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Buckling and ultimate load prediction models for perforated steel beams using machine learning algorithms

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Abstract

Large web openings introduce complex structural behaviors and additional failure modes of steel cellular beams, which must be considered in the design using laborious calculations (e.g., exercising SCI P355). This paper presents seven machine learning (ML) models, including decision tree (DT), random forest (RF), k-nearest neighbor (KNN), gradient boosting regressor (GBR), extreme gradient boosting (XGBoost), light gradient boosting machine (LightGBM), and gradient boosting with categorical features support (CatBoost), for predicting the elastic buckling and ultimate loads of steel cellular beams. Large datasets of finite element (FE) simulation results, validated against experimental data, were used to develop the models. The ML models were fine-tuned via an extensive hyperparameter search to obtain their best performance. The elastic buckling and ultimate loads predicted by the optimized ML models demonstrated excellent agreement with the numerical data. The accuracy of the ultimate load predictions by the ML models exceeded the accuracy provided by the existing design provisions for steel cellular beams published in SCI P355 and AISC De-

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sign Guide 31. The relative feature importance and feature dependence of the models were evaluated and discussed in the paper. An interactive Python-based notebook and a user-friendly web application for predicting the elastic buckling and ultimate loads of steel cellular beams using the developed optimized ML models were created and made publicly available. The web application deployed to the cloud allows for making predictions in any web browser on any device, including mobile. The source code of the application available on GitHub allows running the application locally and independently from the cloud service.

Keywords: Cellular beams, Perforated web, Elastic buckling, Ultimate strength, Predictive models, Machine learning

1. Introduction

Perforated steel beams with repeating web openings have been used in construction for more than a century [1]. They offer several advantages over steel beams with solid webs, including weight reduction, higher strength-to-weight ratio, integration of utilities, and improved aesthetics. Castellated beams with hexagonal openings, which were the first type of beams with perforated web sections, have practically been replaced in modern construction by cellular beams with circular openings [2]. Multiple large openings cause a significant reduction in the beam shear strength and introduce additional possible failure modes of the beams, which makes the flexural behavior and design of cellular beams complicated. A cellular beam may exhibit one of the following failure modes: global bending, lateral-torsional buckling, vertical shear, local Vierendeel bending, web post horizontal shear, web post bending, web post buckling, and shear buckling. Many researchers have contributed to the body of knowledge about the strength and structural behavior of steel cellular beams. Several research publications describe numerical studies on the lateral-torsional buckling of cellular beams [3–8], which allowed for determining the effects of different design

parameters on the beam strength governed by the elastic and inelastic lateral-torsional buckling. It was found in particular that the cellular beam geometry affected the moment-gradient coefficient, which is not the case for the solid-web beams [4]. T-shaped stiffeners were proposed to improve the flexural stiffness of cellular beams and reduce the lateral-torsional buckling occurrence [5]. Modified calculations of the cross-sectional properties and a modified buckling curve selection were developed based on the existing European guidelines [6].

Web post buckling of cellular beams and beams with web openings of different shapes was studied in [9–11]. Tsavdaridis and D’Mello [9] demonstrated that particular non-standard opening shapes improved the beam structural performance compared with the beams with standard circular, hexagonal, and elongated web openings. They also proposed an empirical formula for predicting the ultimate vertical shear strength of web posts formed by the different opening shapes. Panedpojaman et al. [10] proposed design equations for predicting the shear strength of local web post buckling in symmetric and asymmetric cellular beams, which demonstrated improved accuracy in predicting the shear strength compared with BS EN 1993-1-1 [12] and AISC 360 [13].

Chung et al. [14] investigated the Vierendeel mechanism in cellular steel beams and found that shear yielding is more critical in steel beams with circular openings than in beams with rectangular openings. They proposed an empirical shear moment interaction curve at the perforated sections. Kang et al. [15] studied the shear behavior and strength of cellular beams and proposed a rational design model for predicting the beam shear strength, which showed a good agreement with the numerical and experimental results. Ellobody [16] investigated combined buckling modes of steel cellular beams and found that the failure load could be significantly reduced when the beams failed in combined web distortional and web post-buckling.

45 Several research papers have been dedicated to the optimal design of cellular
46 beams [9, 17–24]. The studies demonstrated that the strength and weight of
47 the beams with web openings could be significantly improved by using non-
48 standard opening shapes [9, 17, 19, 21], applying special optimization techniques
49 [18, 20, 22], and selecting specific sizes and spacing of web openings [21, 23, 24].

50 Akrami and Erfani [25] assessed design methodologies for perforated steel
51 beams presented in ASCE 23-97 [26], SCI P100 [27], SCI P355 [2], Chung et
52 al. [28], and Tsavdaridis and D’Mello [17]. The two latter methods were found
53 least restrictive and produced the lowest errors. The authors proposed ASCE
54 23-97 modifications, which showed a good agreement with experimental and
55 numerical data.

56 The presented literature review shows that the published research concen-
57 trated mainly on studying specific failure modes of cellular beams. To fill the
58 gap in the information about the global response of such members, Rajana et al.
59 [29] performed an extensive numerical parametric study of the elastic and inelas-
60 tic buckling of cellular beams subjected to strong axis bending. The effects of
61 various parameters on the elastic buckling and ultimate loads of cellular beams
62 were investigated, and an extensive database of the FE simulation results was
63 generated. The study showed that the elastic buckling was affected mainly by
64 the web thickness and the flange geometry. The diameter of web openings, their
65 spacing, flange geometry, and web thickness were the most critical parameters
66 affecting the beam strength. It was also determined that the initial geometric
67 imperfections had an insignificant effect on the predicted beam strength.

68 Artificial intelligence (AI) and machine learning (ML) are emerging fields
69 of computer science that allow for developing machines with simulated human
70 intelligence and creating data-based descriptive models capable of handling very
71 complex problems efficiently. A properly developed ML model for engineering

72 applications reveals hidden relations between the predicted variable and input
73 parameters based on the underlying physics. Many industries have successfully
74 adopted AI and ML [30–33], whereas their deployment in structural engineering
75 is still somewhat limited despite many research publications demonstrating the
76 accuracy and effectiveness of the AI and ML methods.

77 The number of research publications on ML applications in civil and struc-
78 tural engineering had increased exponentially since the second half of the 1980s,
79 when the first papers on this topic were published [34–40]. Many publica-
80 tions described ML models considered in this study for predicting properties
81 of concrete and reinforced concrete structures [41–66]. Fewer papers have been
82 published on ML applications to steel structures, including buckling analysis of
83 beam-columns [67], cold-formed steel (CFS) space structure optimization [68],
84 web crippling strength prediction [69], elastic distortional buckling stress de-
85 termination [70, 71], rotation capacity prediction [72], strength prediction of
86 concrete-filled steel tubular columns [73], failure mode identification of column
87 base plate connection [74], capacity prediction of cold-formed stainless steel
88 tubular columns [75], seismic drift demand estimation for steel moment frame
89 buildings [76], and shear strength of CFS channels with staggered perforated
90 webs [77–80]. ML techniques were previously applied to steel cellular beams.
91 Sharifi et al. [81] developed an artificial neural network (ANN) to predict the
92 flexural strength of steel cellular beams governed by lateral-torsional buckling
93 using a relatively small dataset with 99 samples. The predicting abilities of
94 the developed ANN were superior to those by the Australian Standard [82].
95 Abambres et al. [83] developed an ANN model and an ANN-based formula for
96 predicting the elastic buckling load of cellular beams using a large dataset of
97 numerical results described in [29]. The ANN and the proposed formula showed
98 an excellent agreement with the FE simulation results. An ANN and ANN-

99 based formula for predicting the lateral-torsional buckling resistance of slender
100 steel cellular beams were presented by Ferreira et al. [84]. Limbachiya and
101 Shamass [85] presented an ANN and ANN-based formula for predicting web-
102 post buckling shear strength of cellular beams, which demonstrated a higher
103 level accuracy compared with the existing design provisions.

104 The presented review indicates that ML has excellent potential for developing
105 structural engineering expert tools. ML models cannot currently be solely
106 used for final designs because building codes do not permit them. However,
107 they can be employed in the preliminary design stages to quickly evaluate and
108 select options that may work and consider them in the detailed analysis and
109 design per building codes. Due to the superior performance of ML models com-
110 pared with conventional models demonstrated on many engineering problems,
111 the question of what should be done to adopt them in building codes will need
112 to be eventually answered. ML models are based on solid mathematical algo-
113 rithms, well-described in the literature. The novelty of the algorithms, which
114 structural engineers do not fully understand, is one of the significant barriers
115 today to their adoption, which will eventually change with more education,
116 research, and experience.

117 ML models built on top of the available test or numerical data are compu-
118 tationally efficient and often more accurate than the existing design methods
119 based on the traditional approaches, which often rely on fewer data points and
120 engineering intuition. They can replace computationally intensive finite element
121 simulations when the design parameters are within the ranges of the data used
122 for the ML model training. It should also be noted that accurate finite element
123 simulations require advanced software resources, which are not always available
124 to designers, and advanced techniques, thus skills and knowledge. Even when
125 the appropriate software is available, and the designers possess the required ex-

126 pertise, it is impractical to perform advanced finite element simulations during
127 the project design phase due to time constraints. Because of that, engineers are
128 often using simplified FEA to perform stress analyses. The downside is that
129 these are not very accurate due to the number of assumptions, leading to the
130 very same initial problem: the need of higher safety factors and the excessive
131 use of material where it is not needed.

132 This study aims to explore various ML algorithms for predicting the elastic
133 buckling and ultimate loads of steel cellular beams. Considering the complexity
134 of the structural behavior and design of such members, ML models are deemed to
135 be a promising alternative to the existing design guidelines and computationally
136 expensive FE modeling. The objectives of the study were as follows:

- 137 1. Develop and optimize ML models for predicting the elastic buckling and ul-
138 timate loads of steel cellular beams based on seven popular ML regressors,
139 including decision tree (DT), random forest (RF), k-nearest neighbors
140 (KNN), gradient boosting regressor (GBR), extreme gradient boosting
141 (XGBoost), light gradient boosting machine (LightGBM), and gradient
142 boosting with categorical features support (CatBoost).
- 143 2. Interpret and explain the developed models using the permutations and
144 SHapley Additive exPlanations (SHAP) [86] methods.
- 145 3. Compare predictions by the developed ML models with those per SCI
146 P355 [2] and AISC Design Guide 31 [87].

147 ML models were trained using FE simulation results of steel cellular beams
148 published in [29]. The elastic buckling load dataset included 3645 samples. The
149 ultimate load (inelastic buckling load) dataset consisted of 78390 samples. All
150 models were implemented in open-source Python-based frameworks, and their
151 hyperparameters were optimized via an extensive tuning process. The ten-fold
152 cross-validation method was employed for the model training and performance

153 evaluation. The final evaluation of the models was performed on the data unseen
154 by the models during training. The ML model predictions showed an excellent
155 agreement with the FE simulation results. The ultimate loads of the cellular
156 beams predicted by the models compared with the FE analysis data considerably
157 better than the ultimate loads predicted by SCI P355 [2] and AISC Design Guide
158 31 [87]. The developed ML models allow for computing the elastic buckling
159 and ultimate loads of cellular beams with a wide range of variables, including
160 intermediate values of variables not considered in numerical studies used for the
161 model training.

162 A web application for predicting the elastic buckling and ultimate loads of
163 steel cellular beams was created in Streamlit. A light version of the application
164 was deployed to the cloud at <https://scba-cb.herokuapp.com/>. It allows for
165 making predictions in any web browser on any device, including mobile. The
166 source codes of the full and lite application versions are available on GitHub
167 at <https://github.com/vitdegyarev/SCBA-Streamlit> and <https://github.com/vitdegyarev/SCBA-Streamlit-CB>, respectively. They allow for
168 running the application on a local machine. The scientific research part of this
169 study consists of creating and optimizing ML models for predicting the behavior
170 of cellular beams, while the web application is a convenient tool for obtaining
171 predictions by the developed models.

172 The novelty of the presented work consists of the development of new opti-
173 mized ML models for accurate and computationally efficient predictions of the
174 elastic buckling and ultimate loads of steel cellular beams, interpretation and ex-
175 planation of the developed models using the permutations and SHAP methods,
176 comparison of the performance of seven different ML models, and development
177 of a web application based on the optimized ML models for the ease of use by
178 engineers in practice.

180 **2. Datasets**

181 The elastic buckling load, w_{cr} , and ultimate load (inelastic buckling load),
 182 w_{max} , datasets of FE simulation results from [29] were used for training and per-
 183 formance evaluation of the ML models. The FE models were validated against
 184 the experimental data, as described in [29]. The w_{cr} and w_{max} datasets consist
 185 of 3645 and 78390 samples, respectively. Fig. 1 shows dimensional parameters
 186 of the cellular beams considered in the numerical parametric study, including
 187 beam span length, L ; beam height, H ; flange width, b_f ; flange thickness, t_f ;
 188 web thickness, t_w ; opening diameter, D_o ; web post width, WP ; and opening
 189 end distance, L_{ed} .

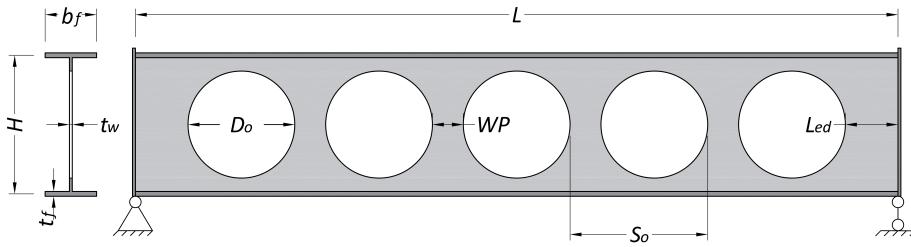


Figure 1: Dimensional parameters of steel cellular beams

190 In addition to the dimensional parameters of the beams, the ultimate load
 191 dataset included steel yield stress, F_y ; steel ultimate stress, F_u ; steel yield strain,
 192 ϵ_y ; steel ultimate strain, ϵ_u ; and initial geometric imperfections considered in
 193 the FE models. The dimensional beam characteristics shown in Fig. 1 and F_y
 194 (in the w_{max} models only) were considered the ML models' input parameters.
 195 The initial geometric imperfections were excluded from the input parameters
 196 because they have an insignificant effect on w_{max} [29], and their exact shape
 197 and magnitude are not usually known to the designer.

198 Distributions of the parameters in the elastic buckling and ultimate load
 199 datasets presented in Figs. 2 and 3 demonstrate that the datasets cover a wide

range of the beams and represent the steel cellular beams used in construction.

