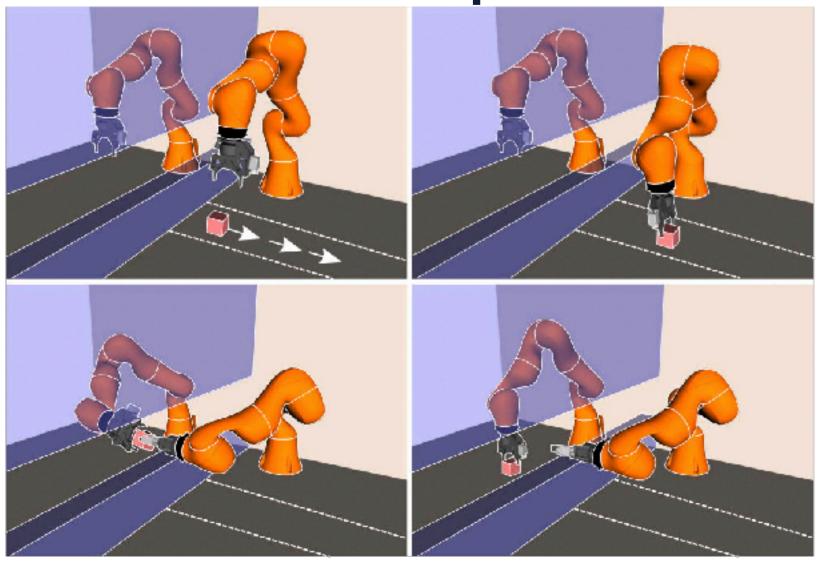


Modeling and Planning Manipulation in Dynamic Environments

Presenter: Yiming Zhao 2020.5.12

Outline

- Introduction
- Related work
- Method
- Experiments
- Conclusion

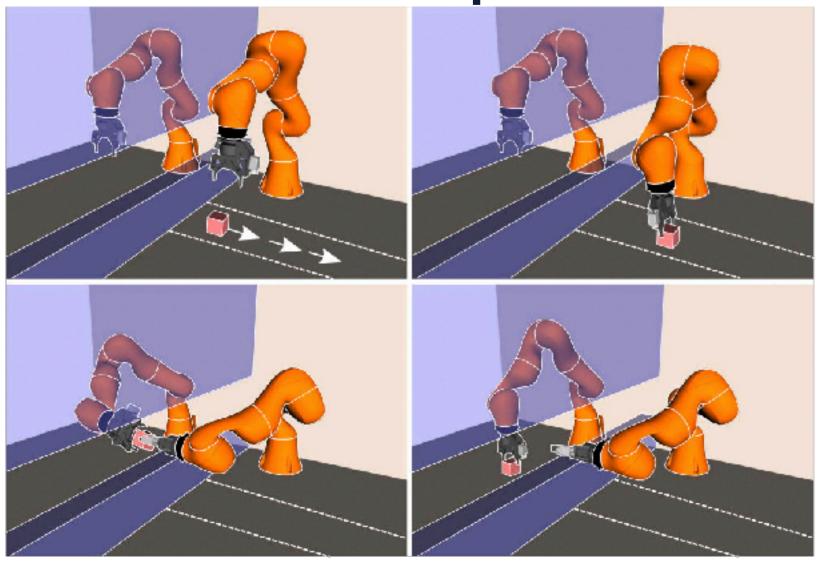


Introduction

- Property of Tasks
 - Variety of tasks
 - Example: moving conveyer belt, collaboration between robots
 - Dynamic and uncertain environments
 - Noisy environment
 - Need instantaneous reactions
 - Sequential interdependence of motions and actions
 - Subtle geometric and kinematics difference requires entirely different motion sequence

