

Article

Initial Field Testing Results from Building-Integrated Solar Energy Harvesting Windows Installation in Perth, Australia

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Featured Application: Unconventional, highly transparent building integrated photovoltaics.

Abstract: We report on the field testing datasets and performance evaluation results obtained from a commercial property-based visually-clear solar window installation site in Perth-Australia. This installation was fitted into a refurbished shopping center entrance porch and showcases the potential of glass curtain wall-based solar energy harvesting in built environments. In particular, we focus on photovoltaic (PV) performance characteristics such as the electric power output, specific yield, day-to-day consistency of peak output power, and the amounts of energy generated and stored daily. The dependencies of the generated electric power and stored energy on multiple environmental and geometric parameters are also studied. An overview of the current and future application potential of high-transparency, visually-clear solar window-based curtain wall installations suitable for practical building integration is provided.

Keywords: renewables; energy saving and generation; built environments; solar windows; advanced glazings; photovoltaics

1. Introduction

The global building integrated photovoltaics (BIPV) market is likely to expand from USD 6.7 billion to USD 32.2 billion by 2024, witnessing a compound annual growth rate (CAGR) of 23.4% over the forecast period [1]. This growth trend is due to both the increasing availability of new and innovative BIPV products, and the growing attention of the architects, city planners, property developers, and governments towards the sustainable construction practices and the integration of renewable energy generators into urban landscapes. At the same time, the worldwide annual energy consumption continues to grow, and is projected to exceed 0.74 billion TJ by 2040, with the generation contributions from fuels other than coal (mainly renewables) being on the increase [2]. Global warming-related concerns and environmental protection trends and policies also continue to favor the development of renewable energy generation and storage facilities [3–6]. At present, the BIPV technologies and products are only beginning to experience their expected widespread adoption, and a range of different novel technologies are being introduced into the well-established market of construction materials [7–12]. The benefits of distributed energy generation (an approach based on employing a combination of small-scale technologies to produce electricity close to the end users of power) include the avoidance of significant transmission-line losses and the provision of blackout resistance. Generating electricity at the point of its use can also lead to making the urban built environments potentially grid-independent, even if this energy supply independency is provided

only on limited time-scales. Multiple recent literature sources emphasize the importance of distributed generation networks and the development of sustainable microgrids [13–15]. Advanced building-scale integration of renewable energy generators utilizing most of the available deployment areas, including walls and windows, can lead towards future city-scale distributed generation networks in “smart cities”. Additionally, the emergent concept of “smart facades” that provide locally window-embedded self-powering environmental sensor systems integrated with window-powered equipment, such as motorized blinds, is gaining increasing attention in commercial engineering circles [16]. The most desired attributes of building wall-integrated PV are either the highly-transparent, perfectly-clear visual appearance, or a possibility of significant (active or passive) control over their transparency, appearance, and color. A number of recent and detailed reviews of the current trends in BIPV are available [17–20], with the most recent sources underscoring the importance of transparent photovoltaics and solar windows, which have just started to appear on the market at present, packaged as installation-ready framed systems suitable for long-term environmental exposure.

The importance of energy-efficient construction practices is currently gaining substantial attention from multiple governments and research groups worldwide, leading to the emergence of a large range of principally new construction materials and their components, such as advanced coatings which ensure improved thermal insulation and/or change transparency in response to external conditions [21]. It is the combination of the energy saving and energy generation functionalities possible to be engineered in modern windows that is of primary interest for leading architects and property developers. In early 2019, Vicinity Centres (a real estate investment trust company based in Melbourne, Australia) has installed 18 transparent solar windows supplied by Clearvue Technologies Ltd. (Perth, Australia), into a refurbished entrance porch of Warwick Grove Shopping Centre in Warwick (a northern suburb of Perth), in order to evaluate their suitability and practical application potential in commercial property settings. The installation site is illustrated in Figure 1.

The solar window design type was derived from the previous transparent solar window designs, multiple prototype models of which have been developed by Edith Cowan University (ECU) and Clearvue Technologies over several recent years and were trialed in 2017 at a grid-independent bus stop in Melbourne [22]. Several engineering features related to the glazing system structure, window size, system packaging-related details, and solar modules circuitry implementation have changed since these were reported originally [22], improving the peak-rated electric power output of transparent solar windows towards $30 \text{ W}_\text{p}/\text{m}^2$, measured at standard test conditions (STC) using the manufacturer-sourced large-scale flash-lamp PV testing equipment. The core design and assembly-related features of solar windows remained almost the same, and included the triple-glazed structure, low-iron glass plates, low-emissivity heat-mirror coating, and particles of high Stokes-shift inorganic luminescent materials embedded into a lamination interlayer. More technical details are available from [23–26], whilst the general system design philosophy has been derived from the approaches reported throughout the last several decades in [27–30], and in references therein. This present study represents, to the best of our knowledge, a world-first report on the field performance characteristics and practical application potential of high-transparency, clear glass-based solar windows built using all-inorganic functional materials, in built environments where the windows are mounted in multiple geometric orientations.

The following sections of this article provide the installation-specific microgrid configuration details, the results of preliminary microgrid modelling, and the results of a case study of the energy harvesting efficiency conducted over May–June 2019. Additional datasets extending the system monitoring results until early September 2019 are presented within the Supplementary data file (Table S1 and multiple additional Worksheets within the file). We then summarize the data and main results, providing an outlook for the future application potential of transparent solar windows, and propose some new future application areas.



Figure 1. Entrance porch (atrium) of Warwick Grove Shopping Centre in Warwick (Perth, WA, Australia) constructed using 18 solar windows supplied by Clearvue Technologies Ltd. (Perth, WA, Australia). (a) front view and (b) top view, with the inset showing satellite image of the same entrance atrium structure prior to solar windows installation. The site orientation-related data are also shown; the roof sides are tilted at $\approx 37^\circ$ from horizontal plane.