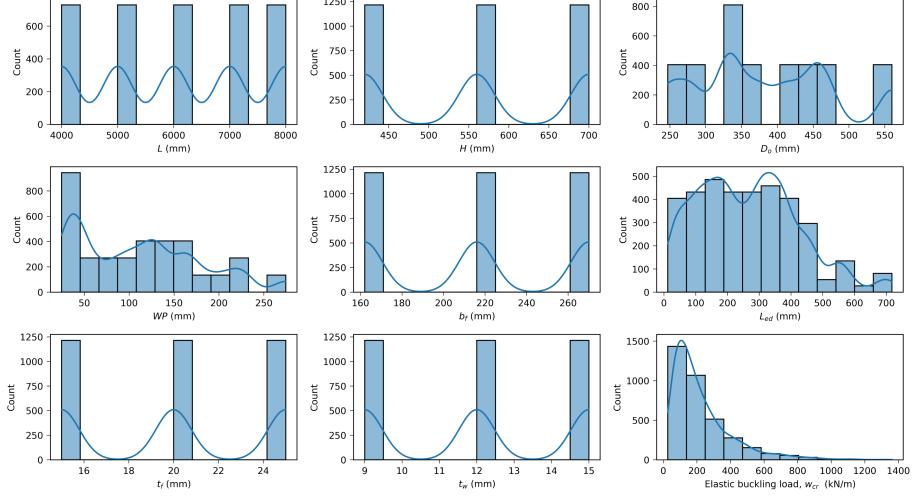


Figure 2: Distributions of variables of the elastic buckling load dataset

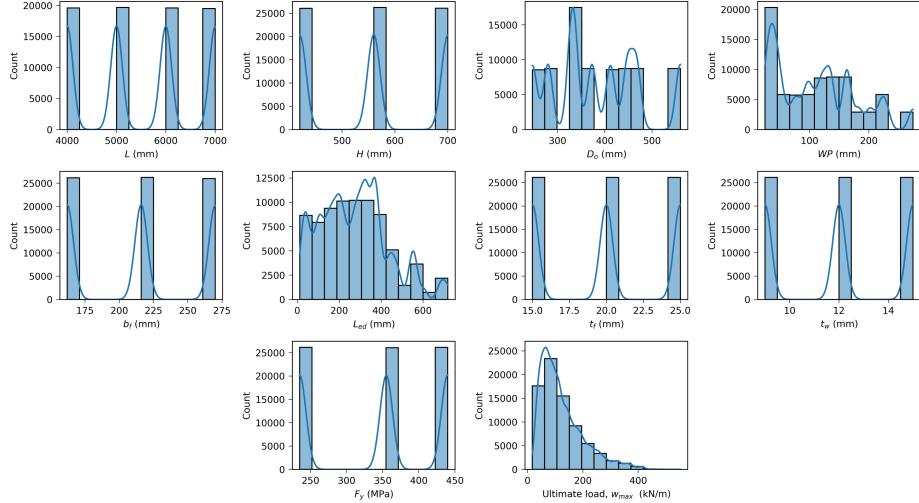


Figure 3: Distributions of variables of the ultimate load dataset

Fig. 4 and 5 show correlation matrices for the dataset variables. The beam span length, L , has the highest negative correlation with w_{cr} and w_{max} , characterized by moderate coefficients of correlation of -0.67 and -0.60, respectively.

204 All other variables have weak correlations with w_{cr} and w_{max} , with coefficients
 205 of correlation not exceeding 0.37. It is interesting to note that w_{max} has a con-
 206 siderably stronger correlation with WP than w_{cr} , which indirectly highlights
 207 the positive contribution of the web post plastic behavior to the ultimate load
 208 of the cellular beams. D_o has a strong positive correlation with H because the
 209 D_o values were set as fractions of the H values in the numerical parametric
 210 study. All other dataset variables have weak correlations between themselves.

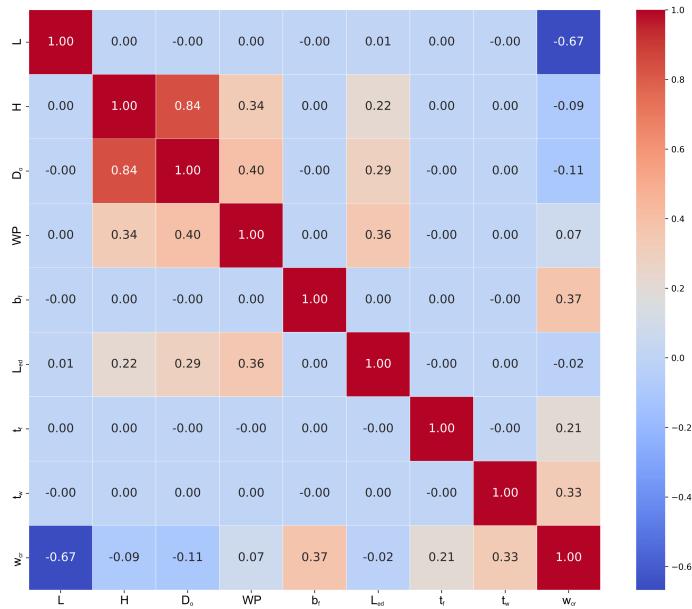


Figure 4: Correlation matrix for the elastic buckling load dataset

211 The datasets used in this study can be found at the following link: <https://www.kaggle.com/vitdegyarev/buckling-and-ultimate-loads-of-cellular-beams>.
 212
 213

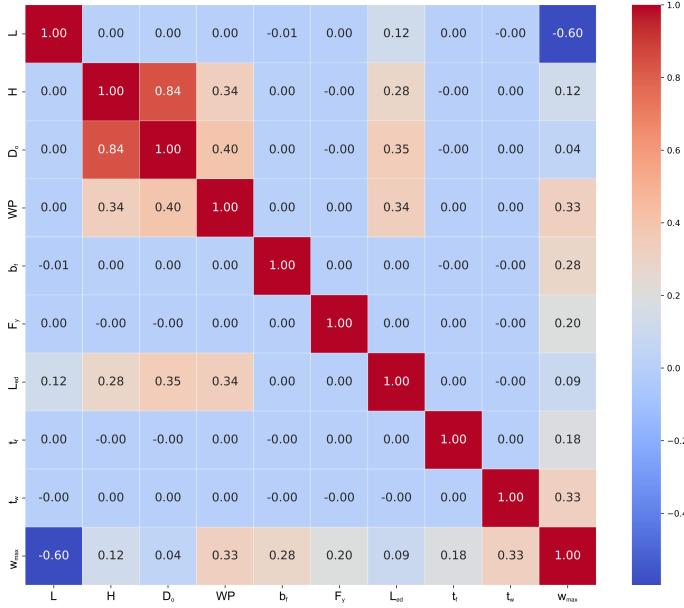


Figure 5: Correlation matrix for the ultimate load dataset

214 3. Review of machine learning algorithms

215 The abilities of seven popular supervised ML algorithms to predict the elas-
 216 tic buckling load, w_{cr} , and ultimate load, w_{max} , of steel cellular beams were
 217 evaluated. Supervised ML algorithms learn by example using labeled train-
 218 ing data, which consist of input parameters (also known as features) and one
 219 or more output values (also known as targets). The evaluated ML algorithms
 220 included decision tree (DT), random forest (RF), k-nearest neighbors (KNN),
 221 gradient boosting regressor (GBR), extreme gradient boosting (XGBoost), light
 222 gradient boosting machine (LightGBM), and gradient boosting with categorical
 223 features support (CatBoost). These algorithms are commonly employed to de-
 224 velop predictive ML models in civil/structural engineering (as was discussed in
 225 the Introduction section) and other domains. They are based on different prin-
 226 ciples and may result in different performances when used for different problems.
 227 One algorithm may demonstrate a better predictive accuracy than others on

228 one problem and inferior performance on a different problem. Therefore, it is
 229 important to find an algorithm and its optimal hyperparameters that works the
 230 best for a given problem.

231 Fig. 6 demonstrates the schematic architecture of the considered ML models
 232 for predicting w_{cr} and w_{max} . The models consisted of features, ML algorithms,
 233 and targets. The features of the models for predicting w_{cr} were L , H , b_f , t_f ,
 234 t_w , D_o , WP , and L_{ed} . The w_{max} models also included F_y as a feature.

235 All ML algorithms have hyperparameters, or the parameters specified before
 236 the model training to control the learning process and avoid overfitting or un-
 237 derfitting. Overfitting is characterized by the ability of a model to make good
 238 predictions for the samples used in training while making poor predictions on
 239 the new samples of data unseen by the model before. An underfitted model
 240 produces poor predictions on the seen and unseen data. The ability of an ML
 241 model to make good predictions for previously unseen data is referred to as gen-
 242 eralization. Finding optimal hyperparameters is essential for obtaining a model
 243 with the best performance and generalization [54, 77]. It is equivalent to finding
 244 the form and coefficients of a regression equation that gives the best prediction
 245 accuracy for a given problem.

246 The following sections present a brief overview of each ML algorithm con-
 247 sidered in the study. Detailed information about the ML algorithms and their
 248 practical implementation can be found in published literature, including [88]
 249 and [89].

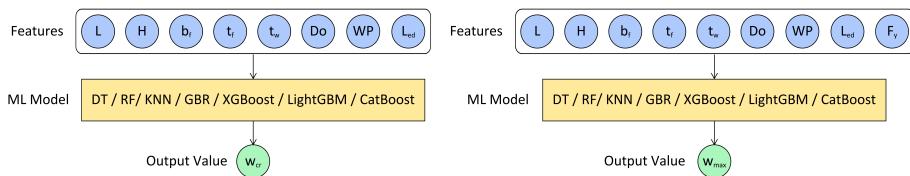


Figure 6: Architecture of ML models

250 3.1. Decision tree

251 The DT algorithm bears its name from its tree structure incrementally de-
252 veloped by splitting the dataset into smaller subsets. DT models have three
253 types of nodes: root node, decision nodes, and terminal nodes (also known as
254 leaves). The learning starts at the root node, which includes all training data.
255 The root node splits into two or more decision nodes, which include subsets of
256 the original training data. The splitting occurs based on a series of questions
257 determined by the algorithm. It continues for the subsequent levels until a pre-
258 defined maximum depth of the tree is reached or when the nodes have only one
259 sample of the training data. The algorithm stops at the terminal nodes, which
260 do not split.

Various algorithms for growing a DT exist. They differ by the possible tree structure, the split finding criteria, the splitting stoppage criteria, and the model estimation within the terminal nodes. The classification and regression trees (CART) algorithm [88] was used in this study. In this algorithm, a dataset (x_i, y_i) for $i = 1, 2, \dots, N$, with $x_i = (x_{i1}, x_{i2}, \dots, x_{ip})$ is considered, where x_i and y_i are features and targets, N is the number of samples, and p is the number of features. The original dataset is split into M regions R_1, R_2, \dots, R_M . The model prediction in each region is a constant c_m described by Eq. 1.

$$f(x) = \sum_{m=1}^M c_m I(x \in R_m) \quad (1)$$

261 where $I(x \in R_m)$ is the identity function that returns 1 if x is in the subset R_m
262 and 0 otherwise.

The best \hat{c}_m is the average of y_i in region R_m when the sum of squared errors $\sum(y_i - f(x_i))^2$ is used as the criterion of minimization:

$$\hat{c}_m = \text{ave}(y_i \mid x_i \in R_m) \quad (2)$$

263 The following greedy algorithm is employed to find the best binary partition
264 of each node in terms of the minimum sum of squared errors. The pair of
265 half-planes partitioned by a splitting variable j and a split point s is defined as
266 follows.

$$R_1(j, s) = \{X \mid X_j \leq s\} \text{ and } R_2(j, s) = \{X \mid X_j > s\} \quad (3)$$

267 The splitting variable j and the split point s that solve Eq. (4) are sought.

$$\min_{j,s} \left[\min_{c_1} \sum_{x_i \in R_1(j,s)} (y_i - c_1)^2 + \min_{c_2} \sum_{x_i \in R_2(j,s)} (y_i - c_2)^2 \right] \quad (4)$$

268 The inner minimization is solved by

$$\hat{c}_1 = \text{ave}(y_i \mid x_i \in R_1(j,s)) \text{ and } \hat{c}_2 = \text{ave}(y_i \mid x_i \in R_2(j,s)) \quad (5)$$

269 Once the best split is found, the dataset is partitioned into two resulting
270 subsets, after which the splitting process is repeated for each subset and each
271 node in the subsequent levels.

272 The DT advantages consist of the relative ease of data preparation, the ease
273 of understanding and interpretation, and robustness against missing values. One
274 of the main disadvantages of DT is their proneness to overfitting when the tree
275 is very large [90, 91]. To avoid overfitting, the DT model should not be very
276 large. At the same time, the model should be large enough to capture the
277 important relationships between the features and targets to avoid underfitting.
278 DT hyperparameters include the maximum depth of the tree, the minimum
279 number of samples required to split an internal node, the minimum number of
280 samples required to be at a leaf node, and others.

281 3.2. Random forest

282 RF is an ensemble of DTs generally trained via *bagging*, which stands for
283 *bootstrap aggregating* [88]. In this method, the same algorithm (DT) is trained
284 many times on different random subsets of the entire training set. The sampling
285 is performed with replacement, meaning that the same sample may appear
286 in different subsets. Predictions from multiple randomly generated DTs are
287 averaged to obtain the final output value of the RF algorithm.

288 The RF regression algorithm consists of the following steps [88].

289 1. For $b=1$ to B , where b is an individual DT and B is the total number of
290 DTs (estimators):

- 291 (a) A bootstrap sample of size N is drawn from the training data.
292 (b) A tree T_b is grown to the bootstrapped data by repeating the fol-
293 lowing substeps for each node until the maximum tree depth or the
294 minimum node size is reached:
295 i. m variables are randomly selected from p variables.
296 ii. The best variable among m and the best split point is found.
297 iii. The node is split into two nodes.

298 2. The ensemble of trees $\{T_b\}_1^B$ is output.

299 3. The final prediction is made as $\hat{f}_{RF}^B(x) = \frac{1}{B} \sum_{b=1}^B T_b(x)$.

300 The RF advantages include those listed in Subsection 3.1 for DT and its
301 robustness against overfitting due to the presence of multiple independent DTs
302 making predictions. On the negative side, RF requires more computational
303 power and resources to build numerous trees and combine their outputs com-
304 pared with DT. The RF hyperparameters include those for DTs plus the number
305 of trees in the forest.

