

Supporting Information for: Porosity-Permeability Relationships in Mudstone from Pore-Scale Fluid Flow Simulations using the Lattice Boltzmann Method

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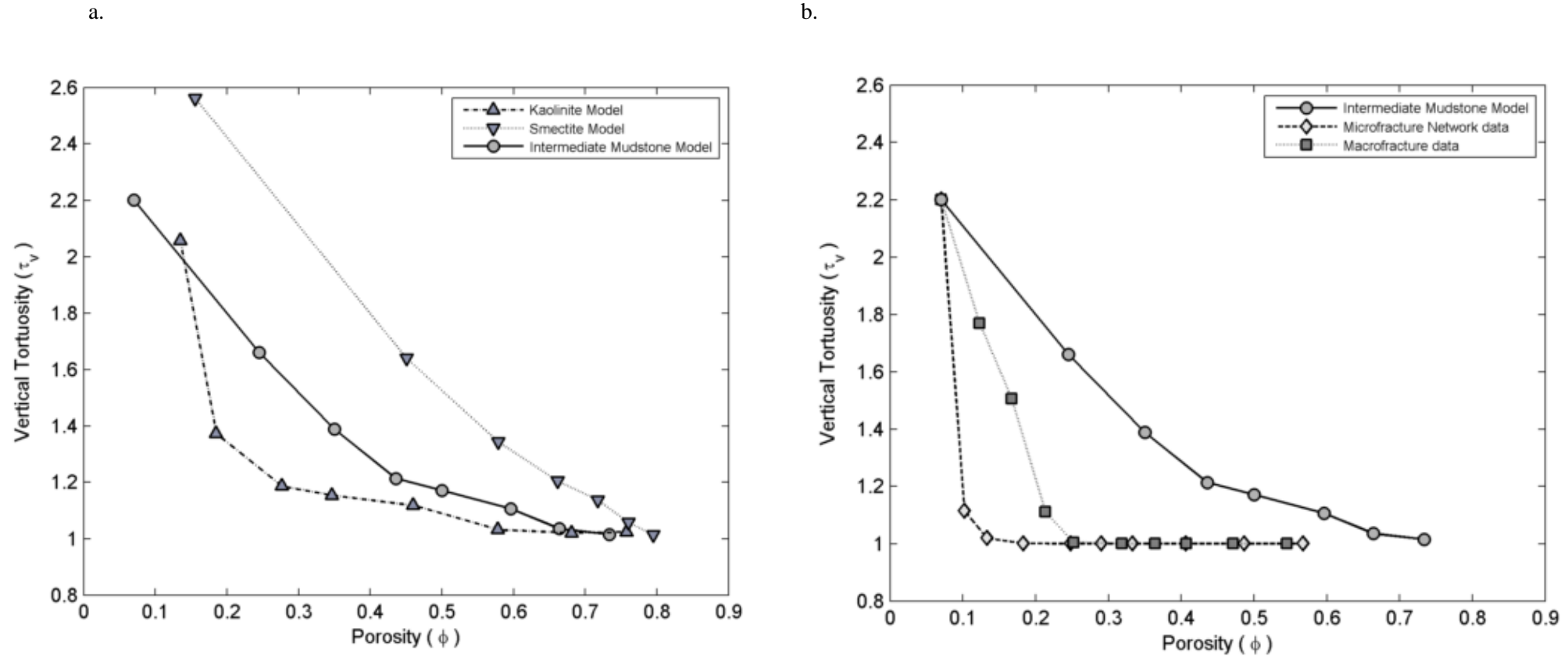
This supporting information includes six parts:

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Table S1: Vertical (q_v) and horizontal (q_h) flux during compaction of kaolinite, smectite and intermediate mudstone models, simulated by step-wise decrease in intrabed (ξ) and interbed pore throat diameters (λ).

