

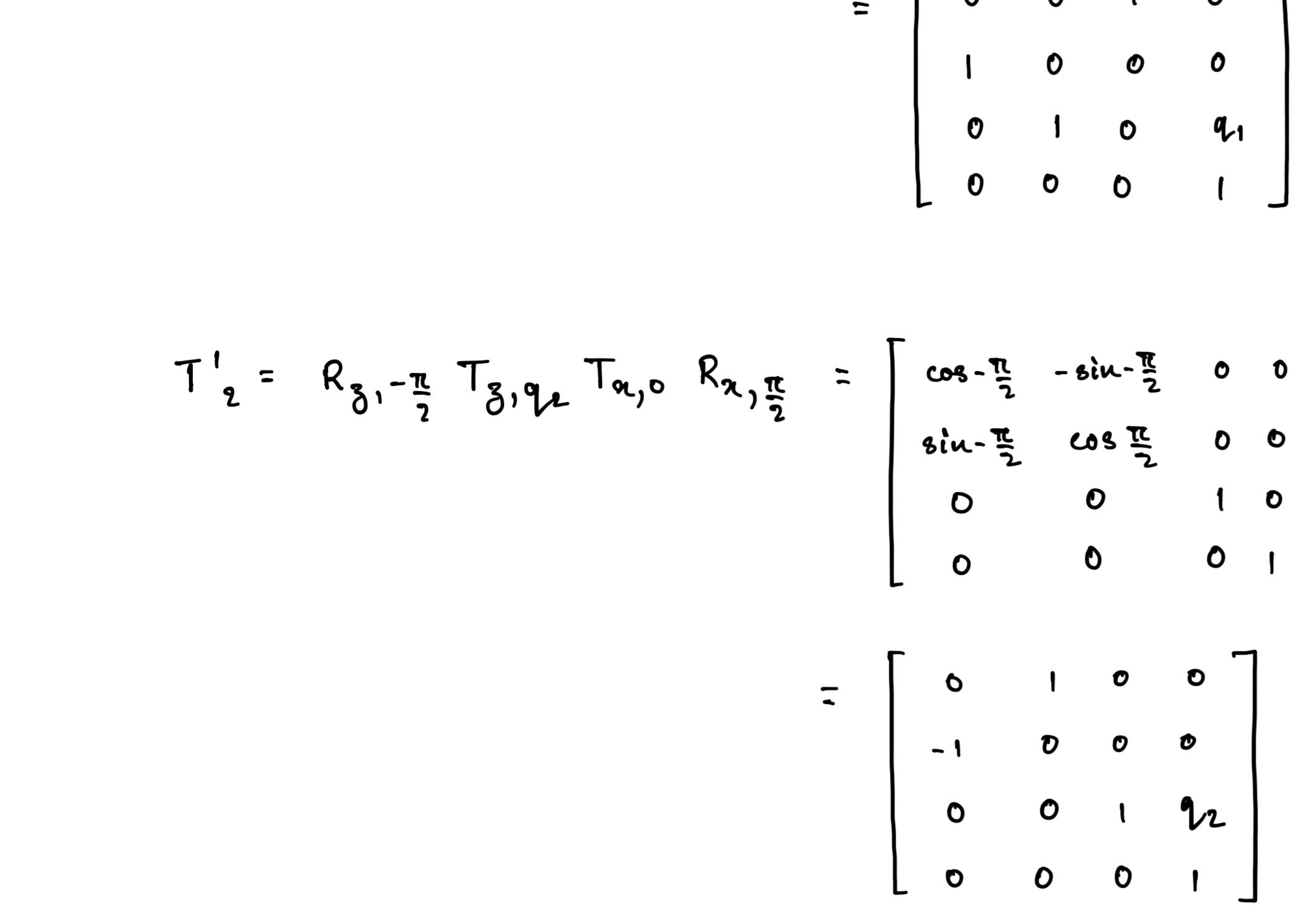
1. A singular configuration occurs when the robot's end effector's velocity (linear + angular) space has dimension less than the number of joint variables.

Mathematically, singularities occur when determinant of the manipulator jacobian is zero.

$$\det(J) = 0$$

We can find singular configurations by finding all vectors q for which the jacobian $J(q)$ is singular.