2. System Design Features, Methodologies of Energy Harvesting Performance Assessment, and Principal Results

Each of the 18 solar windows, factory-assembled at Qingdao Rocky Technical Glass Co., Ltd. (Qingdao, China) have been re-tested following their shipment to Perth, in outdoor morning sunlight conditions, confirming stable operation and the expected power outputs. Approximately (27 ± 1) W of electric output has been obtained from each window at close to their optimal geometric orientation and tilt angles towards the incoming natural sunlight, and at solar module surfaces being at $> 37^\circ\text{C}$. The weather conditions in mid-April in Perth (at the time of testing) were typical for autumn, and without strong UV irradiation background (likely at UV index near 5, out of the yearly maximum

of 12 [31]). The typical measured output parameters from each window were as follows: Open-circuit voltage $V_{oc} = 58.85V$, short-circuit current $I_{sc} = 0.723\text{ A}$, and Fill Factor $FF = 0.639$. The maximum power point (MPP) parameters corresponded to $V_{MPP} = 49.5\text{ V}$ and $I_{MPP} = 0.55\text{ A}$. The same windows of area size near 1.3 m^2 ($1.087\text{m} \times 1.2\text{m}$) have been tested at STC previously, resulting in electric outputs being in excess of 36 W ; the differences with the outdoor test results were due to both the solar cell temperature effects, and also the weather-dependent solar irradiation power density. The strip-shaped PV modules used in solar windows at and near their glass panel edges were custom-fabricated by China Solar Ltd. (Shenzhen, China), by way of encapsulating multiple series-connected monocrystalline silicon cells of nominal efficiency near 20%, using a proprietary process.

2.1. System Configuration Features and Preliminary Modeling Results

Three principal deployment areas were available on-site for the installation of 16 unshaded solar window units: (i) An East-facing tilted roof section, with 4 parallel-connected windows; (ii) a North-facing vertical wall section, containing 8 windows, and (iii) a West-facing tilted roof section with 4 windows. An additional deployment area on the east-facing vertical wall housed 2 more window units, which were strongly shaded by the nearby car-park roofing during most of the daylight hours. The shopping center atrium installation at Warwick Grove Shopping Centre (Figure 1) was completed in early 2019 [32], and a systematic study of its energy harvesting performance commenced in May 2019, following a short period of initial configuration tests and some reconfiguration of the microgrid equipment and circuitry used. Vicinity Centres has stated their commitment to achieving Net Zero carbon emissions by 2030 [33], and solar energy harvesting can be expected to play a major role in reaching this objective. Vicinity Centres' giant solar energy program and roadmap of renewable energy installations have led to winning the "People's Choice" award at the Property Council of Australia/Rider Levett Bucknall Innovation and Excellence Awards 2019 [34].

Figure 2 shows a graphical summary of the microgrid circuitry details and equipment configuration installed, as well as sample plots of the daily power generation and use waveforms recorded by Enphase Energy's Enlighten Systems applications programming interface (API) over several days in May 2019. Four Enphase microinverters (Enphase Energy Inc., Fremont, CA, USA) were installed to service the four separate solar window installation areas described above; each microinverter collected the combiner-box bundled parallel-connected electric output from the windows placed into each installation area. A LED TV panel (powered by the generated energy stored in batteries) was installed in the shopping center entrance foyer and was configured to display a graphic summary of the system operation state (also shown in Figure 2). The main system parameters displayed, related to the generation of energy and carbon offset capacity, were also configured for online live internet broadcasting at <http://tcp.iotstream.io/vicinity-warwickgrove/index.php>. The live power generation data are being refreshed every 15–20 minutes, and the amounts of daily and total generated energy (since May 14, 2019) are also shown. Electric loads other than LED TV included a computer system (Intel NUC small-form mini PC), modem (D-Link GSM), and two 30 W LED ceiling lamps within the foyer area, used continually for about 12 h daily. The energy storage was enabled by installing twin LiFePO₄ Enphase AC batteries providing 1.2 kWh capacity each. The Enphase Envoy-S Metered™ communications gateway system delivered the real-time solar production and energy consumption data to Enphase Enlighten™ monitoring and analysis software for comprehensive, remote maintenance and management of the complete microgrid system. Fuses were installed into each window's output cabling lines to safeguard against any possible issues related to the accidental (however unlikely) electric faults leading to the high reverse-current loading of any individual modules. These protective components were necessary, considering the high maximum I_{sc} (~0.75 A) generated by individual PV windows, and the numbers (up to 8) of the parallel-connected window modules installed into bundles. Parallel electric connection of the individual windows placed into the same deployment areas (presumed uniformly lit in clear weather conditions) has been selected to improve the stability of the combined electric output to differential shading effects, originating from the possible glass surface

contamination and variable cloud-related shading. Additionally, this allowed minimization of the system output voltage to safe levels, and the selection of a suitable low-power microinverter model with matched electric input characteristics and having maximum power point tracking (MPPT) capabilities. The benefits of using the parallel and also the massively-parallel electric circuit configurations of PV modules installed into low-power solar energy harvesters have been well documented and reported previously [35].

