

# **Rigid-Body Velocity and Robot Kinematics**

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# Review: Homogenous Transformation

- General Rigid-body Motion:
  - $T^{4 \times 4} = \begin{bmatrix} R & p \\ 0_{1 \times 3} & 1 \end{bmatrix}$ , where  $R \in SO(3), p \in R^3$
  - $T$  represent position and orientation in a single matrix
  - $\tilde{p} \triangleq \begin{bmatrix} p \\ 1 \end{bmatrix} \in R^4$
  - $T\tilde{p}$  change reference frame of  $p$

# Review: Physical Interpretation

- Rotation (**axis-angle**):
  - Any rotation in  $R^3$  is equivalent to rotation about a fixed axis  $\hat{\omega} \in R^3$  through an positive angle  $\theta$
  - Rotation:  $\{\hat{\omega}, \theta\}$
- General Rigid-Body Motion (**screw motion**):
  - Any  $SE(3)$  motion is equivalent to rotating about axis  $\hat{\omega} \in R^3$  through angle  $\theta$  while also translating along axis for  $d$ . This axis pass through point  $q \in R^3$
  - Homogenous Transformation:  $\{\hat{\omega}, \theta, q, d\}$

# Topics

- **Exponential Coordinate of SE(3)**
- Rigid-Body Velocity
- Robot Kinematics
- Case study: Hand-Eye Calibration

# Recall: the Lie Algebra of $SO(3)$

- Exponential coordinate:
  - $\hat{\omega}\theta \in R^3$
- Skew-symmetric Matrix:
  - $[\hat{\omega}]\theta \in so(3)$
- Rotation matrix:
  - $R = e^{[\hat{\omega}]\theta} \in SO(3)$
- Interpretation:
  - Axis-angle

# Goal: The Lie Algebra of SE(3)

- Exponential coordinate:
  - $\hat{\omega}\theta \in R^3$
- Skew-symmetric Matrix:
  - $[\hat{\omega}]\theta \in so(3)$
- Rotation matrix:
  - $R = e^{[\hat{\omega}]\theta} \in SO(3)$
- Interpretation:
  - Axis-angle
- Exponential coordinate:
  - $\hat{\xi}\theta \in R^6$
- $se(3)$  matrix:
  - $[\hat{\xi}]\theta \in se(3)$
- Homogenous transformation matrix:
  - $T = e^{[\hat{\xi}]\theta} \in SE(3)$
- Interpretation:
  - Screw motion

# Recall: Find $\mathfrak{so}(3)$ via ODE

- Consider a point  $q$  in body frame. At time  $t = 0$ , the position is  $q_0$ . Rotate  $q$  with **unit angular velocity** around axis  $\hat{\omega}$ :

- $v = \hat{\omega} \times r$

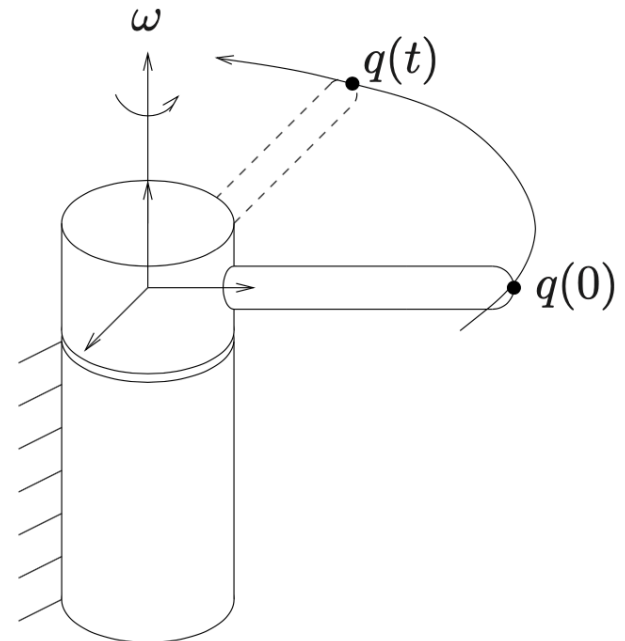
- $\dot{q}(t) = \hat{\omega} \times q(t) = [\hat{\omega}]q(t)$

- $q(t) = e^{[\hat{\omega}]t}q_0$

- Since  $\theta(t) = t$

$$p(\theta) = e^{[\hat{\omega}]\theta}p_0$$

- $[\hat{\omega}] \in \mathfrak{so}(3)$



# Find $se(3)$ via ODE of Screw Motion

- Consider a point  $p$  in body frame. Rotate  $p$  with **unit angular velocity** around fixed axis  $\hat{\omega}$ ,  $q$  is any point on this axis, the linear velocity along axis  $\hat{\omega}$  is  $v_\omega$ :

- $\dot{p}(t) = \hat{\omega} \times (p(t) - q) + v_\omega = [\hat{\omega}]p(t) - \hat{\omega} \times q + v_\omega$

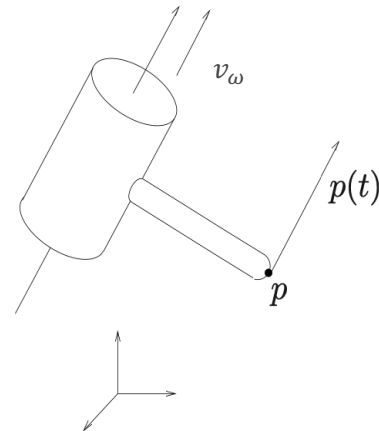
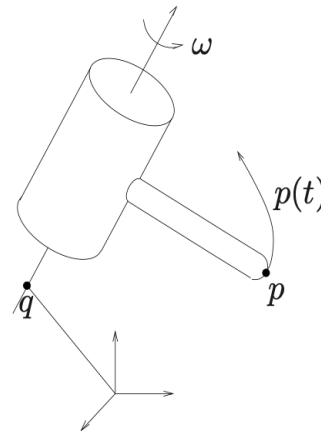
- $A \triangleq \begin{bmatrix} [\hat{\omega}] & -[\hat{\omega}]q + v_\omega \\ 0 & 0 \end{bmatrix} \triangleq \begin{bmatrix} [\hat{\omega}] & v \\ 0 & 0 \end{bmatrix}, \tilde{p}(t) = e^{At}\tilde{p}_0$

- Since  $\theta(t) = t$

$$\tilde{p}(\theta) = e^{A\theta}\tilde{p}_0$$

- For matrix  $A$ ,  $e^{A\theta} \in SE(3)$

$$A\theta \in se(3)$$





# Exponential Coordinate of SE(3)

- For rotation, define  $[\hat{\omega}]\theta \in so(3)$
- For homogenous transformation,  $\hat{\xi}\theta = \begin{bmatrix} \hat{\omega} \\ v \end{bmatrix} \theta \in R^6$ :

$$se(3) \triangleq \{[\hat{\xi}]\theta = \begin{bmatrix} [\hat{\omega}] & v \\ 0 & 0 \end{bmatrix} \theta : [\omega]\theta \in so(3)\}$$

- Recall:  $\hat{\omega}\theta$  is the exponential coordinate of 3D rotation
- Similarly,  $\hat{\xi}\theta \in R^6$  is the **exponential coordinate** of  $SE(3)$
- $\hat{\xi}$  is the **direction of motion**, which is also called **Unit Twist**

# Exponential Mapping of $se(3)$

- $\hat{\xi} = \begin{bmatrix} \hat{\omega} \\ v \end{bmatrix}$ ,  $e^{[\hat{\xi}]\theta} \in SE(3)$

$$e^{[\hat{\xi}]\theta} = I + [\hat{\xi}] + \frac{1 - \cos\theta}{\theta^2} [\hat{\xi}]^2 + \frac{\theta - \sin\theta}{\theta^3} [\hat{\xi}]^3$$