Model	Step	Porosity ϕ	Intrabed Pore Throat Width ξ	Interbed Pore Throat Width λ	Platelet Orientation Θ	Vertical Flux q_v	Reynolds Number Vertical flow Re_v	Vertical Permeability k_v	Vertical Tortuosity τ_v	Horizontal Flux q_h	Reynolds Number Horizontal flow Re_h	Horizontal Permeability k_h	Horizontal Tortuosity τ_h
			(nm)	(nm)	Degrees	(m/s)		(m ²)		(m/s)		(m ²)	
Kaolinite	1	0.76	3.60×10^2	3.60×10^2	45	7.15×10^{-1}	2.41×10^0	8.31×10^{-15}	1.02	1.12×10^{-1}	1.88×10^{-2}	1.10×10^{-14}	6.56
Kaolinite	2	0.68	2.60×10^2	2.60×10^2	35	3.56×10^{-1}	1.20×10^0	3.42×10^{-15}	1.02	5.16×10^{-2}	8.69×10^{-3}	4.96×10^{-15}	7.05
Kaolinite	3	0.58	1.80×10^2	1.80×10^2	25	9.81×10^{-2}	3.31×10^{-1}	7.84×10^{-16}	1.03	1.77×10^{-2}	2.99×10^{-3}	1.68×10^{-15}	5.71
Kaolinite	4	0.46	1.20×10^2	1.20×10^2	20	2.63×10^{-2}	8.85×10^{-2}	1.78×10^{-16}	1.12	9.27×10^{-3}	1.56×10^{-3}	8.67×10^{-16}	3.17
Kaolinite	5	0.35	8.00×10^1	8.00×10^1	15	5.73×10^{-3}	1.93×10^{-2}	3.42×10^{-17}	1.15	2.33×10^{-3}	3.93×10^{-4}	2.16×10^{-16}	2.83
Kaolinite	6	0.28	6.00×10^1	6.00×10^1	10	1.92×10^{-3}	6.49×10^{-3}	1.07×10^{-17}	1.19	8.69×10^{-4}	1.47×10^{-4}	8.02×10^{-17}	2.63
Kaolinite	7	0.19	4.00×10^1	4.00×10^1	5	3.91×10^{-4}	1.32×10^{-3}	2.02×10^{-18}	1.37	2.60×10^{-4}	4.39×10^{-5}	2.39×10^{-17}	2.06
Kaolinite	8	0.14	4.00×10^1	4.00×10^1	0	1.23×10^{-4}	4.14×10^{-4}	6.33×10^{-19}	2.06	1.56×10^{-4}	2.63×10^{-5}	1.43×10^{-17}	1.62
Smectite	1	0.80	9.00×10^0	9.00×10^0	45	3.56×10^{-1}	4.00×10^{-2}	6.84×10^{-17}	1.01	4.18×10^{-2}	9.40×10^{-5}	1.33×10^{-16}	8.64
Smectite	2	0.76	7.00×10^0	7.00×10^0	35	2.10×10^{-1}	2.36×10^{-2}	3.61×10^{-17}	1.06	5.08×10^{-2}	1.14×10^{-4}	1.60×10^{-16}	4.37
Smectite	3	0.72	5.00×10^0	5.00×10^0	25	1.08×10^{-1}	1.21×10^{-2}	1.63×10^{-17}	1.14	4.11×10^{-2}	9.24×10^{-5}	1.29×10^{-16}	2.98
Smectite	4	0.66	4.00×10^0	4.00×10^0	15	3.50×10^{-2}	3.93×10^{-3}	4.60×10^{-18}	1.20	1.66×10^{-2}	3.72×10^{-5}	5.16×10^{-17}	2.54
Smectite	5	0.58	3.00×10^0	3.00×10^0	10	5.02×10^{-3}	5.64×10^{-4}	5.59×10^{-19}	1.34	3.18×10^{-3}	7.15×10^{-6}	9.85×10^{-18}	2.12
Smectite	6	0.45	2.00×10^0	2.00×10^0	5	3.04×10^{-4}	3.42×10^{-5}	2.77×10^{-20}	1.64	2.79×10^{-4}	6.28×10^{-7}	8.59×10^{-19}	1.78
Smectite	7	0.16	1.00×10^0	1.00×10^0	0	1.84×10^{-7}	2.06×10^{-8}	1.30×10^{-23}	2.56	3.06×10^{-7}	6.88×10^{-10}	9.35×10^{-22}	1.54
General	1	0.73	13.71×10^1	13.71×10^1	45	1.39×10^{-1}	3.12×10^{-1}	6.10×10^{-16}	1.02	1.75×10^{-2}	1.12×10^{-3}	1.11×10^{-15}	8.06
General	2	0.66	10.28×10^1	10.28×10^1	35	3.73×10^{-2}	8.37×10^{-2}	1.38×10^{-16}	1.04	7.07×10^{-3}	4.54×10^{-4}	4.44×10^{-16}	5.46
General	3	0.60	80.00×10^0	80.00×10^0	25	1.73×10^{-2}	3.88×10^{-2}	5.59×10^{-17}	1.11	5.78×10^{-3}	3.71×10^{-4}	3.60×10^{-16}	3.31
General	4	0.50	57.14×10^0	57.14×10^0	20	6.95×10^{-3}	1.56×10^{-2}	1.93×10^{-17}	1.17	3.00×10^{-3}	1.93×10^{-4}	1.86×10^{-16}	2.71
General	5	0.44	45.71×10^0	45.71×10^0	15	2.98×10^{-3}	6.70×10^{-3}	7.58×10^{-18}	1.21	1.45×10^{-3}	9.31×10^{-5}	8.93×10^{-17}	2.50
General	6	0.35	34.28×10^0	34.28×10^0	10	1.06×10^{-3}	2.38×10^{-3}	2.45×10^{-8}	1.39	7.22×10^{-4}	4.64×10^{-5}	4.43×10^{-17}	2.04
General	7	0.25	22.85×10^0	22.85×10^0	5	2.48×10^{-4}	5.57×10^{-4}	5.16×10^{-19}	1.66	2.33×10^{-4}	1.49×10^{-5}	1.42×10^{-17}	1.77
General	8	0.07	11.42×10^0	11.42×10^0	0	5.54×10^{-6}	1.24×10^{-5}	1.02×10^{-20}	2.20	7.68×10^{-6}	4.93×10^{-7}	4.68×10^{-19}	1.59