306 3.3. *K*-nearest neighbors

307 The KNN regression algorithm predicts the output value by interpolating
308 the output values of k nearest neighbors in the training set. The number of
309 neighbors k is a hyperparameter set before training. The distance between the
310 neighbors is defined by the distance function in the form of the Minkowski metric
311 described by Eq. (6). The Euclidean and Manhattan distances, which are other
312 typical distance metrics, can be obtained from the Minkowski metric by setting
313 the power parameter, p , equal to 1 and 2, respectively.

$$D(X, Y) = \left(\sum_{i=1}^k |x_i - y_i|^p \right)^{\frac{1}{p}} \quad (6)$$

The output values are obtained by taking either an average (Eq.(7)) or an inverse distance weighted average (Eq.(8)) of the k nearest neighbors with similar features. In the latter approach, closer neighbors have a more significant influence on the target than the more distant neighbors.

$$\hat{f}(x) = \frac{1}{k} \sum_{x_i \in N_k(x)} y_i \quad (7)$$

$$\hat{f}(x) = \frac{\sum_{x_i \in N_k(x)} \frac{1}{d_i} y_i}{\sum_{x_i \in N_k(x)} \frac{1}{d_i}} \quad (8)$$

314 where $N_k(x)$ is the neighborhood of x defined by the k closest points x_i in the
315 training data, d_i is the distance from the i^{th} point to the estimated point.

316 The KNN advantages include the ease of implementation, the ability to
317 add new data without the effect on the algorithm's accuracy, and the training
318 period absence, which makes the KNN algorithm significantly faster than other
319 ML algorithms when the dataset size and the number of input variables are
320 relatively small. The KNN disadvantages consist of sensitivity to noisy data,
321 missing values and outliers, and slow predictions for large datasets and datasets

322 with a large number of features. The KNN hyperparameters are the number of
323 neighbors, the weight function (uniform or inverse distance weighted), and the
324 distance metric.

325 *3.4. Gradient boosting*

326 Boosting algorithms, or boosting machines, are ensemble methods that com-
327 bine several weak learners (usually DTs) to produce a strong learner. Boosting
328 machine predictors are trained sequentially, with each subsequent learner im-
329 proving the predecessor's predictions. The algorithm stops when a predefined
330 number of predictors is reached or when the perfect fit is achieved. The two
331 common boosting algorithms are gradient boosting and adaptive boosting.

332 In gradient boosting, the boosting algorithm is combined with gradient de-
333 scent, which is an iterative optimization algorithm for finding a local minimum
334 of a function. New predictors are fitted to the residual errors from the previous
335 predictors. The gradient boosting algorithm includes the following steps [92]:

- 336 1. For a training set $(x_i, y_i)_{i=1}^n$, the model is initialized with a constant value
337 of

$$F_0(x) = \underset{\gamma}{\operatorname{argmin}} \sum_{i=1}^n L(y_i, \gamma) \quad (9)$$

338 where i and n denote the i^{th} sample and the total number of samples

- 339 2. For $m=1$ to M , where m and M are the m^{th} iteration and the total number
340 of iterations:

- 341 (a) Pseudo-residuals are computed as follows:

$$r_{im} = - \left[\frac{\partial L(y_i, F(x_i))}{\partial F(x_i)} \right]_{F(x)=F_{m-1}(x)} \quad (10)$$

- 342 (b) The training set $(x_i, r_{im})_{i=1}^n$ is used to fit a predictor $h_m(x)$ to
343 pseudo-residuals.

344 (c) Multiplier γ_m is computed by solving the following optimization prob-
345 lem:

$$\gamma_m = \operatorname{argmin}_{\gamma} \sum_{i=1}^n L[y_i, F_{m-1}(x_i) + \gamma h_m(x_i)] \quad (11)$$

346 (d) The model is updated using the following equation:

$$F_m(x) = F_{m-1}(x) + \gamma_m h_m(x) \quad (12)$$

347 3. $F_M(x)$ is obtained.

348 The gradient boosting algorithm's advantages include high accuracy, flexi-
349 bility, and the ability to handle missing data. It is generally considered resistant
350 to overfitting due to many weak learners involved in the prediction. However,
351 the algorithm may overfit when its hyperparameters are poorly selected. The
352 disadvantages of gradient boosting are computation cost, the number of hyper-
353 parameters that require proper tuning, and limited interpretability.

354 The gradient boosting hyperparameters include learning rate, the number of
355 boosting iterations, maximum depth of the individual regression estimators, the
356 minimum number of samples required to split an internal node, the minimum
357 number of samples required to be at a leaf node, and others.

358 The gradient boosting algorithms have been implemented in several frame-
359 works: GBR [93], XGBoost [94], LightGBM [95], and CatBoost [96]. XGBoost,
360 LightGBM, and CatBoost are improved implementations of GBR. XGBoost was
361 optimized for more accurate and faster predictions via regularization, custom
362 loss functions, parallel processing, and other algorithm improvements. Light-
363 GBM offers improved training speed, higher efficiency, better accuracy, lower
364 memory use, and the ability to process large datasets by applying the Gradient-
365 based One-Side Sampling (GOSS) method and parallel learning. CatBoost can

366 process categorical features to improve accuracy for datasets with categorical
367 features, ordered boosting to fight overfitting, missing value support, and others.

368 **4. Implementation and results**

369 The ML algorithms were implemented in the following Python-based open-
370 source libraries: *scikit-learn* (DT, RF, KNN, and GBR) [93], *XGBoost* [94],
371 *LightGBM* [95], and *CatBoost* [96]. The models were optimized, validated, and
372 tested using the ten-fold cross-validation method. The w_{cr} and w_{max} datasets
373 were randomly divided into training and test sets in the 80/20 proportion. The
374 training set of each dataset was partitioned into ten groups. The models were
375 trained on nine groups of the training set and validated on the remaining group.
376 The process was repeated for the remaining groups of the training set until each
377 group had served as the validation set. The final performance of the models was
378 evaluated on the test data unseen by the models in training. Compared with the
379 hold-out method, where the dataset is divided into training, validation, and test
380 sets, with each set used for its purpose only, the ten-fold cross-validation method
381 makes more samples available for model training and excludes model dependence
382 on a particular random choice of the samples selected for the training, validation,
383 and test sets. As a result, the ten-fold cross-validation method usually produces
384 more accurate models with better generalization performance.

385 Figs. 2 and 3 demonstrate that the numerical ranges of the features ranged
widely in the datasets, which is not ideal for ML models, as it might cause
difficulties for the algorithms in finding optimal model parameters. Each feature
value in the training set was standardized using Eq. (13) to make the features'
scales uniform. Each feature in the test set was also standardized using the
mean and standard deviation values of the feature obtained for the training set.

$$x' = \frac{x - \mu}{\sigma} \quad (13)$$

385 where x' is the standardized value of the input parameter, x is the original
 386 (non-standardized) value of the input parameter, μ is the mean of the original
 387 values of the input parameter, and σ is the standard deviation of the original
 388 values of the input parameter.

Performance of the ML learning models was evaluated based on the mean squared error (MSE) values obtained for the test set calculated as follows.

$$MSE = \frac{1}{n} \sum_{i=1}^n (y - \hat{y})^2 \quad (14)$$

389 where n is the number of samples, y is the output value, and \hat{y} is the predicted
 390 output value.

Mean absolute error (MAE), mean absolute percentage error (MAPE), the coefficient of determination (R^2), the minimum, maximum, mean, and coefficient of variation values of the prediction-to-FEA ratios, which are metrics commonly used for performance evaluation of ML models [97], calculated using the following equations were also determined for the training and test sets.

$$MAE = \frac{1}{n} \sum_{i=1}^n |y - \hat{y}| \quad (15)$$

$$MAPE = \frac{100}{n} \sum_{i=1}^n \left| \frac{y - \hat{y}}{y} \right| \quad (16)$$

$$R^2 = 1 - \frac{\sum_{i=1}^n (y - \hat{y})^2}{\sum_{i=1}^n (y - \bar{y})^2} \quad (17)$$

391 where \bar{y} is the mean of the y values.

392 Extensive hyperparameter tuning was carried out for each ML model using
 393 the grid and random searches to find optimal hyperparameter values that
 394 give the best model performance. The obtained optimal hyperparameters for

395 each ML model are listed below. The hyperparameter designations used in the
396 Python libraries [93–96] are shown in parentheses. The hyperparameters not
397 presented below had default values.

398 • DT:

- 399 – the maximum depth of the tree (`max_depth`): None for w_{cr} and w_{max} ,
400 – the minimum number of samples required to split an internal node
401 (`min_samples_split`): 4 for w_{cr} and 2 for w_{max} ,
402 – the minimum number of samples at a leaf node (`min_samples_leaf`):
403 2 for w_{cr} and w_{max} .

404 • RF:

- 405 – the number of trees in the forest (`n_estimators`): 80 for w_{cr} and 200
406 for w_{max} ,
407 – the maximum depth of the tree (`max_depth`): None for w_{cr} and w_{max} ,
408 – the minimum number of samples required to split an internal node
409 (`min_samples_split`): 2 for w_{cr} and w_{max} ,
410 – the minimum number of samples at a leaf node (`min_samples_leaf`):
411 1 for w_{cr} and w_{max} .

412 • KNN

- 413 – the number of neighbors (`n_neighbors`): 5 for w_{cr} and 4 for w_{max} ,
414 – weight function (`weights`): uniform for w_{cr} and w_{max} ,
415 – the power parameter for the Minkowski metric (`p`): 1 for w_{cr} and
416 w_{max} ,
417 – leaf size (`leaf_size`): 20 for w_{cr} and 30 for w_{max} .

418 • GBR:

- 419 – learning rate (`learning_rate`): 0.1 for w_{cr} and w_{max} ,
- 420 – the number of boosting stages (`n_estimators`): 200 for w_{cr} and 1300
421 for w_{max} ,
- 422 – maximum depth of individual regression estimators (`max_depth`): 5
423 for w_{cr} and 9 for w_{max} ,
- 424 – the minimum number of samples required to split an internal node
425 (`min_samples_split`): 2 for w_{cr} and w_{max} ,
- 426 – the minimum number of samples at a leaf node (`min_samples_leaf`):
427 3 for w_{cr} and 4 for w_{max} .

428 ● XGBoost:

- 429 – learning rate (`eta`): 0.2 for w_{cr} and w_{max} ,
- 430 – minimum loss reduction required to make a further partition on a
431 leaf node of the tree (`gamma`): 1 for w_{cr} and w_{max} ,
- 432 – the maximum tree depth of base learners (`max_depth`): 5 for w_{cr} and
433 12 for w_{max} ,
- 434 – the minimum sum of instance weight (`hessian`) needed in a child
435 (`min_child_weight`): 3 for w_{cr} and 6 for w_{max} .

436 ● LightGBM:

- 437 – learning rate (`learning_rate`): 0.1 for w_{cr} and w_{max} ,
- 438 – the number of boosting iterations (`num_iterations`): 100 for w_{cr} and
439 3800 for w_{max} ,
- 440 – maximum tree leaves for base learners (`num_leaves`): 50 for w_{cr} and
441 w_{max} ,
- 442 – the minimum number of observations that must fall into a tree node
443 for it to be added (`min_data_in_leaf`): 10 for w_{cr} and w_{max} ,

- 444 – maximum tree depth for base learners (`max_depth`): -1 (None) for
 445 w_{cr} and w_{max} ,
 446 – the maximum number of bins (`max_bin`): 100 for w_{cr} and w_{max} .

447 • CatBoost

- 448 – learning rate (`learning_rate`): 0.03 for w_{cr} and w_{max} ,
 449 – the number of iterations (`iterations`): 850 for w_{cr} and 4000 for
 450 w_{max} ,
 451 – tree depth (`depth`): 6 for w_{cr} and 11 for w_{max} ,
 452 – L2 regularization term coefficient of the cost function (`l2_leaf_reg`):
 453 3 for w_{cr} and 1 for w_{max} ,
 454 – the amount of randomness to use for scoring splits when the tree
 455 structure is selected (`random_strength`): 1 for w_{cr} and 2 for w_{max} .

456 Figs. 7 and 8 show the performance of the developed ML models with the op-
 457 timal hyperparameters for predicting w_{cr} and w_{max} , respectively. The compar-
 458 isons of the ML model predictions with FE simulation results are demonstrated
 459 for the training and test datasets in each figure. The values of R^2 , minimum,
 460 maximum, mean, and coefficient of variation of the prediction-to-FEA ratios
 461 are presented in Figs. 7 and 8. The MSE, MAE, and MAPE values are given in
 462 Tables 1 and 2.

Table 1: Performance metrics of ML models for predicting elastic buckling loads of steel cellular beams, w_{cr} (Train/Test)

Model	MSE ((kN/m) ²)	MAE (kN/m)	MAPE (%)
DT	155.94/1538.26	6.04/19.07	2.35/7.05
RF	83.79/682.24	4.44/13.00	1.83/5.27
KNN	1320.87/2617.14	21.09/28.99	10.22/12.66
GBR	39.68/319.27	3.85/7.66	1.99/3.24
XGBoost	48.44/294.91	4.51/8.59	2.51/3.95
LightGBM	41.88/366.81	3.57/7.56	1.82/3.06
CatBoost	33.90/295.43	3.16/6.15	1.52/2.48

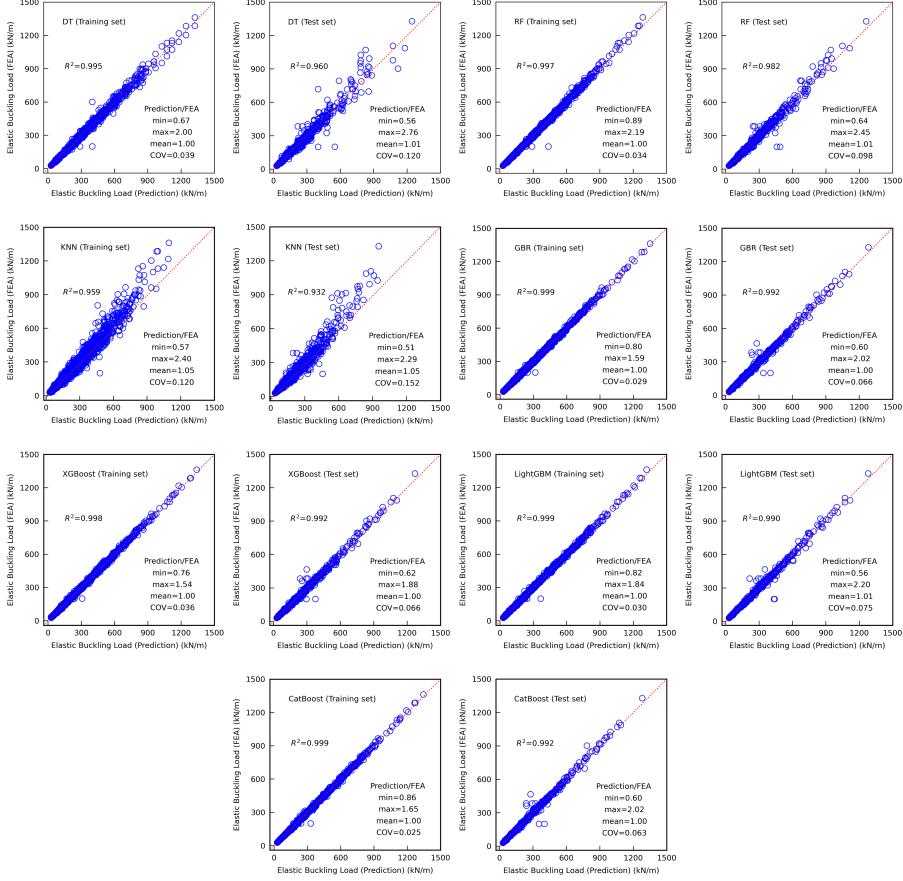


Figure 7: Performance of ML models for predicting elastic buckling load of steel cellular beams

