

PHY3110 SP23 Notes

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0 Introduction

Grading: 30% homework, 30% midterm, 40% final.

Textbooks:

- H. Goldstein, C. Poole, J. Safko, Classical Mechanics, 3rd Edition, Pearson.
- J.R. Taylor, Classical Mechanics, University Science Books.
- T.W.B. Kibble, F.H. Berkshire, Classical Mechanics, 5th Edition, Imperial College Press.
- 梁昆森, 力学 (下册) 理论力学, 4th Edition, 高等教育出版社.

Classical mechanics describe the motion of macroscopic objects, which are not extremely massive and not extremely fast.

1 Newtonian Mechanics

Vectorial quantities of motion: position \mathbf{r} , velocity \mathbf{v} , force \mathbf{F} , momentum $\mathbf{p} = m\mathbf{v}$, angular momentum $\mathbf{L} = \mathbf{r} \times \mathbf{p}$. Equations of motion are derived from those vector quantities.

Analytical mechanics uses scalar quantities of motion

- Kinetic energy $T = \frac{1}{2}m\mathbf{v}^2$
- Potential energy $V = V(\mathbf{r})$

Equations of motion are derived from those scalar quantities.

1.1 Newton's Laws

Theorem 1.1 (Newton's 2nd law).

$$\mathbf{F} = \frac{d\mathbf{p}}{dt} = m\mathbf{a} \quad (1)$$

The formula is valid in an inertial frame.

Angular momentum \mathbf{L} and torque \mathbf{N} are also related

$$\frac{d\mathbf{L}}{dt} = \frac{d}{dt}(\mathbf{r} \times \mathbf{p}) = \mathbf{r} \times \mathbf{F} = \mathbf{N} \quad (2)$$

Work done by external forces (note that $d\mathbf{s} = \mathbf{v} dt$)

$$W_{12} = \int_1^2 \mathbf{F} d\mathbf{s} = \int_1^2 m \frac{d\mathbf{v}}{dt} d\mathbf{s} = \int_1^2 m\mathbf{v} d\mathbf{v} = \frac{1}{2}m\mathbf{v}^2 \Big|_1^2 \quad (3)$$

Define a scalar function $V(\mathbf{r})$, then $\mathbf{F} = -\nabla V(\mathbf{r})$ is a conservative force.

$$\oint \mathbf{F} d\mathbf{s} = 0 \quad (4)$$

Center of mass of the system

$$\mathbf{R} = \frac{\sum_i m_i \mathbf{r}_i}{\sum_i m_i} = \frac{\sum_i m_i \mathbf{r}_i}{M} \quad (5)$$

Total momentum

$$\mathbf{P} = \sum_i m_i \mathbf{p}_i = M \dot{\mathbf{R}} \quad (6)$$

Hence \mathbf{P} is conserved if external force $\mathbf{F}^{(e)}$ is zero.

Total angular momentum

$$\frac{d\mathbf{L}}{dt} = \frac{d}{dt} \sum_i \mathbf{r}_i \times \mathbf{p}_i = \sum_i \mathbf{r}_i \times \left(\mathbf{F}_i^{(e)} + \sum_j \mathbf{F}_{ij} \right) = \sum_i \mathbf{r}_i \times \mathbf{F}_i^{(e)} + \sum_{ij} \mathbf{r}_i \times \mathbf{F}_{ij}$$

Since \mathbf{r}_{ij} parallel to \mathbf{F}_{ij} , then

$$\sum_{ij} \mathbf{r}_i \mathbf{F}_{ij} = \frac{1}{2} \sum_{ij} \mathbf{r}_{ij} \times \mathbf{F}_{ji} = 0 \quad (7)$$

Therefore

$$\frac{d\mathbf{L}}{dt} = \mathbf{N}^{(e)} \quad (8)$$

Decomposition of the angular momentum

$$\mathbf{L} = \sum_i \mathbf{r}_i \times \mathbf{p}_i = \sum_i (\mathbf{R} + \mathbf{r}_i) \times m_i (\mathbf{V} + \mathbf{v}'_i) = \sum_i \mathbf{R} \times m_i \mathbf{V} + \sum_i \mathbf{r}'_i \times m_i \mathbf{v}'_i \quad (9)$$

1.2 Constraints

Holonomic constraint

$$f(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N, t) = 0 \quad (10)$$

Example: rigid body

$$(\mathbf{r}_i - \mathbf{r}_j)^2 - c_{ij}^2 = 0 \quad (11)$$

Example: non-sliding cylinder

$$\dot{x} - R\dot{\theta} = 0 \Rightarrow x - R\theta = \text{const}$$

A constraint of the form

$$\sum_i g_i(\mathbf{x}_1, \mathbf{x}_2, \dots, \mathbf{x}_n) d\mathbf{x}_i = 0 \Rightarrow dG(\mathbf{x}_1, \dots) = 0 \Rightarrow G(\mathbf{x}_1, \dots) = \text{const} \quad (12)$$

Non-holonomic constraint: cannot be written in the form of holonomic constraint.

1.3 Generalized coordinates

Suppose we have a N -particle system, we will have $3N$ DOFs. With k constraints, we will have $3N - k$ DOFs. Define q_1, \dots, q_{3N-k} generalized coordinates, we have

$$\mathbf{r}_i = \mathbf{r}_i(q_1, \dots, q_{3N-k}, t) \quad (13)$$

2 Lagrange Formalism

2.1 D'Alembert's Principle

Hint from the rigid body: internal forces of constraints do not work.

Virtual displacement: $\delta \mathbf{r}_i$ is consistent with the constraints imposed on the system at a given time

$$\mathbf{r}_i \rightarrow \mathbf{r}_i + \delta \mathbf{r}_i \quad (1)$$

Theorem 2.1 (D'Alembert's principle). Consider a system in equilibrium

$$\mathbf{F}_i = 0 \Rightarrow \sum_i \mathbf{F}_i \cdot \delta \mathbf{r}_i = 0 \quad (2)$$

Separate $\mathbf{F}_i = \mathbf{F}_i^{(a)} + \mathbf{f}_i$ where \mathbf{f}_i is the constraint force. Hence

$$\sum_i (\mathbf{F}_i^{(a)} + \mathbf{f}_i) \cdot \delta \mathbf{r}_i = 0 \Rightarrow \sum_i \mathbf{F}_i^{(a)} \cdot \delta \mathbf{r}_i = 0 \quad (3)$$

For a system moving under external forces

$$\mathbf{F}_i - \dot{\mathbf{p}}_i = 0 \Rightarrow \sum_i (\mathbf{F}_i - \dot{\mathbf{p}}_i) \delta \mathbf{r}_i = 0 \Rightarrow \sum_i (\mathbf{F}_i^{(a)} - \dot{\mathbf{p}}_i) \delta \mathbf{r}_i = 0 \quad (4)$$

For holonomic constraints

$$\mathbf{r}_i = \mathbf{r}_i(q_1, \dots, q_n, t), \quad \mathbf{v}_i = \frac{d\mathbf{r}_i}{dt} = \frac{\partial \mathbf{r}_i}{\partial t} + \sum_j \frac{\partial \mathbf{r}_i}{\partial q_j} \dot{q}_j, \quad \delta \mathbf{r}_i = \sum_j \frac{\partial \mathbf{r}_i}{\partial q_j} \delta q_j \quad (5)$$

Define generalized force Q_j

$$\sum_i \mathbf{F}_i \delta \mathbf{r}_i = \sum_{ij} \mathbf{F}_i \frac{\partial \mathbf{r}_i}{\partial q_j} \delta q_j = \sum_j Q_j \delta q_j \quad (6)$$

Then

$$\sum_i \dot{\mathbf{p}}_i \cdot \delta \mathbf{r}_i = \sum_{ij} m_i \ddot{\mathbf{r}}_i \cdot \frac{\partial \mathbf{r}_i}{\partial q_j} \delta q_j = \sum_{ij} \left[\frac{d}{dt} \left(m_i \dot{\mathbf{r}}_i \cdot \frac{\partial \mathbf{r}_i}{\partial q_j} \right) - m_i \dot{\mathbf{r}}_i \cdot \frac{d}{dt} \frac{\partial \mathbf{r}_i}{\partial q_j} \right] \delta q_j \quad (7)$$

$$= \sum_j \left[\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_j} \right) - \frac{\partial T}{\partial q_j} \right] \delta q_j = \sum_j Q_j \delta q_j \quad (8)$$

$$(9)$$

where

$$\frac{\partial T}{\partial q_j} = \sum_{ik} \frac{\partial \dot{\mathbf{r}}_k}{\partial q_j} \frac{\partial}{\partial \dot{\mathbf{r}}_k} T = \sum_k m_k \dot{\mathbf{r}}_k \frac{\partial \dot{\mathbf{r}}_k}{\partial q_j} = \sum_k m_k \dot{\mathbf{r}}_k \frac{d}{dt} \frac{\partial \mathbf{r}_k}{\partial q_j} \quad (10)$$

Hence $\forall j$ we have

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_j} \right) - \frac{\partial T}{\partial q_j} - Q_j = 0 \quad (11)$$

Let the potential energy $V = V(\mathbf{r}_i, \dots) = V(q_j, \dots)$, then we have

$$Q_j = \sum_i \mathbf{F}_i \frac{\partial \mathbf{r}_i}{\partial q_j} = \sum_i -\nabla_i V \frac{\partial \mathbf{r}_i}{\partial q_j} = -\frac{\partial V}{\partial q_j} \quad (12)$$

Therefore

$$\frac{d}{dt} \left(\frac{\partial(T-V)}{\partial \dot{q}_j} \right) - \frac{\partial(T-V)}{\partial q_j} - Q_j = 0 \quad (13)$$

Theorem 2.2 (Lagrange's equation). Define $L = T - V$, then

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_j} \right) - \frac{\partial L}{\partial q_j} = 0 \quad (14)$$

The choice of Lagrangian is not unique, L' where

$$L' = L + \frac{dF(q, t)}{dt} \quad (15)$$

will give the same equations of motion as L .

