

- 1.) When the dimension of the robot's end effector's velocity (linear + angular) space is fewer than the total number of joint variables, a singular configuration occurs.

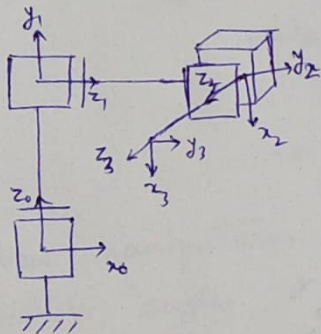
Mathematically, singularities happen when the manipulator jacobian's determinant is zero.

$$\Rightarrow \det(J(q)) = 0$$

By identifying all vectors q for which the jacobian $J(q)$ is singular, we can identify singular configurations.

On the other hand, if $\det(J(q)) = 0$ or close to zero for a particular configuration represented by vector q , we can argue that we are getting close to a unique configuration.

5.)



Let DH parameters be of ⁱⁿ the order $(\theta_1, d_1, a_1, \alpha_1)$

$$\therefore J_1 : \left(\frac{\pi}{2}, q_1, 0, \frac{\pi}{2} \right)$$

$$J_2 : \left(-\frac{\pi}{2}, q_2, 0, \frac{\pi}{2} \right)$$

$$J_3 : (0, q_3, 0, 0)$$

$$\therefore H_0^1 = {}^H R_{z, \frac{\pi}{2}} \cdot {}^R H_{z, q_1} \cdot {}^H R_{x, 0} \cdot {}^H R_{x, \frac{\pi}{2}}$$

$$= \begin{bmatrix} \cos\left(\frac{\pi}{2}\right) & -\sin\left(\frac{\pi}{2}\right) & 0 & 0 \\ \sin\left(\frac{\pi}{2}\right) & \cos\left(\frac{\pi}{2}\right) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos\left(\frac{\pi}{2}\right) & -\sin\left(\frac{\pi}{2}\right) & 0 \\ 0 & \sin\left(\frac{\pi}{2}\right) & \cos\left(\frac{\pi}{2}\right) & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_1^2 = H_{z, -\frac{\pi}{2}} H_{z, q_2} H_{x, 0} H_{x, \frac{\pi}{2}}$$

$$= \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 0 & -1 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

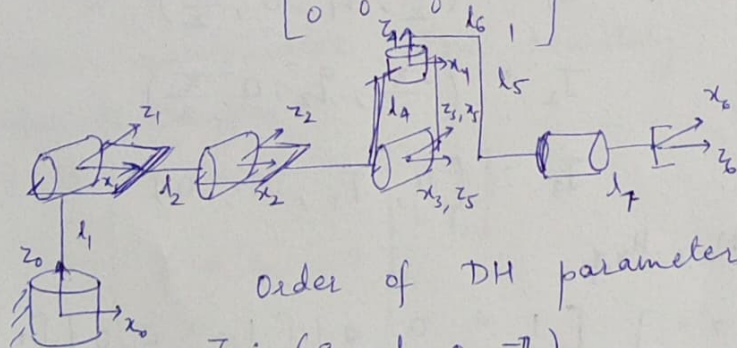
$$H_2^3 = H_{z, 0} H_{z, q_3} H_{x, 0} H_{x, 0}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & q_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_0^3 = H_0^1 H_1^2 H_2^3 = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & -1 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & q_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 1 & 0 & q_2 \\ 0 & 0 & -1 & -q_3 \\ -1 & 0 & 0 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

6.)



Order of DH parameters : $(\theta_i, d_i, a_i, \alpha_i)$

$$J_1: (q_1, l_1, 0, \frac{\pi}{2})$$

$$J_2: (q_2, 0, l_2, 0), J_3: (q_3, 0, l_3, 0)$$

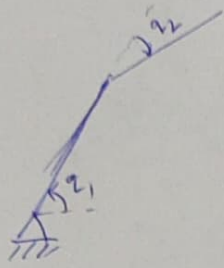
$$J_4: (q_4, 0, 0, \frac{\pi}{2}), J_5: (q_5, 0, 0, \frac{\pi}{2})$$

$$J_6: (q_6, 0, 0, 0)$$

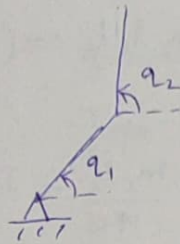
J_4, J_5, J_6 are wrist joints.

$$\therefore l_4 = l_5 = l_6 = l_7 = 0$$

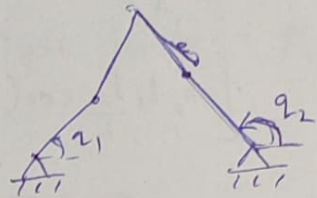
7.)



2R Direct Drive.



2R Remotely driven



5-bar parallelogram

(i) Relative angles are used as joint variables

(i) Absolute angles are used as joint variables.

(i) This does not form a kinematic chain.

(ii) Standardized ~~kinematic~~ kinematics and manipulator jacobian using D-H parameters.