Table 2: Performance metrics of ML models for predicting ultimate loads of steel cellular beams, w_{max} (Train/Test)

Model	MSE ((kN/m) ²)	MAE (kN/m)	MAPE (%)
DT	15.99/20.25	2.08/2.37	1.90/2.18
RF	16.01/20.17	2.08/2.38	1.90/2.18
KNN	18.43/22.61	2.18/2.49	1.99/2.27
GBR	16.01/20.24	2.08/2.38	1.90/2.18
XGBoost	16.03/20.13	2.09/2.39	1.92/2.19
LightGBM	16.10/20.10	2.11/2.40	1.94/2.20
CatBoost	16.05/20.17	2.10/2.39	1.92/2.19

As can be seen from Fig. 7 and Table 1, CatBoost, XGBoost, and GBR demonstrated comparable performances in predicting w_{cr} for the test set. The

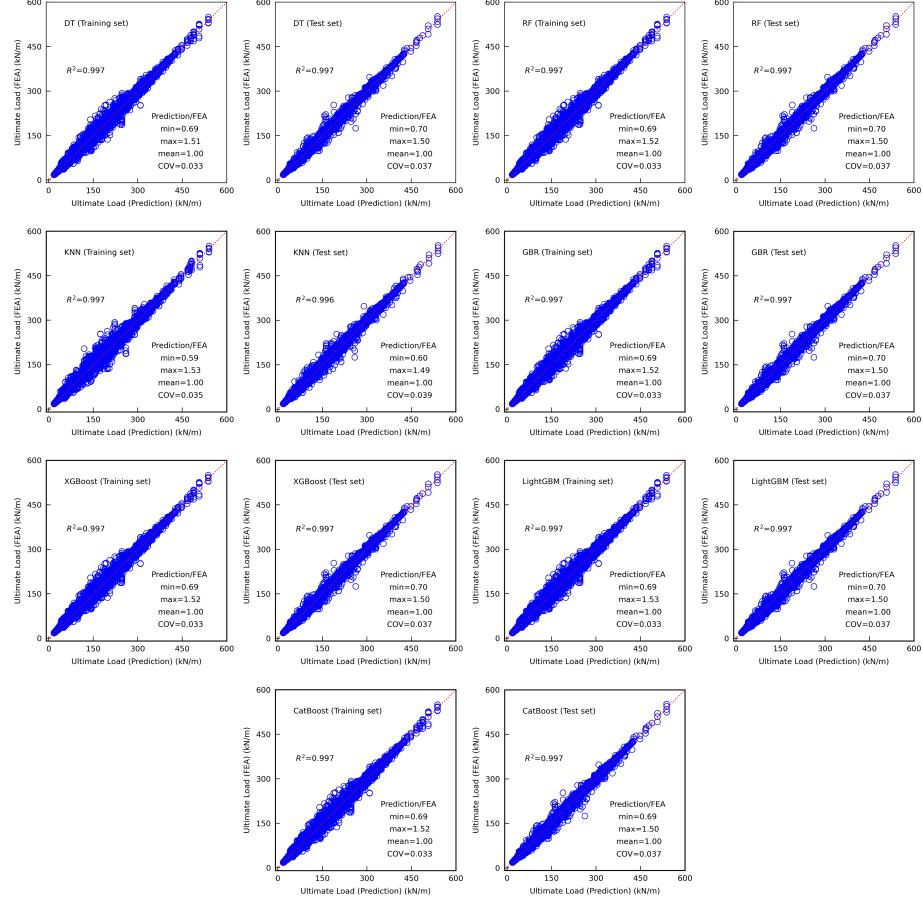


Figure 8: Performance of ML models for predicting ultimate load of steel cellular beams

465 performance metrics for LightGBM were slightly worse than those for CatBoost,
 466 XGBoost, and GBR. KNN provided inferior performance compared with other
 467 considered ML models. Fig. 8 and Table 2 show that all models performed
 468 well in predicting w_{max} , with KNN providing slightly worse metrics than other
 469 algorithms. It is worth reminding that the ultimate load dataset included 78390
 470 samples and was significantly larger than the elastic buckling load dataset with
 471 3645 samples. The good predictions of the ultimate load by all considered
 472 ML models, which was not the case for the elastic buckling dataset, highlight

473 that good data with a very large number of samples contributes more to the
474 accuracy of ML models than the ML algorithm differences. It can also be seen
475 from comparisons of the performance metrics for the training and test sets that
476 the created ML models with the optimal hyperparameters have a reasonably
477 good generalization performance.

478 Developed ML models can be accessed at the following link: [https://ww
479 w.kaggle.com/vitdegyarev/cellular-beams-ml-models](https://www.kaggle.com/vitdegyarev/cellular-beams-ml-models). An interactive
480 notebook for predicting the elastic buckling and ultimate loads of steel cellular
481 beams with the developed ML models can be found at the following link: [https://www.kaggle.com/vitdegyarev/ml-models-for-cellular-beams?scri
482 ptVersionId=63075739](https://www.kaggle.com/vitdegyarev/ml-models-for-cellular-beams?scriptVersionId=63075739).

484 **5. Relative feature importance and feature dependence**

485 Structural engineers often perceive ML methods as black boxes because hu
486 mans cannot easily explain and interpret ML predictions. To remove this barrier
487 to adopting ML methods, several ML explainability and interpretability tech
488 niques are available, including relative feature importance, partial dependence,
489 feature interactions, and SHAP [98]. These techniques shed light on why and
490 how an ML model made its predictions and expose how ML model predictions
491 compare with mechanics-based knowledge. The application of the explainability
492 and interpretability methods to the developed ML models is described in this
493 section.

494 Relative effects of the features on the w_{cr} and w_{max} predictions by each con
495 sidered ML model were analyzed using the permutation and SHAP methods.
496 The permutation feature importance is a decrease in a model score when the
497 feature values are randomly shuffled (permuted). A feature with a more sig
498 nificant score decrease is more important than others. The model score in the

499 form of coefficient of determination, R^2 , was used in this study. The random
500 shuffling of values is repeated several times for each feature to obtain the mean
501 and the standard deviation of the permutation importance score.

502 The SHAP method [86] aims to explain a prediction for a sample by deter-
503 mining the contribution of each feature to the prediction by computing Shapley
504 values from coalitional game theory [99]. The Shapley value represents the av-
505 erage contribution of one player, which is a model feature in our case, to the
506 model predictions taken for all possible combinations, which may consist of all
507 dataset samples or a predefined portion of them. SHAP uses an additive feature
508 attribution method – a linear explanation model of the summation of present
509 features. The feature importance is determined based on the absolute average
510 Shapley values. Features with larger Shapley values are more important than
511 others. SHAP feature importance is based on the magnitude of feature attri-
512 butions, while permutation feature importance is based on the decrease in the
513 model performance. Thus, the relative feature importance predicted by these
514 two methods might be different.

515 The relative feature importance was determined for all considered ML models
516 using both methods. The relative feature importance plots were similar for all
517 models. Therefore, the relative feature importance for the CatBoost models,
518 which are ones of the most accurate models for predicting w_{cr} and w_{max} , is
519 presented and discussed hereafter. Fig. 9 shows permutation and SHAP feature
520 importance plots for the optimized CatBoost models for predicting w_{cr} and
521 w_{max} .

522 The relative feature importance in predicting the elastic buckling load, w_{cr} ,
523 of steel cellular beams is discussed first. The span length, L , has the most
524 significant importance according to both methods, which was expected. The
525 next important beam parameters are the flange width, b_f , the web thickness,

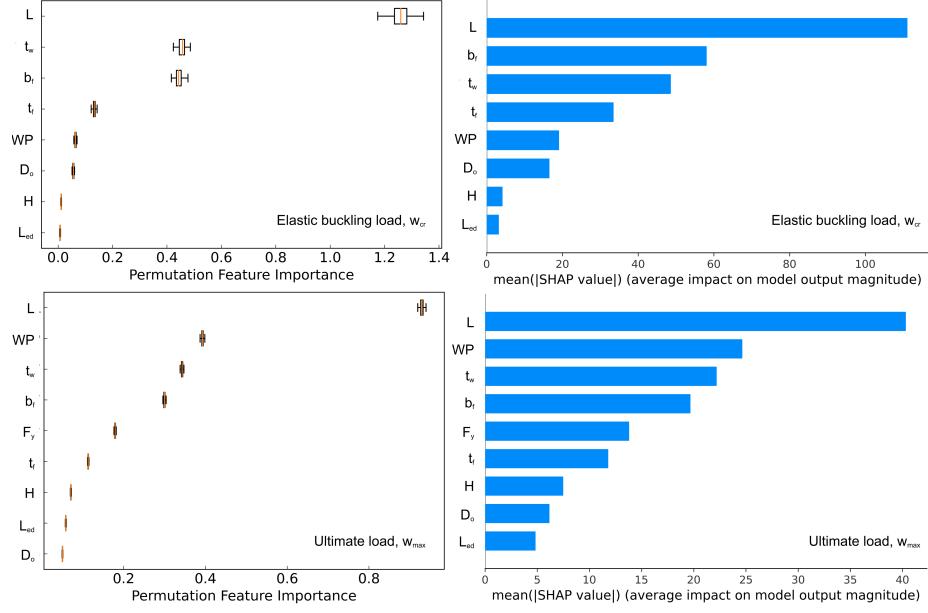


Figure 9: Permutation and SHAP feature importance for CatBoost models

526 t_w , and the flange thickness, t_f . The permutation method indicated that t_w
 527 is more important than b_f in predicting w_{cr} , while the SHAP method showed
 528 b_f above t_w . However, the difference in the importance scores for b_f and t_w is
 529 small, especially per the permutation method. These results compare well with
 530 the conclusions made in [29], indicating that the CatBoost model can capture
 531 the mechanics of the cellular beam behavior. The relative importance of the
 532 web post width, WP , the opening diameter, D_o , the beam height, H , and the
 533 opening end distance, L_{ed} , have relatively small importance in predicting w_{cr}
 534 according to both methods.

535 The permutation and SHAP relative feature importance plots for w_{max}
 536 demonstrate that the span length, L , is the most important feature, followed
 537 by WP , t_w , b_f , F_y , and t_f . It should be noted that WP has a more significant
 538 impact on w_{max} than on w_{cr} . These results align with the conclusion made
 539 in [29] and confirm the positive contribution of the web post plastic behavior

540 to the strength of steel cellular beams mentioned in Section 2. The relative
 541 importance of H , D_o , and L_{ed} for predicting w_{max} is minor.

542 SHAP feature importance plots provide useful information, which is, how-
 543 ever, somewhat limited. SHAP summary plots shown in Fig. 10 are more
 544 informative as they combine feature importance and feature effects. Each point
 545 on the summary plots represents a Shapley value for a dataset sample. The
 546 color shows the feature value from low (blue) to high (red). Points with the
 547 same Shapley values are scattered vertically to demonstrate their distribution
 548 for each feature. The order of the features follows their importance; so, it is
 549 the same as shown in Fig. 9. The SHAP summary plots presented in Fig.
 550 10 indicate that w_{cr} and w_{max} increase when the beam span reduces and vice
 551 versa. Wide web posts have higher w_{cr} and w_{max} , which decrease when the
 552 web post width reduces. Greater values of t_w , b_f , t_f , and L_{ed} produce higher
 553 w_{cr} and w_{max} , whereas an increase in the opening diameter D_o results in w_{cr}
 554 and w_{max} reductions. The beam height H affects w_{cr} and w_{max} differently:
 555 w_{cr} goes down when H increases, while w_{max} increases when H goes up. The
 556 reduction of w_{cr} with an increase in H can be explained by an increase in the
 557 web post slenderness, which results in the elastic buckling load reduction.

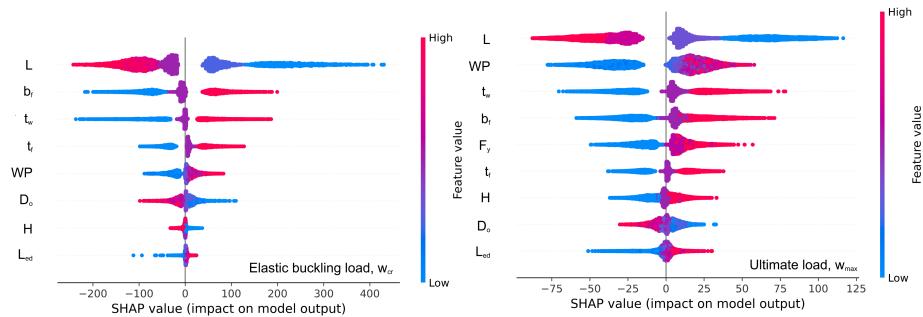


Figure 10: SHAP summary plots for CatBoost models

558 SHAP dependence plots given in Figs. 11 and 12 for w_{cr} and w_{max} illus-
 559 trate exact relationships between feature values and predictions. Each point

560 represents a prediction for a dataset sample. Feature values are shown on the
 561 horizontal axes, while SHAP values are given on the vertical axes. The SHAP
 562 values demonstrate the magnitude of change in w_{cr} and w_{max} when the feature's
 563 value is known. The color of each point corresponds to the second feature, which
 564 was determined by the algorithm to have the highest interaction with the con-
 565 sidered feature shown on the horizontal axis.