Example 2.1 (Lagrange's formalism).

1) For a single particle moving under force \mathbf{F}

$$L(\mathbf{x}, \dot{\mathbf{x}}, t) = \frac{1}{2} m \dot{\mathbf{x}}^2 + \mathbf{F} \cdot \mathbf{x}$$

2) Motion in a 2D plane using polar coordinates

$$L(r, \theta, \dot{r}, \dot{\theta}, t) = \frac{1}{2} m (\dot{r}^2 + r^2 \dot{\theta}^2) + \mathbf{F} \cdot \mathbf{r}$$

Generalized forces

$$Q_r = \mathbf{F} \cdot \frac{\partial \mathbf{r}}{\partial r} = \mathbf{F} \cdot \mathbf{e}_r$$

$$Q_\theta = \mathbf{F} \cdot \frac{\partial \mathbf{r}}{\partial \theta} = \mathbf{F} \cdot r \mathbf{e}_\theta$$

where

$$\mathbf{e}_r = \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix} \quad \mathbf{e}_\theta = \begin{bmatrix} -\sin \theta \\ \cos \theta \end{bmatrix}$$

Equations of motion

$$m\ddot{r} - mr\dot{\theta}^2 = \mathbf{F} \cdot \mathbf{e}_r$$

$$mr^2\ddot{\theta} + 2mr\dot{r}\dot{\theta} = r\mathbf{F}_\theta$$

3) Atwood's machine

$$L = \frac{1}{2} (M_1 + M_2) \dot{x}^2 + M_1 g x + M_2 g (l - x)$$

The equation of motion is

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{x}} - \frac{\partial L}{\partial x} = 0$$

$$\Rightarrow (M_1 + M_2) \ddot{x} = (M_1 - M_2) g$$

Suppose we have a potential dependent on velocity (generalized potential) and the generalized force is defined as

$$U = U(q_j, \dot{q}_j), \quad Q_j = -\frac{\partial U}{\partial q_j} + \frac{d}{dt} \frac{\partial U}{\partial \dot{q}_j} \quad (16)$$

Define $L = T - U$, then we still have

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{q}_j} - \frac{\partial L}{\partial q_j} = 0 \quad (17)$$

Example 2.2 (Lorentz force on a moving charge). The Lorentz force

$$\mathbf{F} = q(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

Define the scalar and vector potentials

$$\mathbf{E} = -\nabla\phi - \frac{\partial \mathbf{A}}{\partial t}, \quad \mathbf{B} = \nabla \times \mathbf{A}$$

Hence

$$\mathbf{F} = q \left[-\nabla\phi - \frac{\partial \mathbf{A}}{\partial t} + \mathbf{v} \times (\nabla \times \mathbf{A}) \right]$$

2.2 Hamilton's principle, variational principle

Configuration space: a space formed by the set of generalized coordinates.

$$(q_1, q_2, \dots, q_n) \text{ as function of } t \quad (18)$$

Theorem 2.3 (Hamilton's principle). Define the action integral I , where $L = T - V$ or $L = T - U$ (U is the generalized potential)

$$I = \int_{t_1}^{t_2} L dt \quad (19)$$

Then the variation of the action integral equals to zero

$$\delta I = \delta \int_{t_1}^{t_2} L(q_1, \dots, q_n, \dot{q}_1, \dots, \dot{q}_n) dt = 0 \quad (20)$$

Add small variation on the path

$$q_i(t, \alpha) = q_i(t) + \alpha \eta(t) \quad (21)$$

where $\eta(t_1) = \eta(t_2) = 0$. Then the action will be the function of α , $I = I(\alpha)$. Hence

$$\delta I = \int_{t_1}^{t_2} \left(\sum_i \frac{\partial L}{\partial q_i} \delta q_i + \frac{\partial L}{\partial \dot{q}_i} \delta \dot{q}_i \right) dt \quad (22)$$

Change the order of differentiation $\delta \dot{q}_i = d\delta q_i / dt$, then

$$\delta I(\alpha) = \int_{t_1}^{t_2} \sum_i \left[\frac{\partial L}{\partial q_i} \delta q_i - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) \delta q_i \right] dt + \sum_i \frac{\partial L}{\partial \dot{q}_i} \delta q_i \Big|_{t_1}^{t_2} \quad (23)$$

$$= \int_{t_1}^{t_2} \sum_i \left[\frac{\partial L}{\partial q_i} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) \right] \delta q_i dt = 0 \quad (24)$$

$$\Rightarrow \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q_i} = 0 \quad (25)$$

Example 2.3 (Shortest path problem). $y = y(x)$, $ds = \sqrt{dx^2 + dy^2}$, then the action integral (path) is

$$I = \int_1^2 ds = \int_1^2 \sqrt{1 + \dot{y}^2} dx \quad (26)$$

Apply the Lagrange's equation we get

$$\frac{d}{dx} \frac{d\sqrt{1 + \dot{y}^2}}{d\dot{y}} = 0 \Rightarrow \frac{d\dot{y}}{dx} = 0 \Rightarrow y = ax + b \quad (27)$$

Example 2.4 (Solid of revolution). Differential of area $2\pi x ds = 2\pi x \sqrt{1 + \dot{y}^2} dx$, then the total area is

$$\int_1^2 2\pi x \sqrt{1 + \dot{y}^2} dx \quad (28)$$

Define the Lagrangian $L(x, y, \dot{y}) = 2\pi x \sqrt{1 + \dot{y}^2}$, by Lagrange's equation we can get

$$\frac{x\dot{y}}{\sqrt{1 + \dot{y}^2}} = \text{const} \Rightarrow y = a \cosh^{-1} \frac{x}{a} + b \quad (29)$$

Example 2.5 (The curve of fastest descent). Question: along which trajectory from point 1 to point 2, the time is shortest? The total time is

$$T = \int_1^2 \frac{ds}{v} = \int_1^2 \frac{ds}{\sqrt{2gy}} \quad (30)$$

According to Newton's laws we have $y = gv^2$, then

$$T = \int_1^2 \frac{\sqrt{1 + \dot{y}^2}}{\sqrt{2gy}} dx \quad (31)$$

Then we have $L(x, y, \dot{y})$ and we get

$$2y\ddot{y} + 1 + \dot{y}^2 = 0 \quad (32)$$

$$\Rightarrow 2y\dot{y}\ddot{y} + \dot{y} + \dot{y}^3 = \dot{y}(1 + \dot{y}^2) + y(2\dot{y}\ddot{y}) = \frac{d}{dt} \dot{y}(1 + \dot{y}^2) = 0 \quad (33)$$

$$\Rightarrow y(1 + \dot{y}^2) = \text{const} \quad (34)$$

which means that $y(1 + \dot{y}^2) = \text{const}$. The solution is $x = A(\theta - \sin \theta)$, $y = A(1 - \cos \theta)$.

2.3 Constraint

Holonomic constraints

$$f(q_1, \dots, q_n, t) = 0 \quad (35)$$

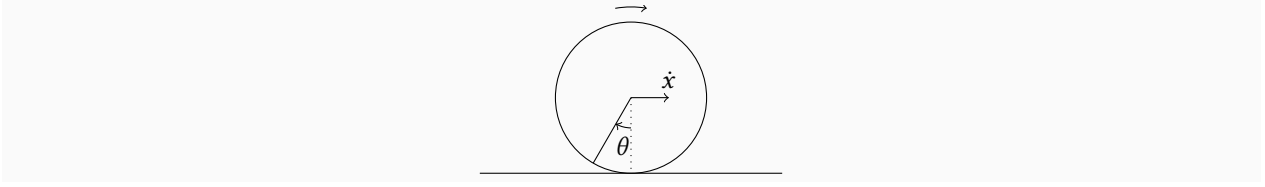
Non-holonomic constraints

$$f(q_1, \dots, q_n; \dot{q}_1, \dots, \dot{q}_n; t) = 0 \quad (36)$$

Sometimes we can convert $f(\dot{q}_i) = 0$ to $f'(q_i) = 0$.

