

20110029

— Ashutosh-Goyal — MEG39 —
Assignment - 2

$$\boxed{① \quad R S(a) R^T = S(Ra)}$$

\downarrow
 R is a rotation matrix

We know that, In case of rotation matrix

$$\boxed{\rightarrow R(axb) = (Ra) \times (Rb)} - ①$$

Also,

$$\boxed{S(a) \cdot p = a \times p} - ②$$

Also,

$$\boxed{S(\alpha a + \beta b) = \alpha S(a) + \beta S(b)}$$

Therefore, From ① & ② we can write

$$(Ra) \times (RR^T b) = R \underbrace{(a \times R^T b)}_{\downarrow} \\ S(a) \cdot R^T b$$

Hence,

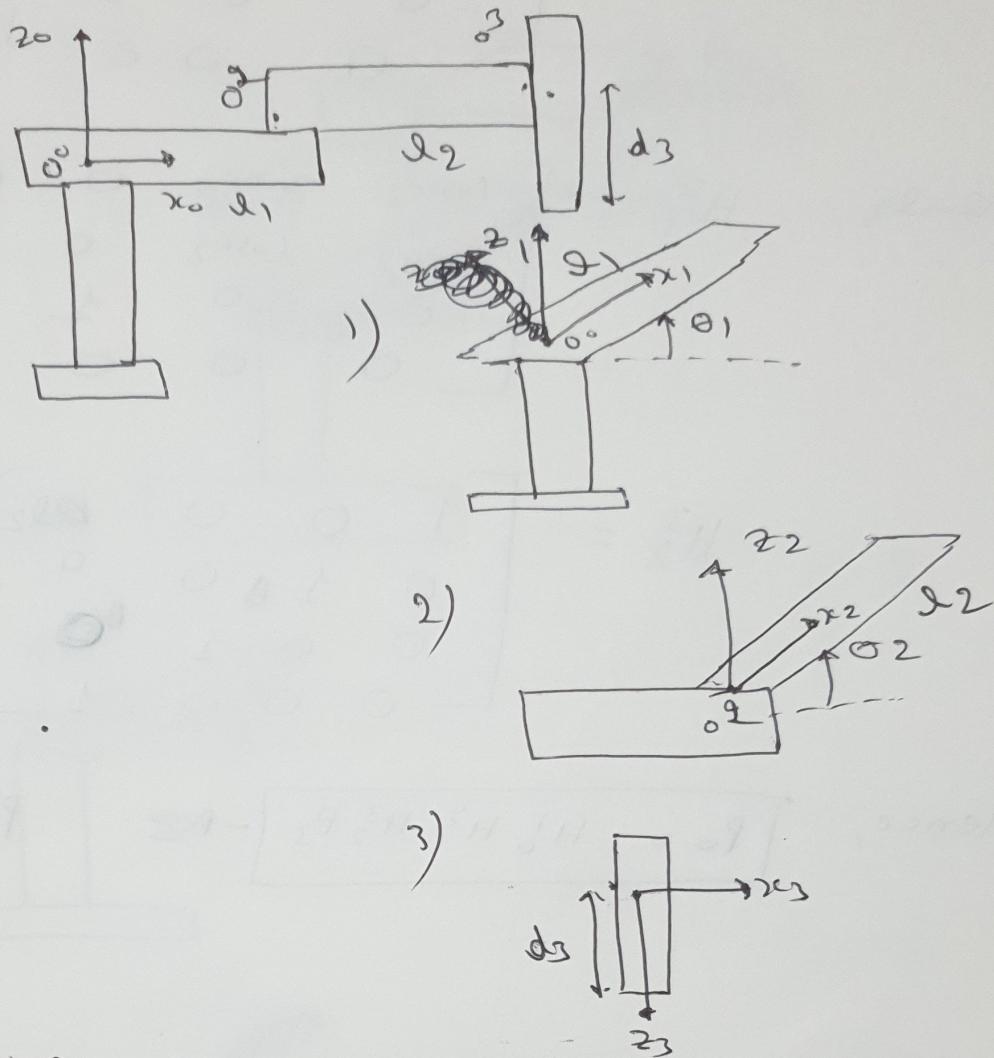
$$RS(a) \cdot R^T b = (Ra) \times \underbrace{(RR^T b)}_{+ I} \\ = (Ra) \times b$$

$$\boxed{RS(a) \cdot R^T b = S(Ra)b}$$

Hence, we get

$$\boxed{RS(a) R^T = S(Ra)} \xrightarrow{\text{Hence proved}}$$

(2)