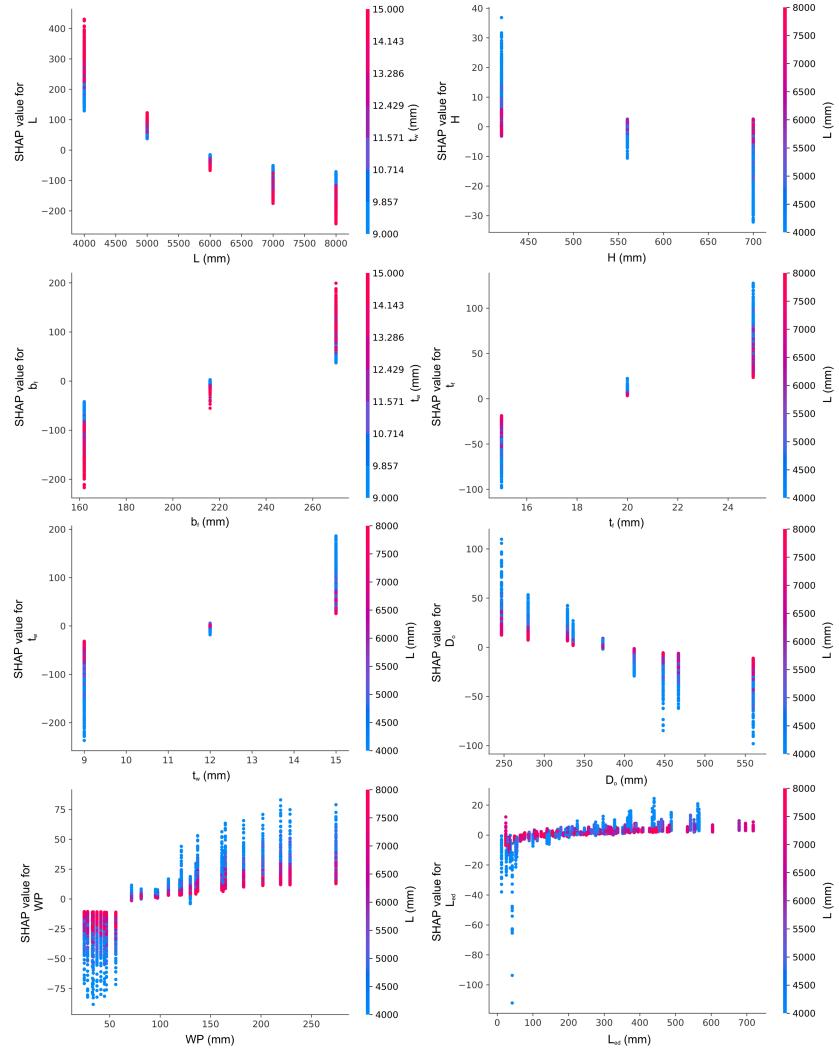


Figure 11: SHAP dependence plots for CatBoost model for predicting elastic buckling load

566 The SHAP dependence plots for w_{cr} show that L and b_f have the highest
567 interactions with t_w , while other features interact with L most frequently. An
568 increase in L results in an exponential decrease in w_{cr} , which is more pronounced
569 for the cellular beams with thicker webs. An increase in H results in reductions
570 of w_{cr} for the beams with short spans and smaller reductions or no reduction
571 for the beams with long spans, which can be seen from the comparison of the
572 SHAP values for the beams with long spans (red dots) with the SHAP values for
573 the beams with short spans (blue dots). These results indicate that the elastic
574 buckling load of the beams with short spans was likely governed by the local web
575 buckling. In contrast, the elastic buckling load of the beams with long spans was
576 likely governed by the global lateral-torsional buckling of the beams, which was
577 less sensitive to the changes in H for the beams considered in this study. The
578 elastic buckling loads increase when b_f increases, especially for the beams with
579 thicker webs. The elastic buckling load, w_{cr} , increases when t_f and t_w increase,
580 especially in the beams with short spans. The elastic buckling loads reduce
581 when D_o goes up. The w_{cr} reduction is more significant due to the D_o increase
582 for the cellular beams with short spans. When WP increases, w_{cr} increases,
583 especially for the beams with short spans. The plot also shows that web posts
584 with widths of 56 mm and narrower contribute to w_{cr} reductions, indicated by
585 the negative SHAP values, while web posts of 72 mm wide and wider contribute
586 to w_{cr} positively. An increase in L_{ed} results in a more significant increase in w_{cr}
587 for the beams with short spans and a smaller increase in w_{cr} for those with long
588 spans. It should be noted that the beam elastic buckling loads in the dataset
589 were obtained for different buckling modes, including global lateral-torsional
590 buckling of the beams, local buckling of the web posts, and their interaction.
591 Therefore, the effects of the ML model features discussed above reflect possible
592 changes in the buckling modes when the beam geometry changes.

593 The SHAP dependence plots for w_{max} demonstrate that the strongest in-
594 teractions are between L and t_w , H and D_o , b_f/t_f and WP , and L_{ed} and b_f .
595 All other features of the ultimate load model interact with L the most. An
596 increase in L results in a w_{max} reduction, which is more pronounced in the cel-
597 lular beams with thicker webs. Increases in H , b_f , t_f , and t_w cause an increase
598 in w_{max} , which goes down when D_o increases. An increase in WP makes the
599 beam ultimate load higher, which is more pronounced for the beams with short
600 spans. Similar to the observed effect of WP on w_{cr} , web post widths up to 56
601 mm have a negative contribution to the beam ultimate load, while web posts
602 of 72 mm wide and wider contribute to the beam ultimate load positively. It
603 implies that the beam ultimate load in the dataset was governed by the web
604 post strength when WP was 56 mm or lower. The beam ultimate load becomes
605 higher when L_{ed} and F_y increase. The positive effect of F_y on w_{max} is more
606 significant in the beams with short spans and when F_y increases from 235 to
607 355 MPa compared with the F_y increase from 355 to 440 MPa.

608 Fig. 13 shows contour plots of w_{cr} predicted by the developed CatBoost
609 model as functions of H/D_o and S_o/D_o (where S_o is the center-to-center spacing
610 of the web openings) for the beams with different span lengths and cross-section
611 dimensions. The beam designations are presented in the $L-H-t_w-b_f-t_f$ format,
612 with all dimensions in mm. Fig. 13 demonstrates that S_o/D_o has a greater
613 influence on w_{cr} than H/D_o for the beams with short spans. For many short-
614 span beams, an increase in S_o/D_o from 1.1 to 1.3 results in a greater increase
615 in w_{cr} than a further increase in S_o/D_o from 1.3 to 1.49. It indicates that
616 web opening spacing of approximately $1.3D_o$ is optimal for many short-span
617 beams. Only short-span beams with $H=420$ mm and $t_w=9$ mm demonstrate
618 an approximately uniform w_{cr} increase when S_o/D_o increases from 1.1 to 1.49.
619 The long-span beams show a wider variety of the w_{cr} contour shapes. For

example, H/D_o has a more significant effect on w_{cr} than S_o/D_o for the beam with $H=420$ mm, $t_w=9$ mm, $b_f=162$ mm, and $t_f=15$ mm compared with other analyzed beams. The w_{cr} values for the 8000-420-9-162-15 and 8000-700-15-162-15 beams reduce slightly when S_o/D_o increase from 1.1 to 1.3 and increase with the further increase in S_o/D_o from 1.3 to 1.49. However, it should be noted that the absolute magnitude of the w_{cr} change is relatively small in those cases. The contour plots also show the effects of the cross-section dimensions on the w_{cr} values of the cellular beams discussed earlier in the paper.

Figs. 14 and 15 present contour plots of w_{max} predicted by the CatBoost model as functions of H/D_o and S_o/D_o for the cellular beams made from steel with F_y of 235 and 440 MPa, respectively. The beam designation format is as described previously, with the steel yield strength added at the end. Similar to w_{cr} , S_o/D_o shows a more significant effect on w_{max} than H/D_o for most of the considered beams. The effect of the opening diameter on w_{max} is more pronounced in the H/D_o range from 1.25 to approximately 1.45 for many beams. A further increase in H/D_o at a constant S_o/D_o value changes w_{max} insignificantly. It can also be seen from the contour plots that for some beams (see 4000-420-15-162-15-235, 7000-420-15-162-15-235, 4000-420-15-270-15-440, and 7000-700-9-270-15-440, for example), the effects of H/D_o varying in the range from 1.25 to 1.45 on w_{max} are relatively small when S_o/D_o is low. They become more pronounced as S_o/D_o increases. The S_o/D_o of approximately 1.3 is optimal for many considered beams. The effects of the cross-section dimensions on w_{max} discussed earlier in the paper can also be seen from Figs. 14 and 15.