Example 2.6 (Rolling cylinder). Rolling cylinder without sliding has the constraint

$$\dot{x} - R\dot{\theta} = 0 \Rightarrow x - R\theta = \text{const} \quad (37)$$



A commonly encountered type of non-holonomic constraint is linear constraint equations

$$\sum_{k=1}^n a_{ik} \frac{dq_k}{dt} + a_{it} = 0 \quad (38)$$

For the virtual displacement δq_i

$$\sum_{k=1}^n a_{ik} \delta q_k = 0 \quad (39)$$

Suppose q_i are not independent, then the Euler-Lagrange's equation could not hold.

$$\int_{t_1}^{t_2} \sum_i \left[\frac{\partial L}{\partial q_i} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) \right] \delta q_i dt = 0 \Rightarrow \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q_i} = 0$$

Include the constraint equation of q_i into the equation

$$\sum_{k=1}^n a_{ik} \delta q_k = 0 \Rightarrow \sum_{i=1}^m \lambda_i \sum_{k=1}^n a_{ik} \delta q_k = 0 \quad (40)$$

Hence

$$\int_{t_1}^{t_2} \sum_{k=1}^n \left[\frac{\partial L}{\partial q_k} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_k} \right) + \sum_{i=1}^m \lambda_i a_{ik} \right] \delta q_k dt = 0$$

Let q_1, \dots, q_{n-m} be independent generalized coordinate, q_{n-m+1}, \dots, q_n dependent generalized coordinates (i.e., they can be expressed by q_1, \dots, q_{n-m}). Choose λ_i s.t.

$$\frac{\partial L}{\partial q_k} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_k} \right) + \sum_{i=1}^m \lambda_i a_{ik} = 0 \quad (41)$$

$\forall k = n-m+1, \dots, n$. In conclusion, we have $q_1, \dots, q_n, \lambda_1, \dots, \lambda_m$ overall $n+m$ unknowns, and n Lagrange's equations and m constraint equations overall $n+m$ equations.

Remark.

- 1) It is inconvenient to reduce all q_k s to independent coordinates
- 2) If we are interested in the constraint forces

$$\sum_{k=1}^n a_{ik} dq_k + a_{it} dt = 0$$

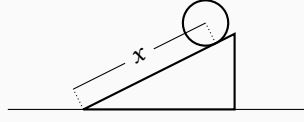
where

$$a_{ik} = \frac{\partial f_i}{\partial q_k}, \quad a_{it} = \frac{\partial f_i}{\partial t}$$

Then

$$df_i = \frac{\partial f_i}{\partial q_k} dq_k + \frac{\partial f_i}{\partial t} dt \Rightarrow df_i = 0, \quad f_i = \text{const}$$

Example 2.7 (Hoop rolling down an inclined plane).



The constraint equation writes

$$\dot{x} - r\dot{\theta} = 0 \Rightarrow x - r\theta = \text{const}$$

$a_x = 1, a_\theta = -r, a_t = 0$.

Energy terms are

$$\begin{aligned} T &= T_{\text{COM}} + T_{\text{relative}} = \frac{1}{2}M\dot{x}^2 + \frac{1}{2}M(r\dot{\theta})^2 \\ V &= Mg(l - x) \sin \phi \\ \Rightarrow L &= \frac{1}{2}M\dot{x}^2 + \frac{1}{2}M(r\dot{\theta})^2 - Mg(l - x) \sin \phi \end{aligned}$$

Then we can write the Lagrange's equation with Lagrange's multipliers

$$\begin{aligned} \frac{\partial L}{\partial x} - \frac{d}{dt} \frac{\partial L}{\partial \dot{x}} + a_x \lambda &= 0 \\ \Rightarrow Mg \sin \phi - M\ddot{x} + \lambda &= 0 \\ -Mr^2\ddot{\theta} - \lambda r &= 0 \\ \dot{x} = r\dot{\theta} \Rightarrow \ddot{x} &= r\ddot{\theta} \end{aligned}$$

we can get $M\ddot{x} = Mr\ddot{\theta} = -\lambda$ and $\ddot{x} = (g \sin \phi)/2$. Note that λ is the constraint force (in this case λ is the frictional force).

Theorem 2.4 (Universal test for holonomic constraints). Let the constraint equation be

$$\sum_j A_j du_j = 0 \quad (42)$$

Then we can test the equation where

$$A_\gamma \left(\frac{\partial A_\beta}{\partial u_\alpha} - \frac{\partial A_\alpha}{\partial u_\beta} \right) + A_\beta \left(\frac{\partial A_\alpha}{\partial u_\gamma} - \frac{\partial A_\gamma}{\partial u_\alpha} \right) + A_\alpha \left(\frac{\partial A_\gamma}{\partial u_\beta} - \frac{\partial A_\beta}{\partial u_\gamma} \right) = 0 \quad (43)$$

2.4 Lagrangian for Lorentz force

The Lorentz force is given by

$$\mathbf{F} = q[\mathbf{E} + \mathbf{v} \times \mathbf{B}] \quad (44)$$

Where

$$\mathbf{E} = -\nabla\phi - \frac{\partial \mathbf{A}}{\partial t}, \quad \mathbf{B} = \nabla \times \mathbf{A} \quad (45)$$

Hence, by defining the Lagrangian

$$L = \frac{1}{2}m\mathbf{v}^2 - q\phi + q\mathbf{A} \cdot \mathbf{v} \quad (46)$$

Applying the Lagrange's equation we can get the EOM (eq. 44). Take x as an example

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{x}} = \frac{d}{dt} (m\dot{x} + qA_x) = m\ddot{x} + q \frac{\partial A_x}{\partial t} + \mathbf{v} \cdot \nabla A_x \quad (47)$$

2.5 Conservation & symmetry of the system

Definition 2.1 (Cyclic coordinate). The generalized coordinate q_i is cyclic (ignorable) if

$$\frac{\partial L}{\partial q_i} = 0 \quad (48)$$

It implies the generalized momentum p_i is conserved.

Rotational symmetry. Let q_j be one of the rotational angle of spacial coordinate \mathbf{r}_i . Hence

$$d\mathbf{r}_i = \mathbf{n}_j \times \mathbf{r}_i dq_j \Rightarrow \frac{\partial \mathbf{r}_i}{\partial q_j} = \mathbf{n}_j \times \mathbf{r}_i dq_j \quad (49)$$

where \mathbf{n}_j is the normal vector of the rotation axis of q_j . Hence the generalized force of q_j writes

$$Q_{q_j} = -\frac{\partial V}{\partial q_j} = -\sum_k \frac{\partial V}{\partial \mathbf{r}_k} \frac{\partial \mathbf{r}_k}{\partial q_j} = -\frac{\partial V}{\partial \mathbf{r}_i} \frac{\partial \mathbf{r}_i}{\partial q_j} = \mathbf{F}_i \cdot (\mathbf{n}_j \times \mathbf{r}_i) = \mathbf{n}_j \cdot (\mathbf{r}_i \times \mathbf{F}_i) = \mathbf{n}_j \cdot \mathbf{N}_i \quad (50)$$

where \mathbf{N}_i stands for the torque on the i^{th} particle. The generalized momentum of q_j writes

$$p_{q_j} = \frac{\partial T}{\partial \dot{q}_j} = \sum_k \frac{\partial T}{\partial \dot{\mathbf{r}}_k} \frac{\partial \dot{\mathbf{r}}_k}{\partial \dot{q}_j} = \sum_k m_k \dot{\mathbf{r}}_k \cdot \frac{\partial \dot{\mathbf{r}}_k}{\partial \dot{q}_j} = m_i \dot{\mathbf{r}}_i \cdot (\mathbf{n}_j \times \mathbf{r}_i) = \mathbf{n}_j \cdot (\mathbf{r}_i \times m_i \dot{\mathbf{r}}_i) = \mathbf{n}_j \cdot \mathbf{L}_i \quad (51)$$

where \mathbf{L}_i stands for the angular momentum of the i^{th} particle. Hence, the rotational invariance implies the conservation of angular momentum.