SCARA

Now, let's suppose, we know the position of end-effector w.r.t 3rd frame, and want to find out the w.r.t 0th frame.

$$P_0 = H_0^1 H_1^2 H_2^3 P_3$$

Rotation
about z -axis
by angle θ_1

translation about
 z -axis by
 d_3
rotation about
 z -axis by
angle θ_2

$$H = \begin{bmatrix} R & d \\ 0 & 1 \end{bmatrix}$$

Hence, $H_0^1 = \begin{bmatrix} \cos\theta_1 & -\sin\theta_1 & 0 & 0 \\ \sin\theta_1 & \cos\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$

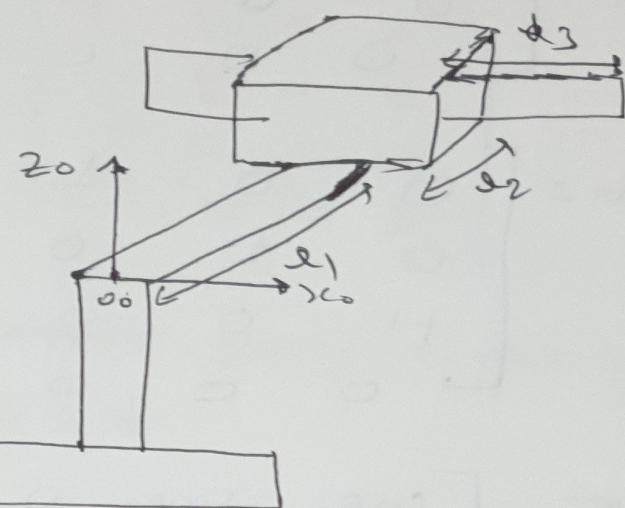
Similarly, $H_1^2 = \begin{bmatrix} \cos\theta_2 & -\sin\theta_2 & 0 & d_1 \\ \sin\theta_2 & \cos\theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$ As $d_1^2 = \begin{bmatrix} d_1 \\ 0 \\ 0 \end{bmatrix}$

$H_2^3 = \begin{bmatrix} 1 & 0 & 0 & d_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$ As $d_2^3 = \begin{bmatrix} d_2 \\ 0 \\ 0 \end{bmatrix}$

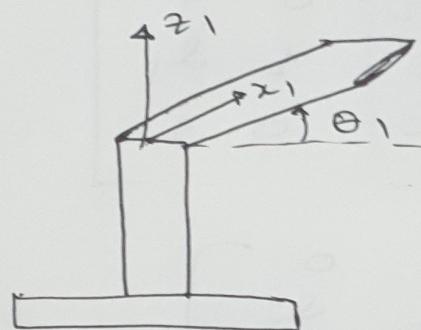
Hence, $P_0 = H_0^1 H_1^2 H_2^3 P_3$ - Ans $P_3 = \begin{bmatrix} 0 \\ 0 \\ -d_3 \\ 1 \end{bmatrix}$

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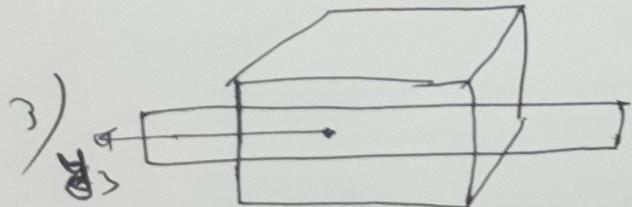
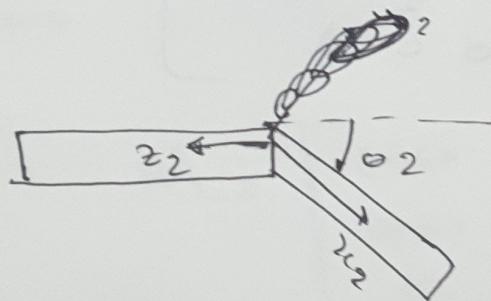
Standford-type



1)



2)



(Moment is occurring inside the plane)

Hence,

$$P_0 = H_0^1 H_1^2 H_2^3 P_3 \Rightarrow P_0 = H_0^1 R_{y, \theta_0} H_1^2 H_2^3 P_3$$

There will also be a rotation about y-axis, if we want to align both the z-axis in same direction.

$$\Rightarrow H_0^1 = \begin{bmatrix} \cos\theta_1 & -\sin\theta_1 & 0 & 0 \\ \sin\theta_1 & \cos\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$R_{Y,-90^\circ} = \begin{bmatrix} 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\textcircled{*} H_1^2 = \begin{bmatrix} \cos\theta_2 & -\sin\theta_2 & 0 & 0 \\ \sin\theta_2 & \cos\theta_2 & 0 & 0 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_2^3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$P_3 = \begin{bmatrix} 0 \\ d_3 \\ 0 \end{bmatrix}$$

