

1. A car hits a tree at an estimated speed of 35 mi/h on a 3% downgrade. If skid marks of 100 ft are observed on dry pavement (F=0.45), followed by 250 ft (F=0.20) on a grass-stabilized shoulder, estimate the initial speed of the vehicle just before the pavement skid was begun.

Solution:

$$d_b(\text{shoulder}) = \frac{S^2(\text{shoulder}) - S^2(\text{hit})}{30(F(\text{shoulder}) - 0.01G)}$$

$$S^2(\text{shoulder}) = 250 * 30 * (0.20 - 0.03) + 35 * 35(\text{mi/h})^2 = 2500 (\text{mi/h})^2$$

$$d_b(\text{pavement}) = \frac{S^2(\text{pavement}) - S^2(\text{shoulder})}{30(F(\text{pavement}) - 0.01G)}$$

$$S(\text{pavement}) = \sqrt{100 * 30 * (0.45 - 0.03) + 2500} = 61.32 (\text{mi/h})$$

2. What is the safe stopping distance for a section of rural freeway with a design speed of 80 mi/h on a 4% upgrade?

Solution:

$$d_r = 1.47 * S * t$$

$$d_b = \frac{S^2}{30(0.348 + 0.01G)}$$

$$d = d_r + d_b = 1.47 * 80 * 2.5 + \frac{80^2}{30 * (0.348 + 0.04)} \text{ ft} = 294 + 549.83 \text{ ft} = 843.83 (\text{ft})$$

3. A highway reconstruction project is being undertaken to reduce accident rates. The reconstruction involves a major realignment of the highway such that a 60-mph design speed is attained. At one point on the highway, an 800-ft equal tangent crest vertical curve exists. Measurements show that, at 3 + 52 stations from the PVC, the vertical curve offset is 3 ft. Assess the adequacy of the existing curve in light of the reconstruction design speed of 60 mph and, if the existing curve is inadequate, compute a satisfactory curve length. (Consider both minimum and desirable SSDs.)

Solution:

For minimum SSD, the assumed average running speed is 52 mph from Table 3.1. The coefficient of friction is 0.29 from Table 3.1.

$$g = 32.2 \text{ ft/s}^2$$

$$t_r = 2.5 \text{ s}$$

$$Y = \frac{A}{200L} x^2, 3 = \frac{A}{200 * 800} 352^2, A = 3.87$$

$$SSD = \frac{v_1^2}{2g(f-G)} + v_1 t_r = \frac{(52 * 1.47)^2}{2 * 32.2 * (0.29 - 0.0387)} + 52 * 1.47 * 2.5 \text{ ft} = 552.15 \text{ ft}$$

$$SSD < L, L_m = \frac{A(SSD)^2}{1329} = \frac{3.87 * (552.15)^2}{1329} \text{ ft} = 887.77 \text{ ft}$$

Since 887.77 > 552.15, the assumption that SSD < L is valid.

For desirable SSD, the initial vehicle speed is assumed to be equal to the highway's design speed.

$$SSD = \frac{v_1^2}{2g(f-G)} + v_1 t_r = \frac{(60 \cdot 1.47)^2}{2 \cdot 32.2 \cdot (0.29 - 0.0387)} + 60 \cdot 1.47 \cdot 2.5 \text{ ft} = 701.18 \text{ ft}$$

$$SSD < L, L_m = \frac{A(SSD)^2}{1329} = \frac{3.87 \cdot (701.18)^2}{1329} \text{ ft} = 1431.68 \text{ ft}$$

Since $1431.68 > 701.18$, the assumption that $SSD < L$ is satisfied.

4. A horizontal curve is being designed through mountainous terrain for a four-lane road with 10-ft lanes. The central angle (Δ) is known to be 40° ; the tangent distance is **510 ft**; and the stationing of the tangent intersection (PI) is $2700 + 00$. If the roadway surface has a coefficient of side friction of **0.082** and a superelevation of **0.09** ft/ft, determine the design speed and the stationing of the PC and PT.

Solution:

$$T = R \cdot \tan(\Delta/2), 510 = R \cdot \tan(40 \cdot 3.14/180/2), R = 1401.99 \text{ ft}$$

$$D = 5729.6/R, L = 100\Delta/D = 100\Delta R/5729.6, L = 100 \cdot 40 \cdot 1401.99/5729.6 \text{ ft} = 978.77 \text{ ft}$$

$$\text{design speed } S = \sqrt{15R(0.01e + f)} = \sqrt{15 \cdot 1401.99 \cdot (0.09 + 0.082)} \text{ mi/h} = 60.14 \text{ mi/h}$$

$$\text{stationing PC} = 2700 + 00 - (5 + 10) = 2694 + 90$$

$$\text{stationing PT} = \text{stationing PC} + L = 2694 + 90 + 9 + 78.77 = 2704 + 68.77$$

5. A developer is having a single-lane raceway constructed with a **100-mph** design speed. A curve on the raceway has a radius of **1000 ft**, a central angle of **30** degrees, and PI stationing at **1125 + 10**. If the design coefficient of side friction is **0.2**, determine the superelevation required at the design speed. Also, compute the degree of curve, length of curve, and stationing of the PC and PT?