Time translation

$$\frac{d}{dt}L = \sum_i \frac{\partial L}{\partial q_i} \dot{q}_i + \frac{\partial L}{\partial \dot{q}_i} \ddot{q}_i + \frac{\partial L}{\partial t} \quad (52)$$

$$= \sum_i \frac{d}{dt} \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i + \frac{\partial L}{\partial \dot{q}_i} \ddot{q}_i + \frac{\partial L}{\partial t} \quad (53)$$

$$= \frac{d}{dt} \sum_i \left(\frac{\partial L}{\partial \dot{q}_i} \dot{q}_i \right) + \frac{\partial L}{\partial t} \quad (54)$$

$$\Rightarrow \frac{\partial L}{\partial t} + \frac{d}{dt} \underbrace{\left(\sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i \right)}_H = 0 \quad (55)$$

Note that

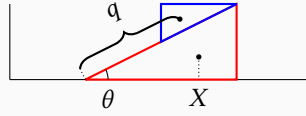
$$\sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i = 2T \quad (56)$$

Proof. Suppose r_i does not have explicit time dependence ($\partial r_i / \partial t = 0$)

$$\begin{aligned} T &= \sum_i \frac{1}{2} m_i \dot{r}_i^2 = \sum_i \frac{1}{2} m_i \left(\sum_j \frac{\partial r_i}{\partial q_j} \dot{q}_j + \frac{\partial r_i}{\partial t} \right)^2 \\ &= \sum_{ijk} \frac{1}{2} m_i \frac{\partial r_i}{\partial q_j} \frac{\partial r_i}{\partial q_k} \dot{q}_j \dot{q}_k \\ &\Rightarrow \sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i = \sum_i \dot{q}_i \sum_{jk} m_k \frac{\partial r_k}{\partial q_i} \frac{\partial r_k}{\partial q_j} \dot{q}_j = \sum_{ijk} m_k \frac{\partial r_k}{\partial q_i} \frac{\partial r_k}{\partial q_j} \dot{q}_i \dot{q}_j = 2T \quad \square \end{aligned}$$

Hence we can define Hamiltonian $H = T + V$ which stands for the total energy, and H conserved if L doesn't depend on time explicitly.

Example 2.8 (Two blocks). Let M be the mass of the big block, m be the mass of the small block. Define two generalized coordinates: X stand for the position of COM of the big block, q stand for the position of COM of the small block (sloped).



Hence we can easily define the Lagrangian

$$L = \frac{1}{2}M\dot{X}^2 + \frac{1}{2}m[(\dot{X} + \dot{q} \cos \theta)^2 + \dot{q}^2 \sin^2 \theta] - mgq \sin \theta$$

There is no X dependence on the system, hence X is a cyclic coordinate.

$$\begin{aligned} \frac{d}{dt} \frac{\partial L}{\partial \dot{X}} &= \frac{d}{dt} M\dot{X} + m(\dot{X} + \dot{q} \cos \theta) = 0 \\ \Rightarrow M\dot{X}m(\dot{X} + \dot{q} \cos \theta) &= p_X = \text{const} \end{aligned}$$

3 The Central Force Problem

3.1 Reduction to the equivalent one-body problem

For the two-body problem, we have two choices of generalized coordinate

- (a) $\mathbf{r}_1, \mathbf{r}_2$ stand for spacial coordinates of two masses
- (b) \mathbf{R} spacial coordinate of the COM, $\mathbf{r} = \mathbf{r}_1 - \mathbf{r}_2$

Hence, we can rewrite the kinetic energy in terms of \mathbf{R} and \mathbf{r}

$$T = \frac{1}{2}m_1\dot{\mathbf{r}}_1^2 + \frac{1}{2}m_2\dot{\mathbf{r}}_2^2 \quad (1)$$

$$= \frac{1}{2}m_1\left(\dot{\mathbf{R}} + \frac{m_2}{m_1+m_2}\dot{\mathbf{r}}\right)^2 + \frac{1}{2}m_2\left(\dot{\mathbf{R}} - \frac{m_1}{m_1+m_2}\dot{\mathbf{r}}\right)^2 \quad (2)$$

$$= \frac{1}{2}(m_1+m_2)\dot{\mathbf{R}}^2 + \frac{m_1m_2}{m_1+m_2}\dot{\mathbf{r}}^2 = \frac{1}{2}M\dot{\mathbf{R}}^2 + \frac{1}{2}\mu\dot{\mathbf{r}}^2 \quad (3)$$

Hence we can write the Lagrangian

$$L = \frac{1}{2}M\dot{\mathbf{R}}^2 + \frac{1}{2}\mu\dot{\mathbf{r}}^2 - V \quad (4)$$

Suppose $V = V(\mathbf{r})$, then \mathbf{R} is a cyclic coordinate, We have $\dot{\mathbf{R}} = \text{const}$, and we can drop $\dot{\mathbf{R}}$ terms in L . Moreover, if $V = V(\|\mathbf{r}\|)$, the total angular momentum is conserved.

Use r, θ as generalized coordinates, we have

$$L = \frac{1}{2}\mu(\dot{r}^2 + r^2\dot{\theta}^2) - V(r) \quad (5)$$

The Lagrange's equation wrt r writes

$$\mu\ddot{r} - \mu r\dot{\theta}^2 + \frac{\partial V}{\partial r} = 0 \quad (6)$$

Easy to find that θ is cyclic, hence

$$\frac{d}{dt}\frac{\partial L}{\partial \dot{\theta}} = \frac{d}{dt}\mu r^2\dot{\theta} = 0 \Rightarrow p_\theta = \mu r^2\dot{\theta} = l = \text{const} \quad (7)$$

Theorem 3.1 (Kepler's 2nd law). Radius vector sweeps out equal areas in equal time.

Substitute $\mu r\dot{\theta}^2$ term by l , we have

$$\mu\ddot{r} - \frac{l^2}{\mu r^3} + \frac{\partial V}{\partial r} = 0 \quad (8)$$

$$\Rightarrow \mu\ddot{r} = -\frac{\partial}{\partial r}\left(V + \frac{l^2}{2\mu r^2}\right) \quad (9)$$

$$\mu\ddot{r} = -\frac{\partial}{\partial r}\dot{r}\left(V + \frac{l^2}{2\mu r^2}\right) \quad (10)$$

$$\Rightarrow \frac{d}{dt}\left(\frac{1}{2}\mu\dot{r}^2 + V + \frac{l^2}{2\mu r^2}\right) = \frac{d}{dt}E = 0 \quad (11)$$

Hence we can get the expression of \dot{r} and a differential equation

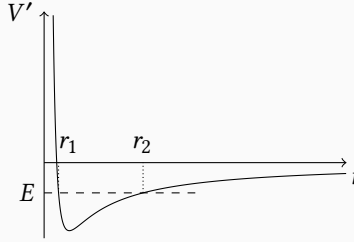
$$\dot{r} = \sqrt{\frac{2}{\mu}\left(E - V - \frac{l^2}{2\mu r^2}\right)} \quad (12)$$

Define the new effective force $f'(r)$ with an effective potential $V' = V + l^2/2\mu r^2$, we have

$$\mu\ddot{r} = -\frac{\partial V}{\partial r} + \frac{l^2}{\mu r^3} = f'(r), \quad E = \frac{1}{2}\mu\dot{r}^2 + V' = \text{const} \quad (13)$$

Example 3.1 (Gravitational force). Suppose we have $f(r) = -kr^{-2}$ and $V = -kr^{-1}$, then

$$V' = -\frac{k}{r} + \frac{l^2}{2\mu r^2}$$



- 1) $E = E_1 \geq 0$, the motion has a lower bound, $r \geq r_1$.
- 2) $V_{\min} < E_2 < 0$, the motion has lower and upper bound, $r_1 \leq r \leq r_2$.
- 3) $E_3 = V_{\min}$, the motion will shrink to a single circle $r_1 = r_2 = \text{const}$, hence it is a circular motion. In this case, the gravitational force is equal to the centrifugal force

$$\mu \ddot{r} = f(r) + \frac{l^2}{\mu r^3} = f(r) + \mu r \dot{\theta}^2 = 0 \Rightarrow f(r) = -\mu r \dot{\theta}^2$$

Remark. Let the potential be $V = -kr^{-\alpha}$, then the motion cannot have periodic behavior if $\alpha > 2$.

Example 3.2 (Harmonic oscillator). $V = kr^2/2$, we have

$$V' = \frac{1}{2}kr^2 + \frac{l^2}{2\mu r^2}$$

Theorem 3.2 (Conditions for closed orbitals, Bertrand's theorem). Stable orbitals require

$$\left. \frac{\partial^2 V'}{\partial r^2} \right|_{r=r_0} = -\frac{\partial f}{\partial r} + \frac{3l^2}{mr^4} \Big|_{r=r_0} > 0 \Rightarrow \left. \frac{\partial f}{\partial r} \right|_{r=r_0} < -\frac{3f(r_0)}{r_0} \quad (14)$$

Let $f = -kr^n$, then we have

$$-knr^{n-1} < 3kr^{n-1} \Rightarrow n > -3 \quad (15)$$

For a small perturbation from the minimum, we can write the effective potential as Taylor expansion

$$V'(r) = V'(r_0) + \left. \frac{\partial V'}{\partial r} \right|_{r=r_0} (r - r_0) + \frac{1}{2} \left. \frac{\partial^2 V'}{\partial r^2} \right|_{r=r_0} (r - r_0)^2 + \dots \quad (16)$$

$$= V'(r_0) + \frac{1}{2} \left. \frac{\partial^2 V'}{\partial r^2} \right|_{r=r_0} (r - r_0)^2 + O(|r - r_0|^3) \quad (17)$$