Fig. S1: Vertical tortuosity (τ_v) (a) increases as porosity declines during compaction of kaolinite, smectite and intermediate mudstone models (b) declines with growth of microfracture network and macrofracture propagation during simulated fluid injection in compacted intermediate mudstone model.



Text S1: Incorporating heterogenous platelet geometry in mudstone models: We employ inputs of mineral weight fractions of smectite, illite and chlorite to model the mudstone pore structures. We assume constant density of clay minerals; the modeled weight of each clay platelet can be calculated as $m\beta \times m\beta \times \beta$. The maximum number of smectite ($no_{smectite}^{max}$), illite (no_{illite}^{max}) and chlorite ($no_{chlorite}^{max}$) platelets in the models are calculated as:

$$no_{smectite}^{max} = [0.1 \mu m * 0.1 \mu m * 0.002 \mu m] * input \text{ smectite wt\%}, \quad (S1)$$

$$no_{illite}^{max} = [2 \mu m * 2 \mu m * 0.1 \mu m] * input \text{ illite wt\%}, \quad (S2)$$

$$no_{chlorite}^{max} = [2.5 \mu m * 2.5 \mu m * 0.1 \mu m] * input \text{ chlorite wt\%}. \quad (S3)$$

The number of smectite ($no_{smectite}$), illite (no_{illite}) and chlorite ($no_{chlorite}$) platelets in a model are determined using the highest common factor (HCF) between