Solution:

$$S = \sqrt{15R(0.01e + f)}, 100 = \sqrt{15 \cdot 1000 \cdot (0.01e + 0.2)}, e = 46.7$$

$$\text{superelevation} = 0.467 \text{ ft/ft}$$

$$T = R \cdot \tan(\Delta/2), T = 1000 \cdot \tan(30 \cdot 3.14/180/2) \text{ ft}, T = 267.81 \text{ ft}$$

$$\text{stationing PC} = 1125 + 10 - (2 + 67.81) = 1122 + 42.19$$

$$\text{length of curve } L = 100\Delta/D = 100\Delta R/5729.6, L = 100 \cdot 30 \cdot 1000/5729.6 \text{ ft} = 523.60 \text{ ft}$$

$$\text{stationing PT} = \text{stationing PC} + L = 1122 + 42.19 + 5 + 23.60 = 1127 + 65.79$$

6. Find the minimum length of curve for the following scenarios:

Entry Grade	Exit Grade	Design Speed	Reaction Time
3%	7%	55mi/h	2.5s
-5%	2%	60mi/h	2.5s
2%	-3%	70mi/h	2.5s

Solution:

Consider desirable SSD:

①

$$SSD = \frac{v_1^2}{2g(f+G)} + v_1 t_r = \frac{(55 \cdot 1.47)^2}{2 \cdot 32.2 \cdot (0.30 + 0.03)} + 55 \cdot 1.47 \cdot 2.5 \text{ ft} = 509.71 \text{ ft}$$

$$L_m = 2SSD - \frac{1329}{A} = 2 \cdot 509.71 - \frac{1329}{4} \text{ ft} = 687.17 \text{ ft (SSD > L is unsatisfied)}$$

$$L_m = \frac{A(SSD)^2}{1329} = \frac{4 \cdot (509.71)^2}{1329} \text{ ft} = 781.95 \text{ ft (SSD < L is satisfied)}$$

$$L_m = 781.95 \text{ ft}$$

②

$$SSD = \frac{v_1^2}{2g(f-G)} + v_1 t_r = \frac{(60 \cdot 1.47)^2}{2 \cdot 32.2 \cdot (0.29 - 0.05)} + 60 \cdot 1.47 \cdot 2.5 \text{ ft} = 723.82 \text{ ft}$$

$$L_m = 2SSD - \frac{1329}{A} = 2 \cdot 723.82 - \frac{1329}{7} \text{ ft} = 1257.78 \text{ ft (SSD > L is unsatisfied)}$$

$$L_m = \frac{A(SSD)^2}{1329} = \frac{7 \cdot (723.82)^2}{1329} \text{ ft} = 2759.52 \text{ ft (SSD < L is satisfied)}$$

$$L_m = 2759.52 \text{ ft}$$

③

$$SSD = \frac{v_1^2}{2g(f-G)} + v_1 t_r = \frac{(70 \cdot 1.47)^2}{2 \cdot 32.2 \cdot (0.28 - 0.03)} + 70 \cdot 1.47 \cdot 2.5 \text{ ft} = 914.92 \text{ ft}$$

$$L_m = 2SSD - \frac{1329}{A} = 2 \cdot 914.92 - \frac{1329}{5} \text{ ft} = 1564.04 \text{ ft (SSD > L is unsatisfied)}$$

$$L_m = \frac{A(SSD)^2}{1329} = \frac{5 \cdot (914.92)^2}{1329} \text{ ft} = 3149.28 \text{ ft (SSD < L is satisfied)}$$

$$L_m = 3149.28 \text{ ft}$$

Consider minimum SSD:

①

$$SSD = \frac{v_1^2}{2g(f+G)} + v_1 t_r = \frac{(48 \cdot 1.47)^2}{2 \cdot 32.2 \cdot (0.30 + 0.03)} + 48 \cdot 1.47 \cdot 2.5 \text{ ft} = 410.67 \text{ ft}$$

$$L_m = 2SSD - \frac{1329}{A} = 2 \cdot 410.67 - \frac{1329}{4} \text{ ft} = 489.09 \text{ ft (SSD > L is invalid)}$$

$$L_m = \frac{A(SSD)^2}{1329} = \frac{4 \cdot (410.67)^2}{1329} \text{ ft} = 507.60 \text{ ft (SSD < L is valid)}$$

$$L_m = 507.60 \text{ ft}$$

②

$$SSD = \frac{v_1^2}{2g(f-G)} + v_1 t_r = \frac{(52 \cdot 1.47)^2}{2 \cdot 32.2 \cdot (0.29 - 0.05)} + 52 \cdot 1.47 \cdot 2.5 \text{ ft} = 569.15 \text{ ft}$$

$$L_m = 2SSD - \frac{1329}{A} = 2 \cdot 569.15 - \frac{1329}{7} \text{ ft} = 948.44 \text{ ft (SSD > L is invalid)}$$

$$L_m = \frac{A(SSD)^2}{1329} = \frac{7 \cdot (569.15)^2}{1329} \text{ ft} = 1706.19 \text{ ft (SSD < L is valid)}$$

$$L_m = 1706.19 \text{ ft}$$

③

$$SSD = \frac{v_1^2}{2g(f-G)} + v_1 t_r = \frac{(58 * 1.47)^2}{2 * 32.2 * (0.28 - 0.03)} + 58 * 1.47 * 2.5 \text{ ft} = 664.66 \text{ ft}$$

$$L_m = 2SSD - \frac{1329}{A} = 2 * 664.66 - \frac{1329}{5} \text{ ft} = 1063.52 \text{ ft (SSD > L is invalid)}$$

$$L_m = \frac{A(SSD)^2}{1329} = \frac{5 * (664.66)^2}{1329} \text{ ft} = 1662.05 \text{ ft (SSD < L is valid)}$$

$$L_m = 1662.05 \text{ ft}$$