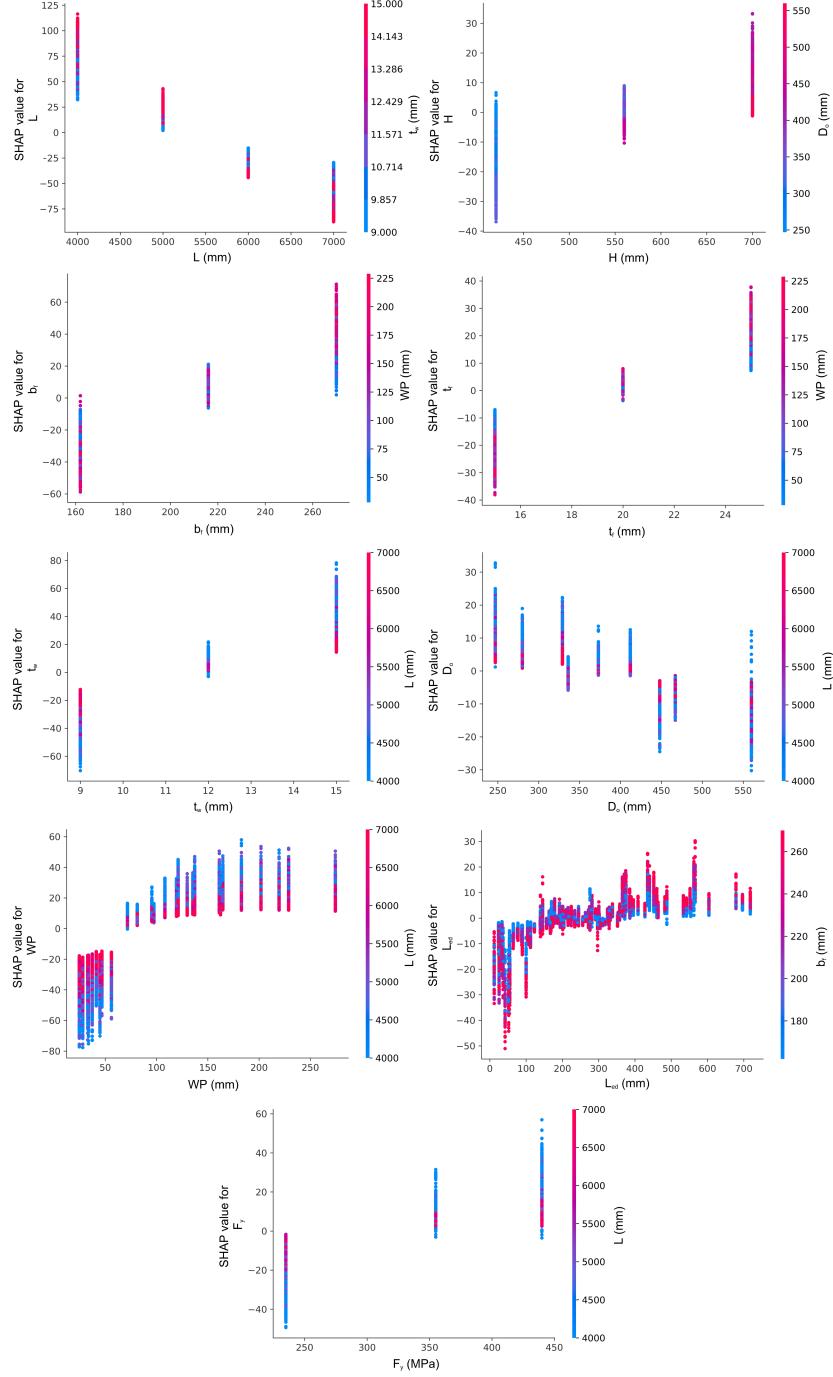


Figure 12: SHAP dependence plots for CatBoost model for predicting ultimate load

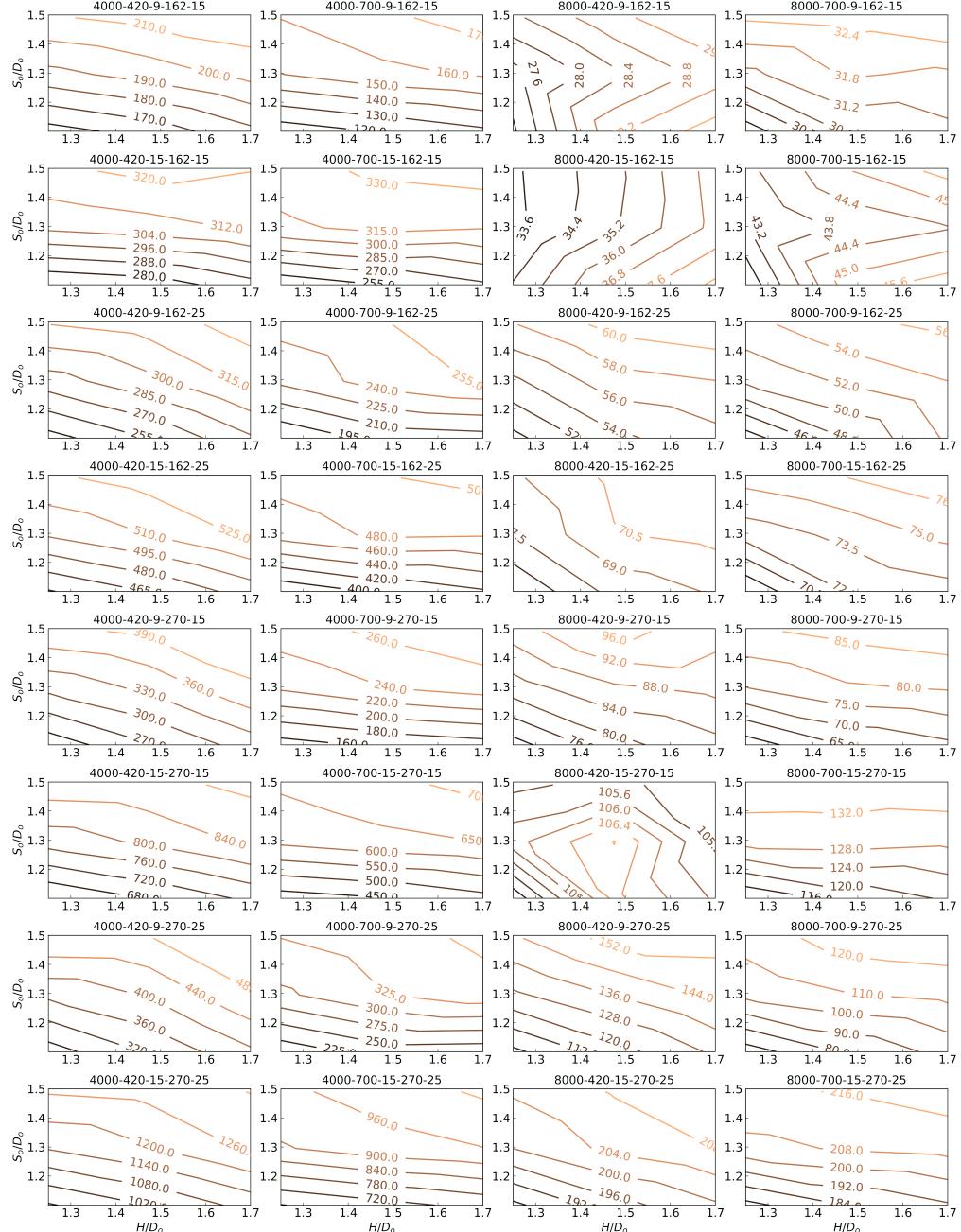


Figure 13: Contour plots of w_{cr} (kN/m) as functions of H/D_o and S_o/D_o

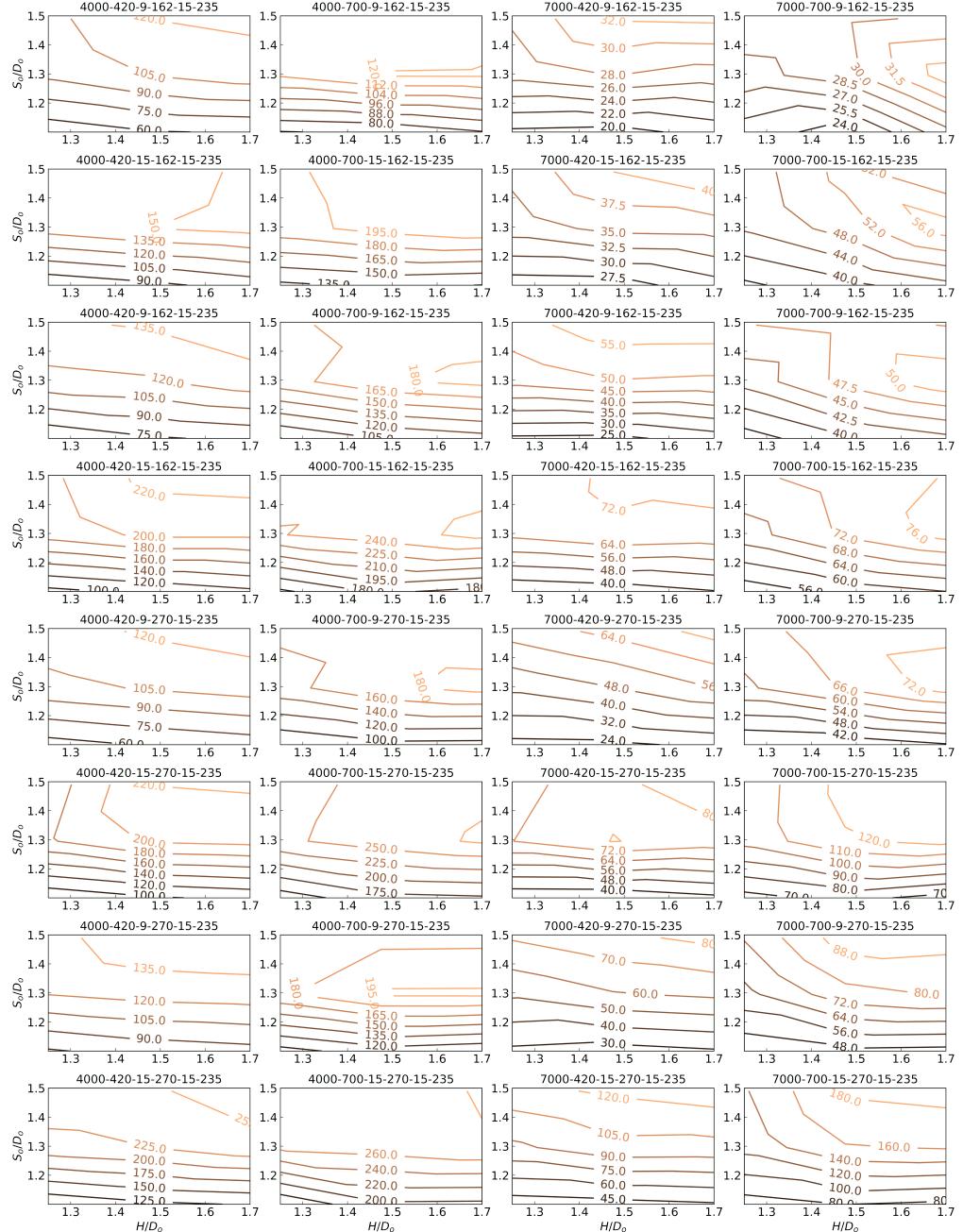


Figure 14: Contour plots of w_{max} (kN/m) as functions of H/D_o and S_o/D_o for beams made from 235 MPa steel

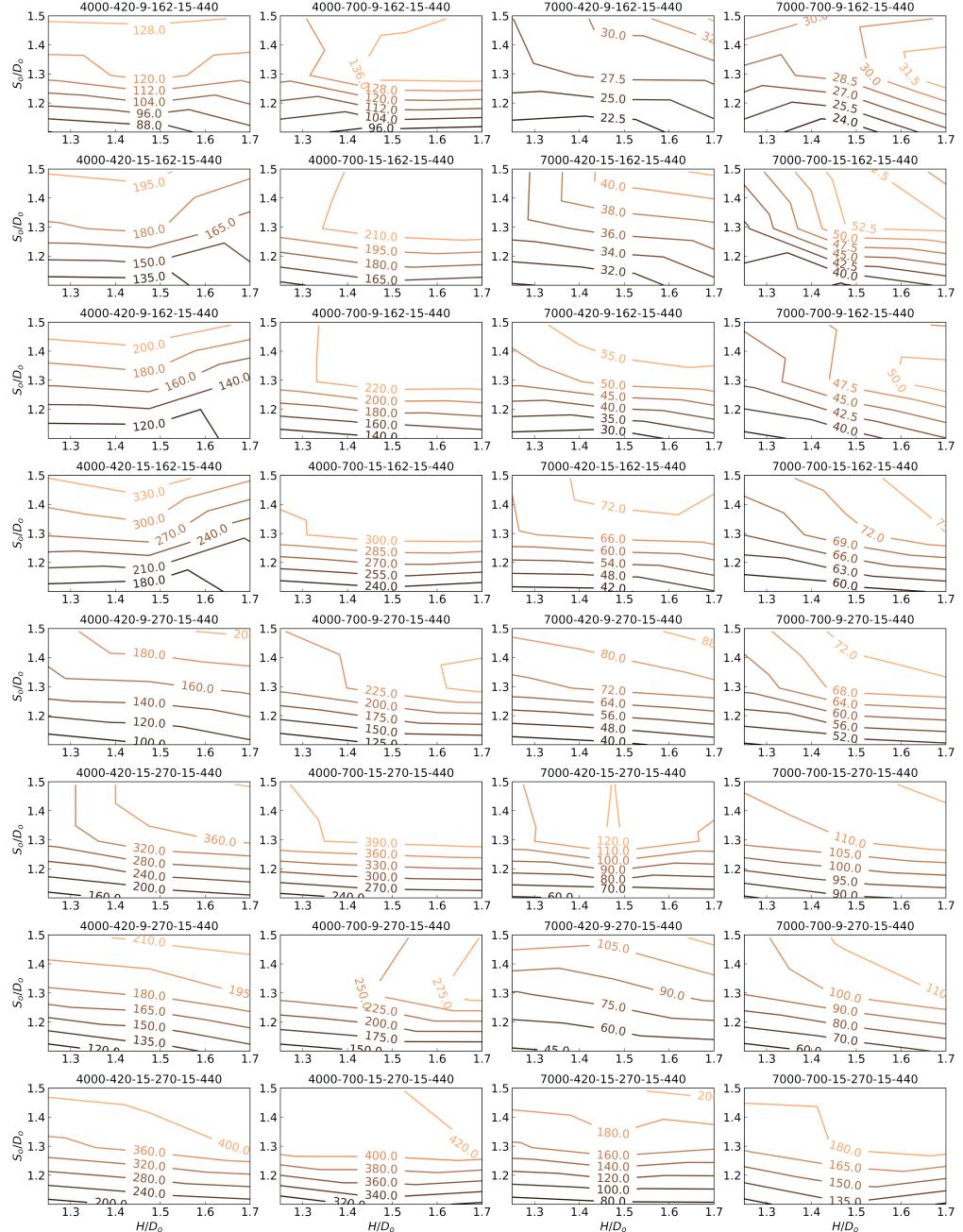


Figure 15: Contour plots of w_{max} (kN/m) as functions of H/D_o and S_o/D_o for beams made from 440 MPa steel

643 **6. Comparisons of ultimate loads of cellular beams predicted by ML**
644 **models, SCI P355, and AISC Design Guide 31**

645 The ultimate loads of cellular beams predicted by the developed ML models
646 were compared with the nominal beam strengths determined per SCI P355 [2]
647 and AISC Design Guide 31 [87]. According to SCI P355 and AISC Design
648 Guide 31, the cellular beam strength may be governed by shear resistance of
649 perforated beam section, shear resistance of solid beam section, shear buckling
650 resistance of perforated web, bending resistance of beam at the centerline of
651 opening, bending resistance of tees, web post shear resistance, and web post
652 buckling resistance. The beam, tee, and web post resistances are computed
653 per EN 1993-1-1 [12] and EN 1993-1-5 [100] in SCI P355 and per AISC 360
654 [101] in AISC Design Guide 31. The most significant differences between the
655 SCI P355 and AISC Design Guide 31 provisions are in the web post buckling
656 resistance and lateral-torsional buckling calculations [102]. In SCI P355, the
657 web post buckling resistance is calculated using analytical equations, which
658 account for the web post slenderness, while AISC Design Guide 31 adopted
659 empirical equations from SCI P100 [27]. SCI P355 also requires checking web
660 shear buckling near openings, whereas AISC Design Guide 31 does not include
661 such a requirement.

662 The SCI P355 provisions apply to cellular beams with the following geo-
663 metric limits: $H/D_o \geq 1.25$, $2.0 \geq S_o/D_o \geq 1.3$, $L_{ed}/D_o \geq 0.5$, and the
664 depth of tees not less than $t_f + 30$ mm. The beams considered in the study
665 had the following parameters: $1.70 \geq H/D_o \geq 1.25$, $1.49 \geq S_o/D_o \geq 1.10$,
666 $1.49 \geq L_{ed}/D_o \geq 0.04$, and the depth of tees between $t_f + 29.5$ mm and $t_f + 136.5$
667 mm. S_o/D_o , L_{ed}/D_o , and the depth of tees of some beams did not comply
668 with the SCI P355 limits. Therefore, the SCI P355 predictions were com-
669 pared with the FE simulation results for all beams and 17,982 beams that met

670 the geometric limits. AISC Design Guide 31 applies to cellular beams with
671 $1.75 \geq H/D_o \geq 1.25$ and $1.50 \geq S_o/D_o \geq 1.08$. All beams considered in the
672 present study complied with the AISC Design Guide 31 limits.

673 Fig. 16 compares the ultimate loads of the cellular beams from the FE
674 simulations with those predicted by the developed ML models, SCI P355, and
675 AISC Design Guide 31. Fig. 16 clearly shows that the developed ML models
676 predict the ultimate loads of the cellular beams considerably better than SCI
677 P355 and AISC Design Guide 31. For the best models, the mean ratio and the
678 coefficient of variation of the ML predictions to the FE simulation results are
679 1.00 and 0.034, respectively. The coefficient of determination, R^2 , is 0.997. The
680 corresponding metrics for SCI P355 are 0.75, 0.253, and 0.638 for all beams
681 and 0.75, 0.298, and 0.535 for the beams meeting the geometric limits. It is
682 interesting to note that the SCI P355 provisions demonstrate better comparison
683 with the FE simulation results when all beams are considered neglecting the
684 geometric limits. AISC Design Guide 31 showed even worse accuracy than SCI
685 P355, characterized by the mean ratio and the coefficient of variation of the
686 prediction-to-FEA ratios of 0.69 and 0.429, and the coefficient of determination
687 of 0.416.

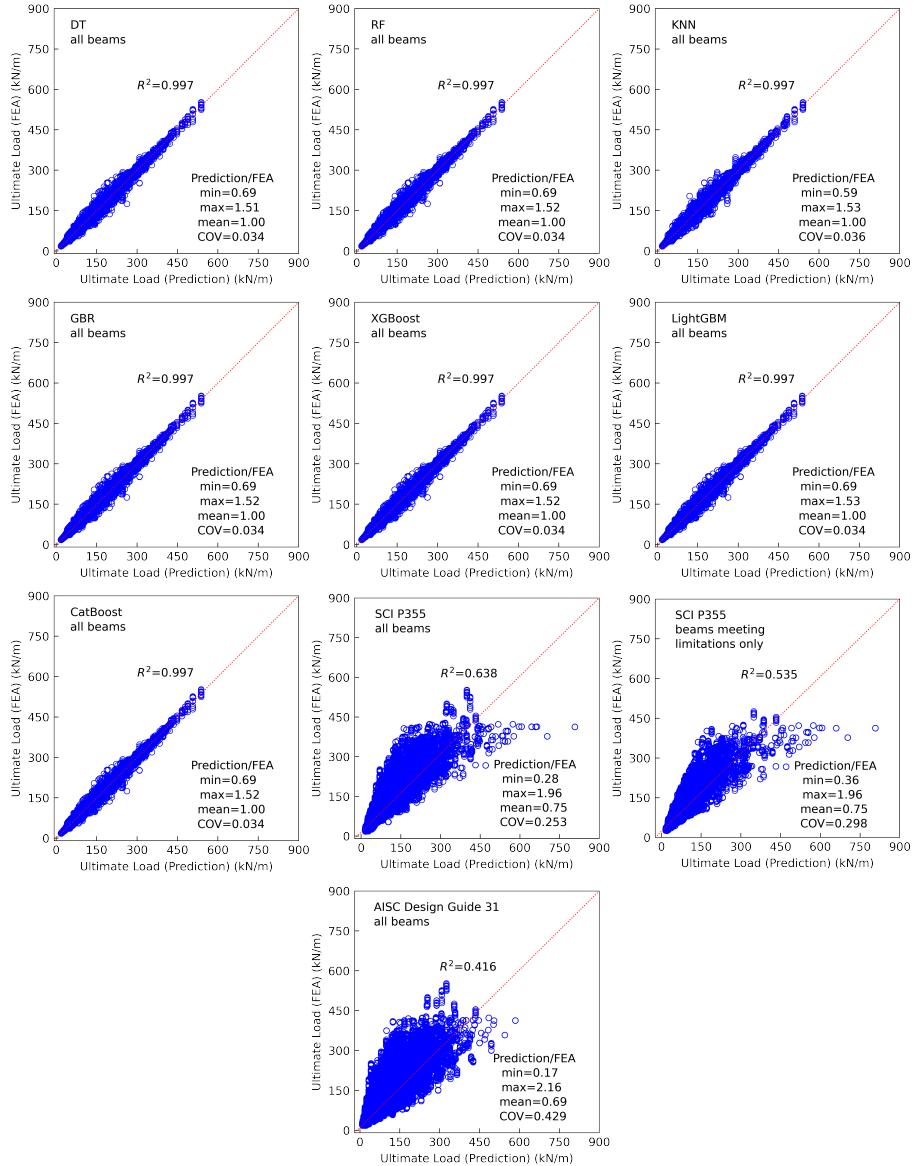


Figure 16: Comparisons of ultimate loads of steel cellular beams predicted by ML models, SCI P355, and AISC Design Guide 31 with FE simulation results

688 7. Web application

689 A user-friendly web application was created in the Streamlit framework ([ht
690 tps://streamlit.io](https://streamlit.io)) to predict the elastic buckling and ultimate loads of

⁶⁹¹ steel cellular beams with the ML models developed in the present work. Fig.
⁶⁹² 17 demonstrates a flow chart of the web application.