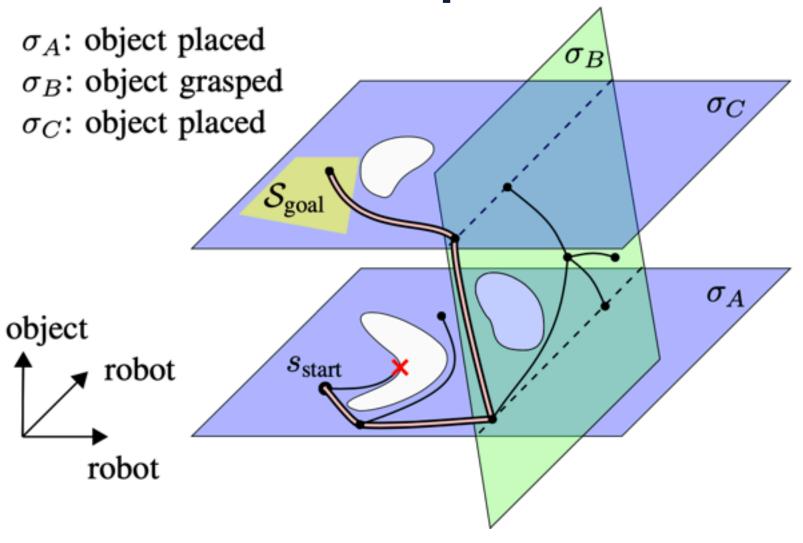
Related Works

- Constrained model based on or related to:
 - J. De Schutter, T. De Laet, J. Rutgeerts, W. Decre´, R. Smits, E. Aertbelie¨n, K. Claes, and H. Bruyninckx, "Constraint-based task specification and estimation for sensor-based robot systems in the presence of geometric uncertainty," *The Int. Journal of Robotics Research*, vol. 26, no. 5, pp. 433–455, 2007.
 - R. Alami, T. Simeon, and J.-P. Laumond, "A geometrical approach to planning manipulation tasks. the case of discrete placements and grasps," in *The fifth Int. Symposium on Robotics Research*. MIT Press, 1990, pp. 453–463.
 - J. Mirabel and F. Lamiraux, "Manipulation planning: addressing the crossed foliation issue," in *Int. Conf. on Robotics and Automation*. IEEE, 2017, pp. 4032–4037.
- Controller based on or related to:
 - E. Aertbelie n and J. De Schutter, "eTaSL/eTC: A constraint-based task specification language and robot controller using expression graphs," in *Int. Conf. on Intelligent Robots and Systems*. IEEE, 2014, pp. 1540–1546.
- Search Algorithm
 - D. Hsu, R. Kindel, J.-C. Latombe, and S. Rock, "Randomized kino-dynamic motion planning with moving obstacles," *The Int. Journal of Robotics Research*, vol. 21, no. 3, pp. 233–255, 2002.



System State

- Dynamic constrained graph
 - A configuration $q \in \mathbb{R}^n$
 - Including DOF of robot grippers and the cube
 - 7 DOF for each robot, 6 DOF for the cube, 20 DOF in total
 - A discrete mode $\sigma \in \Sigma$
 - Indicator about which face of the object is in contact with which surface (surface, conveyer, hand(s))
 - There are 24 modes in total in the example
 - There are different constrains and dynamics for different modes
 - If we can change from one mode to another one, then there is an edge between these two modes, thus making it a graph
 - Full State of the System: $s = (\sigma, q, \dot{q}, t)$



Constraints on States

- $f_{\sigma}(q,t)=0$ e.g., when a cube is on a surface, its height should be a fixed height since it cannot go up or down
- $g_{\sigma}(q,t) \leq 0$ e.g.,collision-free constraint: we use pairwise penetration depths to denote distance between objects. Ideally the depth should be negative so that no object collides with other objects
- $v_{\sigma}(q,\dot{q},t)=0$: time-derivative constraint: e.g., when a robot is grasping the cube, at contact points, the relative velocity between the cube and the robot gripper should be 0
- $\omega_{\sigma}(q,\dot{q},t) \leq 0$: time-derivative constraint: e.g., Axisvelocity-limits are given as inequality constraints.

Goal

• Goal of the planner: to find a finite sequence of controllers $\{\pi_i\}_{1\leq i\leq k}$ that steer the system from a start state s_{start} to a goal region s_{goal}

Affine Dynamics Model

- Vector u as input (14 robot axis accelerations)
- $\ddot{q} = a_{\sigma}(q, \dot{q}, t) + B_{\sigma}(q, \dot{q}, t)u$, $u_{min} \le u \le u_{max}$
- Note:
 - q includes both object (cube) and gripper configuration
 - But u only includes gripper axis acceleration
- Why affine?:
 - In case of a grasp, the acceleration of its pose is determined by the forward-kinematics of the grasping robot.
 - When the cube is placed on a surface its acceleration is zero.
 - If an object is placed on a conveyor belt, the equation is time dependent.



