

# 3F1 Signals and Systems: Handout 16

## Course summary

Jossy Sayir

Michaelmas Term 2024

1 / 14

## Continuous-time signals and systems

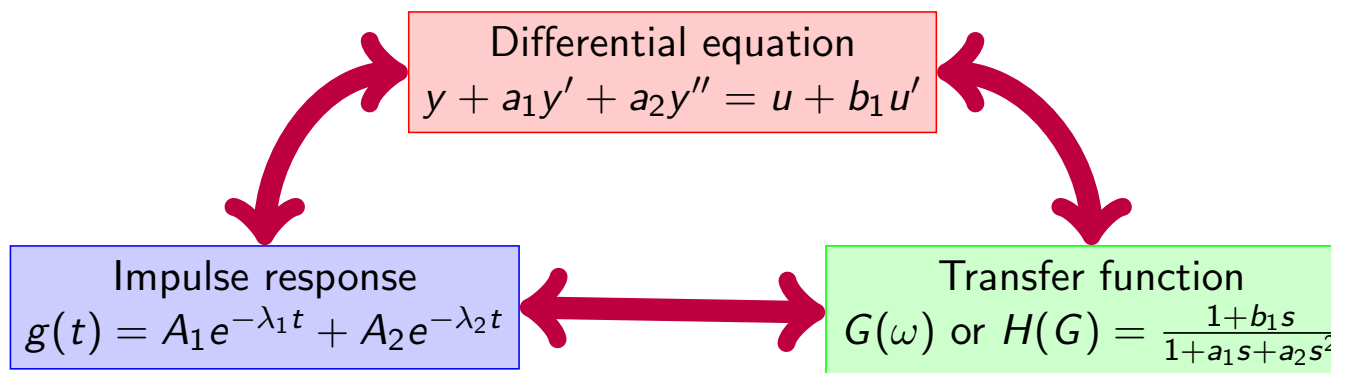


Figure: The 3 equivalent descriptions of a continuous-time LTIS

### Tools:

- ▶ Bode diagrams (stationary response to sinusoids)
- ▶ Nyquist diagrams (stability of closed-loop system)

2 / 14

# Discrete-time signals and systems

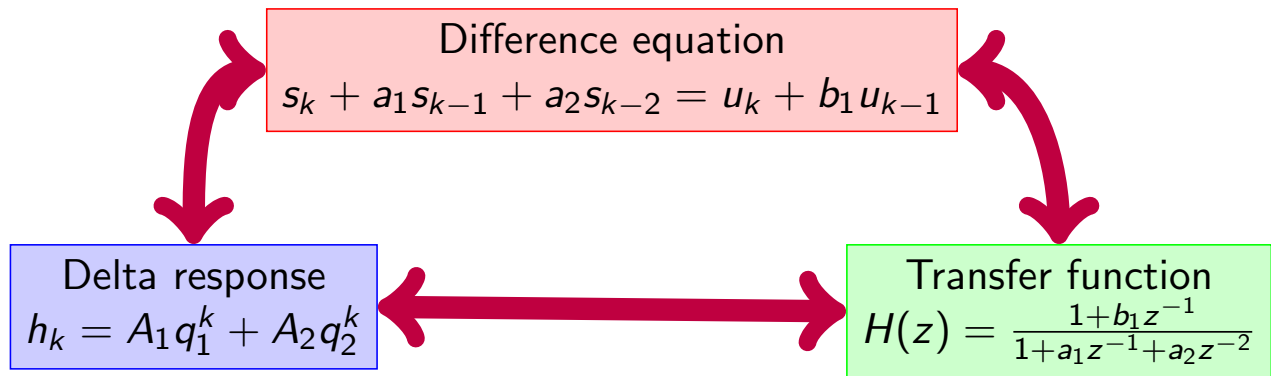


Figure: The 3 equivalent descriptions of a discrete-time LTIS

Tools:

- ▶ Bode diagrams (stationary response to sinusoidals)
- ▶ Nyquist diagrams (stability of closed-loop system)

3 / 14

## Discrete Transforms

- ▶ For a signal  $\{u_k\}$ , the  $z$  transform is defined as

$$U(z) = \sum_{k=0}^{\infty} u_k z^{-k}$$

- ▶ For a signal  $\{u_k\}$ , the DTFT is defined as

$$U(\theta) = \sum_{k=-\infty}^{\infty} u_k e^{-jk\theta}$$

- ▶ both transforms have a convolution property, shift properties, conjugate symmetry properties (the DTFT also has a reverse conjugate symmetry property)
- ▶ both transforms can be inverted by inspection but the DTFT also has an inversion expression

$$s_k = \frac{1}{2\pi} \int_{-\pi}^{\pi} S(\theta) e^{jk\theta} d\theta$$

4 / 14

# Stability

## Theorem (Conditions for stability of a discrete time system)

Let  $G$  be a discrete time system with a rational transfer function,

$$G(z) = \frac{b(z)}{a(z)} = \frac{b_0 + \dots + b_m z^{-m}}{1 + a_1 z^{-1} + \dots + a_n z^{-n}}$$