- This formula has **different form** compared to  $e^{[\hat{\omega}]\theta}$  for rotation
- Similarly, a log function exists uniquely:  $SE(3) \rightarrow se(3)$
- Note that  $\hat{\xi}$  means that the **first three value** has norm one, in another word  $\hat{\omega}$  is a unit vector, **no guarantee for  $v$**

# Example: $\hat{\xi}\theta$ to SE(3)

- Given  $\hat{\xi}_{sb}^s \theta = [\pi, 0, 0, 0, \pi, 0]^T$ , superscript:  $\{s\}$  frame

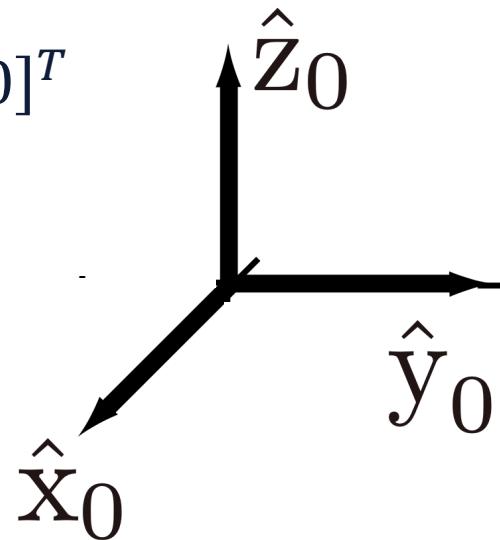
1. Find  $\hat{\xi}_{sb}^s = [1, 0, 0, 0, 1, 0]^T$ ,  $\theta = \pi$

2. Find rotation matrix by  $\hat{\omega} = [1, 0, 0]^T$

3. Find screw axis  $(\hat{\omega}, q)$  by  $v = -\hat{\omega} \times q + v_\omega$

$$v_\omega = [0, 0, 0]^T, -\hat{\omega} \times q = [0, 1, 0]^T$$
$$q = [0, 0, 1]^T$$

4. Find origin after transformation



# Example: $\hat{\xi}\theta$ to $\text{SE}(3)$

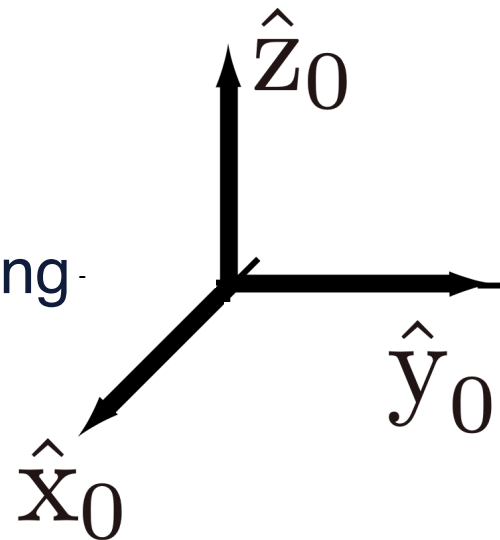
- Given  $\hat{\xi}_{sb}^s \theta = [\pi, 0, 0, 0, \pi, 0]^T$ , superscript:  $\{s\}$  frame

1.  $q = [0, 0, 1]^T, \hat{\omega} = [1, 0, 0]^T, v_\omega = [0, 0, 0]^T$

2. Recall screw motion

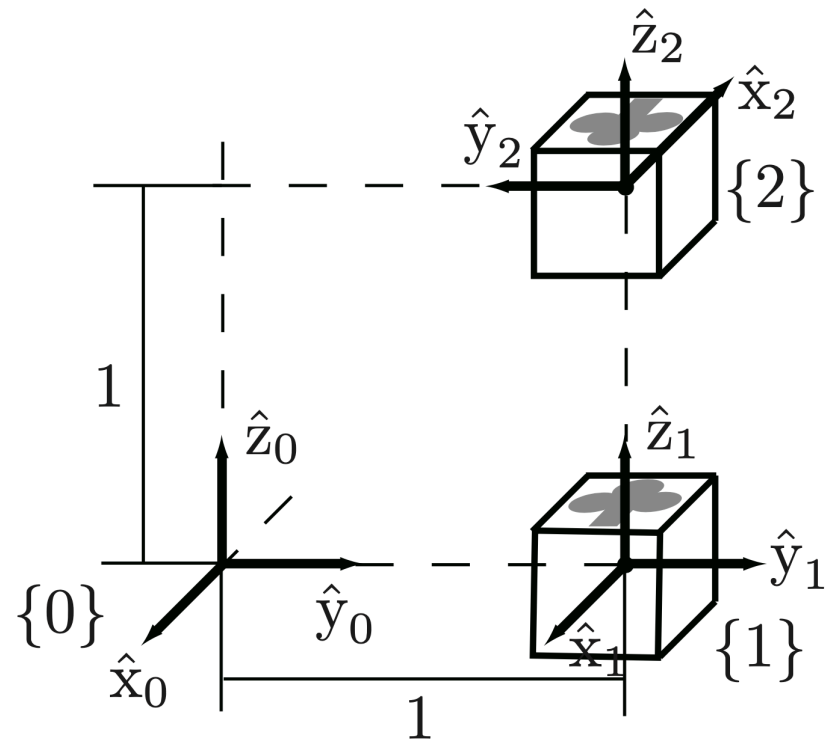
$$T_{sb} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & -1 & 2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Same result using exponential mapping



# Example: $SE(3)$ to $\hat{\xi}\theta$

Given  $SE(3)$ , find screw motion  $T_{02} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$



# Example: $SE(3)$ to $\hat{\xi}\theta$

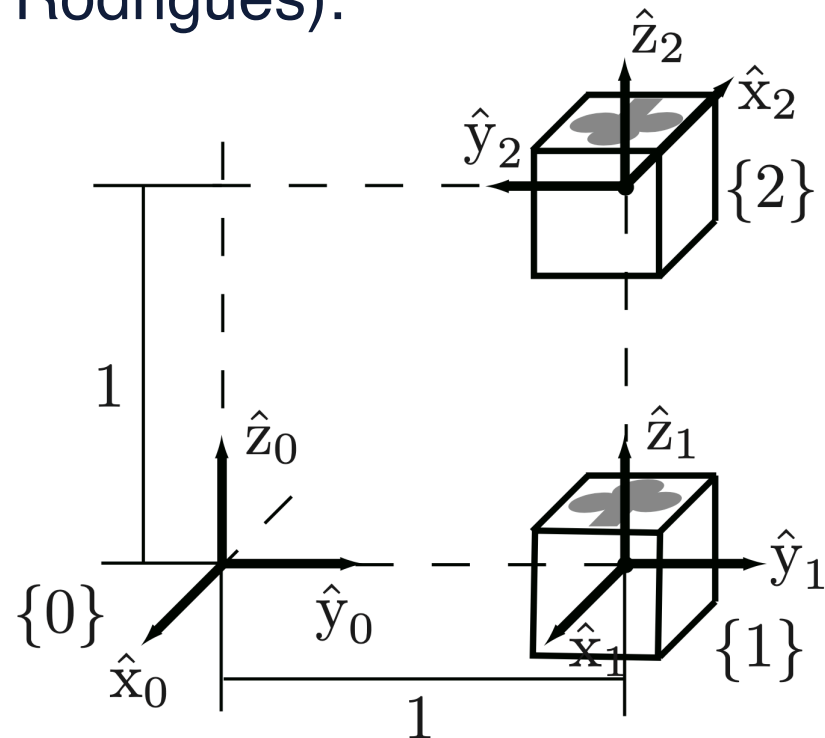
Given  $SE(3)$ , find screw motion

- $T_{02} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$

- Consider **rotation only** (Inverse Rodrigues):