Hence the EOM becomes

$$m\ddot{r} = -\frac{\partial V'}{\partial r} = -\left. \frac{\partial^2 V'}{\partial r^2} \right|_{r=r_0} (r - r_0) \quad (18)$$

$$\dot{\theta} = \frac{l}{mr^2} \quad (19)$$

The solution takes the form

$$u = u_0 + a \cos \beta \theta, \quad u = \frac{1}{r}, \quad \beta^2 = \left. \frac{r}{f} \frac{\partial f}{\partial r} + 3 \right|_{r=r_0} \quad (20)$$

For finite perturbation, the orbit can be a closed only if $\beta^2 = 1$ or 4 . Then there are only two types of central-force scalar problem with the property that all bound orbitals are closed orbitals.

$$\left. \frac{r}{f} \frac{\partial f}{\partial r} \right|_{r=r_0} = \pm 2 \Rightarrow f = -kr^{-2} \text{ or } -kr \quad (21)$$

check the theorem on other books

3.2 Virial theorem

Consider a multi-particle system $1 \leq i \leq N$.

$$\dot{\mathbf{p}}_i = \mathbf{F}_i \quad (22)$$

Define new function

$$G = \sum_i \mathbf{p}_i \cdot \mathbf{r}_i \quad (23)$$

Then the time derivative of G writes

$$\frac{d}{dt}G = \sum_i m_i \dot{\mathbf{r}}_i^2 + \sum_i \mathbf{F}_i \cdot \mathbf{r}_i \quad (24)$$

Hence the time average of dG/dt is

$$\frac{1}{\tau} \int_0^\tau \frac{d}{dt}G dt = 2\bar{T} + \overline{\sum_i \mathbf{F}_i \cdot \mathbf{r}_i} = \frac{1}{\tau} [G(\tau) - G(0)] \quad (25)$$

The time average equals to 0 if τ is the period of the periodic motion; even for non-periodic motion, if $\tau \rightarrow \infty$, the average will approach 0. Hence

$$2\bar{T} + \overline{\sum_i \mathbf{F}_i \cdot \mathbf{r}_i} = 0 \Rightarrow \bar{T} = -\frac{1}{2} \underbrace{\overline{\sum_i \mathbf{F}_i \cdot \mathbf{r}_i}}_{\text{virial of Clausius}} \quad (26)$$

Example 3.3 (Ideal gas). Temperature $T \propto T_i$ kinetic energy of i^{th} particle.

$$T_i = \frac{3}{2} k_B T \quad (27)$$

Hence the time average of total kinetic energy is

$$\overline{\sum_i T_i} = \frac{3}{2} N k_B T \quad (28)$$

The virial could be written as

$$\overline{\sum_i \mathbf{F}_i \cdot \mathbf{r}_i} = \int d\mathbf{F} \cdot \mathbf{r} \quad (29)$$

Note that

$$d\mathbf{F} = -p d\mathbf{A}\mathbf{n}$$

Applying Gauss's law we have

$$\overline{\sum_i \mathbf{F}_i \cdot \mathbf{r}_i} = - \int p d\mathbf{A} \mathbf{n} \cdot \mathbf{r} = - \int p dV (\nabla \cdot \mathbf{r}) = -3pV \quad (30)$$

Hence by the equation we get $pV = nk_B T$.

Example 3.4 (Gravational force). Since $\mathbf{F}_i = -\nabla_i V$, given $V_i = ar_i^{n+1}$, we have

$$\bar{T} = \frac{1}{2} \overline{\sum_i \nabla_i V \cdot \mathbf{r}_i} = \frac{n+1}{2} \overline{\sum_i ar_i^{n+1}} = \frac{n+1}{2} \bar{V} \quad (31)$$

This theorem is particularly important when the potential energy is a homogeneous function of the coordinates, i.e.

$$U(\alpha \mathbf{r}_1, \dots, \alpha \mathbf{r}_n) = \alpha^k U(\mathbf{r}_1, \dots, \mathbf{r}_n) \quad (32)$$

Note that

$$\frac{dU}{d\alpha} = \sum_a \frac{\partial \alpha \mathbf{r}_a}{\partial \alpha} \cdot \frac{\partial U}{\partial \alpha \mathbf{r}_a} = \sum_a \frac{\mathbf{r}_a}{\alpha} \cdot \frac{\partial U}{\partial \mathbf{r}_a} = k \alpha^{k-1} U \quad (33)$$

Then the equation 26 becomes

$$2\bar{T} = k\bar{U} \quad (34)$$

Equivalently

$$\bar{U} = \frac{2E}{k+2}, \quad \bar{T} = \frac{kE}{k+2} \quad (35)$$

3.3 Inverse-square force

Consider $f = -k/r^2$, $V = -k/r$, then we have EOM

$$\dot{r} = \left[\frac{2}{m} \left(E + \frac{k}{r} - \frac{l^2}{2mr^2} \right) \right]^{1/2} \Rightarrow \theta = \theta_0 + \int_{r_0}^{r_1} \frac{dr}{r^2 \left(\frac{2mE}{l^2} - \frac{2mV}{l^2} - \frac{1}{r^2} \right)^{1/2}} \quad (36)$$

Define $u = 1/r$, let $\theta_0 = 0$, then

$$\theta = \theta_0 - \int_{u_0}^{u_1} \frac{du}{\left(\frac{2mE}{l^2} + \frac{2mku}{l^2} - u^2 \right)^{1/2}} \quad (37)$$

$$\Rightarrow \theta = -\arccos \frac{\frac{l^2 u}{mk} - 1}{\sqrt{1 + \frac{2El^2}{mk^2}}}, \quad r = \frac{\frac{l^2}{mk}}{1 + \sqrt{1 + \frac{2El^2}{mk^2}} \cos \theta} = \frac{r_0}{1 + \epsilon \cos \theta} \quad (38)$$

ϵ is called the eccentricity.

ϵ	Energy	Orbit
$\epsilon > 1$	$E > 0$	Hyperbola
$\epsilon = 1$	$E = 0$	Parabola
$0 < \epsilon < 1$	$E < 0$	Ellipse
$\epsilon = 0$	$E < 0$	Circle

The major semi-axis a and minor semi-axis b are given by

$$a = \frac{r_0}{1 - \epsilon^2} = -\frac{k}{2E}, \quad b = a\sqrt{1 - \epsilon^2} = \frac{k}{\sqrt{-2mE}} \quad (39)$$

Since $mr^2\dot{\theta} = l$, then

$$\int_0^T dA = \frac{1}{2} \int_0^T r^2 \dot{\theta} dt = \frac{1}{2} \int_0^T \frac{l}{m} \theta dt = \frac{l}{2m} T = \pi ab \Rightarrow T = 2\pi a^{3/2} \sqrt{\frac{m}{k}} \quad (40)$$

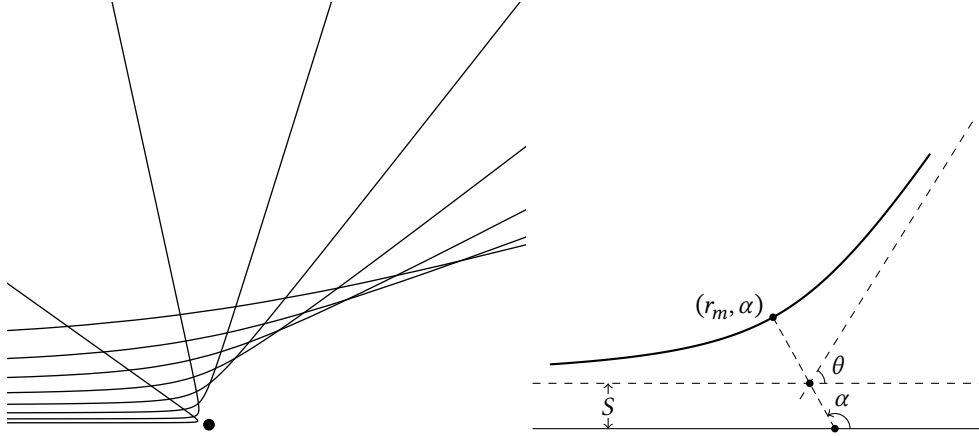
Alternatively

$$\int dt = \int \frac{dr}{\sqrt{\frac{2}{m} \left(E - V - \frac{l^2}{2mr^2} \right)}} = \sqrt{\frac{ma}{k}} \int_{r_0}^{r_1} \frac{r dr}{\sqrt{-r^2 + 2ar - b^2}} = \sqrt{\frac{ma}{k}} \int_{r_0}^{r_1} \frac{r dr}{\sqrt{-(r-a)^2 + a^2 \epsilon^2}} \quad (41)$$

Let $r - a = -a\epsilon \cos \zeta$, hence

$$t = \sqrt{\frac{ma}{k}} \int \frac{(a - a\epsilon \cos \zeta) a\epsilon \sin \zeta d\zeta}{\sqrt{a\epsilon^2(1 - \cos^2 \zeta)}} = \sqrt{\frac{ma}{k}} \int (a - a\epsilon \cos \zeta) d\zeta = \sqrt{\frac{ma^3}{k}} (\zeta - \epsilon \sin \zeta) + C \quad (42)$$

3.4 Scattering



Question: how many particles will be scattered in the given solid angle region (scattering cross section). Let $V \sim 1/r$, $f \sim 1/r^2$. Define the intensity of incident beam I

$I = \#$ of particles crossing a unit area perpendicular to the beam in unit time

The the number of particles scattered into $d\Omega$ could be expressed as

$$dN = \sigma I d\Omega, \quad \sigma = \frac{dN}{I d\Omega} \quad (43)$$

where σ is called differential cross section, which has the unit of area.