$no_{smectite}^{max}$, no_{illite}^{max} and $no_{chlorite}^{max}$ as:

$$no_{smectite} = no_{smectite}^{max} / HCF, \quad (S4)$$

$$no_{illite} = no_{illite}^{max} / HCF, \quad (S5)$$

$$no_{chlorite} = no_{chlorite}^{max} / HCF. \quad (S6)$$

The number of bedding layers is determined as the highest common factor (HCF_beds) between $no_{smectite}$, no_{illite} and $no_{chlorite}$. The minimum value of HCF_beds is three. The number of smectite, illite and chlorite platelets in each bedding layer is calculated as $(no_{smectite}/HCF_beds)$, (no_{illite}/HCF_beds) and $(no_{chlorite}/HCF_beds)$ respectively. Each bed is simulated by random three-dimensional spatial distribution of $(no_{smectite}/HCF_beds)$ smectite platelets, (no_{illite}/HCF_beds) illite platelets and $(no_{chlorite}/HCF_beds)$ chlorite platelets with intrabed pore throats of diameter ε between platelets. The simulated beds are stacked vertically with interbed pore throat of diameter λ to develop the unrotated mudstone model [Fig. S3]. The developed matrix is transformed by input grain orientation angle, θ , to simulate the final mudstone model.

Figure S2: Scaled-down model of mudstone pore structure *NM2*, replicating mineralogy of natural sample 1324B-7H-7, at $\phi=0.79$. The mudstone model consists of 31% smectite, 41% illite and 28% chlorite by volume ($\theta=0^\circ$). (a) Cross sectional view of *NM2* pore structure with smectite, illite and chlorite platelets; and (b) Orthogonal view of *NM2* with directions of vertical (q_v) and horizontal flow (q_h).

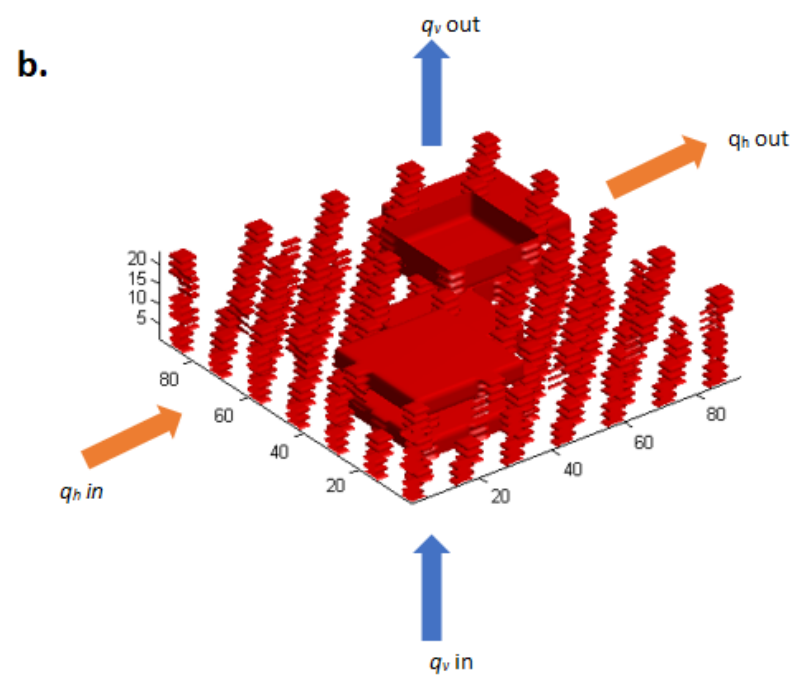
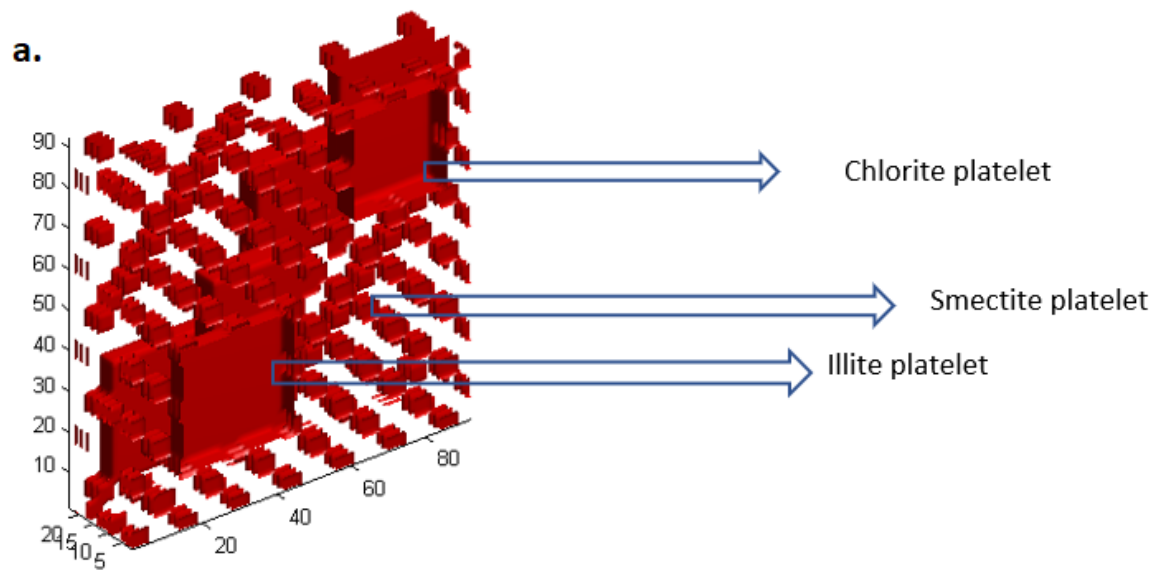


