

- 1) A  $50\text{Hz}$  generating unit has  $H$ -constant of  $2\text{MJ/MVA}$ . The machine is initially operating in steady state at synchronous speed, and producing  $1\text{pu}$  of real power. The initial value of the rotor angle  $\delta$  is  $5^\circ$ , when a bolted three phase to ground short circuit fault occurs at the terminal of the generator. Assuming the input mechanical power to remain at  $1\text{pu}$ , the value of  $\delta$  in degrees,  $0.02$  seconds after the fault is \_\_\_\_\_.
- 2) A sustained three-phase fault occurs in the power system shown in the figure 2.1. The current and voltage phasors during the fault (on a common reference), after the natural transients have died down, are also shown. Where is the fault located?

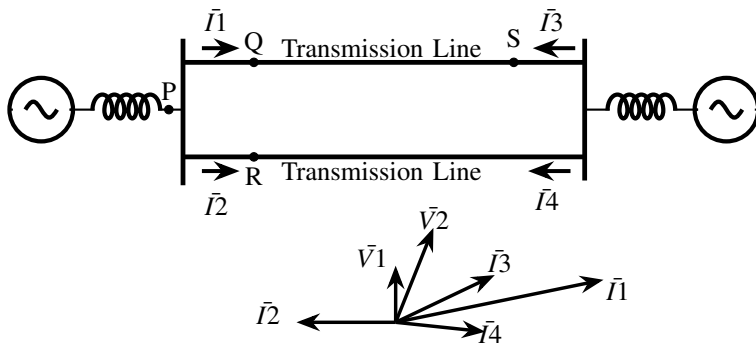


Fig. 2.1

- a) Location P
  - b) Location Q
  - c) Location R
  - d) Location S
- 3) The circuit shown in the figure 3.1 has two sources connected in series. The instantaneous voltage of AC source (in Volt) is given by  $v(t) = 12 \sin t$ . If the circuit is in steady state, then the rms value of the current (in Ampere) flowing in the circuit is \_\_\_\_\_.

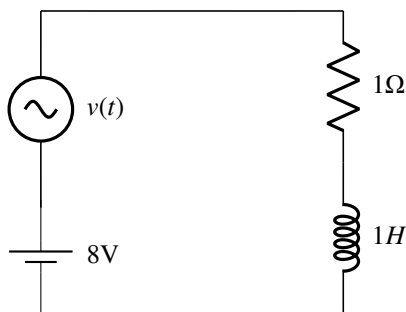


Fig. 3.1

- 4) In a linear two-port network, when  $10V$  is applied to Port 1, a current of  $4A$  flows through Port 2 when it is short-circuited. When  $5V$  is applied to Port 1, a current of  $1.25A$  flows through a  $1\Omega$  resistance connected across Port 2. When  $3V$  is applied to Port 1, the current (in Ampere) through a  $2\Omega$  resistance connected across Port 2 is \_\_\_\_\_.
- 5) In the given circuit, the parameter  $k$  is positive, and the power dissipated in the  $2\Omega$  resistor is  $12.5W$ . The value of  $k$  is \_\_\_\_\_.

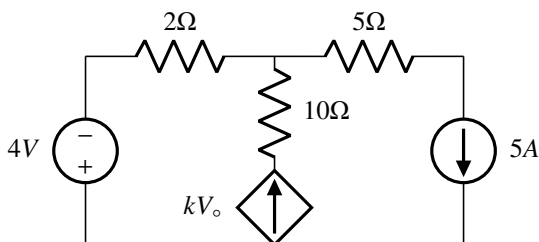


Fig. 5.1

- 6) A separately excited DC motor runs at  $1000\text{ rpm}$  on no load when its armature terminals are connected to a  $200V$  DC source and the rated voltage is applied to the field winding. The armature resistance of this motor is  $1\Omega$ . The no-load armature current is negligible. With the motor developing its full load torque, the armature voltage is set so that the rotor speed is  $500\text{ rpm}$ . When the load torque is reduced to  $50\%$  of the full load value under the same armature voltage conditions, the speed rises to  $520\text{ rpm}$ . Neglecting the rotational losses, the full load armature current (in Ampere) is \_\_\_\_\_.
- 7) A DC motor has the following specifications:  $10\text{ hp}$ ,  $37.5A$ ,  $230V$ ; flux / pole =  $0.01\text{ Wb}$ , number of poles =  $4$ , number of conductors =  $666$ , number of parallel paths =  $2$ . Armature resistance =  $0.267\Omega$ . The armature reaction is negligible and rotational losses are  $600W$ . The motor operates from a  $230V$  DC supply. If the motor runs at  $1000\text{ rpm}$ , the output torque produced (in  $Nm$ ) is \_\_\_\_\_.
- 8) A  $200/400V$ ,  $50\text{Hz}$ , two-winding transformer is rated to  $20kVA$ . Its windings are

connected as an auto-transformer of rating 200/600V. A resistive load of  $12\Omega$  is connected to the high voltage (600V) side of the auto-transformer. The values of equivalent load resistance (in Ohm) as seen from low voltage side is \_\_\_\_\_.