- $tr(R) = -1 \Rightarrow \theta = \pi$

- $\hat{\omega} = \frac{1}{\sqrt{2(1+r_{33})}} \begin{bmatrix} r_{13} \\ r_{23} \\ 1 + r_{33} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$



# Example: $SE(3)$ to $\hat{\xi}\theta$

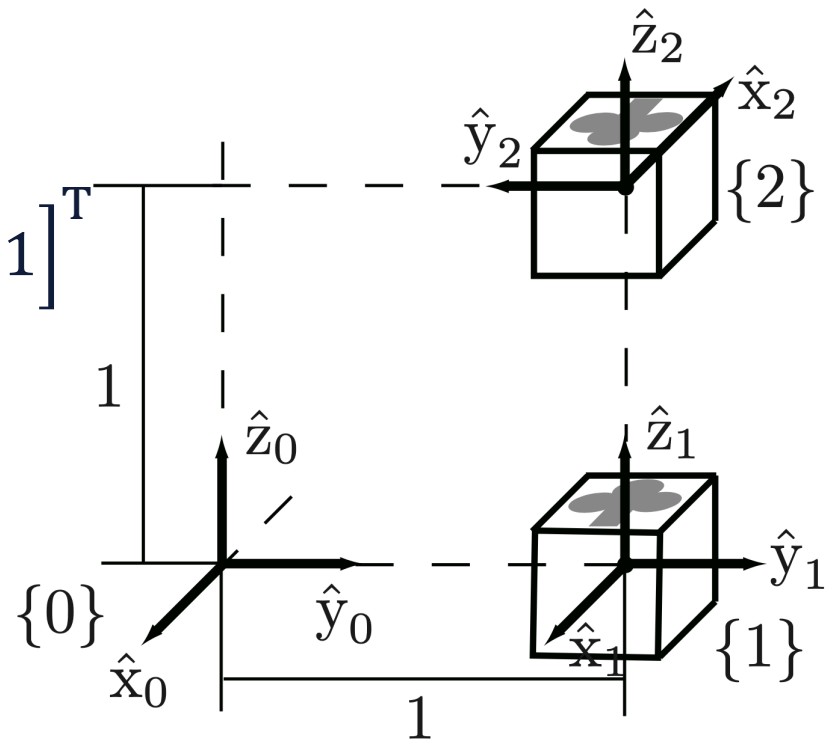
Given  $SE(3)$ , find screw motion

- $T_{02} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \hat{\omega} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$

- Find screw axis  $q = \left[0, \frac{1}{2}, 0\right]^T$

- Since  $v\theta = -\omega \times q + v_\omega \theta = \left[\frac{\pi}{2}, 0, 1\right]^T$

- Find  $\hat{\xi}\theta = \left[0, 0, \pi, \frac{\pi}{2}, 0, 1\right]^T$



# Comparison: $SO(3)$ and $SE(3)$

- Exponential coordinate:
  - $\hat{\omega}\theta \in R^3$
- Skew-symmetric Matrix:
  - $[\hat{\omega}]\theta \in so(3)$
- Rotation matrix:
  - $R = e^{[\hat{\omega}]\theta} \in SO(3)$
- Interpretation:
  - Axis-angle
- Exponential coordinate:
  - $\hat{\xi}\theta \in R^6$
- $se(3)$  matrix:
  - $[\hat{\xi}]\theta \in se(3)$
- Homogenous transformation matrix:
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- Interpretation:
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# Topics

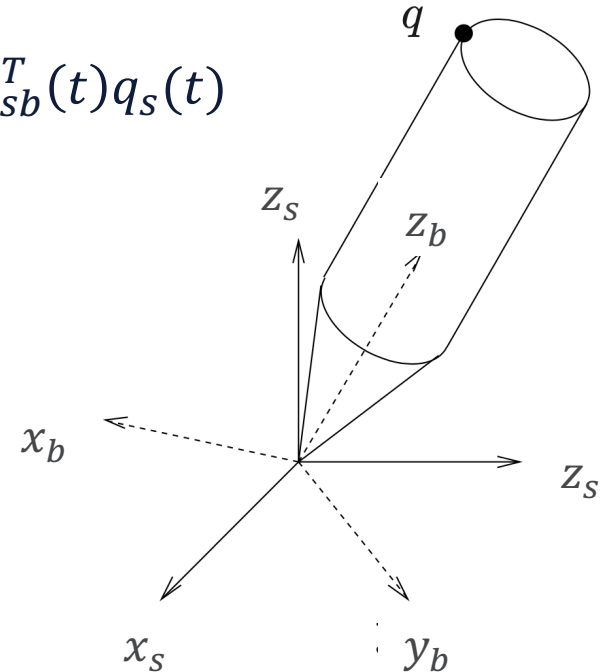
- Exponential Coordinate of SE(3)
- **Rigid-Body Velocity**
- Robot Kinematics
- Case study: Hand-Eye Calibration

# Angular Velocity from SO(3)

Question: for moving frame  $R(t)$ , find angular velocity  $\omega$  at any time  $t$

Consider a point  $q$  fixed on a moving frame  $\{b\}$ :

- Fact 1, change reference frame:
  - $q_s(t) = R_{sb}(t)q_b \rightarrow \dot{q}_s(t) = \dot{R}_{sb}(t)q_b$
  - $\dot{q}_s(t) = \dot{R}_{sb}(t)R_{sb}^T(t)R_{sb}(t)q_b = \dot{R}_{sb}(t)R_{sb}^T(t)q_s(t)$
- Fact 2, physical interpretation:
  - $\dot{q}_s(t) = [\omega(t)]q_s(t) = [\omega(t)]q_s(t)$



# Angular Velocity from SO(3)

Question: for moving frame  $R(t)$ , find angular velocity  $\omega$  at any time  $t$

- Fact 1:
  - $q_s(t) = R_{sb}(t)q_b \rightarrow \dot{q}_s(t) = \dot{R}_{sb}(t)q_b$
  - $\dot{q}_s(t) = \dot{R}_{sb}(t)R_{sb}^{-1}(t)R_{sb}(t)q_b = \dot{R}_{sb}(t)R_{sb}^{-1}(t)q_s(t)$
- Fact 2, physical interpretation:
  - $\dot{q}_s(t) = [\omega(t)]q_s(t)$
- For any  $q$  and  $\omega$   $[\omega(t)]q_s(t) = \dot{R}_{sb}(t)R_{sb}^{-1}(t)q_s(t)$ :

$$[\omega(t)] = \dot{R}_{sb}(t)R_{sb}^{-1}(t)$$

# Angular Velocity of Rigid-Body

$$[\omega(t)] = \dot{R}_{sb}(t)R_{sb}^{-1}(t)$$

- Why  $\dot{R}_{sb}(t)R_{sb}(t)$  can represent angular velocity?
- $\dot{R}_{sb}(t)R_{sb}(t)$  is a skew-symmetric matrix:
  - $R(t)R^T(t) = I \xrightarrow{\text{derivative}} \dot{R}(t)R^T(t) + R(t)\dot{R}^T(t) = 0$
  - $\dot{R}(t)R^T(t) = -R(t)\dot{R}^T(t) = -\left(\dot{R}(t)R^T(t)\right)^T$
  - $R(t)\dot{R}^T(t) \in so(3)$ , which is a skew-symmetric matrix