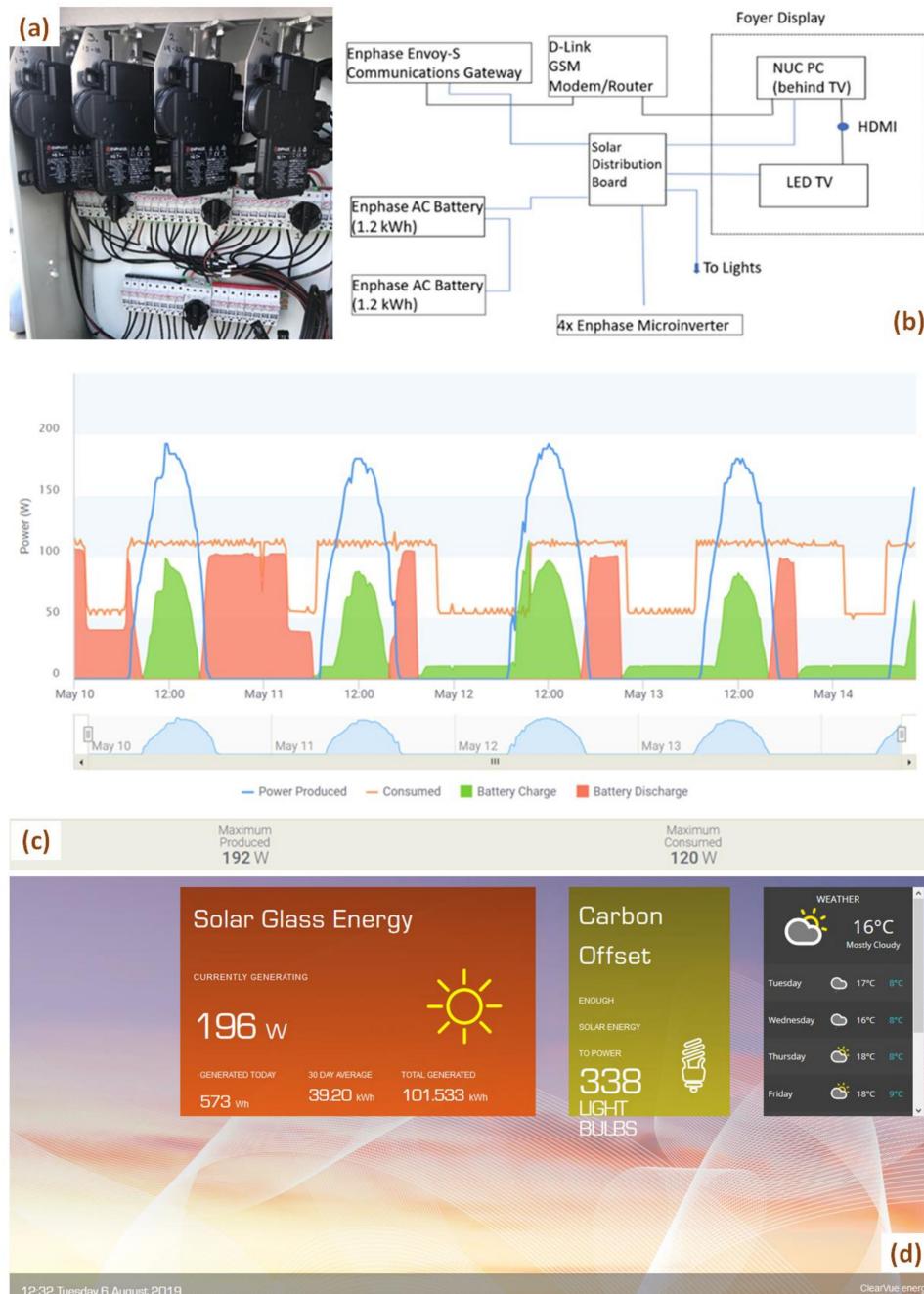


Figure 2. A graphical summary of the microgrid configuration details (a,b), sample data logs for the daily energy generation and use (c), and a photo of TV screen data showing a summary of system state (d), which is also available through live Internet broadcast at <http://tcp.iotstream.io/vicinity-warwickgrove/index.php> with 15-minute data sampling intervals.

Predictive modelling of the electric energy outputs expected to be generated by the atrium installation and each of its parts annually (and also monthly) has been performed using HOMER Pro

microgrid analysis software package (HOMER Energy Inc., Boulder, CO, USA). The unconventional PV generators (solar windows) have been approximated in the software-assisted microgrid model as “generic flat plate PV” outputting 30 W per window at peak irradiation conditions, at the nominal operating cell temperature (NOCT). This power rating per window closely approximates their expected performance at the peak orientation and peak-weather conditions, when the temperature of solar cell surfaces is near 40 °C. The model has also fully accounted for the local monthly and yearly climate-related solar irradiation datasets corresponding to the exact geographic location of installation. The geometric orientation (tilt) and also the azimuth orientation angles of all system parts were fully accounted for in the software model. Figure 3 shows a graphical summary of the energy generation modeling results, obtained for each PV windows subsystem and for the overall atrium installation.



Figure 3. A summary of the predicted monthly and yearly microgrid energy output results modeled using HOMER Pro software package; the measured electric energy generation amounts during the month of August 2019 are also shown (data obtained from the Enphase Enlighten™ monitoring software records).

The modeling results indicated that the annual energy output in excess of 0.6 MWh can be expected, composed mainly of the roof sections contribution over the warmer months, and dominated by the contributions from the North Wall section between April and August. The atrium’s measured monthly energy production during August 2019 (from the data logged by the Enphase Enlighten™ monitoring system) was 38.54 kWh, which was about 10% less than the corresponding monthly output predicted by the software model, not accounting for the small extra contributions from the strongly

shaded East Wall window units (which were nevertheless modeled as two 30W east-facing generators placed vertically). The measured monthly electric energy output from the North Wall units in August was 16.8 kWh (or 43.6% of the total generated energy), which also corresponded closely to the model predicting about 50% energy contribution from these units. The north-oriented front entrance windows have frequently been subjected to the intermittent shading conditions from the people traffic, reducing the power generation. Considering the local annual sun-path geometry, strong contributions from the vertically-mounted North Wall windows were also expected during the colder months, when the mid-day Sun altitude angles are low, and with the Sun azimuth direction shifting towards north, even at sunrise times. In addition, the Supplementary data file (Table S1) contains multiple daily generation data records obtained during this study from the installation measurement systems and other system observation datasets.

2.2. Detailed System Performance Observations, Evaluation, and Analysis

After configuring the microgrid connections, electric loads, storage system, and system management software in May 2019, a detailed case study of the system performance started, and the electric characteristics were monitored almost daily, at regular time intervals, and in varying weather conditions. The amounts of storage-ready electric energy generated by all four individual (differently-oriented) bundles of solar windows were monitored in different conditions. Energy losses at the microinverters and inside cabling would have amounted to several percent of the total generated energy, yet these were ignored and not monitored specifically. Regular system performance and electric output observations continued until the end of June 2019, resulting in obtaining a large dataset suitable for system performance characterization. Weather-dependent solar irradiation and cumulative daily solar exposure data were also collected (at the same times as the electric outputs) from the online live data broadcasts of nearby Wanneroo Weather Station operated by the Department of Primary Industries and Regional Development, Government of Western Australia [36]. Additional solar geometry-related data for the current (and local) Sun azimuth and Sun altitude angles at the times of data logging were recorded from SunCalc.org online solar astronomy calculator [37].

Figure 4 shows the dependencies of the generated electric power and stored energy on the time of day, measured over several sunny days in May and June of 2019. It is interesting to note the high consistency of the power generation on different sunny days, even measured weeks apart. The effects of variable weather conditions such as cloud cover are also seen in the graphs.