Conversely, for a given configuration represented by vector q if $\det(J(q))$ is zero or close to zero, we can say we are near a singular configuration.



$$T^0 = R_{z, \frac{\pi}{2}} T_{z, q_1} T_{x, 0} R_{x, \frac{\pi}{2}} = \begin{bmatrix} \cos \frac{\pi}{2} & -\sin \frac{\pi}{2} & 0 & 0 \\ \sin \frac{\pi}{2} & \cos \frac{\pi}{2} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \frac{\pi}{2} & -\sin \frac{\pi}{2} & 0 \\ 0 & \sin \frac{\pi}{2} & \cos \frac{\pi}{2} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

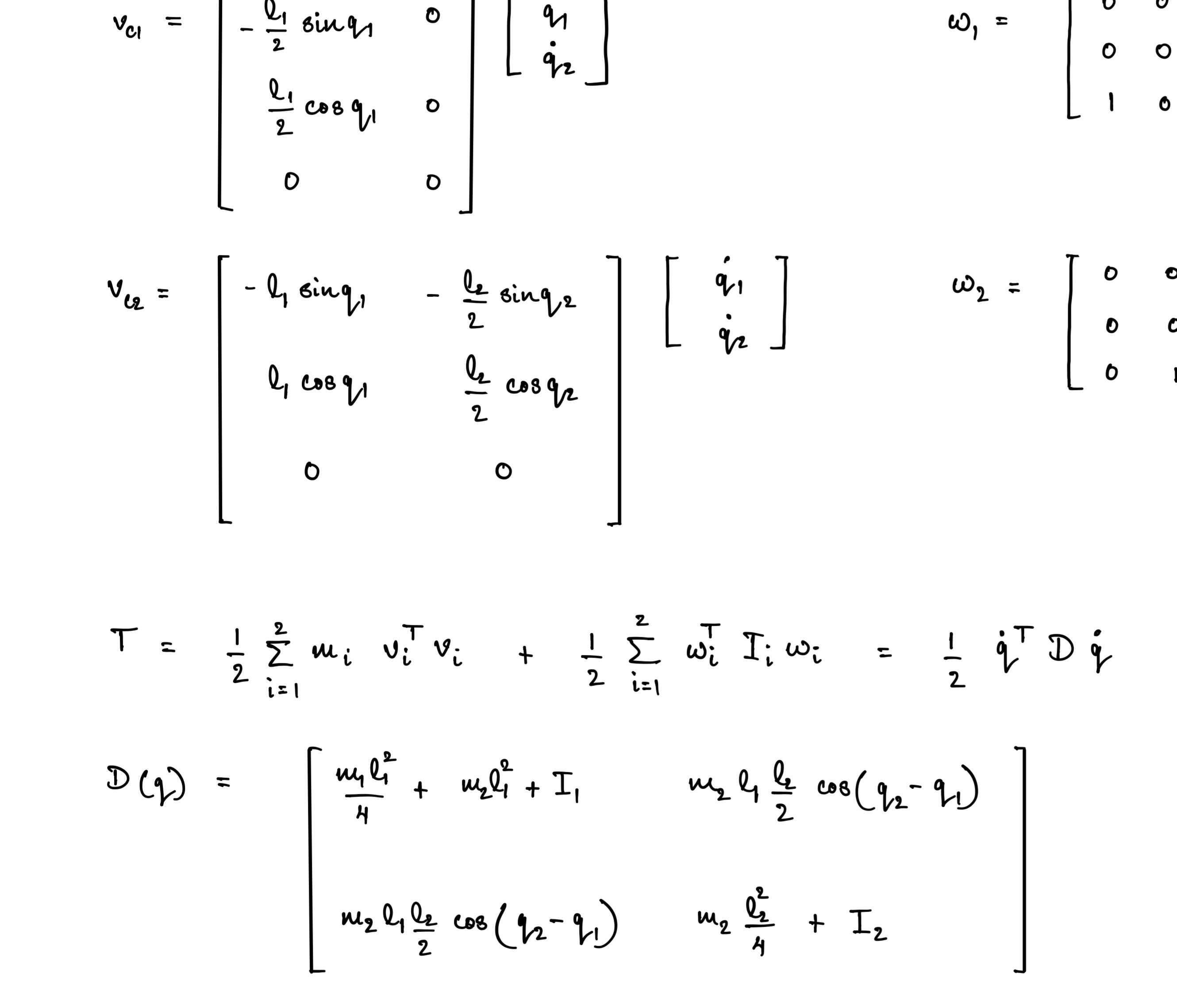
$$T^1_2 = R_{z, -\frac{\pi}{2}} T_{z, q_2} T_{x, 0} R_{x, \frac{\pi}{2}} = \begin{bmatrix} \cos -\frac{\pi}{2} & -\sin -\frac{\pi}{2} & 0 & 0 \\ \sin -\frac{\pi}{2} & \cos -\frac{\pi}{2} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \frac{\pi}{2} & -\sin \frac{\pi}{2} & 0 \\ 0 & \sin \frac{\pi}{2} & \cos \frac{\pi}{2} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 1 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 & -1 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T^2_3 = R_{z, 0} T_{z, q_3} T_{x, 0} R_{x, 0} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & q_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

