ELECTRONIC WARFARE QUICK REFERENCE GUIDE Frequency (MHz) Frequency (GHz) THE ELECTROMAGNETIC SPECTRUM Wavelength (Meters) 200 300 500 1.5 2 3 4 5 6 8 10 15 20 30 40 60 80 100 200 300 400 MICROWAVE INFRARED VISIBLE **ULTRAVIOLET GAMMA RAY** U.S. Industry Standard Bands (IEEE Radar Designation) 10⁻¹² **Band** Frequency **Designation** Range 8 (VHF) 9 (UHF) 10 (SHF) 11(EHF) **HF** 3–30 MHz VHF | 30–300 MHz Frequency (Hz) UHF | 300–1,000 MHz **International Standard Bands** L 1-2 GHz S 2-4 GHz C 4–8 GHz X 8-12 GHz K_{II} 12–18 GHz K 18–27 GHz **Military Standard Bands** K_a 27–40 GHz * "u" stands for unabsorbed or under K: "a" stands for absorption region or above K V 40–75 GHz W 75–110 GHz RF Propagation RADAR HORIZON $S = \frac{P_{t_{radar}} G_{t_{radar}} G_{r} \lambda^{2}}{(4\pi)^{3} R^{4}} \sigma$ $J_{self} = P_{t_{jam}} G_{t_{jam}} \left(\frac{\lambda}{4\pi R_{jr}}\right)^{2} \frac{G_{r_{radar}}}{L_{r_{radar}}}$ $s(\tau) = e^{j2\pi(f_c\tau + \frac{1}{2}b\tau^2)}, -\frac{\tau}{2} \le \tau \le \frac{\tau}{2}$ $D_h = \sqrt{2HR_e}$ Target _ (Target Range - $\sqrt{2HRe}$)² $P_r = P_t G_t G_r \left(\frac{1}{4\pi R} \right)$ $x(\tau, t) = \int_{-\infty}^{\infty} s(t) s^*(t - \tau) e^{i2\pi ft} dt$ Height 2Re $f(x_1, x_2, ..., x_n | \theta) = f(x_1 | \theta) \times f(x_2 | \theta) \times ... \times f(x_n | \theta)$ $B_p = b\tau_p$ γ (frequency) Pt: Transmit Power Gt: Transmit Gain S(t): Complex Baseband Pulse Gr: Receive Gain τ: Time Delay R: Range Re: Earth Radius ~ 6,371 km Re: Earth Radius ~ 6,371 km $L(\theta; x_1, ..., x_n) = f(x_1, x_2, ..., x_n | \theta) = \prod_{i=1}^{n} f(x_i | \theta)$ Detection & Estimation Probabilit CRAMER RAO LOWER BOUND RF Propagation WAVELENGTH $\lambda = \frac{c}{c}$ $\frac{J}{S} = \left(\frac{EIRP_{jam}}{EIRP_{radar}}\right) \left(\frac{4\pi R^2}{\sigma}\right) \left(\frac{BW_{radar}}{BW_{jam}}\right)$ Reduction in Normalized R_{max} $CRB = \left(E\left\{\left[\frac{\partial \ln p(x,\theta)}{\partial \theta}\right]\left[\frac{\partial \ln p(x,\theta)}{\partial \theta}\right]^{T}\right\}\right)^{-1}$ $f_d = -2v_r/\lambda$ determines signal energy *Noise Power in Receiver* = $kT_sB_NN_f$ $\ln L(\theta; x_1, ..., x_n) = \sum_{i=1}^{n} \ln f(x_i | \theta)$ f Wavelength Reduction in Radar Detection Range due to JNR Reduction in Radar Detection Range due to JNR VHF100 MHz 3.00 m s(): Transmitted Signal Waveform X-band S-band 0.10mf.: Center Frequency kT_s : = -174 dBm **Velocity** 300 m/s 300 m/s τ: Range Time (fast time) *K*: Boltzmann's constant = $1.38*10^{-23}$ J/K 6GHz 0.05mτ_p: Pulse Length B_n : Noise Bandwidth Wavelength 0.03 m 0.1 m 10GHz b: Chirp Rate **Doppler Shift** 20 kHz 6 kHz B_p: Pulse Bandwidth p: Probability distribution