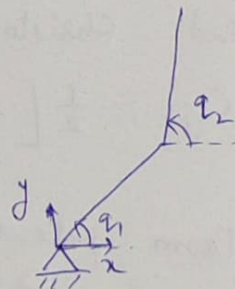
(ii) The motors are not moving. Thus, it is not necessary to take into consideration the mass, inertia and the angular momentum of the motor and gearbox in the dynamic analysis.

(ii) The motors are not moving. Furthermore, because remote links are automatically restricted by geometry, no belts / pulley are needed to deliver torque to them.

8.) Elbow manipulator with remotely driven links ~~not~~ using absolute angles.

$$\dot{x}_1 = \begin{bmatrix} -\frac{l_1}{2} \sin(q_1) & 0 \\ \frac{l_1}{2} \cos(q_1) & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$\dot{x}_2 = \begin{bmatrix} -l_1 \sin(q_1) & -\frac{l_2}{2} \sin(q_2) \\ l_1 \cos(q_1) & \frac{l_2}{2} \cos(q_2) \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$



$$\dot{w}_1 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$\dot{w}_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$E^K = \frac{1}{2} \sum_{i=1}^2 m_i \dot{v}_i^T \dot{v}_i + \frac{1}{2} \sum_{i=1}^2 \omega_i^T I_i \omega_i = \frac{1}{2} \dot{q}^T D \dot{q}$$

$$\therefore D(q) = \begin{bmatrix} \frac{m_1 l_1^2}{4} + m_2 l_1^2 + I_1 & m_2 l_1 \frac{l_2}{2} \cos(q_2 - q_1) \\ m_2 l_1 \frac{l_2}{2} \cos(q_2 - q_1) & \frac{m_2 l_2^2}{4} + I_2 \end{bmatrix}$$

$$V = m_1 g \frac{l_1}{2} \sin(q_1) + m_2 g (l_1 \sin(q_1) + \frac{l_2}{2} \sin(q_2))$$

Here,

$$C_{112} = -C_{221} = \frac{1}{2} m_2 l_1 l_2 \sin(q_2 - q_1)$$

$$\text{and, } C_{111} = C_{121} = C_{122} = C_{211} = C_{212} = C_{222} = 0$$

$$\text{Also, } \phi_1 = m_1 g \frac{l_1}{2} \cos q_1 + m_2 g l_1 \cos q_1$$

$$\phi_2 = m_2 g \frac{l_2}{2} \cos q_2$$

$$\therefore \sum_j d_{kj} \ddot{q}_j + \sum_{ij} C_{ijk}(q) \dot{q}_i \dot{q}_j + \phi_k(q) = \tau_k$$

10.) Given, $D(q) = [d_{ij}(q)]$ and $V(q)$

(i) Find $\frac{\partial d_{ij}}{\partial q_k}$ for each element d_{ij} in $D(q)$ and for each joint variable q_k

(ii) Find Christoffel's symbols of 1st kind -

$$C_{ijk} = \frac{1}{2} \left[\frac{\partial d_{kj}}{\partial q_i} + \frac{\partial d_{ki}}{\partial q_j} - \frac{\partial d_{ij}}{\partial q_k} \right]$$

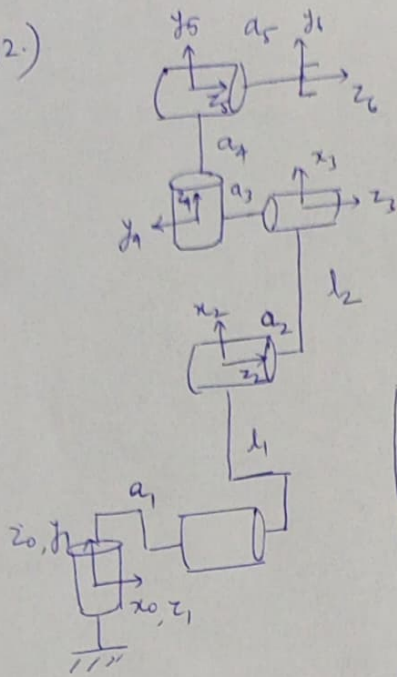
(ii) From potential field,

$$\phi_k = \frac{\partial V(q)}{\partial q_k}$$

After calculating all the terms, write the k^{th} eqⁿ as.

$$\sum_j d_{kj} \ddot{q}_j + \sum_{ij} C_{ijk} \dot{q}_i \dot{q}_j + \phi_k(q) = \tau_k$$

12.)



Here,

Number of links = 2

Number of joints = 6

Type Nature of all joints = R

DH parameters :

links	joints	θ_i	d_i	a_i	α_i
1		q_1	0	0	$\frac{\pi}{2}$
2		q_2	a_1	l_1	0
3		q_3	a_2	l_2	0
4		q_4	a_3	0	$-\frac{\pi}{2}$
5		q_5	a_4	0	$\frac{\pi}{2}$
6		q_6	a_5	0	0

currently, $q_1 = \frac{\pi}{2}$

$q_2 = \frac{\pi}{2}$

$q_3 = 0$

$q_4 = -\frac{\pi}{2}$

$q_5 = 0$

$q_6 = 0$

Also, a_1, a_2, a_3, a_4, a_5 - ~~offset~~ offsets

l_1, l_2 - link lengths.