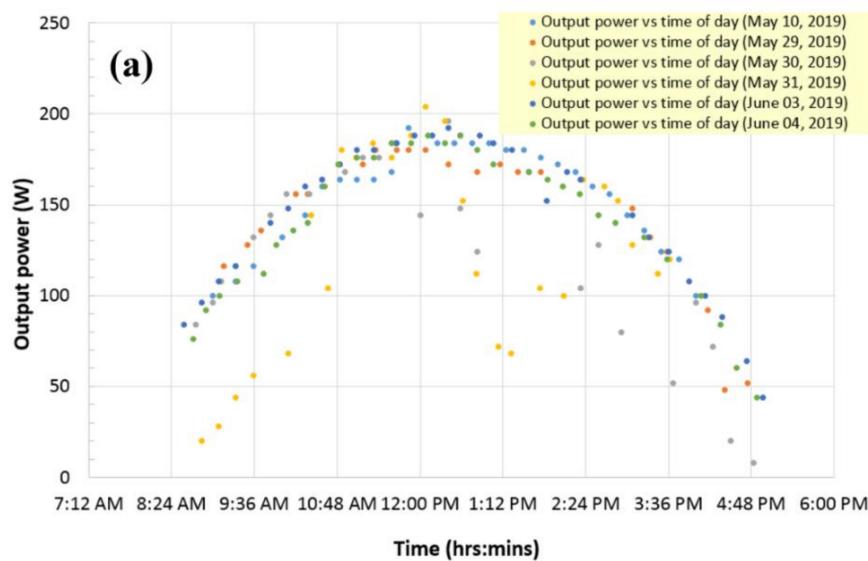


Figure 4. Cont.

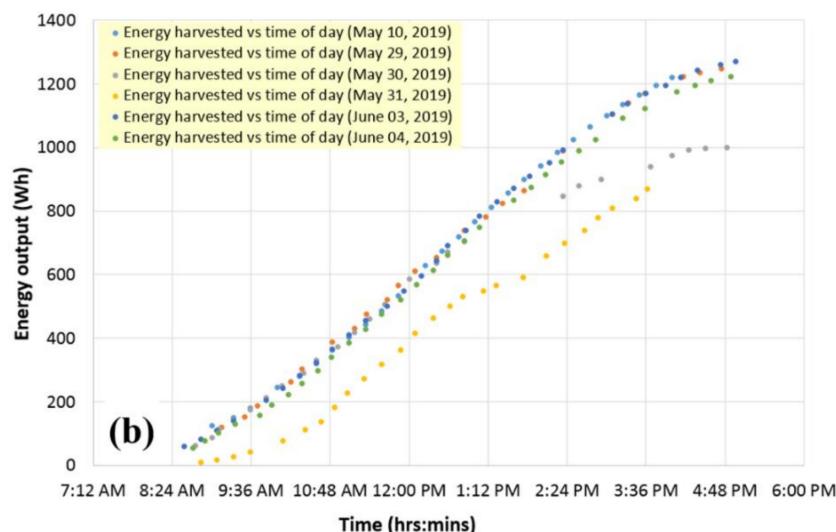


Figure 4. Energy harvesting performance of 18-window solar atrium versus time of day. **(a)** Electric power output readings recorded over several days in May–June 2019; **(b)** the amounts of stored electric energy vs time of day; the data points used are from the same dataset of system-state records as in part **(a)**.

It can also be noted from the data of Figure 4 that the time distribution of the power generation follows the “bell curve” shape well-known in conventional roof-based PV installations. This is despite the fact that this installation does not include any optimally-tilted, north-oriented roof sections, but rather is composed of an unequal number of PV generators placed into four deployment areas of substantially different geometric orientations, tilts, and shading exposure conditions. Also notable is the almost-linear time dependency of the stored electric energy, observed until late afternoons on sunny days. Considering that the sun-path geometry over the course of day involves large changes in both the azimuth and sun altitude angles, all occurring simultaneously with weather- and time-dependent irradiation intensity variations across all planes, these data confirm that all four main parts of this solar-window atrium provided important contributions to the daily energy generation function.

Figure 5 shows the solar irradiation intensity dependencies of the output power (recorded on different sunny days during the study), and the dependency of stored electric energy on the total cumulative amount of incoming solar energy received during the day by each 1m^2 of horizontal (land) surface area. Both datasets are notable in terms of the data points clustering around nearly-linear function shapes. Since only the horizontal-plane solar irradiation intensity was measured by the weather station, and because most of the daily total energy was being generated by the eight vertically-mounted north-facing windows, the data trends seen in Figure 5a,b (and also in Figure 4b) confirm the relative insensitivity of the electric power output and energy storage rate on the geometry of sunlight incidence. This is because the transparent solar windows are of solar concentrator design type, which improves the angular stability of power generation compared to conventional PV panels.

It can be noted from Figure 5a that the maximum output power readings have been recorded for moderate horizontal-plane solar irradiance values between $300\text{-}400 \text{ W/m}^2$. These irradiances correspond to the smaller Sun altitude angles during the morning hours, when a stronger UV irradiation background is usually present (compared to the afternoon hours), and colder ambient air temperatures. A combination of incidence angles (in both the horizontal and vertical planes) thus exists, favoring the power generation from the east-tilted roof and also the north-facing wall sections. A maximum electric power output registered so far was 232 W, recorded on May 08, 2019, shortly after 11 am. Since this data point was acquired outside a systematic study conducted later, it hasn’t been included in the dataset of Figure 5. For sunny Australian autumn days in May, each 1 kWh (3.6 MJ) of harvested electric energy corresponded to approximately 11 MJ/m^2 of daily

land-area cumulative solar exposure. Considering the land-area footprint of this atrium structure being approx. 12.5 m^2 ($5\text{m} \times 2.5\text{ m}$), the combined (installation-scale) direct estimate of its actual solar energy harvesting efficiency is then approximately 2.6%. This figure is only marginally smaller than the rated efficiency of individual solar windows at standard test conditions (~3.0%), despite the absence of any optimally-tilted deployment areas and seasonal weather conditions without strong UV irradiation background. Interestingly, these field-measured performance data show some contrast with the recently reported figures for the “real” (field-measured) energy harvesting efficiencies of conventional PV generator types (solar panels) evaluated in major Australian cities [38]. In particular, these field-evaluated (“real”) efficiencies of most conventional solar panel types stood at only about one-half of their rated energy conversion efficiency specifications. Environmental factors such as partial shading and soiling of solar panels, and installation-related geometric factors such as panel orientation and tilt angles, all affect the energy harvesting performance characteristics significantly [39–42].