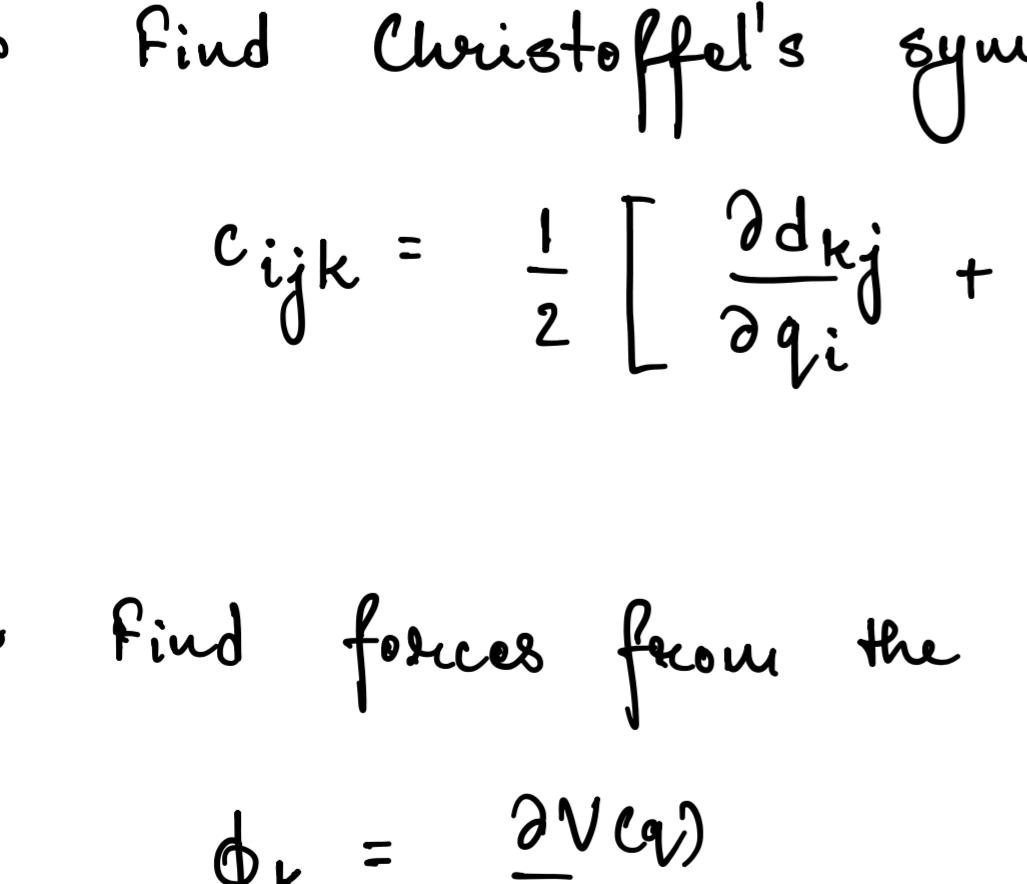
$$\therefore T^0_3 = T^0_1 T^1_2 T^2_3 = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & -1 & -q_3 \\ -1 & 0 & 0 & 0 \\ 0 & 1 & 0 & q_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 1 & 0 & q_2 \\ 0 & 0 & -1 & -q_3 \\ -1 & 0 & 0 & q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



- 7.
- 2R Direct Drive 2R Remotely driven 5-bar parallelogram
- Relative angles as joint variables
 - Absolute angles as joint variables
 - Does not form a kinematic chain
 - Standardized kinematics and manipulator jacobian using DH parameters.
 - Motors are stationary. Hence, dynamic analysis does not require to account for motor and gearbox mass, inertia and angular momentum.
 - Motors are stationary. Moreover, no belts/pulleys required to transfer torque to remote links as they are automatically constrained by geometry.