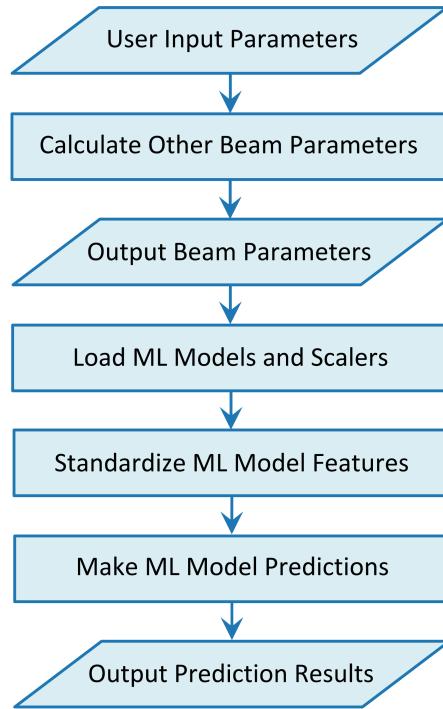


Figure 17: Flow chart of the web application

⁶⁹³ In the beginning, the user specifies the following parameters via the web
⁶⁹⁴ application sliders and radio buttons: L , H , b_f , t_f , t_w , H/D_o , S_o/D_o , and F_y .
⁶⁹⁵ Ranges of the parameters available in the application correspond to the feature
⁶⁹⁶ ranges in the datasets used for the ML training. At the next step, the following
⁶⁹⁷ parameters are computed: D_o , S_o , L_{ed} , the number of openings evenly spaced
⁶⁹⁸ along the beam length, the cellular beam weight, and the percentage of the
⁶⁹⁹ beam weight reduction due to the openings compared with the identical solid-
⁷⁰⁰ web beam. The parameters specified by the user and the computed ones are
⁷⁰¹ displayed on the screen. Next, the developed ML models and scalers are loaded;
⁷⁰² the features are standardized, and predictions by all ML models considered

703 in this study are made and displayed. The code runs automatically after any
 704 change of input variables. The prediction process takes only several seconds.
 705 The graphical user interface of the web application is presented in Fig. 18.

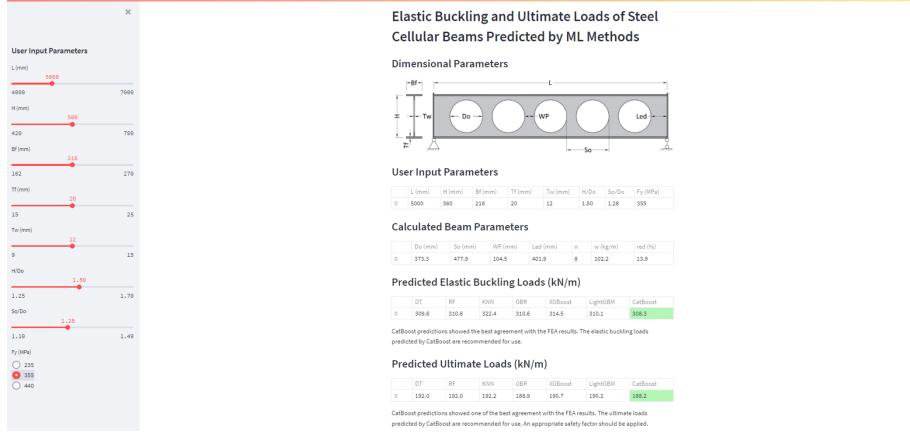


Figure 18: Graphical user interface of the developed web application

706 It was found challenging to deploy the web application with all considered
 707 ML to cloud platforms due to the application size and required computational
 708 resources, which exceeded the limits of free cloud accounts. Therefore,
 709 a lite version of the application based on CatBoost predictions was created
 710 and successfully deployed on Heroku at the following address: <https://scba-cb.herokuapp.com/>. The deployed lite version of the application
 711 opens and runs in any web browser on any device, including mobile.

713 It should be noted that the computational resources provided by the free
 714 Heroku account are sufficient for running the application by one user at a time.
 715 Multiple users can open the application, but it crashes when two or more users
 716 run the computations simultaneously. If that happens, it is recommended to
 717 close the application and use it later. The use of a paid Heroku account, which
 718 offers more powerful computational resources, would resolve this issue.

719 The source codes of the full and lite application versions can be accessed

720 on GitHub at <https://github.com/vitdegyarev/SCBA-Streamlit> and
721 <https://github.com/vitdegyarev/SCBA-Streamlit-CB>, respectively. The
722 GitHub pages include instructions on how the web applications can be used
723 independently from the cloud services on a local machine.

724 **8. Conclusions**

725 ML models for predicting the elastic buckling and ultimate loads of steel
726 cellular beams were developed and optimized using the following algorithms:
727 decision tree (DT), random forest (RF), k-nearest neighbor (KNN), gradient
728 boosting regressor (GBR), extreme gradient boosting (XGBoost), light gradient
729 boosting machine (LightGBM), and gradient boosting with categorical features
730 support (CatBoost). Large datasets of FE simulation results from the literature
731 [29], validated against experimental data, were employed to train and evaluate
732 the ML models implemented in open-source Python-based libraries.

733 The ML models were optimized by tuning their hyperparameters via ex-
734 tensive grid and random searches and validated through the ten-fold cross-
735 validation method. The final evaluation of the ML models was performed on
736 the test sets unseen by the models during training. The elastic buckling and
737 ultimate loads predicted by the optimized ML models demonstrated excellent
738 agreements with the numerical data. The accuracy of the ultimate load predic-
739 tions by the ML models exceeded the accuracy provided by the existing design
740 provisions for steel cellular beams. An interactive Python-based notebook for
741 predicting the elastic buckling and ultimate loads of steel cellular beams using
742 the developed optimized ML models was created and made publicly available
743 at the following link: [https://www.kaggle.com/vitdegyarev/ml-models-
for-cellular-beams?scriptVersionId=63075739](https://www.kaggle.com/vitdegyarev/ml-models-for-cellular-beams?scriptVersionId=63075739).

745 The developed ML models were explained and interpreted by evaluating the

relative feature importance using the permutations and SHAP methods. SHAP
feature dependence was also determined and discussed. It was demonstrated
that the beam span length, beam flange width, and beam web thickness are
the most important features in predicting the elastic buckling by the developed
models, with the opening end distance and beam height being the least im-
portant parameters. The most important features in predicting the ultimate
load are the beam span length, web post width, beam web thickness, and beam
flange width. The opening end distance and opening diameter are the least
important characteristics. These results align well with the mechanics-based
knowledge demonstrating that the developed ML models can capture the web
opening effects from the data used for their training. Contour plots of w_{cr} and
 w_{max} predicted by the CatBoost model as functions of H/D_o and S_o/D_o were
presented and discussed. For most beams, S_o/D_o affects w_{cr} and w_{max} more
significantly than H/D_o , with $S_o/D_o=1.3$ being the optimal value.

A web application for predicting the elastic buckling and ultimate loads was
created in Streamlit. The lite version of the application has been deployed to
the cloud at: <https://scba-cb.herokuapp.com/>. It can be opened and
run in any web browser on any device, including mobile. The source codes
of the full and lite application versions can be accessed on GitHub at <https://github.com/vitdegyarev/SCBA-Streamlit> and <https://github.com/vitdegyarev/SCBA-Streamlit-CB>, respectively.

The presented study demonstrates the opportunities for using ML methods
for predicting the elastic buckling and ultimate loads of cellular beams. However,
it should be noted that the developed models are based on the data for cellular
beams with relatively short spans, not exceeding 8 m in the elastic buckling
load dataset and 7 m in the ultimate load dataset. Therefore, the developed
models are limited to beams with such spans. In modern construction, cellular

773 beams are often used for spans ranging from 9 to 18 m [103]. Future work
774 should concentrate on extending the datasets to the beams with longer spans
775 and retraining the ML models using the extended data. The reliability of the
776 ultimate load predictions by the ML models should also be evaluated, and an
777 appropriate safety factor determined.

778 **References**

- 779 [1] P. K. Das, S. L. Srimani, Handbook for the design of castellated beams,
780 Central Mechanical Engineering Research Institute, Oxford & IBH Pub-
781 lishing Company, New Delhi, Delhi, India, 1984.
- 782 [2] R. Lawson, S. Hicks, Design of composite beams with large web openings
783 SCI P355, Steel Construction Institute, Berkshire, UK, 2011.
- 784 [3] M. I. M. H. Martini, Elasto-plastic lateral torsional buckling of steel
785 beams with perforated web, Ph.D. thesis, United Arab Emirates Uni-
786 versity (2011).
- 787 [4] A. M. Sweedan, Elastic lateral stability of I-shaped cellular steel beams,
788 Journal of Constructional Steel Research 67 (2) (2011) 151–163. doi:
789 [10.1016/j.jcsr.2010.08.009](https://doi.org/10.1016/j.jcsr.2010.08.009).
- 790 [5] M. M. Sehwail, Lateral torsional buckling of steel i-section cellular beams,
791 Ph.D. thesis, Eastern Mediterranean University (EMU)-Doğu Akdeniz
792 Üniversitesi (DAÜ) (2013).
- 793 [6] D. Sonck, J. Belis, Lateral-torsional buckling resistance of cellular beams,
794 Journal of Constructional Steel Research 105 (2015) 119–128. doi:10.1
795 [10.1016/j.jcsr.2014.11.003](https://doi.org/10.1016/j.jcsr.2014.11.003).

- 796 [7] P. Panedpojaman, W. Sae-Long, T. Chub-uppakarn, Cellular beam design
797 for resistance to inelastic lateral-torsional buckling, Thin-Walled Struc-
798 tures 99 (2016) 182–194. doi:[10.1016/j.tws.2015.08.026](https://doi.org/10.1016/j.tws.2015.08.026).
- 799 [8] F. P. V. Ferreira, A. Rossi, C. H. Martins, Lateral-torsional buckling of
800 cellular beams according to the possible updating of EC3, Journal of Con-
801 structional Steel Research 153 (2019) 222–242. doi:[10.1016/j.jcsr.2018.10.011](https://doi.org/10.1016/j.jcsr.2018.10.011).
- 803 [9] K. D. Tsavdaridis, C. D'Mello, Web buckling study of the behaviour and
804 strength of perforated steel beams with different novel web opening shapes,
805 Journal of Constructional Steel Research 67 (10) (2011) 1605–1620. doi:
806 [10.1016/j.jcsr.2011.04.004](https://doi.org/10.1016/j.jcsr.2011.04.004).
- 807 [10] P. Panedpojaman, T. Thepchatri, S. Limkatanyu, Novel design equations
808 for shear strength of local web-post buckling in cellular beams, Thin-
809 Walled Structures 76 (2014) 92–104. doi:[10.1016/j.tws.2013.11.007](https://doi.org/10.1016/j.tws.2013.11.007).
- 810 [11] L. F. Grilo, R. H. Fakury, G. de Souza Veríssimo, et al., Design procedure
811 for the web-post buckling of steel cellular beams, Journal of Constructional
812 Steel Research 148 (2018) 525–541. doi:[10.1016/j.jcsr.2018.06.020](https://doi.org/10.1016/j.jcsr.2018.06.020).
- 813 [12] BS EN 1993-1-1: 2005. Design of steel structures—Part 1-1 General rules
814 and rules for buildings, British Standards Institution, London, UK, 2005.
- 815 [13] ANSI/AISC 360-10. Specification for structural steel buildings, American
816 Institute of Steel Construction, Chicago, Illinois, USA, 2010.
- 817 [14] K. F. Chung, T. Liu, A. Ko, Investigation on Vierendeel mechanism in
818 steel beams with circular web openings, Journal of Constructional Steel
819 Research 57 (5) (2001) 467–490. doi:[10.1016/S0143-974X\(00\)00035-3](https://doi.org/10.1016/S0143-974X(00)00035-3).