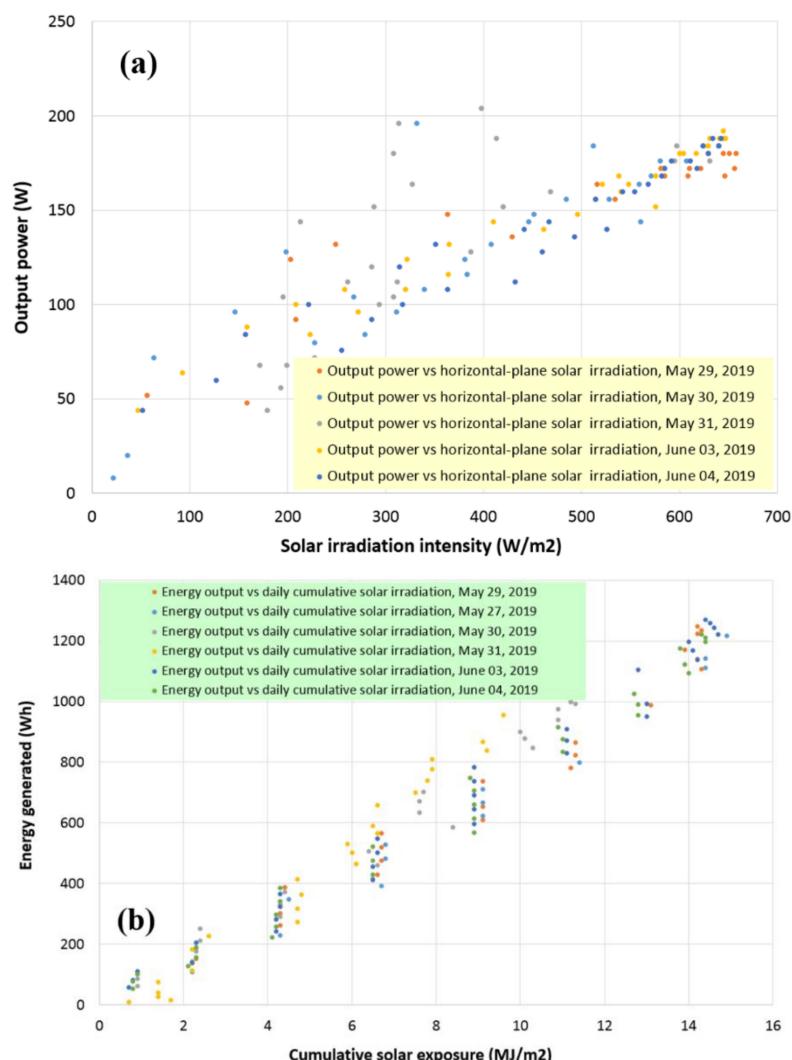


Figure 5. Energy harvesting performance vs solar exposure parameters. (a) Output power vs solar irradiation intensity measured in the horizontal plane by a local weather station; (b) generated electric energy vs daily land-area cumulative solar exposure (measured by the same weather station since midnight of the same day).

Table 1 shows an example of a typical daily system-related and environmental data-related dataset obtained during the study. It is important to note, that Enphase data interface has always rounded the output power readings to the nearest even number of Watts; this is possibly related to the fact that

the live data were sampled in 3-minute intervals, followed by the data averaging occurring every 15 minutes prior to internet broadcasting. Also, the cumulative solar exposure figures have apparently been adjusted by the weather station (however infrequently), to sometimes correct the sensor readings towards smaller values (compared to the data published at previous data sampling intervals) during the course of day.

Table 1. Example of the daily dataset collected from the installation data interface and online data sources on June 4th, 2019.

Time	Energy stored (Wh)	Power (W)	Solar exposure (MJ/m ²)	Horiz. Irradiance (W/m ²)	Sun Altitude (deg)	Sun Azimuth (deg)
8:43	54	76	0.8	255	15.8	50.09
8:54	77	92	0.8	286	17.56	48.17
9:06	102	100	0.9	317	19.41	46.01
9:21	129	108	2.1	363	21.64	43.18
9:44	157	112	2.3	432	24.83	38.55
9:55	189	128	2.3	460	26.24	36.21
10:10	223	136	4.1	493	28.04	32.88
10:22	258	140	4.2	526	29.37	30.11
10:37	298	160	4.2	554	30.88	26.5
10:49	341	172	4.3	585	31.95	23.51
11:05	385	176	4.3	592	33.19	19.37
11:20	429	176	6.5	611	34.14	15.37
11:35	475	184	6.5	624	34.87	11.25
11:52	521	184	6.5	640	35.42	6.5
12:07	568	188	8.9	642	35.67	2.25
12:22	614	184	8.9	640	35.67	357.98
12:35	661	188	8.9	634	35.48	354.3
12:50	706	180	8.9	629	35.05	350.08
13:04	749	172	8.8	618	34.44	346.22
13:35	834	168	11	582	32.42	337.98
13:51	875	164	11	568	31.03	333.95
14:04	915	160	10.9	542	29.76	330.8
14:19	954	156	12.8	514	28.12	327.31
14:35	990	144	12.8	467	26.2	323.76
14:50	1025	140	12.7	441	24.25	320.6
15:15	1093	132	14	351	20.71	315.66
15:35	1123	120	13.9	314	17.66	311.99
16:04	1175	100	13.8	221	12.93	307.09
16:21	1196	84	14.4	157	10.02	304.42
16:35	1211	60	14.4	127	7.57	302.32
16:53	1222	44	14.3	52	4.36	299.74