Particles in $[S, S + dS]$ would be scattered into $[\Omega, \Omega + d\Omega]$, since $d\Omega = 2\pi \sin \theta d\theta$

$$2\pi I S |dS| = \sigma I d\Omega = 2\pi \sigma I \sin \theta |d\theta| \Rightarrow \sigma = \frac{S |dS|}{\sin \theta |d\theta|} \quad (44)$$

The angular momentum of the incoming particles (wrt. to force center) is

$$l = mv_0 S = S \sqrt{2mE} \quad (45)$$

From the equation derived from central force problem

$$\alpha = \int \frac{dr}{r^2 \sqrt{\frac{2mE}{l^2} - \frac{rmV}{l^2} - \frac{1}{r^2}}} \quad (46)$$

$$= \pi + \int_{-\infty}^{r_m} \frac{dr}{r^2 \sqrt{\frac{2mE}{l^2} - \frac{rmV}{l^2} - \frac{1}{r^2}}} \quad (47)$$

Let $r_m \equiv r_{\min}$ is the closest distance. Define ψ where

$$\alpha = \pi + \int_{-\infty}^{r_m} \frac{dr}{r^2 \sqrt{\frac{2mE}{l^2} - \frac{rmV}{l^2} - \frac{1}{r^2}}} = \pi - \psi \quad (48)$$

Hence $\theta = \pi - 2\psi$. Change the variable $u = 1/r$, then

$$\psi = \int_0^{u_m=1/r_m} \frac{S du}{\sqrt{1 - \frac{V}{E} - S^2 u^2}} \quad (49)$$

Also note that

$$\sin \frac{\theta}{2} = \sin \frac{\pi - 2\psi}{2} = \cos \psi = \frac{1}{\epsilon} \quad (50)$$

Example 3.5 (Coulomb interaction). Let

$$f = \frac{ZZ'e^2}{r^2}, \quad V = \frac{ZZ'e^2}{r}, \quad r = \frac{r_0}{1 + \epsilon \cos(\alpha - \alpha')} \quad (51)$$

choose $\alpha' = \pi$. One can derive that

$$\epsilon = \sqrt{1 + \frac{2El^2}{m(ZZ'e^2)^2}} = \sqrt{1 + \left(\frac{2ES}{ZZ'e^2} \right)^2} \quad (52)$$

Using the trigonometric relationship between θ and ϵ , we have

$$S = \frac{ZZ'e^2}{2E} \cot \frac{\theta}{2}, \quad \left| \frac{dS}{d\theta} \right| = \frac{ZZ'e^2}{4E} \frac{1}{\sin^2 \frac{\theta}{2}} \quad (53)$$

$$\Rightarrow \epsilon(\theta) = \left(\frac{ZZ'e^2}{4E} \right)^2 \frac{1}{\sin^4 \frac{\theta}{2}} \quad (54)$$

check if $\alpha' = \pi$ or $\alpha' = \alpha_m$

4 Rigid Body

4.1 Coordinates of rigid body

A rigid body is a system of point masses satisfying the constraint that distance between any two points is a constant ($r_{ij} = \text{const}$ for all i, j). Let \mathbf{r}_i , \mathbf{r}_j , and \mathbf{r}_k be three points in the rigid body. Let \mathbf{r}_i has 3 DOFs, since r_{ij} is a constant, \mathbf{r}_j has two DOFs. Hence, \mathbf{r}_k only have 1 DOFs. The system has $3 + 2 + 1 = 6$ DOFs.

Or, alternatively, a rigid body has 3 coordinates for the origin of the coordinate system fixed on the rigid body, and 3 angular variables to specify the orientation of the rotated coordinate system.

4.2 Orthogonal transformations

Consider an orthogonal transformation $\mathbf{x} \mapsto \mathbf{x}'$

$$x'_1 = a_{11}x_1 + a_{12}x_2 + a_{13}x_3 \quad (1)$$

$$x'_2 = a_{21}x_1 + a_{22}x_2 + a_{23}x_3 \quad (2)$$

$$x'_3 = a_{31}x_1 + a_{32}x_2 + a_{33}x_3 \quad (3)$$

Let $\mathbf{x}^2 = \mathbf{x}'^2$, we have

$$\mathbf{x}^2 = x_i x_i = x'_i x'_i = a_{ij} x_j a_{ik} x_k = \delta_{jk} x_j x_k = x_j x_j \Rightarrow a_{ij} a_{ik} = \delta_{jk} \quad (4)$$

This equation implies the orthogonal transformations have three DOFs.

Different views on rotational transformation

1. Passive view the coordinate system is transformed
2. Active view: the vector is transformed

Consider two rotational matrix A and B , let $C = AB$, then

$$C_{ij} C_{ik} = A_{im} B_{mj} A_{in} B_{nk} = A_{im} A_{in} B_{mk} B_{nk} = \delta_{nm} B_{mj} B_{nk} = B_{nj} B_{nk} = \delta_{jk} \quad (5)$$

Non-commutative $AB \neq BA$.

Define the inverse transformation

$$x_i = a'_{ij} x'_j = a'_{ij} a_{jk} x_k \Rightarrow a'_{ij} a_{jk} = \delta_{ik} \quad (6)$$

Note that

$$\left. \begin{aligned} \underbrace{a_{im} a_{ij}}_i a'_{jk} &= \delta_{mk} a'_{jk} = a'_{mk} \\ a_{im} \underbrace{a_{ij} a'_{jk}}_j &= a_{im} \delta_{ik} = a_{km} \end{aligned} \right\} \Rightarrow a_{km} = a'_{mk} \quad (7)$$

4.3 Euler angles

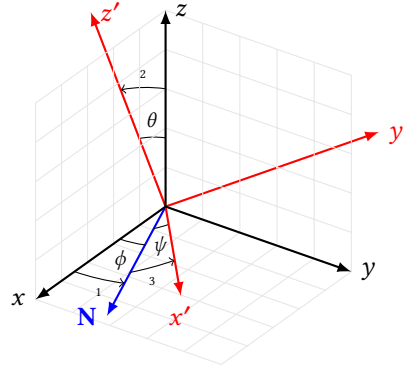
A convenient choice of angle variables: Euler angles. Steps:

1. Rotate around z axis by an angle ϕ , rotational matrix D
2. Rotate around ξ axis by an angle θ , rotational matrix C
3. Rotate around ξ' axis by an angle ψ , rotational matrix B

We can always write any rotational matrix A as $A = BCD$ Note that all rotations are rotations of **coordinate system**, which means, A is a change-of-basis matrix.

$$A = \begin{bmatrix} \cos \psi & \sin \psi & 0 \\ -\sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & \sin \theta \\ 0 & -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad (8)$$

$$= \begin{bmatrix} \cos \phi \cos \psi - \cos \theta \sin \phi \sin \psi & \cos \psi \sin \phi + \cos \theta \cos \phi \sin \psi & \sin \theta \sin \psi \\ -\cos \theta \cos \psi \sin \phi - \cos \phi \sin \psi & \cos \theta \cos \phi \cos \psi - \sin \phi \sin \psi & \cos \psi \sin \theta \\ \sin \theta \sin \phi & -\cos \phi \sin \theta & \cos \theta \end{bmatrix} \quad (9)$$



Theorem 4.1 (Euler's theorem). The general displacement of a rigid body with one point fixed is a rotation around some axis \mathbf{R} . Then

$$\mathbf{R}' = \mathbf{A}\mathbf{R} = \mathbf{R} \Rightarrow (\mathbf{A} - \mathbf{I})\mathbf{R} = 0, \quad \det(\mathbf{A} - \mathbf{I}) = 0 \quad (10)$$

Infinitesimal rotation transformation

$$\mathbf{x}' = \mathbf{A}\mathbf{x} = (1 + \epsilon)\mathbf{x} \Rightarrow x'_i = x_i + \epsilon_{ij}x_j = (\delta_{ij} + \epsilon_{ij})x_j \quad (11)$$

Hence

$$(\delta_{ki} + \epsilon'_{ki})x'_i = (\delta_{ki} + \epsilon'_{ki})(\delta_{ij} + \epsilon_{ij})x_j = (\delta_{kj} + \epsilon'_{kj} + \epsilon_{kj} + \epsilon'_{ki}\epsilon_{ij})x_j = x_k \quad (12)$$