# General Velocity of Rigid-Body

Velocity of general motion can be represented as **twist**:

$$\text{Similarly, } [\xi] = \dot{T}(t) T^{-1}(t), T \in SE(3)$$

$$\xi_{sb}^s = \dot{T}_{sb} T_{sb}^{-1}, \text{ which is called } \mathbf{Spatial Twist}$$

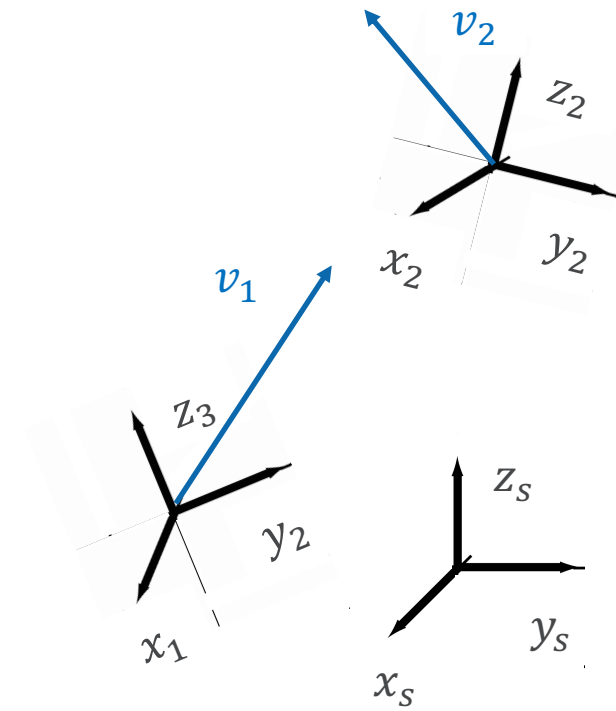
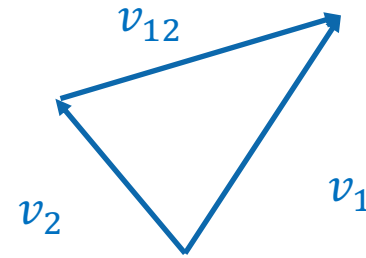
- Recall: exponential coordinate of  $SE(3)$  is  $\hat{\xi}\theta$
- $\hat{\xi}$  is called **unit twist**, where the  $\hat{\omega}$  in  $\hat{\xi}$  is a unit vector

# What is a Twist?

- **Unit twist** is the **direction of motion**:
  - $\hat{\xi}\theta$  can represent  $SE(3)$  motion
- **Twist** is the **velocity** of general rigid-body motion:
  - $\xi$  contains angular velocity and “linear velocity”
  - $\xi t$  can represent  $SE(3)$  motion

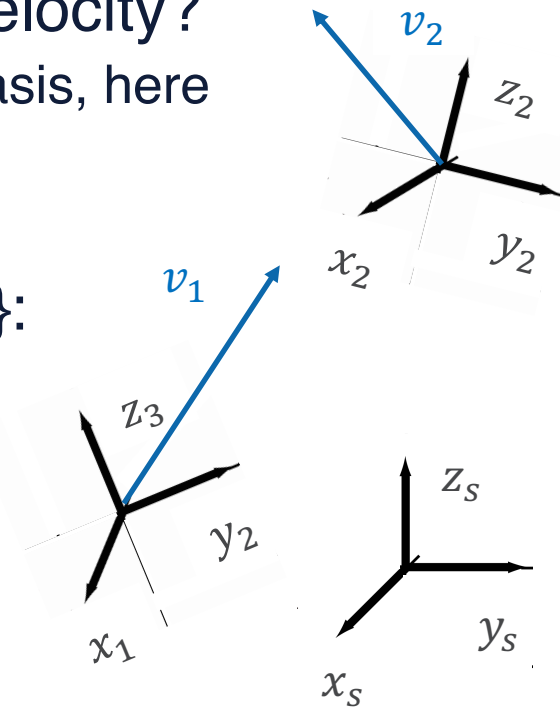
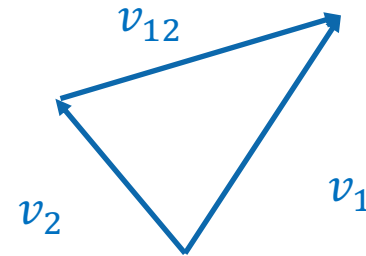
# How to Record a Velocity

- Any motion is relative: e.g. the velocity of frame {2} with respect to frame {1}
- Velocity of {2} relative to {1} is  $v_{12}$  :



# How to Record a Velocity

- Any motion is relative: e.g. the velocity of frame {2} with respect to frame {1}
- Velocity of {2} relative to {1} is  $v_{12}$  :
- Question: in which frame we record the velocity?
  - In order to write down  $v_{12}$ , we need a set of  $x, y, z$  basis, here we have three sets:  $\{s\}, \{1\}, \{2\}$
- If we record this velocity using basis of  $\{s\}$ :
  - The vector  $v_{12}$  is recorded as  $v_{12}^s$
- Similarly, using  $\{1\}$  to record:
  - The velocity  $v_{12}$  is recorded as  $v_{12}^1$





# Record a Twist

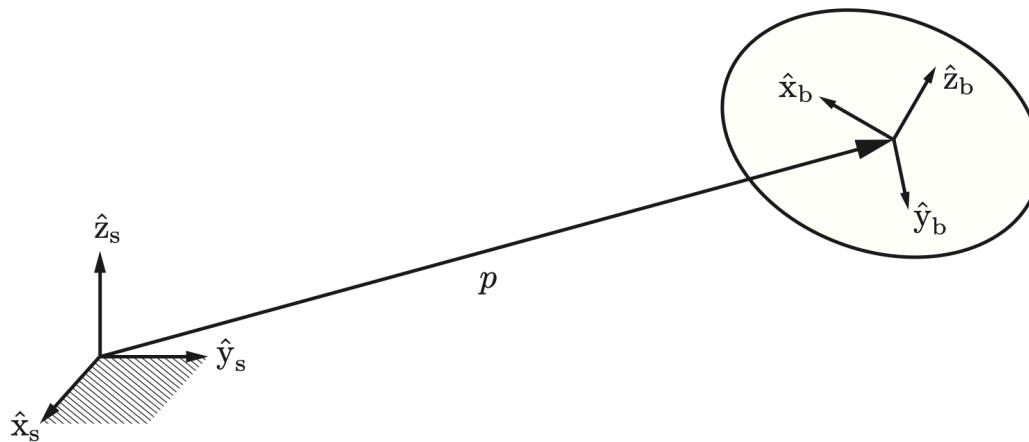
- Any twist is relative: e.g. the twist of frame  $\{2\}$  with respect to frame  $\{1\}$ , since **twist is a generalized velocity**
- Twist of  $\{2\}$  relative to  $\{1\}$  is  $\xi_{12}$  :
- Thus,  $\xi_{12}^s$  means record  $\xi_{12}$  using basis of  $\{s\}$
- The superscription of twist  $\xi^X$  is where the twist is recorded
- This is a reflection of Galilean Transformation Invariance

# Adjoint Matrix

- How to change the reference frame of a twist
- Adjoint matrix is used to change the reference frame of twist
- Adjoint matrix:  $[Ad_T] \triangleq \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \in R^{6 \times 6}$
- $\xi_{12}^s = [Ad_{T_{sb}}] \xi_{12}^b = \begin{bmatrix} R_{sb} \omega_{12}^b \\ [p_{sb}] R_{sb} \omega_{12}^b + R_{sb} v_{12}^b \end{bmatrix}$ 
  - Where  $T_{sb} = \begin{bmatrix} R_{sb} & p_{sb} \\ 0 & 1 \end{bmatrix}$ ,  $\xi_{12}^b = \begin{bmatrix} \omega_{12}^b \\ v_{12}^b \end{bmatrix}$
- Equivalently,  $[\xi_{12}^s] = T_{sb} [\xi_{12}^b] T_{sb}^{-1}$