The datasets shown in Figure 6 illustrate the details of the atrium's power generation trends with respect to the variables such as the solar path-related angles, instantaneous irradiance intensity, time of day, and weather conditions. During this study conducted over autumn and winter months, the Sun altitude angle reached a maximum of only about 36° near mid-day, and therefore the solar atmospheric path-length always exceeded its standardized value (air-mass 1.5, corresponding to the AM1.5 NREL standard for solar spectrum measurements). Solar azimuth angles, on the other hand, varied across a wide range between about 40° (NNE) and −60° (WNW) between 9:00 and 17:00. The electric output power correlated well with both the Sun altitude angle and horizontal-plane irradiance, despite most of the power generation obtained consistently (throughout the days) from the north-oriented vertical wall of windows. It is important to note (Figure 6d) that the output power readings exceeding 150 W (out of the typical maximum-recorded output powers near 200 W) have been obtained consistently on different days, in a range of solar exposure conditions, between 10:00 and 15:00, and at a large range of horizontal-plane solar irradiance variations (between about 250–650 W/m²). This confirms the capability of this solar window atrium to collect energy efficiently in a wide range of solar incidence

geometry conditions, at least during clear and sunny weather conditions. The dataset of Figure 6d has only been collected over several weeks (and therefore, not all possible independent time/solar irradiation variable combinations could be evaluated); it also contains some weather-related “noise” affecting the low-power readings. This dataset is, however, quite representative of the system power generation capabilities seen during most winter conditions on sunny, cloudless days. We included this additional two-dimensional surface-plot representation as “a guide for the eye” only, to demonstrate and visualize the time- and weather-related correlations of the output power. The irradiation data used for plotting Figure 6d have been grouped, so that all data points for the horizontal irradiation values measured inside small intervals between eg 150–200 W/m² were all assigned a 200 W/m² value for plotting. For all “missing” output power data points (due to the limited duration of study not covering all possible weather conditions) corresponding to some locations across the time-irradiance data grid used, these points were approximated to correspond to the minimum actually measured power values observed at boundaries of the corresponding data intervals.

The amounts of electric energy generated by each individual sub-section of the atrium installation have also been monitored. During the daylight hours of May 28, the daily total energy generation by the two shaded east-wall windows was only 54 Wh, while the four east-roof windows produced 268 Wh, and the 8 windows on northern wall contributed 743 Wh; the 4 west-roof windows generated 191 Wh. On a different day (June 03, 2019, which was slightly sunnier than May 28), the 8 front-wall windows produced a total of 794 Wh of energy during the daylight hours. Therefore, the vertically-mounted north-oriented wall windows, which were often shaded temporarily by the people traffic near the shopping center entrance, contributed daily, on average, almost 100 Wh per window unit, in late-autumn conditions. Per unit window module, the daily energy generation from shaded windows (on eastern wall) was a factor of 3.4 smaller compared to the north-facing vertically-mounted units. Increased energy collection efficiencies are expected to be observed during the spring and summer months, due to both the stronger solar irradiation intensity levels, and (most importantly) the substantially longer daily sunshine durations. The Supplementary data file (Table S1) contains daily-total energy generation data for all window groups, as measured by the system after sunset each day, for the period between May–early September 2019. The angle-dependent solar illumination flux-cross-section differences between the vertically-mounted and peak-tilted window orientations (eg if placed onto optimally-tilted North-facing roof section) are also significant. These geometric factors correspond to approximately a factor of $(1/\cos 45^\circ)$ in peak-power output difference, which allows predicting the orientation-related increases in the energy outputs per window by up to several tens of percent, in future optimally-mounted units. In conventional southern-hemisphere PV installations, the preferred geometric orientation of PV panels corresponds to mounting them on building roof sections facing the North direction (with the horizontal projection of the normal to the solar-cell area aligned with azimuth 0°) and tilted to the horizontal plane at an angle equaling the local latitude. This optimizes the daily (for most seasons), and also the yearly energy production by ensuring a close-to-normal incidence angle of the solar radiation onto cells at times around midday. Other factors which may affect the precise PV panel orientation preferences include the site-specific shading conditions, and the preferences of system owners in relation to their peak energy production requirements being shifted towards either the morning or evening hours. A common way to approximate the expected daily energy production per orientation-optimized panel is by multiplying the rated nominal (peak) power (measured at standard testing conditions) by the number of peak-equivalent sunshine hours. The latter depend significantly on the geographic location and the day of year, but the data are often available from industry publications reliant on the local weather bureau data. The panel orientation-dependent solar irradiation flux intercepted by the PV panels is also modified according to the cosine function of the angle between the panel normal and the Sun direction. Therefore, if at noon the Sun altitude is at 45°, a vertically-positioned north-facing PV panel will generate about 0.7 of the amount of energy (produced per unit time) by an optimally-tilted, north-oriented roof panel.