Kinodynamic Planner

- randomController(σ): returns a **controller** that **steers towards** a randomly chosen robot configuration satisfying the constraints of mode σ
- π = randomController(σ) can be simulated by simulateController(s, π), which will return the state s_{new} to which the system is moved by the random controller
- Similarly, transitionController(σ , σ_{new}) returns a controller π that steers towards the intersection of both mode's constraint manifolds while satisfying the constraints of σ

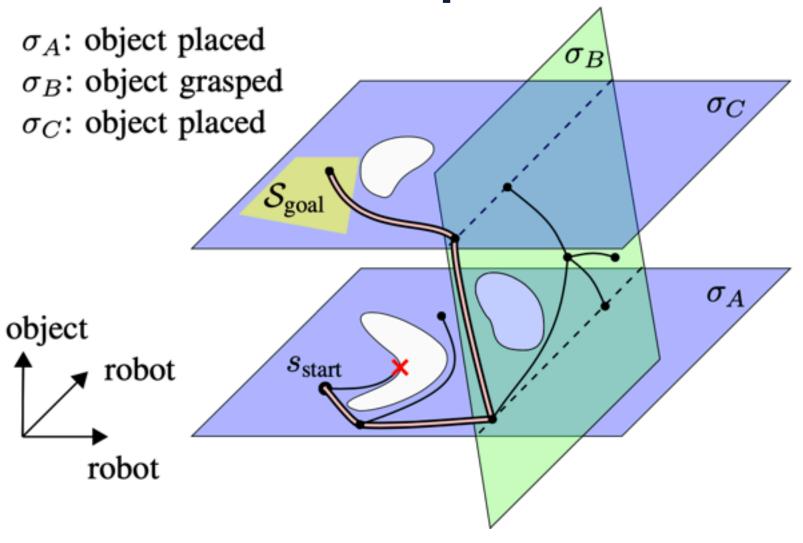
Procedure: buildSearchTree(s_{start}) infinite version

$$N \leftarrow \{s_{\text{start}}\}, \quad E \leftarrow \{\}$$

while true do

$$s \leftarrow (\sigma, q, \dot{q}, t) \leftarrow \text{sampleWeighted}(N)$$

$$\pi \leftarrow \operatorname{randomController}(\sigma) \\ s_{\operatorname{new}} \leftarrow \operatorname{simulateController}(s, \pi) \\ N.\operatorname{add}(s_{\operatorname{new}}), \quad E.\operatorname{add}((s, \pi, s_{\operatorname{new}}))$$
 Explore on the same mode



Controller Design with State Constraints

- Trajectories $\{q(t), \dot{q}(t)\}_t$ generated by transitionController has to satisfy
 - $f_{\sigma}(q,t) = 0$, $g_{\sigma}(q,t) \leq 0$
 - $v_{\sigma}(q, \dot{q}, t) = 0$, $\omega_{\sigma}(q, \dot{q}, t) \leq 0$
- If we could directly control f_{σ} , then we would generate the control signal for f_{σ} as

$$\ddot{f}_{\sigma} = -K_p^{f_{\sigma}} f_{\sigma} - K_d^{f_{\sigma}} \dot{f}_{\sigma},$$

• But we can only control u (axis acceleration)

•

• If we could directly control f_{σ} , then we would generate the control signal for f_{σ} as

$$\ddot{f}_{\sigma} = -K_p^{f_{\sigma}} f_{\sigma} - K_d^{f_{\sigma}} \dot{f}_{\sigma},$$

- But we can only control u (axis acceleration). Let us connect \ddot{f}_{σ} and u
- Note that \ddot{f}_{σ} is from the constraint on configurations, thus a function of \ddot{q} , and the **affine dynamics model** says \ddot{q} is a function of u:

$$\ddot{q} = a_{\sigma}(q, \dot{q}, t) + B_{\sigma}(q, \dot{q}, t)u, \qquad u_{min} \le u \le u_{max}$$

- . So we can approximate $\ddot{f}_{\sigma}(u)\approx \ddot{f}_{\sigma,u=0}+\frac{\partial f_{\sigma,u=0}}{\partial u}u$
- This gives us the control signal u:

$$\ddot{f}_{\sigma,0} + \frac{\partial \dot{f}_{\sigma}}{\partial u} u = -K_p^{f_{\sigma}} f_{\sigma} - K_d^{f_{\sigma}} \dot{f}_{\sigma},$$