# Spatial Twist and Body Twist

- $\xi_{sb}^s = \dot{T}_{sb} T_{sb}^{-1}$ , which is called **Spatial Twist**
- $\xi_{sb}^b = T_{sb}^{-1} \dot{T}_{sb}$ , which is called **Body Twist**
- Spatial Twist: velocities of the point in the body frame that corresponds with **the origin of the world frame**

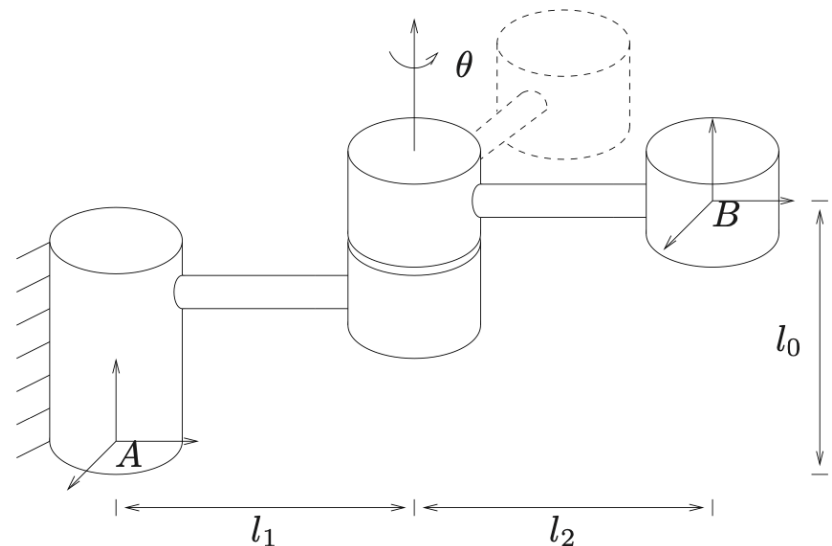


# Example: General Rigid-Body Velocity

- Given the motion of rigid-body

- $$T_{BA}(t) = \begin{bmatrix} \cos\theta(t) & -\sin\theta(t) & 0 & -l_2\sin\theta(t) \\ \sin\theta(t) & \cos\theta(t) & 0 & l_1 + l_2\cos\theta(t) \\ 0 & 0 & 1 & l_0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- What is the spatial twist?
- What is the body twist?

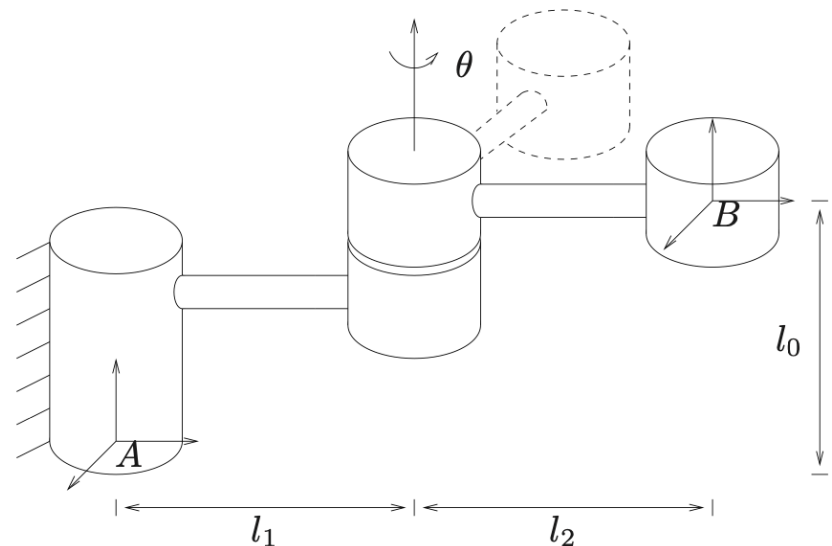


# Example: General Rigid-Body Velocity

$$T_{AB}(t) = \begin{bmatrix} \cos\theta(t) & -\sin\theta(t) & 0 & -l_2\sin\theta(t) \\ \sin\theta(t) & \cos\theta(t) & 0 & l_1 + l_2\cos\theta(t) \\ 0 & 0 & 1 & l_0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- $[\xi_{AB}^A] = \dot{T}T^{-1}, \xi_{AB}^A = [0, 0, 1, l_1, 0, 0]$

- $\xi_{AB}^B = T^{-1}\dot{T} = [Ad_{T_{AB}^{-1}}][\xi_{AB}^A]$



# Topics

- Exponential Coordinate of  $SE(3)$
- Rigid-Body Velocity
- **Robot Kinematics**
- Case study: Hand-Eye Calibration

# Robot Kinematics

Kinematics:

- Motion of bodies including spatial relationship of different objects and their velocity. Kinematics **does not consider** how to achieve motion via force



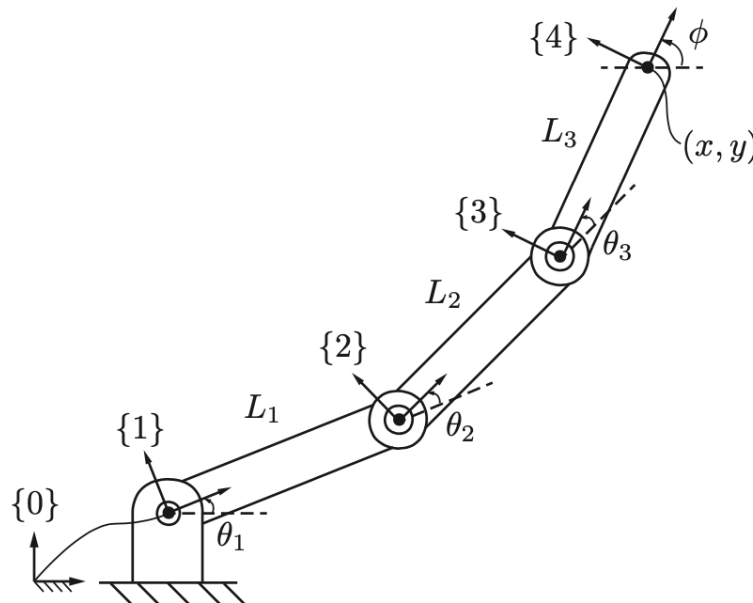
# Link and Joint

Link:

- **Links** are the rigid-body connected in sequence

Joint:

- **Joints** are the movable components of a **robot/object** that cause relative motion between adjacent links

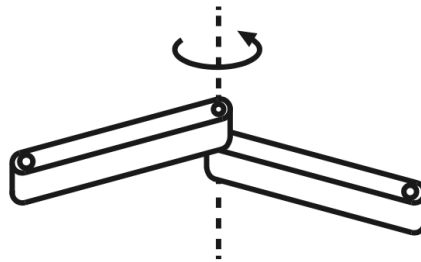




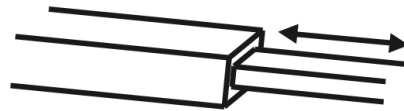
# Two Common Joint Type

Joint:

- Revolute/Hinge/Rotational joint
- Prismatic/Translational joint



Revolute  
(R)