function (or joint) T_s usually set to $T_0 = 290K$ N_f : Noise figure of receiver c: Speed Average Log-Likelihood γ̂: Range Frequency θ : Distribution parameters can be vectors f: Frequency $\hat{\ell} = \frac{1}{n} \ln L$ Burn- through range for SNR = 13 dB $\hat{\ell} = (\theta | x) = \frac{1}{n} \sum_{i=1}^{n} \ln f(x_i | \theta)$ 10 15 20 25 30 35 40 Speed of Light (approx) Units Jammer to Noise Ratio (dB) ----- Rmax Jammed $p(r) = \begin{cases} \frac{r}{\sigma^2} e^{-r} \end{cases}$ Range (km) $\int_{-\infty}^{+\infty} |x(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{+\infty} |X(\omega)|^2 d\omega$ $\begin{array}{cccc} \sigma = 0.5 & & \\ \sigma = 1 & & \\ \sigma = 2 & & \\ \sigma = 3 & & \\ \sigma = 4 & & \\ \end{array}$ *3x10*^8 m/sec $f(k; n, p) = Pr(X = k) = \binom{n}{k} p^k (1-p)^{n-k}$ $L_{r_{radar}}$: Radar Receiver Losses $P_{t_{radar}}$: Radar Transmit Power J_{self}: Self Protect Jammer Power R_{max}: Max Radar Range 300 m/usec J/N: Jammer to Noise Ratio J/S: Jam to Signal Ratio at Radar Receiver G_{t_{radar}: Radar Transmitter Gain} S: Radar Received Signal Power N: Total Noise NM/sec 1.62x10^5 $(r < 0) \quad (0 \le r \le \infty)$ $\frac{1}{T_o} \int_{T_o} |\tilde{x}(t)|^2 dt = \sum_{k=-\infty}^{+\infty} |a_k|^2$ P_{tiam}: Jammer Transmit Power σ: Radar Target Radar Cross Section k: Boltzmann's constant Ft/sec $G_{t_{iam}}$: Jammer Transmit Gain BW_{Radar}: Radar Transmit Bandwidth T_s: Receiver Temperature 1x10^9 BW_{Jam}: Jammer Transmit Bandwidth B_N: Receiver Noise Bandwidth R_{ir}: Range between Jammer and Radar 1x10^3 Ft/usec n: Number of Samples R: Range between Radar Target and Radar J: Jammer Power SNR: Radar Signal to Noise Ratio p: Success probability of each trial σ: Standard Difference f: Is one, or joint, probability distribution(s) λ : Jammer Transmit Wavelength $G_{r_{radar}}$: Radar Receiver Gain $Rmax_{jammed} : Jammed\ Radar\ Range$ N_f : Receiver Noise Figure (>1) k: Number of successes A: Distance between the reference point and θ: Distribution parameters can be vectors (Burn through Range) the center of the bivariate distribution Fourier Relationships CONTINUOUS-TIME FOURIER TRANSFORMATION Fourier Relationships MODULATION PROPERTY Detection & Estimation Probabilit ERROR FUNCTIONS Duality Property $erfc(z)=1-erf(z)=\frac{2}{\sqrt{\pi}}\int_{z}^{\infty}e^{-t^{2}}dt$ Standard Normal Curve $x(t) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(\omega) e^{j\omega t} d\omega \qquad X(\omega) = \int_{-\infty}^{+\infty} x(t) e^{-j\omega t} dt$ for $(A \ge 0, r \ge 0)$ $(\mu_z = 0; \sigma_x = 1.0)$ $2\frac{\sin wt}{2\pi t}$ $s(t) p(t) \gtrsim \frac{1}{2\pi} [S(\omega)P(\omega)]$ PRF $x(t) \stackrel{\mathcal{F}}{\leftrightarrow} X(\omega)$ 100 kHz 1.5 km $erf(z) = \frac{2}{\sqrt{\pi}} \int_0^z e^{-t^2} dt$ 25 kHz 6 km 10 kHz 15 km $h(t) * x(t) \stackrel{\mathcal{F}}{\Leftrightarrow} H(\omega)X(\omega)$ ± 1 - σ : $P(-1 \le z \le 1) = 0.6827$ $\sigma = 1.00$ v = 0.0 v = 0.5 v = 1.0 ± 2 - σ : $P(-2 \le z \le 2) = 0.9545$ c: Speed of Light PRF: Pulse Repetition Frequency ± 3 - σ : $P(-3 \le z \le 3) = 0.9973$ Time Shifting $x(t-t_0) \overset{\mathcal{F}}{\iff} e^{-j\omega t_0} X(\omega)$ v = 2.0 - v = 4.0 - $\frac{dx(t)}{dt} \mathcal{F} j\omega X(\omega)$ $SNR = \frac{P_{R}}{N_{o}} = \frac{P_{t}G_{t}G_{r}\sigma\lambda^{2}G_{p}L}{(4\pi)^{3}R^{4}k_{B}T_{s}B_{n}N_{f}}$ **↑** 68.27% → **↑** 1-σ Ideal Lowpass Filter Differentiator **- 95.45% --** $\int_{-\infty}^{t} x(\tau)d\tau \stackrel{\mathcal{T}}{\Leftrightarrow} \frac{1}{j\omega} X(\omega) + \pi X(0) \delta(\omega)$ $y(t) = \frac{dx(t)}{dt} = >H(\omega) = j\omega$ Pr: Received Power | |*H*(ω)| Pt: Transmit Power *K*: *Boltzmann's constant* = $1.38*10^{-23}$ J/K Gt: Transmit Gain $ax_{1}(t)+bx_{2}(t) \overset{\mathcal{F}}{\longleftrightarrow} aX_{1}(\omega)+bX_{2}(\omega)$ σ: Standard Difference Gr: Receive Gain B_n : Noise Bandwidth A: Distance between the reference point and σ: Standard Difference σ: Standard Difference R: Range T: System Noise Temperature A: Distance between the reference point and No: Noise Power T_s usually set to $T_0 = 290K$ A: Distance between the reference point and the center of the bivariate distribution N_f: Noise figure of receiver the center of the bivariate distribution the center of the bivariate distribution I .: Bessel Function of the first kind with order zero Convolution Property $h(t) * x(t) \lesssim H(\omega) X(\omega)$ Antennas ANTENNA DIRECTIVITY $= rac{Reflected Power to Receiver / Solid Angle}{Incident Power Density / <math>4\pi$ Phased Array, Radians $\theta_{BW_{3dB}} \sim 0.886 \frac{\lambda}{Nd \cos \theta_0} b$ $D \approx 4\pi \frac{\left(\frac{180}{\pi}\right)^2}{\theta_{1d}\theta_{2d}} \approx \frac{40000}{\theta_{1d}\theta_{2d}}$ $G_{ant} = \frac{4\pi A_e}{\lambda^2}$ $\begin{array}{c|c} e^{j\omega_{o}t} & e^{j\omega_{o}t} H(\omega_{o}) \\ \hline \end{array}$ $\theta_{BW_{null}} \sim 1.22 \frac{\lambda}{d} \quad \theta_{BW_{3dB}} \sim 0.88 \frac{\lambda}{d}$ P_r or SFighter Aircraft Radar Cross Section (RCS, σ) θ_{1d} : Half-power beamwidth in one principal plane (degrees) A_e: Effective Aperture Area λ: Wavelength H(ω): Frequency Response θ_{2d} . Half-power beamwidth in the other principal plane (degrees) d: Antenna Diameter *: Convolution operation

RF Propagation Detection & Estimation Probability Antennas Electronic Warfare Fourier Relationships Radar Processing