Table S2: Vertical (q_v) and horizontal (q_h) flux during compaction of *NM1* and *NM2* mudstone models, simulated by step-wise decrease in intrabed (ξ) and interbed pore throat diameters (λ).

Model	Step	Porosity ϕ	Intrabed Pore Throat Width ξ	Interbed Pore Throat Width λ	Platelet Orientation Θ	Vertical Flux q_v	Reynolds Number Vertical flow Re_v	Vertical Permeability k_v	Vertical Tortuosity τ_v	Horizontal Flux q_h	Reynolds Number Horizontal flow Re_h	Horizontal Permeability k_h	Horizontal Tortuosity τ_h
			(nm)	(nm)	Degrees	(m/s)		(m ²)		(m/s)		(m ²)	
NM1	1	0.72	5.05 x 10 ¹	5.05 x 10 ¹	15	5.03 x 10 ⁻²	2.71 x 10 ⁻²	1.54 x 10 ⁻¹⁶	1.74	5.08 x 10 ⁻²	7.42 x 10 ⁻⁴	1.39 x 10 ⁻¹⁵	1.73
NM1	2	0.67	3.85 x 10 ¹	3.85 x 10 ¹	10	1.90 x 10 ⁻²	1.03 x 10 ⁻²	5.19 x 10 ⁻¹⁷	2.06	2.43 x 10 ⁻²	3.55 x 10 ⁻⁴	6.53 x 10 ⁻¹⁶	1.62
NM1	3	0.60	2.65 x 10 ¹	2.65 x 10 ¹	6	3.94 x 10 ⁻³	2.12 x 10 ⁻³	9.39 x 10 ⁻¹⁸	2.44	6.22 x 10 ⁻³	9.08 x 10 ⁻⁵	1.64 x 10 ⁻¹⁶	1.55
NM1	4	0.49	1.45 x 10 ¹	1.45 x 10 ¹	3	3.36 x 10 ⁻⁴	1.81 x 10 ⁻⁴	6.86 x 10 ⁻¹⁹	2.99	6.70 x 10 ⁻⁴	9.78 x 10 ⁻⁶	1.73 x 10 ⁻¹⁷	1.50
NM1	5	0.32	2.5 x 10 ⁰	2.5 x 10 ⁰	0	4.17 x 10 ⁻⁶	2.25 x 10 ⁻⁶	7.09 x 10 ⁻²¹	3.69	1.05 x 10 ⁻⁵	1.53 x 10 ⁻⁷	2.66 x 10 ⁻¹⁹	1.47
NM2	1	0.58	6.25 x 10 ¹	6.25 x 10 ¹	12	1.41x10 ⁻²	7.62 x 10 ⁻³	3.11 x 10 ⁻¹⁷	1.29	8.16 x 10 ⁻³	1.19 x 10 ⁻⁴	2.27 x 10 ⁻¹⁶	2.23
NM2	2	0.50	3.85 x 10 ¹	3.85 x 10 ¹	9	3.13x10 ⁻³	1.69 x 10 ⁻³	6.65 x 10 ⁻¹⁸	1.55	2.63 x 10 ⁻³	3.85 x 10 ⁻⁵	7.07 x 10 ⁻¹⁷	1.85
NM2	3	0.45	2.65 x 10 ¹	2.65 x 10 ¹	6	1.31 x 10 ⁻³	7.09 x 10 ⁻⁴	2.74 x 10 ⁻¹⁸	1.90	1.50 x 10 ⁻³	2.19 x 10 ⁻⁵	3.96 x 10 ⁻¹⁷	1.66