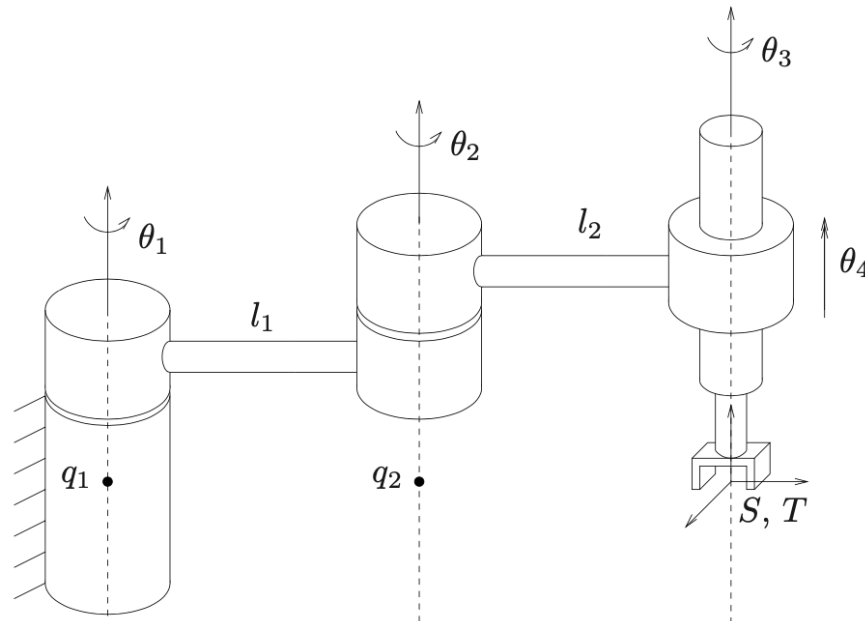


Prismatic  
(P)

# Forward Kinematics

## Robot Forward Kinematics:

- Calculate the position and orientation of a robot link (often end-effector) given its joint variables  $\theta = (\theta_1, \theta_2, \dots, \theta_n)$
- Before calculation, we need to **assign a frame** at each robot link



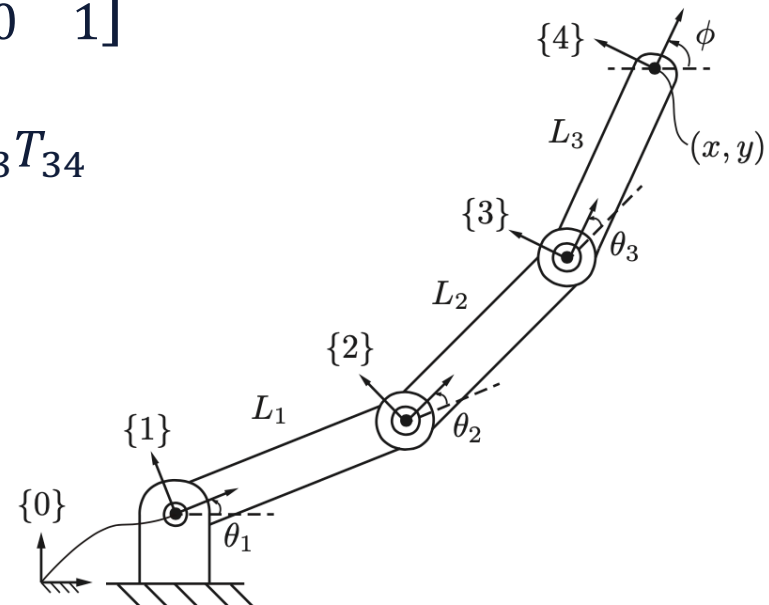
# Example: Forward Kinematics

Robot forward kinematics calculation:

- Represent the motion of each joint in  $SE(3)$
- Simply multiply each matrix

$$T_{01} = Rot(\hat{z}, \theta_1) \begin{bmatrix} \cos\theta_1 & \sin\theta_1 & 0 & 0 \\ \sin\theta_1 & \cos\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \text{ similarly } T_{12}, T_{23}, T_{34}$$

$$T_{04} = T_{01}T_{12}T_{23}T_{34}$$

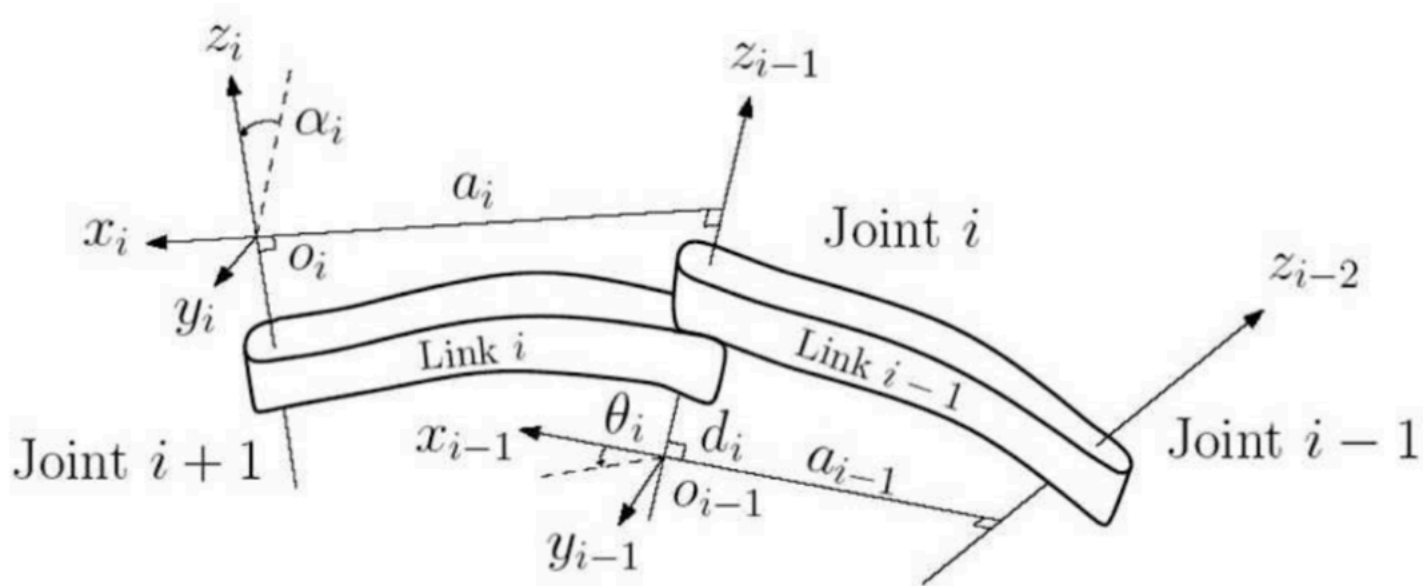


# D-H Parameters

Frame assignment in 3D space is not trivial

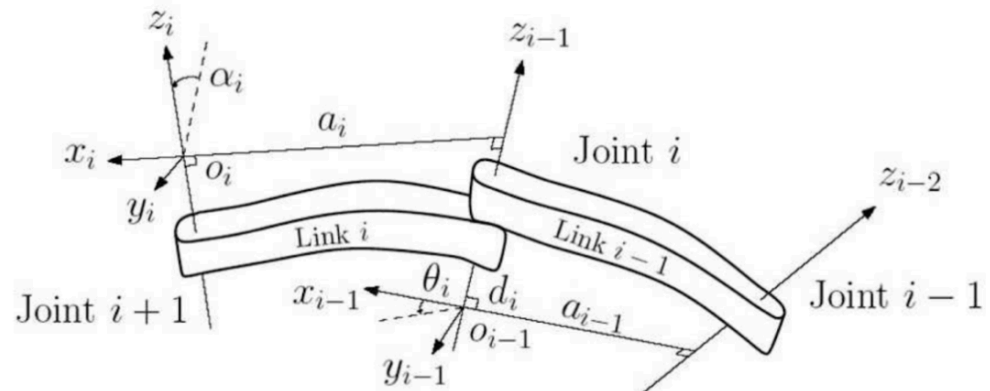
Can we find a unique way to assign frames?