Ignoring $\epsilon'_{ki}\epsilon_{ij}$ term, we have $\epsilon'_{kj} = \epsilon_{jk}^T = -\epsilon_{kj}$, given that ϵ is an antisymmetric matrix. Let

$$\epsilon = \begin{bmatrix} 0 & -d\Omega_3 & d\Omega_2 \\ d\Omega_3 & 0 & -d\Omega_1 \\ -d\Omega_2 & d\Omega_1 & 0 \end{bmatrix}, \quad \Omega = \begin{bmatrix} \Omega_1 \\ \Omega_2 \\ \Omega_3 \end{bmatrix} \quad (13)$$

Then

$$d\mathbf{x} = \epsilon\mathbf{x} = d\Omega \times \mathbf{x} \quad (14)$$

4.4 Rate of change of a vector

Let \mathbf{R} be one point inside the rigid body, then the motion can be decomposed into rotational motion of the body coordinate and the translational motion of the body

$$\left(\frac{d\mathbf{R}}{dt}\right)_{\text{space}} = \left(\frac{d\mathbf{R}}{dt}\right)_{\text{body}} + \frac{d\Omega}{dt} \times \mathbf{R} \quad (15)$$

$$\Rightarrow \mathbf{V}_{\text{space}} = \mathbf{V}_{\text{body}} + \boldsymbol{\omega} \times \mathbf{R} \quad (16)$$

Decompose $\boldsymbol{\omega}$ into unit vectors corresponds to Euler angles and the body coordinate

$$\boldsymbol{\omega} = \dot{\phi}e_\phi + \dot{\theta}e_\theta + \dot{\psi}e_\psi = \omega_{x'}\mathbf{i}' + \omega_{y'}\mathbf{j}' + \omega_{z'}\mathbf{k}' \quad (17)$$

From the figure we can find that

$$e_\phi = \mathbf{k} = \sin \theta \sin \psi \mathbf{i}' + \sin \theta \cos \psi \mathbf{j}' + \cos \theta \mathbf{k}' \quad (18)$$

$$e_\theta = \cos \psi \mathbf{i}' - \sin \psi \mathbf{j}' \quad (19)$$

$$e_{\psi} = \mathbf{k}' \quad (20)$$

Hence

$$\omega_{x'} = \dot{\phi} \sin \theta \sin \psi + \dot{\theta} \cos \psi \quad (21)$$

$$\omega_{y'} = \dot{\phi} \sin \theta \cos \psi - \dot{\theta} \sin \psi \quad (22)$$

$$\omega_{z'} = \dot{\psi} + \dot{\phi} \cos \theta \quad (23)$$

4.5 The Coriolis effect

From equation 16 we have

$$\mathbf{a}_{\text{space}} = \mathbf{a}_{\text{body}} + \boldsymbol{\omega} \times \mathbf{V} \quad (24)$$

$$\Rightarrow m\mathbf{a}_{\text{body}} = \mathbf{F} - 2m\boldsymbol{\omega} \times \mathbf{V}_{\text{body}} - m\boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{R}) \quad (25)$$

The term $-2m\boldsymbol{\omega} \times \mathbf{V}_{\text{body}}$ is the Coriolis force.

Remark. Since \mathbf{V}_{body} is also rotating around $\boldsymbol{\omega}$, we have

$$\frac{d}{dt} \mathbf{V}_{\text{body}} = \mathbf{a}_{\text{body}} + \boldsymbol{\omega} \times \mathbf{V}_{\text{body}} \quad (26)$$

Additional notes on transformation of basis

Remark. One can check Arnold's CM book for comprehensive mathematical formulation for spacial transformation.

5 EOM of rigid body

5.1 Angular momentum and kinetic energy

It is often convenient to choose the COM of the rigid body as the origin of the body system. Suppose the motion only involves rotation, the angular momentum is

$$\mathbf{L} = \sum_i m_i(\mathbf{r}_i \times \mathbf{v}_i) = \sum_i m_i[\mathbf{r}_i \times (\boldsymbol{\omega} \times \mathbf{r}_i)] = \sum_i m_i[\mathbf{r}_i^2 \boldsymbol{\omega} - \mathbf{r}_i(\mathbf{r}_i \cdot \boldsymbol{\omega})] \quad (1)$$

Consider the components of the equation

$$L_x = \sum_i m_i[\omega_x(\mathbf{r}_i^2 - x_i^2) - \omega_y x_i y_i - \omega_z x_i z_i] \quad (2)$$

$$L_y = \sum_i m_i[\omega_y(\mathbf{r}_i^2 - y_i^2) - \omega_x x_i y_i - \omega_z y_i z_i] \quad (3)$$

$$L_z = \sum_i m_i[\omega_z(\mathbf{r}_i^2 - z_i^2) - \omega_x x_i z_i - \omega_y y_i z_i] \quad (4)$$

$$\Rightarrow \begin{bmatrix} L_x \\ L_y \\ L_z \end{bmatrix} = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} \quad (5)$$

Written the equation in the integral form

$$I_{ij} = \int_V \rho(\mathbf{r}) dV (\mathbf{r}^2 \delta_{ij} - r_i r_j) \quad (6)$$

The total kinetic energy is

$$T = \sum_i \frac{1}{2} m_i \mathbf{v}_i^2 = \sum_i \frac{1}{2} m_i (\boldsymbol{\omega} \times \mathbf{r}_i) \cdot \mathbf{v}_i = \frac{1}{2} \boldsymbol{\omega} \cdot \sum_i m_i (\mathbf{r}_i \times \mathbf{v}_i) = \frac{1}{2} \boldsymbol{\omega} \cdot \mathbf{L} = \frac{1}{2} \boldsymbol{\omega}^T \mathbf{I} \boldsymbol{\omega} = \frac{1}{2} I_{ij} \omega_i \omega_j \quad (7)$$

If $\boldsymbol{\omega} = \omega \mathbf{n}$, then

$$T = \frac{1}{2} \omega^2 \mathbf{n}^T \mathbf{I} \mathbf{n} \quad (8)$$

If there is a translational motion

$$\mathbf{v}_i = \mathbf{v}_0 + \boldsymbol{\omega} \times \mathbf{r}_i \quad (9)$$

$$\mathbf{r}_i = \mathbf{r}_0 + \mathbf{r}'_i \quad (10)$$

$$\Rightarrow \mathbf{L} = \sum_i (\mathbf{r}_0 + \mathbf{r}'_i) \times (\mathbf{v}_0 + \boldsymbol{\omega} \times \mathbf{r}_i) = M \mathbf{r}_0 \times \mathbf{v}_0 + \sum_i m_i \mathbf{r}'_i \times (\boldsymbol{\omega} \times \mathbf{r}'_i) \quad (11)$$

Hence, the kinetic energy becomes (let $\boldsymbol{\omega} = \omega \mathbf{n}$)

$$T = \sum_i \frac{1}{2} m_i (\mathbf{v}_0 + \boldsymbol{\omega} \times \mathbf{r}_i)^2 = \sum_i \frac{1}{2} m_i \mathbf{v}_0^2 + m_i \mathbf{v}_0 \cdot (\boldsymbol{\omega} \times \mathbf{r}_i) + \frac{1}{2} \omega^2 m_i (\mathbf{n} \times \mathbf{r}_i)^2 = \frac{1}{2} M \mathbf{v}_0^2 + \frac{1}{2} I \omega^2 \quad (12)$$

Angular momentum around any point

$$L_a = \sum_i m_i (\mathbf{n} \times \mathbf{r}_i)^2 = \sum_i m_i [\mathbf{n} \times (\mathbf{R} + \mathbf{r}'_i)]^2 = \sum_i m_i (\mathbf{n} \times \mathbf{R})^2 + \sum_i m_i (\mathbf{n} \times \mathbf{r}'_i)^2 = M (\mathbf{n} \times \mathbf{R})^2 + I_{\text{COM}} \quad (13)$$

5.2 The eigenvalues of the inertia tensor

We can diagonalize the matrix \mathbf{I} s.t.

$$\mathbf{I} = \begin{bmatrix} I_1 & & \\ & I_2 & \\ & & I_3 \end{bmatrix} \quad (14)$$

The diagonal terms are called the principle moments of inertia, and the axes that diagonalize the matrix are called the principal axes.