8. Elbow manipulator with remotely driven links using absolute angles



$$v_{01} = \begin{bmatrix} -\frac{l_1}{2} \sin q_1 & 0 \\ \frac{l_1}{2} \cos q_1 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$v_{02} = \begin{bmatrix} -l_1 \sin q_1 & -\frac{l_2}{2} \sin q_2 \\ l_1 \cos q_1 & \frac{l_2}{2} \cos q_2 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$\omega_1 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$\omega_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$T = \frac{1}{2} \sum_{i=1}^2 m_i v_i^T v_i + \frac{1}{2} \sum_{i=1}^2 \omega_i^T I_i \omega_i = \frac{1}{2} \dot{q}^T D \dot{q}$$

$$D(\dot{q}) = \begin{bmatrix} \frac{m_1 l_1^2}{4} + m_2 l_1^2 + I_1 & m_2 l_1 \frac{l_2}{2} \cos(q_2 - q_1) \\ m_2 l_1 \frac{l_2}{2} \cos(q_2 - q_1) & m_2 \frac{l_2^2}{4} + I_2 \end{bmatrix}$$

$$V = m_1 g \frac{l_1}{2} \sin q_1 + m_2 g \left(l_1 \sin q_1 + \frac{l_2}{2} \sin q_2 \right)$$

$$c_{112} = -c_{221} = \frac{1}{2} m_2 l_1 l_2 \sin(q_2 - q_1)$$

$$c_{111} = c_{121} = c_{122} = c_{211} = c_{212} = c_{222} = 0$$

$$\phi_1 = m_1 g \frac{l_1}{2} \cos q_1 + m_2 g l_1 \cos q_1$$

$$\phi_2 = m_2 g \frac{l_2}{2} \cos q_2$$

$$\therefore \sum_j d_{kj} \ddot{q}_j + \sum_{ijk} c_{ijk}(\dot{q}) \dot{q}_i \dot{q}_j + \phi_k(\dot{q}) = \tau_k$$

10. Given $D(q) = [d_{ij}(q)]$ and $V(q)$

- Find $\frac{\partial d_{ij}}{\partial q_k}$ for each element d_{ij} in $D(q)$

and for each joint variable q_k

- Find Christoffel's symbols of 1st kind -

$$c_{ijk} = \frac{1}{2} \left[\frac{\partial d_{kj}}{\partial q_i} + \frac{\partial d_{ki}}{\partial q_j} - \frac{\partial d_{ij}}{\partial q_k} \right]$$

- Find forces from the potential field

$$\phi_k = \frac{\partial V(q)}{\partial q_k}$$

After calculating all the terms, write the k th equation as

$$\sum_j d_{kj} \ddot{q}_j + \sum_{ijk} c_{ijk}(\dot{q}) \dot{q}_i \dot{q}_j + \phi_k(\dot{q}) = \tau_k$$

- 12.
-
- Number of links : 6
Number of joints : 6
Nature of joints: All are Revolute

D-H parameters : $\theta_i, d_i, a_i, \alpha_i$

$$J1: (q_1, 0, 0, \frac{\pi}{2}) \quad \text{currently } q_1 = \frac{\pi}{2}$$

$$J2: (q_2, 0, l_1, 0) \quad \text{currently } q_2 = \frac{\pi}{2}$$

$$J3: (q_3, 0, l_2, 0) \quad \text{currently } q_3 = 0$$

$$J4: (q_4, 0, 0, -\frac{\pi}{2}) \quad \text{currently } q_4 = -\frac{\pi}{2}$$

$$J5: (q_5, 0, 0, \frac{\pi}{2}) \quad \text{currently } q_5 = 0$$

$$J6: (q_6, 0, 0, 0) \quad \text{currently } q_6 = 0$$

o_1, o_2, o_3, o_4, o_5 are offsets

l_1 and l_2 are link lengths.