NM2	4	0.37	1.45 x 10 ¹	1.45 x 10 ¹	3	3.16 x 10 ⁻⁴	1.71 x 10 ⁻⁴	6.46 x 10 ⁻¹⁹	2.48	5.06 x 10 ⁻⁴	7.39 x 10 ⁻⁶	1.30 x 10 ⁻¹⁷	1.55
NM2	5	0.25	2.5 x 10 ⁰	2.5 x 10 ⁰	0	2.39 x 10 ⁻⁵	1.29 x 10 ⁻⁵	4.79 x 10 ⁻²⁰	3.66	5.96 x 10 ⁻⁵	8.71 x 10 ⁻⁷	1.51 x 10 ⁻¹⁸	1.47

Table S3: Vertical flux (q_v^{mf}) during growth of microfractures through compacted intermediate mudstone, simulated by step-wise increase in microfracture width (ξ^{mf}).

Step	Porosity ϕ	Micro-fracture Width ξ^{mf}	Effective Fracture Width ϵ_{eff}^{mf}	Interbed Pore Throat Width λ	Vertical Flux q_v^{mf}	Reynolds Number Vertical flow Re_v	Vertical Permeability k_v^{mf}	Vertical Tortuosity τ_v^{mf}
		(nm)	(nm)	(nm)	(m/s)		(m ²)	
1	0.07	11.42 x10 ⁰	0.00 x10 ⁰	11.42 x10 ⁰	5.54 x 10 ⁻⁶	1.24 x 10 ⁻⁵	1.02 x 10 ⁻²⁰	2.20
2	0.10	57.14 x10 ⁰	1.37 x 10 ²	11.42 x10 ⁰	1.56 x 10 ⁻⁴	3.52 x 10 ⁻⁴	2.89 x 10 ⁻¹⁹	1.11
3	0.13	10.20 x10 ¹	2.74 x 10 ²	11.42 x10 ⁰	1.05 x 10 ⁻³	2.37 x 10 ⁻³	1.95 x 10 ⁻¹⁸	1.02
4	0.18	18.28 x10 ¹	5.14 x 10 ²	11.42 x10 ⁰	7.99 x 10 ⁻³	1.79 x 10 ⁻²	1.48 x 10 ⁻¹⁷	1.00
5	0.25	29.71 x10 ¹	8.57 x 10 ²	11.42 x10 ⁰	4.68 x 10 ⁻²	1.05 x 10 ⁻¹	8.66 x 10 ⁻¹⁷	1.00
6	0.29	37.70 x10 ¹	1.10 x 10 ³	11.42 x10 ⁰	1.12 x 10 ⁻⁴	2.52 x 10 ⁻¹	2.07 x 10 ⁻¹⁶	1.00
7	0.33	46.85 x10 ¹	1.37 x 10 ³	11.42 x10 ⁰	2.47 x 10 ⁻¹	5.56 x 10 ⁻¹	4.57 x 10 ⁻¹⁶	1.00
8	0.41	64.00 x10 ¹	1.89 x 10 ³	11.42 x10 ⁰	7.59 x 10 ⁻¹	1.71 x 10 ⁰	1.40 x 10 ⁻¹⁵	1.00
9	0.49	86.85 x10 ¹	2.57 x 10 ³	11.42 x10 ⁰	2.17 x10 ⁰	4.88 x 10 ⁰	4.01 x 10 ⁻¹⁵	1.00
10	0.57	11.54 x10 ²	3.43 x 10 ³	11.42 x10 ⁰	5.19 x10 ⁰	1.17 x 10 ¹	9.59 x 10 ⁻¹⁵	1.00