⑤ Initially, drone moves 10m in z-direction

So,

$$H_0^1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 10 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Now, there is rotation about x-axis by an angle of $\theta = 30^\circ$

Hence,

$$H_1^2 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 30 & -\sin 30 & 0 \\ 0 & \sin 30 & \cos 30 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Now, there is follow-up rotation of $\theta = 60^\circ$ about z-axis

\Rightarrow

$$H_2^3 = \begin{bmatrix} \cos 60 & -\sin 60 & 0 & 0 \\ \sin 60 & \cos 60 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Now, finally obstacle is at 3m above the drone.

Hence

$$P_3 = \begin{bmatrix} 0 \\ 0 \\ 3 \\ 1 \end{bmatrix}$$

↓
Location
of obstacle
w.r.t current/last
frame & Drone's frame

$$\text{Hence, } P_0 = H_0^1 H_1^2 H_2^3 P_3$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 10 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 30 & -\sin 30 & 0 \\ 0 & \sin 30 & \cos 30 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos 60 & -\sin 60 & 0 & 0 \\ \sin 60 & \cos 60 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 3 \\ 1 \end{bmatrix}$$

Hence, By solving this, we get

$$P_0 = \begin{bmatrix} 0 \\ -1.5 \\ 12.98 \\ 1 \end{bmatrix}$$

Hence, the position vector of the obstacle wrt
base frame is

$$(0, -1.5, 12.98)$$

Ans

⑥ There are various types of gearbox which are generally used in motor to provide torque or to alter the velocity.

1) Helical gears: - Helical gears have a diagonal tooth profile which allows them to be quieter and smoother than other gears. They have the ability to be mounted in parallel or crossed but they have disadvantages as they are less efficient.

2) Spur gears: - They have straight teeth that are easy to align and they are very efficient and there is minimal power lost due to slippage. But, we can only use them in parallel only. They also become noisy at high speeds.

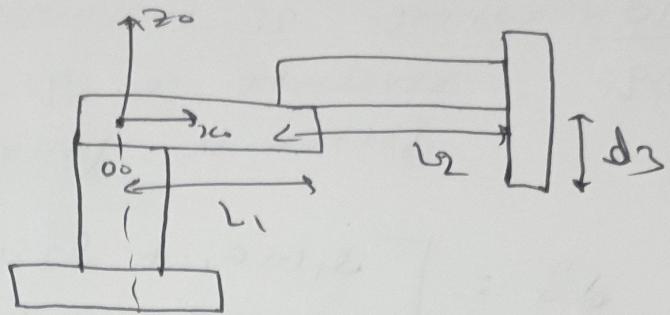
3) Bevel gears: - These are used for intersecting shafts and have a changeable operating angle due to their shape. They have a disadvantage like there are very difficult to assemble due to changeable operating angle.

4) Rack gear: - They have the advantage of like when paired with a spur gear or pinion; they can transfer rotary motion into linear motion. But they cannot run continuously, since the rack will eventually end.

5) Worm gears:- Worm gears are self-locking and quiet, but suffer from high power loss and high thrust load on the worm.

The main work of the gearbox is providing the high torque which is generally done by reducing the speed. But, In drones we need very high speed. Therefore, we ~~use~~ generally prefer to use the gearbox in drone. We generally use BLDC motor in drones which is gearless.

(7)



we know that,

$$\begin{bmatrix} v \\ w \end{bmatrix} = \begin{bmatrix} \dot{x}_v \\ \dot{x}_w \end{bmatrix}_i$$

Here, 2 joints are revolute & 1 is prismatic

Also, $\dot{x}_w = [g_1, g_2, \dots, g_{n-1}]$

Therefore, $\boxed{g_1 = g_2 = 1}$ & $\boxed{g_3 = 0}$

Also, $\boxed{z_i = R_0^{i-1} k}$

For First rotation:-

$$z_0 = \begin{bmatrix} \cos\theta_0 & -\sin\theta_0 & 0 \\ \sin\theta_0 & \cos\theta_0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\Rightarrow z_0 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

similarly, $z_1 = \begin{bmatrix} \cos(\theta_1 + \theta_0) & -\sin(\theta_1 + \theta_0) & 0 \\ \sin(\theta_1 + \theta_0) & \cos(\theta_1 + \theta_0) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$

Hence, $z_1 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$

Hence, $\bar{J}_W = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 0 \end{bmatrix}$

Now, we know that i^{th} column of J_W is $\frac{dq_i}{\delta q_i}$ where q_i is angle if i^{th} joint is revolute & q_i is distance if i^{th} joint is prismatic.