Similarly, since we have to satisfy

•
$$f_{\sigma}(q,t) = 0$$
, $g_{\sigma}(q,t) \leq 0$

•
$$v_{\sigma}(q, \dot{q}, t) = 0, \omega_{\sigma}(q, \dot{q}, t) \le 0$$

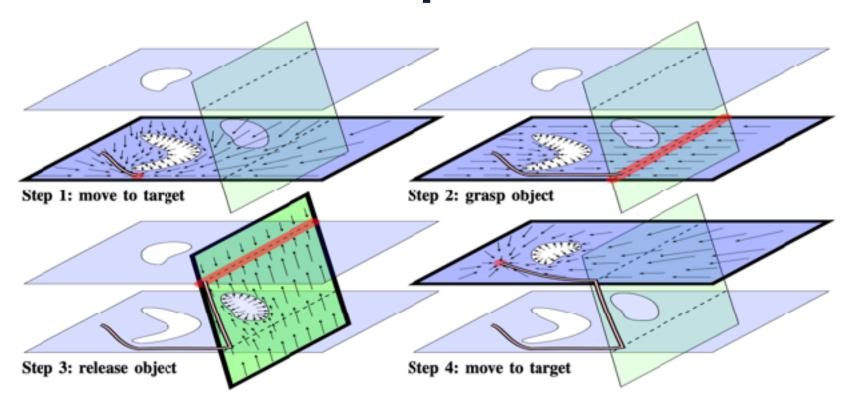
• We will have the full constraints on u

$$\begin{split} \ddot{f}_{\sigma,0} + \frac{\partial \ddot{f}_{\sigma}}{\partial u} u &= -K_p^{f_{\sigma}} f_{\sigma} - K_d^{f_{\sigma}} \dot{f}_{\sigma}, \\ \ddot{g}_{\sigma,0} + \frac{\partial \ddot{g}_{\sigma}}{\partial u} u &\leq -K_p^{g_{\sigma}} g_{\sigma} - K_d^{g_{\sigma}} \dot{g}_{\sigma}, \\ \ddot{f}_{\sigma',0} + \frac{\partial \ddot{f}_{\sigma'}}{\partial u} u &= -K_p^{f_{\sigma'}} f_{\sigma'} - K_d^{f_{\sigma'}} \dot{f}_{\sigma'} + \overbrace{\epsilon_{f'}}{\epsilon_{f'}} &\\ \ddot{g}_{\sigma',0} + \frac{\partial \ddot{g}_{\sigma'}}{\partial u} u &\leq -K_p^{g_{\sigma'}} g_{\sigma'} - K_d^{g_{\sigma'}} \dot{g}_{\sigma'} + \overbrace{\epsilon_{g'}}{\epsilon_{g'}} \end{split}$$

Quadratic Program

minimize
$$x^ op Hx$$
 subject to $L_A \leq Ax \leq U_A$ $L \leq x \leq U.$ Where $x = [u, \epsilon_{f'}, \epsilon_{g'}]^ op$

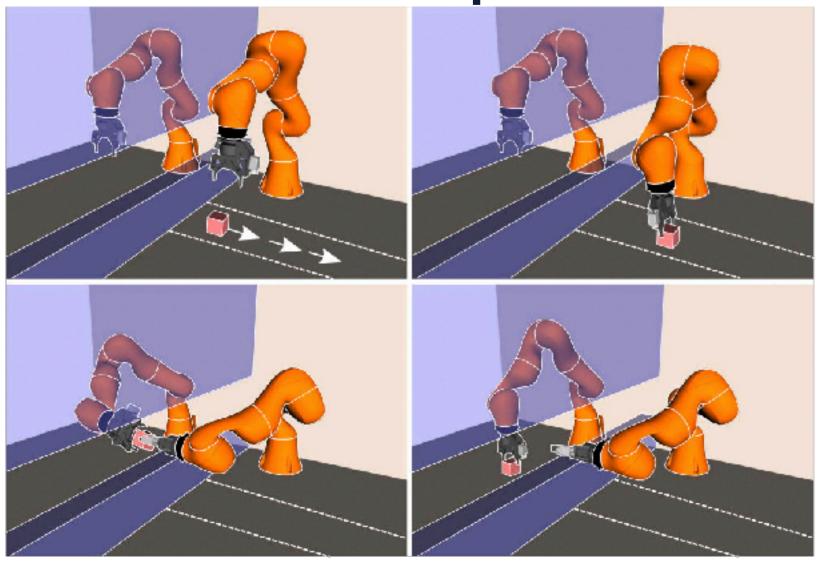
- For transitionController, we have the last two constraints involving σ'
- For randomController, we we only need the first two constraints