- 9) Two single-phase transformers  $T_1$  and  $T_2$  each rated at 500kVA are operated in parallel. Percentage impedances of  $T_1$  and  $T_2$  are  $(1 + j6)$  and  $(0.8 + j4.8)$ , respectively. To share a load of 1000kVA at 0.8 lagging power factor, the contribution of  $T_2$  (in kVA) is \_\_\_\_\_.
- 10) In the signal flow diagram given in the figure 10.1,  $u_1$  and  $u_2$  are possible inputs whereas  $y_1$  and  $y_2$  are possible outputs. When would the SISO system derived from this diagram be controllable and observable?

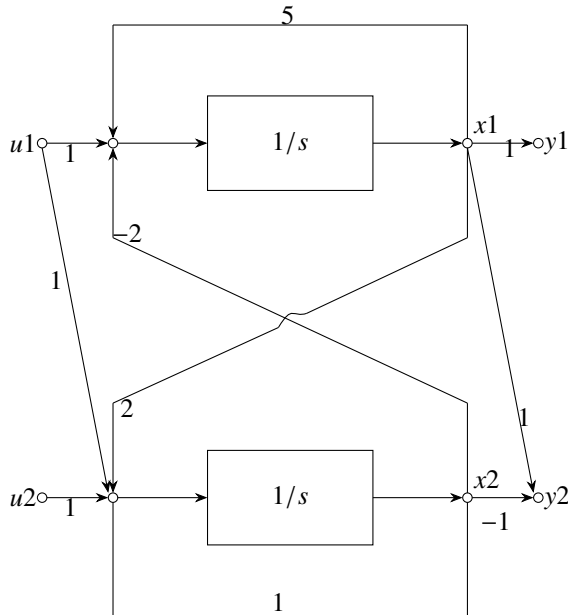


Fig. 10.1

- When  $u_1$  is the only input and  $y_1$  is the only output.
  - When  $u_2$  is the only input and  $y_1$  is the only output.
  - When  $u_1$  is the only input and  $y_2$  is the only output.
  - When  $u_2$  is the only input and  $y_2$  is the only output.
- 11) The transfer function of a second order real system with a perfectly flat magnitude response of unity has pole at  $(2 - j3)$ . List all the poles and zeroes.
- Poles at  $(2 \pm j3)$ , no zeroes.
  - Poles at  $(\pm 2 - j3)$ , one zero at origin.
  - Poles at  $(2 - j3)$ ,  $(-2 + j3)$ , zeroes at  $(-2 - j3)$ ,  $(2 + j3)$
  - Poles at  $(2 \pm j3)$ , zeroes at  $(-2 \pm j3)$
- 12) Find the transfer function  $\frac{Y(s)}{X(s)}$  of the system given below.

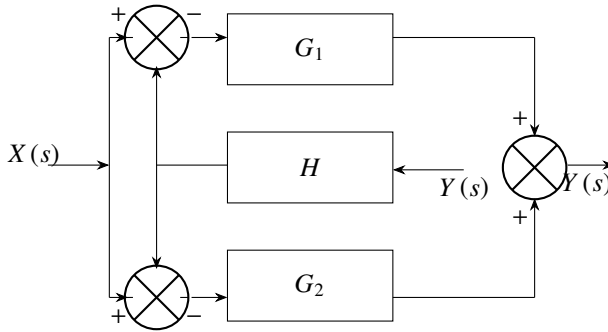


Fig. 12.1

- a)  $\frac{G_1}{1-HG_1} + \frac{G_2}{1-HG_2}$
- b)  $\frac{G_1}{1+HG_1} + \frac{G_2}{1+HG_2}$
- c)  $\frac{G_1+G_2}{1+H(G_1+G_2)}$
- d)  $\frac{G_1+G_2}{1-H(G_1+G_2)}$

- 13) The open loop poles of a third order unity feedback system are  $0, -1, -2$ . Let the frequency corresponding to the point where locus of the system transits to unstable region be  $K$ . Now suppose we introduce a zero in the open loop transfer function at  $-3$ , while keeping all the earlier open loop poles intact. Which one of the following is TRUE about the point where the root locus of the modified system transits to unstable region?
- a) It corresponds to a frequency greater than  $K$
  - b) It corresponds to a frequency less than  $K$
  - c) It corresponds to a frequency  $K$
  - d) Root locus of modified system never transits to unstable region