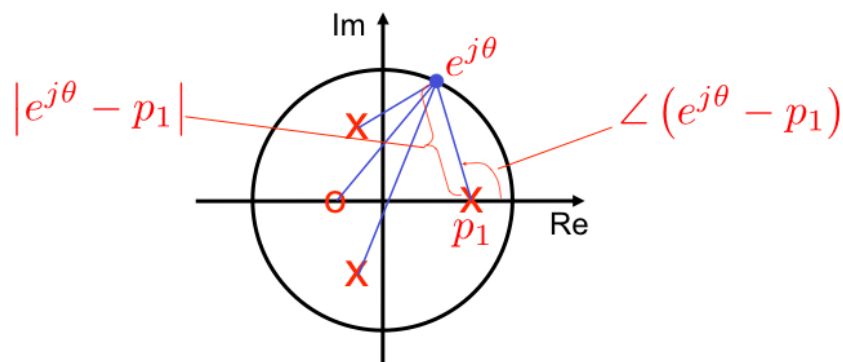
with no common factors between  $b(z)$  and  $a(z)$ . Let the pulse response of  $G$  be  $\{g_k\}_{k \geq 0}$ . Then the following are equivalent:

1.  $G$  is stable
2. All of the roots  $p_i$  of  $a(z)$  (i.e. poles) satisfy  $|p_i| < 1$
3.  $\sum_{k=0}^{\infty} |g_k|$  is finite

5 / 14

## Bode diagram for stable systems

►  $G(z) = c \frac{\prod_{k=1}^m (z - z_k)}{\prod_{k=1}^n (z - p_k)}$



►  $|G(e^{j\theta})| = |c| \frac{\prod_{k=1}^m |e^{j\theta} - z_k|}{\prod_{k=1}^n |e^{j\theta} - p_k|}$   
 $|G(e^{j\theta})|_{dB} = 20 \log(|G(e^{j\theta})|)$   
 $= 20 \left( \log |c| + \sum_{k=1}^m \log |e^{j\theta} - z_k| - \sum_{k=1}^n \log |e^{j\theta} - p_k| \right)$

►  $\angle G(e^{j\theta}) = \angle(c) + \sum_{k=1}^m \angle(e^{j\theta} - z_k) - \sum_{k=1}^n \angle(e^{j\theta} - p_k)$

6 / 14

## The Nyquist stability criterion

The closed loop system is stable if and only if the number of encirclements of  $-1/K$  by  $G(e^{j\theta})$  as  $\theta$  increases from  $-\pi$  to  $\pi$  equals the number of open loop poles strictly outside the unit circle.

7 / 14

## Algebraic transformations from Laplace to $z$ domain

$H(z) = H_c(s)_{s=\psi(z)}$  where  $\psi(\cdot)$  is given by

Euler's method or Forward difference

$$s = \frac{z - 1}{T} \quad (\text{intuition: linear approximation})$$

Backward difference

$$s = \frac{1 - z^{-1}}{T} \quad (\text{intuition } \dot{x} \simeq \frac{x(t) - x(t - T)}{T})$$

Bilinear (Tustin's) transformation

$$s = \frac{2}{T} \frac{z - 1}{z + 1} \quad (\text{or simply } \frac{z - 1}{z + 1})$$

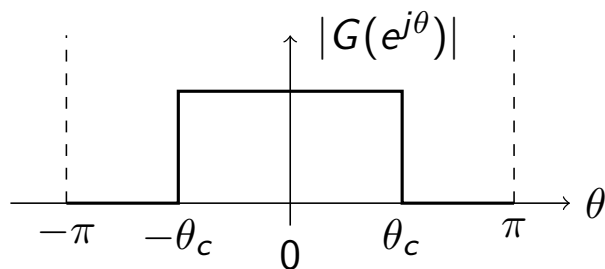
8 / 14

# Response invariant transforms of continuous time systems

- ▶ impulse invariant
- ▶ step invariant
- ▶ ramp invariant

9 / 14

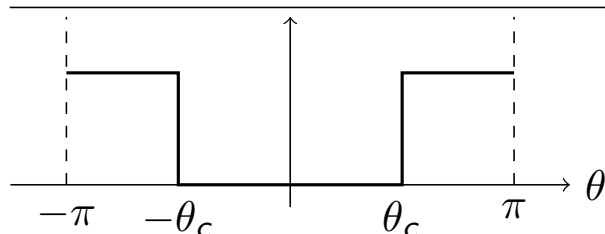
## Filter design: desired frequency responses



stopband passband stopband

Lowpass:

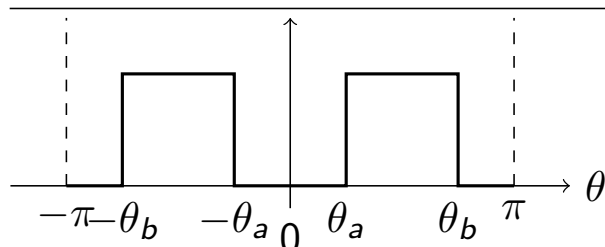
$$G(e^{j\theta}) = \begin{cases} 1 & |\theta| \leq \theta_c \\ 0 & |\theta| > \theta_c \end{cases}$$



passband stopband passband

Highpass:

$$G(e^{j\theta}) = \begin{cases} 0 & |\theta| \leq \theta_c \\ 1 & |\theta| > \theta_c \end{cases}$$