Table S4: Vertical flux (q_v^{frac}) during propagation of macrofracture through compacted intermediate mudstone, simulated by step-wise increase in fracture width (ξ^{frac}).

Step	Porosity ϕ	Macro-fracture Width ξ^{frac}	Effective Fracture Width ϵ_{eff}^{frac}	Interbed Pore Throat Width λ	Vertical Flux q_v^{frac}	Reynolds Number Vertical flow Re_v	Vertical Permeability k_v^{frac}	Vertical Tortuosity τ_v^{frac}
		(nm)	(nm)	(nm)	(m/s)		(m ²)	
1	0.07	11.42 x10 ⁰	0.00 x10 ⁰	11.42 x10 ⁰	5.54 x 10 ⁻⁶	1.24 x 10 ⁻⁵	1.02 x 10 ⁻²⁰	2.20
2	0.12	37.71 x 10 ¹	3.66 x 10 ²	11.42 x10 ⁰	9.41 x 10 ⁻⁶	2.11 x 10 ⁻⁵	1.74 x 10 ⁻²⁰	1.77
3	0.17	70.85 x 10 ¹	6.97 x 10 ²	11.42 x10 ⁰	1.17 x 10 ⁻⁵	2.64 x 10 ⁻⁵	2.17 x 10 ⁻²⁰	1.51
4	0.21	11.09 x 10 ²	1.10 x 10 ³	11.42 x10 ⁰	3.83 x 10 ⁻⁴	8.60 x 10 ⁻⁴	7.07 x 10 ⁻¹⁹	1.11
5	0.25	14.74 x 10 ²	1.46 x 10 ³	11.42 x10 ⁰	5.81 x 10 ⁻³	1.31 x 10 ⁻²	1.07 x 10 ⁻¹⁷	1.01
6	0.32	22.06 x 10 ²	2.19 x 10 ³	11.42 x10 ⁰	6.64 x 10 ⁻²	1.49 x 10 ⁻¹	1.22 x 10 ⁻¹⁶	1.00
7	0.36	27.88 x 10 ²	2.78 x 10 ³	11.42 x10 ⁰	3.00x10 ⁰	6.75 x 10 ⁰	5.55 x 10 ⁻¹⁵	1.00
8	0.41	34.40 x 10 ²	3.43 x 10 ³	11.42 x10 ⁰	7.36 x10 ⁰	1.65 x 10 ¹	1.36 x 10 ⁻¹⁴	1.00
9	0.47	45.83 x 10 ²	4.57 x 10 ³	11.42 x10 ⁰	1.36 x 10 ¹	3.06 x 10 ¹	2.52 x 10 ⁻¹⁴	1.00
10	0.55	62.97 x 10 ²	6.29 x 10 ³	11.42 x10 ⁰	2.09 x 10 ¹	4.69 x 10 ¹	3.85 x 10 ⁻¹⁴	1.00