Example 5.1 (Uniform cube). For a uniform cube lie in $(0, 0, 0)$ to (a, a, a) , we have

$$I_{xx} = \int_V \rho dV (y^2 + z^2) = \int_0^a dx \int_0^a dy \int_0^a dz (y^2 + z^2) \frac{m}{a^3} = \frac{2}{3} ma^2 \quad (15)$$

$$I_{xy} = \int_V \rho dV -xy = - \int_0^a dx \int_0^a dy \int_0^a dz xy \frac{m}{a^3} = -\frac{1}{4} ma^2 \quad (16)$$

Hence the inertia tensor is

$$I = \begin{bmatrix} \frac{2}{3} & -\frac{1}{4} & -\frac{1}{4} \\ -\frac{1}{4} & \frac{2}{3} & -\frac{1}{4} \\ -\frac{1}{4} & -\frac{1}{4} & \frac{2}{3} \end{bmatrix} \quad (17)$$

We can first have a guess of eigenvector

$$A_3 = \frac{1}{\sqrt{3}} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} \quad (18)$$

5.3 Rotational motion of a rigid body

Note that (s means relative to space and b means relative to body)

$$\left(\frac{d\mathbf{L}}{dt} \right)_s = \left(\frac{d\mathbf{L}}{dt} \right)_b + \boldsymbol{\omega} \times \mathbf{L} = \mathbf{N} \quad (19)$$

Hence we can obtain Euler equations

$$\dot{L}_{bi} + \epsilon_{ijk} \omega_j L_{bk} = N_i \quad (20)$$

$$\Rightarrow \begin{cases} I_1 \dot{\omega}_1 - \omega_2 \omega_3 (I_2 - I_3) = N_1 \\ I_2 \dot{\omega}_2 - \omega_3 \omega_1 (I_3 - I_1) = N_2 \\ I_1 \dot{\omega}_3 - \omega_1 \omega_2 (I_1 - I_2) = N_3 \end{cases} \quad (21)$$

Example 5.2 (Precession with $I_1 = I_2 \neq I_3$). Consider force-free motion of a rigid body with $I_1 = I_2 \neq I_3$, then

$$I_1 \dot{\omega}_1 - \omega_2 \omega_3 (I_2 - I_3) = 0 \quad (22)$$

$$I_2 \dot{\omega}_2 - \omega_3 \omega_1 (I_3 - I_1) = 0 \quad (23)$$

$$I_3 \dot{\omega}_3 = 0 \quad (24)$$

Hence we get

$$\dot{\omega}_1 = \frac{I_1 - I_3}{I_1 \omega_3} \omega_2 = -\Omega \omega_2 \quad (25)$$

$$\dot{\omega}_2 = \frac{I_3 - I_1}{I_1 \omega_3} \omega_1 = \Omega \omega_1 \quad (26)$$

$$\omega_3 = \text{const} \quad (27)$$

Hence we can solve the differential equation that

$$\omega_1 = A \cos \Omega t, \quad \omega_2 = A \sin \Omega t \quad (28)$$

6 Oscillation

6.1 Formulation

Consider a system with generalize coordinates q_1, \dots, q_n with $3N - k$ DOFs. Let an equilibrium point be

$$\left(\frac{\partial V}{\partial q_i} \right)_{q_i=q_{0i}} = 0 \quad (1)$$

Expand the potential in the 2nd order

$$V(q_i) = V(q_{0i}) + \left. \frac{\partial V}{\partial q_i} \right|_{q_i=q_{0i}} + \frac{1}{2!} \left. \frac{\partial^2 V}{\partial q_i \partial q_j} \right|_{q_i=q_{0i}} (q_i - q_{0i})(q_j - q_{0j}) + \dots \quad (2)$$

Define $\eta_i = (q_i - q_{0i})$, then at the equilibrium point we have

$$V(q_i) = \frac{1}{2} \left(\frac{\partial^2 V}{\partial q_i \partial q_j} \right)_0 \eta_i \eta_j = \frac{1}{2} V_{ij} \eta_i \eta_j \quad (3)$$

We can also express the kinetic energy wrt η_i

$$T = \sum_i \frac{1}{2} m_i \dot{\mathbf{r}}_i^2 = \sum_i \frac{1}{2} \left(\frac{\partial \mathbf{r}_i}{\partial t} + \sum_j \frac{\partial \mathbf{r}_i}{\partial q_j} \dot{q}_j \right)^2 = \sum_{ijk} \frac{1}{2} m_i \frac{\partial \mathbf{r}_i}{\partial q_j} \frac{\partial \mathbf{r}_i}{\partial q_k} \dot{q}_j \dot{q}_k = \sum_{jk} \frac{1}{2} \left(\sum_i m_i \frac{\partial \mathbf{r}_i}{\partial q_j} \frac{\partial \mathbf{r}_i}{\partial q_k} \dot{q}_j \dot{q}_k \right) = \sum_{jk} \frac{1}{2} M_{jk} \dot{\eta}_j \dot{\eta}_k \quad (4)$$

Suppose M_{ij} has small variation

$$M_{ij}(q_1, \dots, q_n) = M_{ij}(q_{01}, \dots, q_{0n}) + \left(\frac{\partial M_{ij}}{\partial q_k} \right) \eta_k = M_{ij}(q_{01}, \dots, q_{0n}) = T_{ij} \quad (5)$$

Hence

$$T = \frac{1}{2} T_{ij} \dot{\eta}_i \dot{\eta}_j \quad (6)$$

Therefore we have a Lagrangian

$$L = T - V = \frac{1}{2} (T_{ij} \dot{\eta}_i \dot{\eta}_j - V_{ij} \eta_i \eta_j) \quad (7)$$

The EOM becomes

$$T_{ij} \ddot{\eta}_j + V_{ij} \eta_j = 0 \quad (8)$$

6.2 The eigenvalue equation

Let $\eta_i = C_i e^{-i\omega t}$, we have the EOM

$$V_{ij} C_j - \omega^2 T_{ij} C_j = 0 \quad (9)$$

Write it into the matrix form

$$\begin{bmatrix} V_{11} - \omega^2 T_{11} & \dots & V_{1n} - \omega^2 T_{1n} \\ \vdots & \ddots & \vdots \\ V_{n1} - \omega^2 T_{n1} & \dots & V_{nn} - \omega^2 T_{nn} \end{bmatrix} \begin{bmatrix} C_1 \\ \vdots \\ C_n \end{bmatrix} = 0, \quad \det(\mathbf{V} - \omega^2 \mathbf{T}) = 0 \quad (10)$$

Then we get an eigenvalue equation

$$\mathbf{V}\mathbf{C} = \omega^2 \mathbf{T}\mathbf{C} \quad (11)$$

Let ω_α be α^{th} eigenvalue and \mathbf{C}_α be the corresponding eigenvector, then we have

$$\sum_{j=1}^n (V_{ij} - \omega_\alpha^2 T_{ij}) C_{j\alpha} = 0 \quad (12)$$

$$\sum_{j=1}^{n-1} (V_{ij} - \omega_\alpha^2 T_{ij}) C_{j\alpha} = -(V_{in} - \omega_\alpha^2 T_{in}) C_{n\alpha} \quad (13)$$

$$\Rightarrow C_{j\alpha} = \frac{\Delta_{jn}}{\Delta_{nn}} C_{n\alpha} \quad (14)$$

where δ_{ij} is defined as the determinant of a sub-matrix of $\mathbf{A} = \mathbf{V} - \omega_\alpha^2 \mathbf{T}$ removing i^{th} row and j^{th} column.

A general solution is a superposition of all the solutions corresponding to a given eigenfrequency

$$\eta_i(t) = \sum_{\alpha} \eta_{i\alpha}(t) = \sum_{\alpha} C'_{i\alpha} \underbrace{A_{\alpha} e^{-i\omega_{\alpha} t}}_{\xi_{\alpha}(t)} \quad (15)$$

Hence

$$T = \frac{1}{2} T_{ij} \dot{\eta}_i \dot{\eta}_j = \frac{1}{2} T_{ij} C'_{i\alpha} C'_{j\beta} \dot{\xi}_{\alpha} \dot{\xi}_{\beta} \quad (16)$$

$$V = \frac{1}{2} V_{ij} \eta_i \eta_j = \frac{1}{2} V_{ij} C'_{i\alpha} C'_{j\beta} \xi_{\alpha} \xi_{\beta} \quad (17)$$

Note that

$$\mathbf{V} \mathbf{C}_{\alpha} = \omega_{\alpha}^2 \mathbf{T} \mathbf{C}_{\alpha} \quad (18)$$

$$\mathbf{V} \mathbf{C}_{\beta} = \omega_{\beta}^2 \mathbf{T} \mathbf{C}_{\beta} \quad (19)$$

$$\Rightarrow \mathbf{C}_{\beta}^T \mathbf{V} \mathbf{C}_{\alpha} = \omega_{\alpha}^2 \mathbf{C}_{\beta}^T \mathbf{T} \mathbf{C}_{\alpha} \quad (20)$$

$$\mathbf{C}_{\alpha}^T \mathbf{V} \mathbf{C}_{\beta} = \omega_{\beta}^2 \mathbf{C}_{\alpha}^T \mathbf{T} \mathbf{C}_{\beta} \quad (21)$$

$$\Rightarrow (\omega_{\alpha}^2 - \omega_{\beta}^2) \mathbf{C}_{\beta}^T \mathbf{T} \mathbf{C}_{\alpha} = 0 \quad (22)$$

Hence

$$T_{ij} C_{i\alpha} C_{j\beta} = \delta_{ij} \quad (23)$$

$$T = \frac{1}{2} \dot{\xi}_{\alpha} \dot{\xi}_{\beta} \delta_{\alpha\beta} = \frac{1}{2} \dot{\xi}^2 \quad (24)$$

$$V = \frac{1}{2} \omega_{\alpha}^2 \delta_{\alpha\beta} \xi_{\alpha} \xi_{\beta} = \frac{1}{2} \omega_{\alpha}^2 \xi_{\alpha}^2 \quad (25)$$