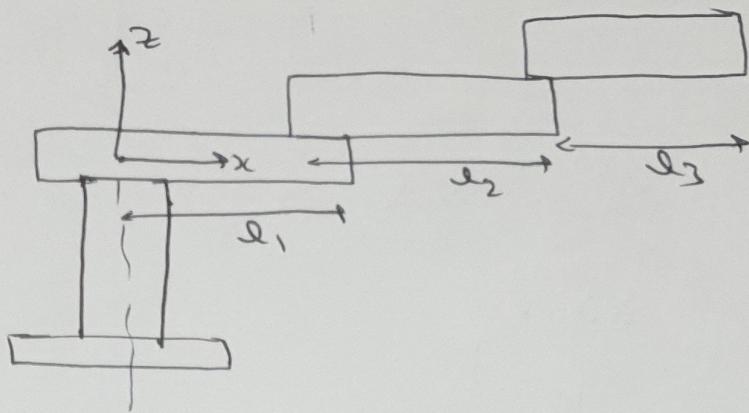
Further, $\frac{dq_i}{\delta q_i} = \begin{bmatrix} l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) \\ l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) \\ -d_3 \end{bmatrix}$

Hence, $\bar{J}_W = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} & -l_2 s_{12} & 0 \\ l_1 c_1 + l_2 c_{12} & l_2 c_{12} & 0 \\ 0 & 0 & -1 \end{bmatrix}$

Therefore, $J = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 0 \\ -(l_1 s_1 + l_2 s_{12}) & -l_2 s_{12} & 0 \\ l_1 c_1 + l_2 c_{12} & l_2 c_{12} & 0 \\ 0 & 0 & -1 \end{bmatrix}$

AM \downarrow
 Jacobian manipulator
 For SCARA

(9)



we know that,

$$\begin{bmatrix} v \\ w \end{bmatrix} = \begin{bmatrix} Jv \\ Jw \end{bmatrix} \dot{q}$$

Here all joints are revolute.

~~10~~

$$Jw = \begin{bmatrix} \delta_1 z_0 & \dots & \delta_n z_{n-1} \end{bmatrix}$$

As all joints are revolute $\Rightarrow \boxed{\delta_1 = \delta_2 = \delta_3 = 1}$

$$z_i = R_0^{i-1} k$$

For First rotation:-

$$z_0 = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 \\ \sin \theta_1 & \cos \theta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\Rightarrow z_0 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

Similarly, $z_1 = \begin{bmatrix} \cos(\theta_1 + \theta_2) & -\sin(\theta_1 + \theta_2) & 0 \\ \sin(\theta_1 + \theta_2) & \cos(\theta_1 + \theta_2) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$

Similarly $z_3 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$

Hence,

$$J_V = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

Now, we know that $\text{the } i^{\text{th}}$ column of J_V is

$$\frac{\partial d_o^n}{\partial q_i}$$

Firstly,

$$d_o^n = \begin{bmatrix} l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) + l_3 \cos(\theta_1 + \theta_2 + \theta_3) \\ l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) + l_3 \sin(\theta_1 + \theta_2 + \theta_3) \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Now $J_V =$

$$\begin{bmatrix} \cancel{l_1} & \cancel{l_2} & \cancel{l_3} & -l_2 \dot{\theta}_{12} - l_3 \dot{\theta}_{123} & -l_3 \dot{\theta}_{123} \\ -l_1 \dot{\theta}_1 - l_2 \dot{\theta}_{12} - l_3 \dot{\theta}_{123} & l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123} & l_3 \dot{\theta}_{123} & \cancel{l_2 \dot{\theta}_{12}} & \cancel{l_3 \dot{\theta}_{123}} \\ l_1 \dot{\theta}_1 + l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123} & l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123} & l_3 \dot{\theta}_{123} & l_3 \dot{\theta}_{123} & l_3 \dot{\theta}_{123} \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

Hence,

$$\downarrow J =$$

Jacobian
Manipulator
Ans

$$J = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \\ -(l_1 \dot{\theta}_1 + l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123}) & -(l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123}) & -l_3 \dot{\theta}_{123} \\ l_1 \dot{\theta}_1 + l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123} & l_2 \dot{\theta}_{12} + l_3 \dot{\theta}_{123} & l_3 \dot{\theta}_{123} \\ 0 & 0 & 0 \end{bmatrix}$$