- **Denavit-Hartenberg (D-H) Parameters:**
  - Applying a set of rules which specify the position and orientation of frames attached to each link of the robot



# D-H Parameters

- **Denavit-Hartenberg (D-H) Parameters:**
  - Redundancy of link relative pose, no need to use 6-DoF  $SE(3)$  representation
  - Link offset  $d_i$ : translate along  $z_{i-1}$
  - Link length  $a_i$ : translate along  $x_i$
  - Twist angle  $\theta_i$ : rotate along  $x_i$
- No need to understand these parameters in this course
- D-H parameters can **represent robot kinematics model**



# Example: D-H Table



$i$	$\alpha_i$	$a_i$	$d_i$	$\theta_i$
1	$\pi / 2$	0	-D1	$q_1$
2	$\pi / 2$	0	0	$q_2$
3	$\pi / 2$	0	-(D2 + D3)	$q_3$
4	$\pi / 2$	0	-e2	$q_4$
5	$\pi / 2$	0	-(D4 + D5)	$q_5$
6	$\pi / 2$	0	0	$q_6$
7	$\pi$	0	-(D6 + D7)	$q_7$

# Jacobian

- Recall: In algebra course, Jacobian of a function  $x = f(\theta)$  can be defined as, where  $x \in R^m, \theta \in R^n$ :

$$J(\theta) \triangleq \left[ \frac{\partial f}{\partial \theta}(\theta) \right] = \left[ \frac{\partial f_i}{\partial \theta_j} \right] \in R^{m \times n}$$

- Jacobian can relate the derivative of two variable together, if both  $x$  and  $\theta$  is the function of another variable  $t$

$$\dot{x} = \left[ \frac{\partial f}{\partial \theta}(\theta) \right] \frac{d\theta}{dt} = J(\theta) \dot{\theta}$$

# Geometric Jacobian

Question: where will robot end-effector move given velocity of each joint?

- Velocity for a  $SE(3)$  pose can be represented as twist  $\xi$
- Geometric Jacobian  $J(\theta)$ :

$$\xi = \begin{bmatrix} \omega \\ v \end{bmatrix} = J(\theta)\dot{\theta}, \text{ where } J(\theta) \in R^{6 \times n}, n \text{ is robot DoF}$$

- The  $i$ -th column of  $J(\theta)$  is the twist when the robot is moving about the  $i$ -th joint at unit speed  $\dot{\theta}_i = 1$  while all other joints stay static



# Geometric Jacobian Calculation

Question: how to compute Geometric Jacobian?

- Using forward kinematics:  $T_{sb}(\theta) = f(\theta)$
- General velocity:  $[\xi_{sb}^s] = \dot{T}_{sb} T_{sb}^{-1}$ , where  $\dot{T}_{sb} = \frac{\partial T_{sb}}{\partial t} = g(\dot{\theta})$
- Compute each column of geometric Jacobian  $J(\theta)$ :

Let  $\dot{\theta}_i = 1$  and  $\dot{\theta}_j = 0$  for  $j \neq i$

i-th column of  $J(\theta)$  will be  $\frac{\partial T_{sb}}{\partial \dot{\theta}} T_{sb}^{-1}$

# Inverse Kinematics

## Inverse Kinematics (IK):

- Given the forward kinematics  $T(\theta)$  and the target pose  $T_{\text{target}} \in SE(3)$ , find solutions  $\theta$  that satisfy  $T(\theta) = T_{\text{target}}$
- **Analytical solution** of IK for robot with more than 3-DoF is very complex:
  - For a 6-DoF robot, you will need a several pages to write down the formula
- If you need analytical solution, just use libraries:
  - IKFast, IKBT

# Numerical Solution of IK

Numerical IK, a root finding problem

- Inverse kinematics can be viewed as finding roots of a nonlinear equation with  $SE(3)$  constrain
- Standard root-finding algorithm can be adapted for  $T(\theta) = \xi^b$ , e.g. Newton-Raphason method
- The gradient for this method is geometric Jacobian

$$J(\theta^i) = \frac{\partial f}{\partial \theta} \big|_{\theta^i}, \Delta\theta^i = J^{\dagger}(\theta^i)\Delta\xi,$$

where  $\Delta\xi$  is the difference of pose in exponential coordinate

$$\theta^{i+1} = \theta + \Delta\theta^i$$

# Kinematic Singularity

Question: is it possible to move end-effector to any direction  $\hat{\xi}$  for a robot with  $DoF \geq 6$

- The pseudo inverse  $J^+(\theta)$  map link twist back to joint velocity
- Kinematic singularity:
  - A **robot configuration** where the robot's end-effector loses the ability to move in one direction instantaneously
- Mathematically,  $J(\theta)$  rank deficiency leads to kinematic singularity
- Kinematic singularity does not mean that there exists a configuration that is not accessible

# Topics

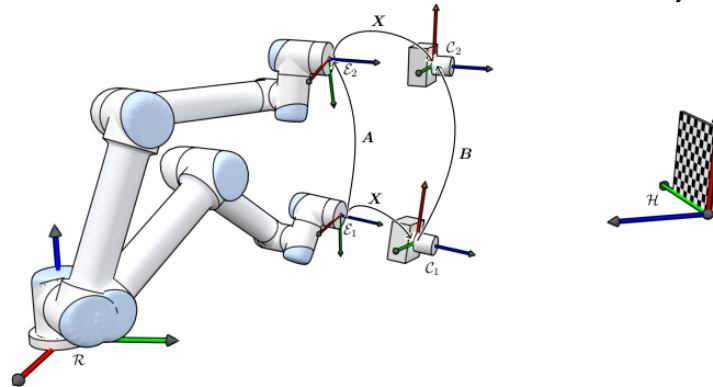
- Exponential Coordinate of  $SE(3)$
- Rigid-Body Velocity
- Robot Kinematics
- **Case study: Hand-Eye Calibration**

# Vision-based Robotic Planning

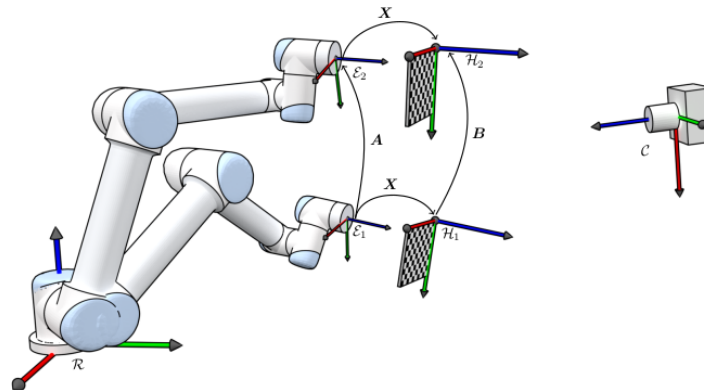
- Visual perception comes from camera/lidar, the position and orientation is captured in sensor frame
  - E.g., point cloud in camera frame
- Moving signal is command in robot frame
  - E.g., move the robot hand left in robot base frame
- Hand-eye Calibration computes the transformation from camera to robot

# Settings of Hand-eye Calibration

- There are two kinds of problem for hand-eye calibration
- Eye-in-hand (camera mounted on hand):



- Eye-to-hand (camera not fixed with hand):