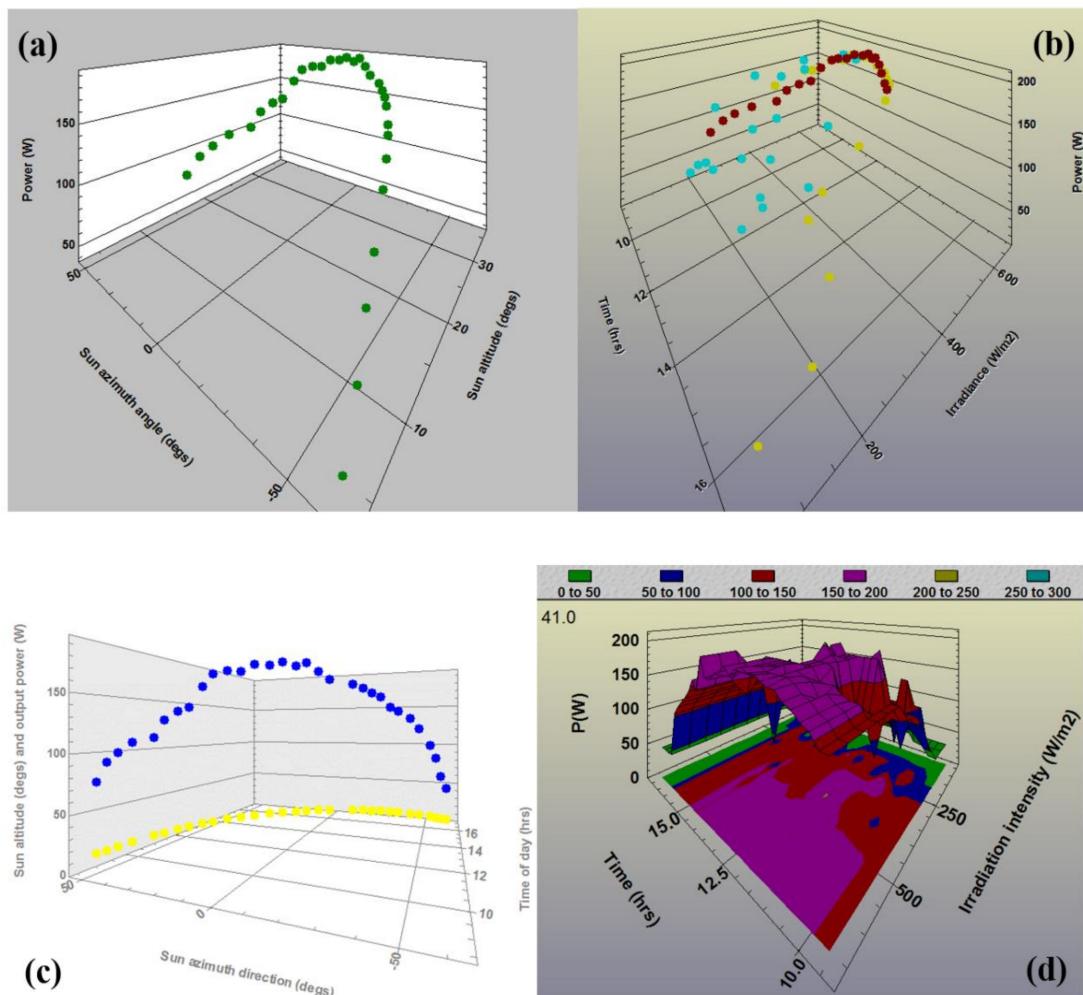


Figure 6. Electric output power trends observed with respect to the solar geometry and irradiation-related parameters. (a) 3D scatter plot of the output power vs the Sun azimuth and Sun altitude angles; (b) 3D scatter plot of the output power vs the time of day and the horizontal-plane solar irradiation intensity; (c) 3D scatter plot of the output power shown in correlation with the Sun altitude angle, vs the Sun azimuth direction and the time of day; (d) 3D surface plot (and its corresponding 2D contour plot shown in the X-Y plane underneath) illustrating the variations in the electric output power with both the time of day, and the instantaneous weather-dependent (horizontal-plane) solar irradiation intensity. The data were collected over the entire period of study (about 2 months) covering a wide range of weather conditions observed at regular intervals at most times of day.

A yearly-averaged estimate for the daily energy output per 1m^2 of solar window area can therefore be made, based on the observed data, being near $0.1 \text{ kWh}/\text{m}^2$, presuming that installation sites are configured favoring the north-facing, azimuth-optimized window orientations. For future dome-type installations, the average daily energy outputs per window can be predicted, by averaging the data from the three main (unshaded) parts of Warwick Grove atrium installation, leading to estimates near $70 \text{ Wh}/\text{m}^2$. These estimates can be considered conservative, since only the seasonal increases in the daily sunshine durations were factored in to produce these year-scale averages. In other geographic locations, where stronger yearly insolations are typically measured (eg, Middle East, or the north-west of Australia), higher energy yields will be obtained.

3. Discussion and Assessment of Future Application Areas

In order to assess the practical applications potential of this emergent class of transparent solar window-based PV, it is necessary to refer to the industry-standard system-level performance indicators, the most common of which is Specific Yield. Specific yield (SY) quantifies the amounts of electric energy (in kWh) harvested annually (per typical calendar year, in each installation location), per each 1 kW_p of installed PV generation capacity [43]. SY values are commonly used in industry to directly compare the performance of different PV system configurations installed at different locations. Typically, measured SY values in the United States reach up to about 1500 kWh/kW_p, according to the data reported in [43] for conventional solar PV module installations. For conventional (silicon modules-based) rooftop PV installations in Perth, Australia, average daily energy generation outputs of about 4.4 kWh/kW_p have been reported [44], which translates into the estimated approx. SY values of near 1320 kWh/kW_p, based on 300 sunny days per year in this location. Accounting for the PV generation amounts during the other 65 days showing at least about a third of maximum generation (compared to the stable-sunshine days, from our observations of Warwick Grove Atrium energy outputs measured on rainy days in winter), a more detailed estimate for the SY figure for typical Perth-based PV systems is then also close to 1500 kWh/kW_p. These data sets are only valid, however, for the optimally-oriented, optimally-tilted roof-based, completely unshaded silicon PV module installations.

In order to evaluate the expected annual energy generation and specific yield of Warwick Grove Atrium, local meteorological datasets for the monthly and yearly cumulative solar exposure values can be used, in conjunction with the data of Figure 5b for the energy yield per each MJ/m² of solar exposure. Quantified during sunny days in May, a conservative estimate (due to the weather being more suitable for PV generation over many other months over the year) for this energy yield per unit solar exposure, is near 1/11 kWh/(MJ/m²). According to the yearly solar exposure data summaries available from a local weather station [36], the annual cumulative solar exposure figures were consistently at near 7400 MJ/m²/year, in several recent years. Therefore, a conservative annual energy output estimate can be obtained, being at least 673 kWh. This figure will likely be exceeded by up to several hundred kWh, due to weather conditions being much more conducive to PV energy harvesting in spring and summer, when both the UV and near-IR irradiation levels are much higher, due to drier atmospheric conditions. Substantially stronger diffused and reflected solar irradiation backgrounds are also present during the warmer months, leading (in our group's experience) to improved energy capture rates in solar windows.

It is possible to evaluate the (over-conservative) lower limit for the expected specific yield of Warwick Grove Atrium installation, by using a nominal, sum-total-based installed generation capacity of 18 solar windows (~0.54 kW_p). Then, a standardized expected SY figure of ~1246 kWh/kW_p is obtained, which is still quite competitive to the typical conventional (even optimally tilted) PV installations in sunny locations like Perth, especially if shading considerations are taking into account, which strongly affected 2 out of 18 windows. Accounting for the real measured peak output powers, and the local site-specifics of windows deployment at Warwick Grove, particularly the geometric orientations of most modules being far from optimal, the actual electric output-related installed capacity rating cannot exceed about 300 W_p. Using this figure, an adjusted (however non-standard) estimate for the SY can be re-calculated, now exceeding 2240 kWh/kW_p. This SY figure estimate confirms the relative strengths of the energy harvesting approach using solar windows, compared to many common types of PV systems. These strengths are due to the improved efficiency of solar energy collection for light rays incident onto harvesting surfaces at large angles, which is a known characteristic of luminescent concentrator-type devices, including transparent energy-generating window systems.

