}]$$

$${}^jF_j = M_j^+ {}^j\dot{V}_j + {}^j\dot{\omega}_j \times {}^jMS_j^+ \quad [\text{A8.7}]$$

$${}^jM_j = {}^jJ_j^+ {}^j\dot{\omega}_j + {}^jMS_j^+ \times {}^j\dot{V}_j \quad [\text{A8.8}]$$

We deduce that:

– if joint j is prismatic (${}^j\dot{\omega}_j = 0$, ${}^jM_j = 0$ and ${}^j\dot{V}_j = [0 \ 0 \ 1]^T$), then:

$${}^jF_j = [0 \ 0 \ M_j^+]^T \quad [\text{A8.9}]$$

$${}^jM_j = [MY_j^+ \ -MX_j^+ \ 0]^T \quad [\text{A8.10}]$$

– if joint j is revolute (${}^j\dot{V}_j = 0$ and ${}^j\dot{\omega}_j = [0 \ 0 \ 1]^T$), then:

$${}^jF_j = [-MY_j^+ \ MX_j^+ \ 0]^T \quad [\text{A8.11}]$$

$${}^jM_j = [XZ_j^+ \ YZ_j^+ \ ZZ_j^+]^T \quad [\text{A8.12}]$$

The recursive backward computation starts by link j and ends with link s , where $\mathbf{a}(s) = 0$. The algorithm is given by the following equations:

– if joint j is prismatic, then:

$${}^j\mathbf{f}_j = {}^jF_j = [0 \ 0 \ M_j^+]^T \quad [\text{A8.13}]$$

$${}^j\mathbf{m}_j = {}^j\mathbf{M}_j = [MY_j^+ \quad -MX_j^+ \quad 0]^T \quad [\text{A8.14}]$$

$$A_{jj} = M_j^+ + I_{a_j} \quad [\text{A8.15}]$$

– if joint j is revolute, then:

$${}^j\mathbf{f}_j = {}^j\mathbf{F}_j = [-MY_j^+ \quad MX_j^+ \quad 0]^T \quad [\text{A8.16}]$$

$${}^j\mathbf{m}_j = {}^j\mathbf{M}_j = [XZ_j^+ \quad YZ_j^+ \quad ZZ_j^+]^T \quad [\text{A8.17}]$$

$$A_{jj} = ZZ_j^+ + I_{a_j} \quad [\text{A8.18}]$$

Then, the following equations are computed for $k=j, a(j), a(a(j)), \dots, s$, where $a(s)=0$:

$${}^{a(k)}\mathbf{f}_{a(k)} = {}^{a(k)}A_k {}^k\mathbf{f}_k \quad [\text{A8.19}]$$

$${}^{a(k)}\mathbf{m}_{a(k)} = {}^{a(k)}A_k {}^k\mathbf{m}_k + ({}^{a(k)}\mathbf{p}_k \times {}^{a(k)}\mathbf{f}_{a(k)}) \quad [\text{A8.20}]$$

$$\Gamma_{a(k)} = A_{a(k),j} = (\sigma_{a(k)} \mathbf{f}_{a(k)} + \bar{\sigma}_{a(k)} \mathbf{m}_{a(k)})^T {}^{a(k)}\mathbf{a}_{a(k)} \quad [\text{A8.21}]$$

NOTES.–

- the element A_{ij} of the inertia matrix is set to zero if link i does not belong to the path between the base and link j ;
- this algorithm provides the elements of the lower part of the inertia matrix. The other elements are deduced using the fact that the inertia matrix A is symmetric.