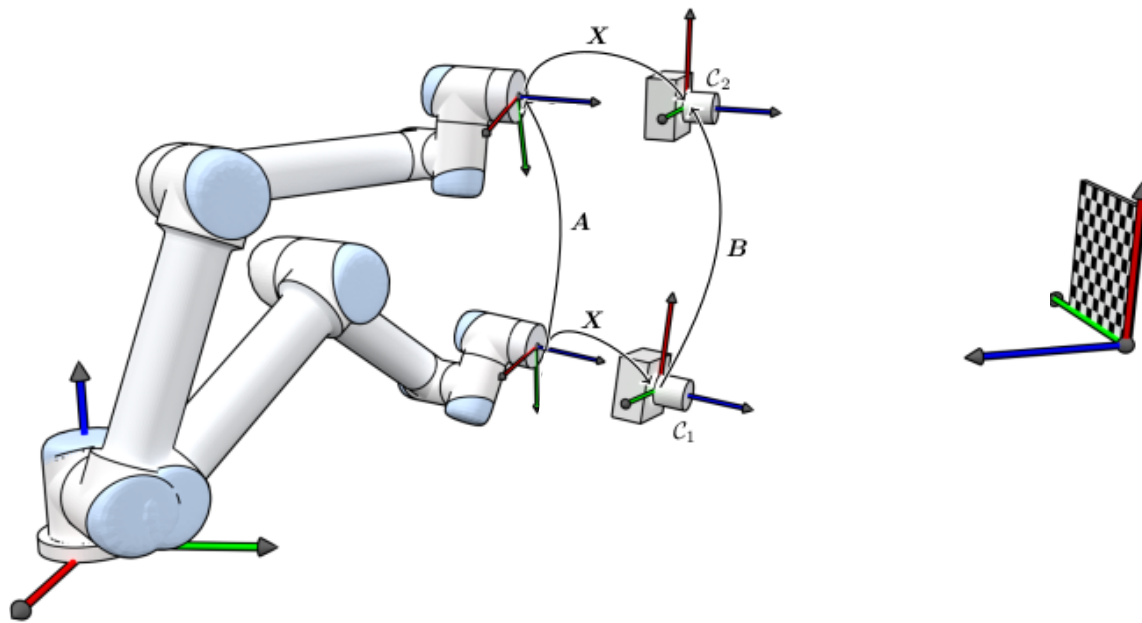


# Hand-Eye Transformation Equation

Take *eye-in-hand* (e.g. camera fixed to hand) as example

- Goal: transformation from camera to hand  $T_{hc}$
- Denote: space frame (robot base)  $\{s\}$ , camera  $\{c\}$ , hand  $\{h\}$ , and marker (auxiliary object)  $\{m\}$

$$T_{sh}T_{hc}T_{cm} = T_{sm}$$



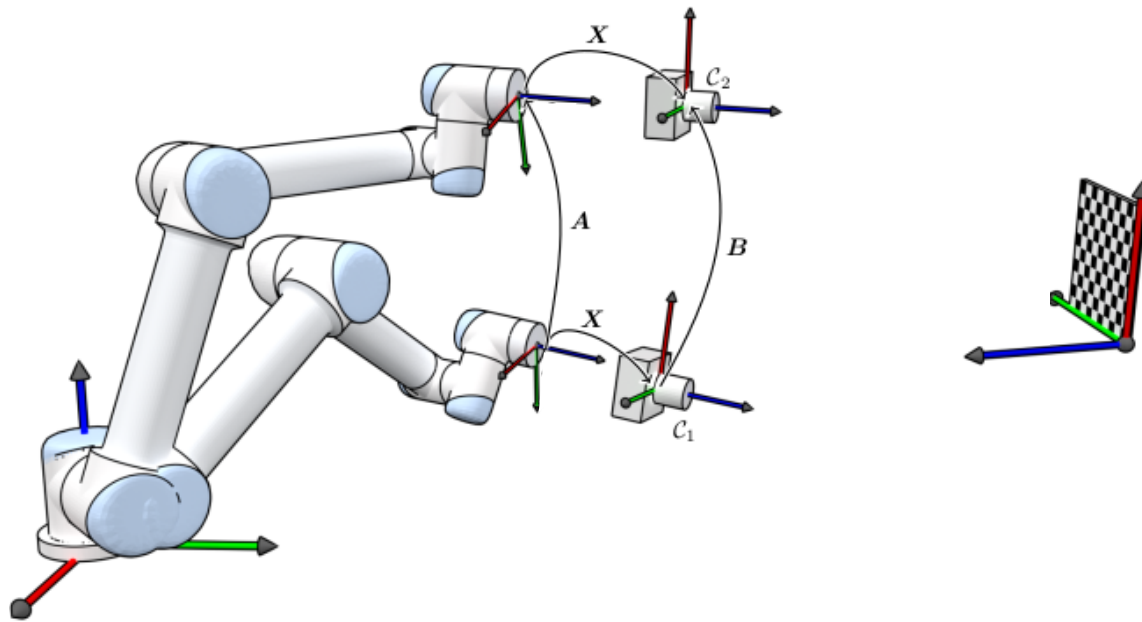


# Hand-Eye Transformation Equation

- Take *eye-in-hand* (e.g. camera fixed to hand) as example
- Assume we can get the pose of marker in camera frame

$$T_{sh} T_{hc} T_{cm} = T_{sm}$$

Known Variant      What we want Constant      Assume known Variant      Unknown Constant



# Capture Calibration Data

To solve the hand-eye transformation equation, we need to prepare multiple pairs of  $T_{sh}$  and  $T_{cm}$

- Repeat the following steps for n-times:
  1. Move the robot hand to a target pose, where camera can see the marker
  2. Capture the  $T_{sh}^i$  for i-th pose of hand to base, often calculated by forward kinematics
  3. Capture the  $T_{cm}^i$  for i-th pose of marker to camera, calculated by a marker-specific algorithm

# $AX=XB$ for Hand-Eye Calibration

- The pose from marker to spatial frame  $T_{sm}$  is fixed

$$T_{sh}^i T_{hc} T_{cm}^i = T_{sm} = T_{sh}^{i+1} T_{hc} T_{cm}^{i+1}$$
$$(T_{sh}^{i+1})^{-1} T_{sh}^i T_{hc} = T_{hc} T_{cm}^{i+1} (T_{cm}^i)^{-1}$$

- Now we get a  $AX = XB$  type function with constraints
  - $A = (T_{sh}^{i+1})^{-1} T_{sh}^i$  and  $B = T_{cm}^{i+1} (T_{cm}^i)^{-1}$  are all known
- It is common to use multiple pairs of data for the equation. Actually, **at least three pairs** are necessary in order for a unique solution.

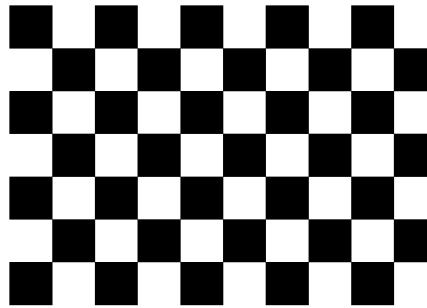
# Solving $AX=XB$

Note that the  $X \in SE(3)$ , which is a constrain to this equation

- Two mainstream to solve this equation
  1. Determine first rotation and then translation<sup>1</sup>
  2. Determine rotation and translation simultaneously<sup>2</sup>
- To solve the equation more precisely:
  - Poses of hand are chosen follow some **solver-specific guidelines**
  - More data

# Markers for Hand-eye Calibration

- Checkerboard is a most common visual marker in robotics:
  - Checkerboard pose can be easily solved using standard method like PnP



- As long as we have method to estimate its pose, anything can be a marker