Significant seasonal variations in the daily amounts of generated energy are expected, due to local climate-related variables. A graphical summary of seasonal climate-related solar irradiation parameter variations for Perth, Australia is presented in Figure 7. It can be noted from Figure 7 that very strong monthly variations exist between the monthly-averaged direct-beam solar irradiation intensities, the horizontal-plane illuminance, and also the mean daily total sunshine hours. The local-based

monthly distribution of peak output-equivalent sunshine hours for many Australian locations is also known from specialized PV industry sources (eg [45]), and generally scales in correlation with the mean daily total sunshine hours shown in Figure 7c. All of the above parameters are directly relevant to the expected daily energy generation from all PV module types; further, longer-term studies are necessary to generate the expected energy generation data per each calendar month.



Average daylight / Average sunshine Perth, Australia

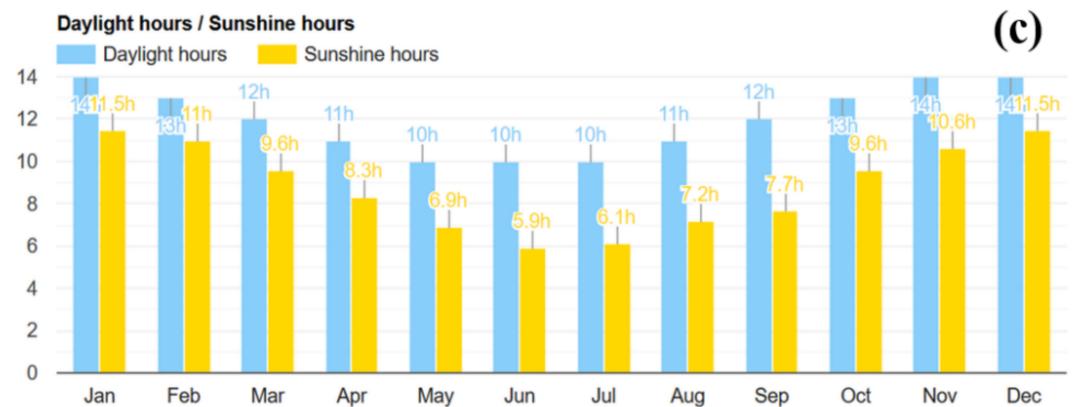


Figure 7. Seasonal yearly climate-related solar irradiation parameter variations for Perth, Australia. (a) Monthly averaged and maximum-recorded direct-beam solar irradiation intensities measured across horizontal plane; (b) monthly averaged and maximum-recorded direct-beam solar illuminance values measured across horizontal plane; (c) monthly distributions of the total daylight hours and the daily sunshine durations. The datasets shown in parts (a) and (b) have been obtained using COMFEN 5 software [46]; the dataset of part (c) has been published online by [31], using the publicly-available Australian Bureau of Meteorology data.

The results of this initial pilot-trial study of shopping center entrance-based solar windows installation lead to a preliminary conclusion regarding the generally expected suitability (and relevance) of transparent solar windows in commercial property-based settings. It is particularly important to note that the amounts (and usefulness) of the generated electric power and renewable energy both

scale favorably with the installation size, presuming that the geographic location is suitable, and the architectural design features are adjusted to maximizing the generated energy. For example, considering a semi-spherical dome-type installation housing 2000 m² of solar window surfaces, the diameter of this dome-shaped roof-based installation area will be near 35 m, a size not uncommon in shopping center properties. Based on 70 Wh/m² estimate for the system-averaged, seasonally-averaged daily energy generation, about 140 kWh of daily energy production can be expected. This corresponds to the total daily electric energy consumption requirements of about 10 3-bedroom Australian households. The area under the modelled solar-window dome and its surrounds will be approximately 40 m × 40 m in footprint, requiring a square 21 × 21 grid of 441 LED lamps separated by about 2 m. Presuming 30W LED lamps and using the calculated daily-average energy production figure, this area-lighting circuit of lamps can be run for approximately 10.5 hours. Accounting for the high visual transparency of windows, with >65% of total (direct and diffused) visible-range transparency, significant reduction in the lighting-related energy consumption can be predicted. Additionally, a large degree of electricity supply blackout resistance provided by on-site distributed generation using these building-material-integrated PV can be expected, provided that suitable battery storage systems are installed. Other expected future application areas of highly transparent energy-generating construction materials and solar windows will likely include roof-top canopies, balcony glazings, skylights, and airport roofs.

4. Conclusions

A case study of a small-scale transparent solar windows installation in Perth (Australia) over the period of May–September 2019 has been reported. The photovoltaic power and energy outputs have been characterized during varying weather conditions and times of day. The results reported elucidate the practical application potential of the described type of solar window products in various public infrastructure and commercial property-based applications. In particular, a small-scale (18 windows, with none installed at optimum orientation) solar window microgrid generated about 1 kWh of stored electric energy per 11 MJ/m² of land-area cumulative solar exposure, as measured by a local weather station, in variable weather conditions. Each vertically-placed, north-facing window unit of area near 1.3 m² harvested approximately 0.1 kWh on each sunny winter day of total sunshine duration ~6–7 h. It can be expected that multiple new commercial and residential building-based installations of the latest transparent BIPV products and technologies will continue to be constructed and trialed, broadening the acceptance of transparent energy-generating construction materials.

Supplementary Materials: The following are available online at <http://www.mdpi.com/2076-3417/9/19/4002/s1>, Table S1: Data summaries.

Author Contributions: All authors (M.V., M.N.A. and K.A.) have contributed to the design features of test installation at Warwick Grove Shopping Centre (Perth, Australia), the design features of solar window modules, the conceptualization of this article, and data collection; M.V. collected and analyzed the electric output and weather-related datasets and prepared the manuscript. All authors discussed the data, graphics, and the presentation; M.N.A. contributed substantially to the data curation and the original draft preparation; M.V. and K.A. further reviewed and edited the manuscript.

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