Bandpass:

$$G(e^{j\theta}) = \begin{cases} 1 & \theta_a \leq |\theta| \leq \theta_b \\ 0 & \text{otherwise} \end{cases}$$

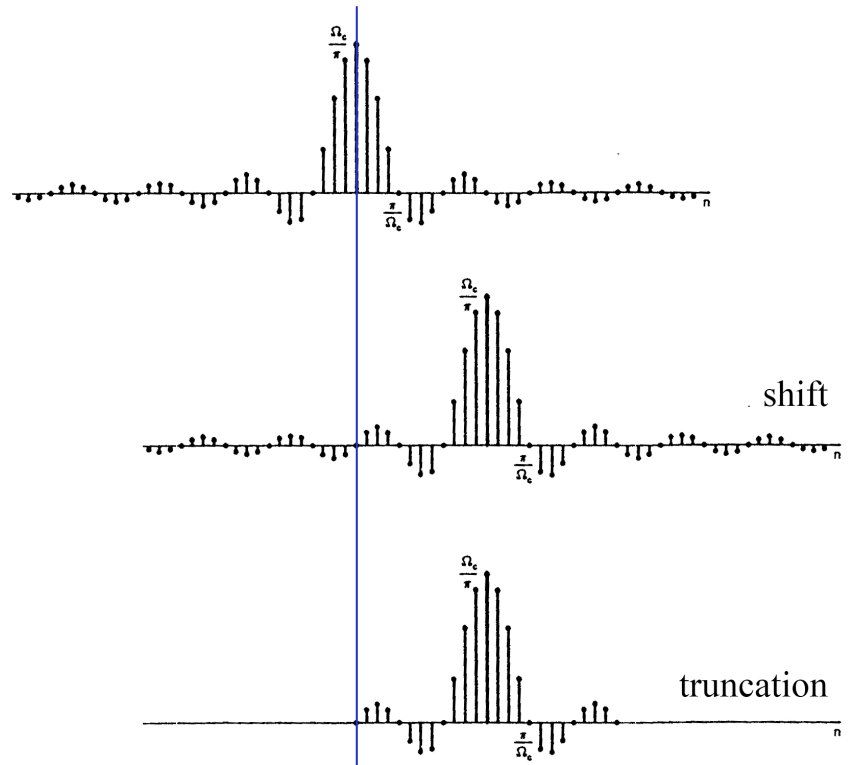
10 / 14

## FIR filter design

$h_k$  is the non-causal impulse response of the ideal filter

New (finite impulse response) filter  $G$  derived by shift and truncation at  $N + 1$  samples of the ideal response

Causality is recovered.  
Intuition: truncation of “small” samples has modest impact...



Use windowing!

11 / 14

## IIR filter design

→ use algebraic transforms starting from continuous time designs

12 / 14

## DFT is a matrix multiplication

$$\mathbf{F} = \begin{bmatrix} 1 & 1 & 1 & \dots & 1 \\ 1 & W_N & W_N^2 & \dots & W_N^{N-1} \\ 1 & W_N^2 & W_N^4 & \dots & W_N^{2(N-1)} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 1 & W_N^{N-1} & W_N^{2(N-1)} & \dots & W_N^{(N-1)^2} \end{bmatrix}$$

- ▶  $W_N = e^{-j\frac{2\pi}{N}}$
- ▶ it has the convolution property, time shift properties, conjugate symmetry properties
- ▶ **all properties are cyclic/circular**
- ▶ the FFT performs the matrix multiplication in  $O(N \log N)$

13 / 14

## Random processes

For stationary ergodic random processes,

		Discrete time	Continuous time
Time	Auto-correl. function	$r_{XX}[k] = E[X_\ell X_{\ell+k}]$ $r_{XY}[k] = E[X_\ell Y_{\ell+k}]$	$r_{XX}(\tau) = E[X(t)X(t+\tau)]$ $r_{XY}(\tau) = E[X(t)Y(t+\tau)]$
Frequency	PSD, CSD	$S_{XX}(\theta), S_{XY}(\theta)$	$S_{XX}(\omega), S_{XY}(\omega)$
Linear filtering		$\begin{cases} S_{YY}(\theta) =  H(\theta) ^2 S_{XX}(\theta) \\ S_{XY}(\theta) = H(\theta) S_{XX}(\theta) \end{cases}$	$\begin{cases} S_{YY}(\omega) =  H(\omega) ^2 S_{XX}(\omega) \\ S_{XY}(\omega) = H(\omega) S_{XX}(\omega) \end{cases}$

- ▶ PSD: power spectral density, CSD: cross spectral density
- ▶ most of the content of these 3 last lectures aims to motivate and explain the content of this slide

14 / 14