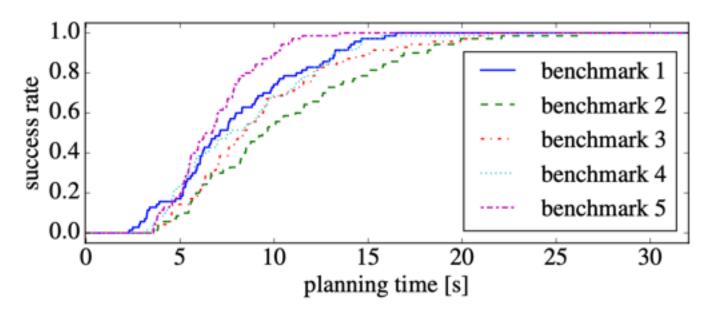
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Experiments

- Five benchmarks based on the two-robot objectpassing example
- Benchmark One
 - No obstacles, no moving conveyer belt
- Benchmark Two
 - Only lower wall
- Benchmark Three and Four
 - With lower and higher walls at different height
- Benchmark Five
 - With walls and a moving conveyer belt



Experiment



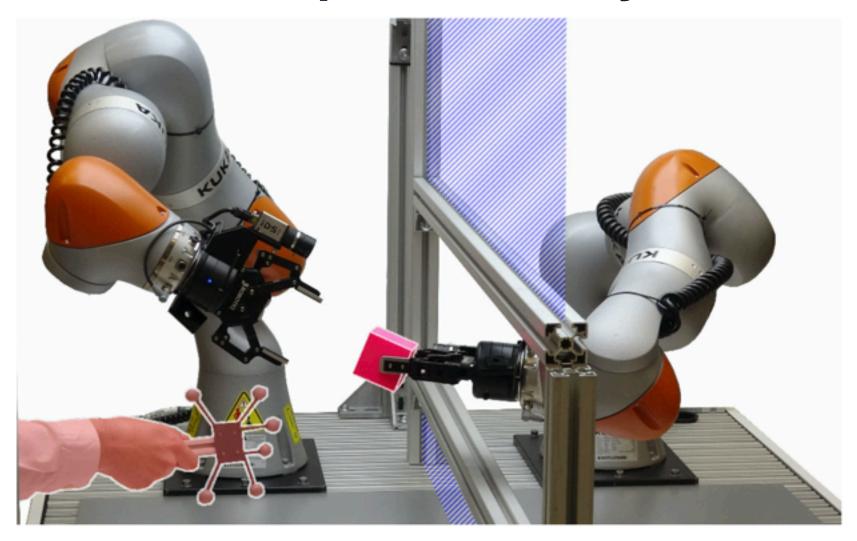
Both planners(this one and RMR algorithm) were implemented in C++, use multiple threads and were run on a ten-core Intel Xeon E5-2650v3

Experiment

PLANNING AND EXECUTION TIMES

all values in seconds [std. error of the mean]		Benchmark				
		1	2	3	4	5
proposed planner	planning time	7.89 [0.43]	10.5 [0.59]	9.27 [0.50]	8.39 [0.46]	6.79 [0.26]
paulier	execution time	14.3 [0.37]	17. 1 [0.36]	17.7 [0.20]	17.3 [0.09]	17.9 [0.14]
RMR*	planning time	6.44 [0.67]	8.18 [0.79]	21.3 [1.54]	>300	/
	execution time of first solution	10.7 [0.34]	11.8 [0.44]	14.9 [0.57]	/	/
	min. time at 60s	5.76	5.90	7.19	/	1

Example In Reality



Conclusion

- Dynamic Constrained Graph
- Kinodynamic Manipulation Planner
- Constraint-Based Controllers as Steering Functions
- Not only a model for robotics simulation but also works in reality. However, no demo is posted.
- Lack of formal guarantee that regarding probabilistic completeness and regions of attraction for the controller sequence.



Thank you for listening

Any questions?