- 820 [15] L. Kang, S. Hong, X. Liu, Shear behaviour and strength design of cellular
821 beams with circular or elongated openings, *Thin-Walled Structures* 160
822 (2021) 107353. doi:10.1016/j.tws.2020.107353.
- 823 [16] E. Ellobody, Nonlinear analysis of cellular steel beams under combined
824 buckling modes, *Thin-Walled Structures* 52 (2012) 66–79. doi:10.1016/
825 j.tws.2011.12.009.
- 826 [17] K. D. Tsavdaridis, C. D'Mello, Vierendeel bending study of perforated
827 steel beams with various novel web opening shapes through nonlinear
828 finite-element analyses, *Journal of Structural Engineering* 138 (10) (2012)
829 1214–1230. doi:10.1061/(ASCE)ST.1943-541X.0000562.
- 830 [18] N. D. Lagaros, L. D. Psarras, M. Papadrakakis, G. Panagiotou, Optimum
831 design of steel structures with web openings, *Engineering Structures* 30 (9)
832 (2008) 2528–2537. doi:10.1016/j.engstruct.2008.02.002.
- 833 [19] K. Tsavdaridis, C. D'Mello, FE investigation of perforated sections with
834 standard and non-standard web opening configurations and sizes, in: The
835 6th International Conference on Advances in Steel Structures (ICASS
836 2009), 16-18 December 2009, pp. 213–220.
- 837 [20] F. Erdal, M. P. Saka, Ultimate load carrying capacity of optimally de-
838 signed steel cellular beams, *Journal of Constructional Steel Research* 80
839 (2013) 355–368. doi:10.1016/j.jcsr.2012.10.007.
- 840 [21] A. Jamadar, P. Kumbhar, Parametric study of castellated beam with
841 circular and diamond shaped openings, *International Research Journal of
842 Engineering and Technology* 2 (2) (2015) 715–722.
- 843 [22] K. D. Tsavdaridis, J. J. Kingman, V. V. Toropov, Application of structural

- 844 topology optimisation to perforated steel beams, Computers & Structures
845 158 (2015) 108–123. doi:10.1016/j.compstruc.2015.05.004.
- 846 [23] S. G. Morkhade, L. M. Gupta, An experimental and parametric study
847 on steel beams with web openings, International Journal of Advanced
848 Structural Engineering (IJASE) 7 (3) (2015) 249–260. doi:10.1007/s4
849 0091-015-0095-4.
- 850 [24] K. D. Tsavdaridis, G. Galatsatos, Assessment of cellular beams with
851 transverse stiffeners and closely spaced web openings, Thin-Walled Struc-
852 tures 94 (2015) 636–650. doi:10.1016/j.tws.2015.05.005.
- 853 [25] V. Akrami, S. Erfani, Review and assessment of design methodologies for
854 perforated steel beams, Journal of Structural Engineering 142 (2) (2016)
855 04015148. doi:10.1061/(ASCE)ST.1943-541X.0001421.
- 856 [26] SEI/ASCE 23-97. Specifications for structural steel beams with web open-
857 ings, American Society of Civil Engineers, Reston, VA, USA, 1999.
- 858 [27] J. Ward, Design of composite and non-composite cellular beams SCI P100,
859 Steel Construction Institute, Berkshire, UK, 1990.
- 860 [28] K. F. Chung, C. Liu, A. Ko, Steel beams with large web openings of
861 various shapes and sizes: an empirical design method using a generalised
862 moment-shear interaction curve, Journal of Constructional Steel Research
863 59 (9) (2003) 1177–1200. doi:10.1016/S0143-974X(03)00029-4.
- 864 [29] K. Rajana, K. D. Tsavdaridis, E. Koltsakis, Elastic and inelastic buckling
865 of steel cellular beams under strong-axis bending, Thin-Walled Structures
866 156 (2020) 106955. doi:10.1016/j.tws.2020.106955.
- 867 [30] F. Jiang, Y. Jiang, H. Zhi, Y. Dong, H. Li, S. Ma, Y. Wang, Q. Dong,
868 H. Shen, Y. Wang, Artificial intelligence in healthcare: past, present and

- 869 future, *Stroke and Vascular Neurology* 2 (4). doi:10.1136/svn-2017-0
870 00101.
- 871 [31] N. R. Tadapaneni, Artificial intelligence in finance and investments, *Interna-*
872 *tional Journal of Innovative Research in Science, Engineering and*
873 *Technology* 9 (5) (2019) 2792–2795.
- 874 [32] Y. Ma, Z. Wang, H. Yang, L. Yang, Artificial intelligence applications in
875 the development of autonomous vehicles: a survey, *IEEE/CAA Journal*
876 *of Automatica Sinica* 7 (2) (2020) 315–329. doi:10.1109/JAS.2020.100
877 3021.
- 878 [33] T. Wuest, D. Weimer, C. Irgens, K.-D. Thoben, Machine learning in man-
879 ufacturing: advantages, challenges, and applications, *Production & Man-*
880 *ufacturing Research* 4 (1) (2016) 23–45. doi:10.1080/21693277.2016.
881 1192517.
- 882 [34] N. Kartam, I. Flood, J. H. Garrett, *Artificial Neural Networks for Civil*
883 *Engineers: Fundamentals and Applications*, American Society of Civil
884 *Engineers*, 1997.
- 885 [35] H. Adeli, Neural networks in civil engineering: 1989–2000, *Computer-*
886 *Aided Civil and Infrastructure Engineering* 16 (2) (2001) 126–142. doi:
887 10.1111/0885-9507.00219.
- 888 [36] H. Salehi, R. Burgueño, Emerging artificial intelligence methods in struc-
889 *tural engineering*, *Engineering Structures* 171 (2018) 170–189. doi:
890 10.1016/j.engstruct.2018.05.084.
- 891 [37] H. Sun, H. V. Burton, H. Huang, Machine learning applications for build-
892 *ing structural design and performance assessment: state-of-the-art review*,

Journal of Building Engineering (2020) 101816doi:10.1016/j.jobe.2020.101816.

- [38] M. Z. Naser, Systematic Integration of Artificial Intelligence Toward Evaluating Response of Materials and Structures in Extreme Conditions, Springer Transactions in Civil and Environmental Engineering, Springer, 2021, p. 183–212. doi:10.1007/978-981-15-5772-9_10.

[39] M. Naser, Mechanistically informed machine learning and artificial intelligence in fire engineering and sciences, *Fire Technology* (2021) 1–44doi:10.1007/s10694-020-01069-8.

[40] H.-T. Thai, Machine learning for structural engineering: A state-of-the-art review, *Structures* (2022) 448–491doi:10.1016/j.istruc.2022.02.003.

[41] A. Çevik, A. E. Kurtoğlu, M. Bilgehan, M. E. Gülsan, H. M. Albegmprli, Support vector machines in structural engineering: a review, *Journal of Civil Engineering and Management* 21 (3) (2015) 261–281. doi:10.3846/13923730.2015.1005021.

[42] C. Liu, C. Liu, C. Liu, X. Huang, J. Miao, W. Xu, Fire damage identification in RC beams based on support vector machines considering vibration test, *KSCE Journal of Civil Engineering* 23 (10) (2019) 4407–4416. doi:10.1007/s12205-019-2353-7.

[43] J. Zhang, G. Ma, Y. Huang, F. Aslani, B. Nener, et al., Modelling uniaxial compressive strength of lightweight self-compacting concrete using random forest regression, *Construction and Building Materials* 210 (2019) 713–719. doi:10.1016/j.conbuildmat.2019.03.189.

[44] S. Mangalathu, S.-H. Hwang, J.-S. Jeon, Failure mode and effects analysis of rc members based on machine-learning-based shapley additive ex-

- 918 planations (SHAP) approach, Engineering Structures 219 (2020) 110927.
919
920 [45] R. Solhmirzaei, H. Salehi, V. Kodur, M. Naser, Machine learning frame-
921 work for predicting failure mode and shear capacity of ultra high per-
922 formance concrete beams, Engineering Structures 224 (2020) 111221.
923
924 [46] M. S. Ahmad, S. M. Adnan, S. Zaidi, P. Bhargava, A novel support vector
925 regression (SVR) model for the prediction of splice strength of the uncon-
926 fined beam specimens, Construction and Building Materials 248 (2020)
927 118475. doi:10.1016/j.conbuildmat.2020.118475.
928 [47] S. Mangalathu, H. Jang, S.-H. Hwang, J.-S. Jeon, Data-driven machine-
929 learning-based seismic failure mode identification of reinforced concrete
930 shear walls, Engineering Structures 208 (2020) 110331. doi:10.1016/j.
931 engstruct.2020.110331.
932 [48] M. Naser, H. Salehi, Machine learning-driven assessment of fire-induced
933 concrete spalling of columns, ACI Materials Journal 117 (6) (2020) 7–16.
934
935 [49] D.-C. Feng, Z.-T. Liu, X.-D. Wang, Y. Chen, J.-Q. Chang, D.-F. Wei,
936 Z.-M. Jiang, Machine learning-based compressive strength prediction for
937 concrete: An adaptive boosting approach, Construction and Building Ma-
938 terials 230 (2020) 117000. doi:10.1016/j.conbuildmat.2019.117000.
939 [50] T. Nguyen-Sy, J. Wakim, Q.-D. To, M.-N. Vu, T.-D. Nguyen, T.-T.
940 Nguyen, Predicting the compressive strength of concrete from its compo-
941 sitions and age using the extreme gradient boosting method, Construction
942 and Building Materials 260 (2020) 119757. doi:10.1016/j.conbuildma
943 t.2020.119757.

- 944 [51] M. R. Kaloop, D. Kumar, P. Samui, J. W. Hu, D. Kim, Compre-
945 sive strength prediction of high-performance concrete using gradient
946 tree boosting machine, Construction and Building Materials 264 (2020)
947 120198. doi:10.1016/j.conbuildmat.2020.120198.
- 948 [52] A. Marani, M. L. Nehdi, Machine learning prediction of compressive
949 strength for phase change materials integrated cementitious composites,
950 Construction and Building Materials 265 (2020) 120286. doi:10.1016/
951 j.conbuildmat.2020.120286.
- 952 [53] W. B. Chaabene, M. Flah, M. L. Nehdi, Machine learning prediction
953 of mechanical properties of concrete: Critical review, Construction and
954 Building Materials 260 (2020) 119889. doi:10.1016/j.conbuildmat.20
955 20.119889.
- 956 [54] H. Nguyen, T. Vu, T. P. Vo, H.-T. Thai, Efficient machine learning models
957 for prediction of concrete strengths, Construction and Building Materials
958 266 (2021) 120950. doi:10.1016/j.conbuildmat.2020.120950.
- 959 [55] M.-C. Kang, D.-Y. Yoo, R. Gupta, Machine learning-based prediction
960 for compressive and flexural strengths of steel fiber-reinforced concrete,
961 Construction and Building Materials 266 (2021) 121117. doi:10.1016/
962 j.conbuildmat.2020.121117.
- 963 [56] M. Su, Q. Zhong, H. Peng, S. Li, Selected machine learning approaches
964 for predicting the interfacial bond strength between FRPs and concrete,
965 Construction and Building Materials 270 (2021) 121456. doi:10.1016/
966 j.conbuildmat.2020.121456.
- 967 [57] O. B. Olalusi, P. O. Awoyera, Shear capacity prediction of slender rein-
968 forced concrete structures with steel fibers using machine learning, Engi-

- neering Structures 227 (2021) 111470. doi:10.1016/j.engstruct.2020
.111470.
- [58] H. D. Nguyen, G. T. Truong, M. Shin, Development of extreme gradient boosting model for prediction of punching shear resistance of r/c interior slabs, Engineering Structures 235 (2021) 112067. doi:10.1016/j.engstruct.2021.112067.
- [59] D.-C. Feng, W.-J. Wang, S. Mangalathu, G. Hu, T. Wu, Implementing ensemble learning methods to predict the shear strength of RC deep beams with/without web reinforcements, Engineering Structures 235 (2021) 111979. doi:10.1016/j.engstruct.2021.111979.
- [60] J. Rahman, K. S. Ahmed, N. I. Khan, K. Islam, S. Mangalathu, Data-driven shear strength prediction of steel fiber reinforced concrete beams using machine learning approach, Engineering Structures 233 (2021) 111743. doi:10.1016/j.engstruct.2020.111743.
- [61] D.-C. Feng, B. Cetiner, M. R. Azadi Kakavand, E. Taciroglu, Data-driven approach to predict the plastic hinge length of reinforced concrete columns and its application, Journal of Structural Engineering 147 (2) (2021) 04020332. doi:10.1061/(ASCE)ST.1943-541X.0002852.
- [62] S. Mangalathu, H. Shin, E. Choi, J.-S. Jeon, Explainable machine learning models for punching shear strength estimation of flat slabs without transverse reinforcement, Journal of Building Engineering 39 (2021) 102300. doi:10.1016/j.jobe.2021.102300.
- [63] S.-H. Hwang, S. Mangalathu, J. Shin, J.-S. Jeon, Machine learning-based approaches for seismic demand and collapse of ductile reinforced concrete building frames, Journal of Building Engineering 34 (2021) 101905. doi:10.1016/j.jobe.2020.101905.

- 995 [64] B. Fu, D.-C. Feng, A machine learning-based time-dependent shear
996 strength model for corroded reinforced concrete beams, Journal of Build-
997 ing Engineering 36 (2021) 102118. doi:10.1016/j.jobe.2020.102118.
- 998 [65] Z. Liu, A. Guo, Empirical-based support vector machine method for
999 seismic assessment and simulation of reinforced concrete columns us-
1000 ing historical cyclic tests, Engineering Structures 237 (2021) 112141.
1001 doi:10.1016/j.engstruct.2021.112141.
- 1002 [66] V. V. Degtyarev, Machine learning models for predicting bond strength
1003 of deformed bars in concrete, ACI Structural Journal (in press).
- 1004 [67] M. Kumar, N. Yadav, Buckling analysis of a beam–column using multi-
1005 layer perceptron neural network technique, Journal of the Franklin Insti-
1006 tute 350 (10) (2013) 3188–3204. doi:10.1016/j.jfranklin.2013.07.
1007 016.
- 1008 [68] A. Tashakori, H. Adeli, Optimum design of cold-formed steel space struc-
1009 tures using neural dynamics model, Journal of Constructional Steel Re-
1010 search 58 (2002) 1545–1566. doi:10.1016/S0143-974X(01)00105-5.
- 1011 [69] I. H. Guzelbey, A. Cevik, A. Erklig, Prediction of web crippling strength
1012 of cold-formed steel sheetings using neural networks, Journal of Construc-
1013 tional Steel Research 62 (10) (2006) 962–973. doi:10.1016/j.jcsr.200
1014 6.01.008.
- 1015 [70] M. Pala, A new formulation for distortional buckling stress in cold-formed
1016 steel members, Journal of Constructional Steel Research 62 (7) (2006)
1017 716–722. doi:10.1016/j.jcsr.2005.09.011.
- 1018 [71] M. Pala, N. Caglar, A parametric study for distortional buckling stress on

- 1019 cold-formed steel using a neural network, Journal of Constructional Steel
1020 Research 63 (5) (2007) 686–691. doi:10.1016/j.jcsr.2006.07.005.
- 1021 [72] M. D’Aniello, E. M. Güneyisi, R. Landolfo, K. Mermerdas, Analytical
1022 prediction of available rotation capacity of cold-formed rectangular and
1023 square hollow section beams, Thin-Walled Structures 77 (2014) 141–152.
1024 doi:10.1016/j.tws.2013.09.015.
- 1025 [73] S. Lee, T. P. Vo, H.-T. Thai, J. Lee, V. Patel, Strength prediction of
1026 concrete-filled steel tubular columns using Categorical Gradient Boosting
1027 algorithm, Engineering Structures 238 (2021) 112109. doi:10.1016/j.
1028 engstruct.2021.112109.
- 1029 [74] M. A. B. Kabir, A. S. Hasan, A. M. Billah, Failure mode identification
1030 of column base plate connection using data-driven machine learning tech-
1031 niques, Engineering Structures 240 (2021) 112389. doi:10.1016/j.engs
1032 truct.2021.112389.
- 1033 [75] Y. Xu, B. Zheng, M. Zhang, Capacity prediction of cold-formed stainless
1034 steel tubular columns using machine learning methods, Journal of Con-
1035 structional Steel Research 182 (2021) 106682. doi:10.1016/j.jcsr.202
1036 1.106682.
- 1037 [76] X. Guan, H. Burton, M. Shokrabadi, Z. Yi, Seismic drift demand esti-
1038 mation for steel moment frame buildings: From mechanics-based to data-
1039 driven models, Journal of Structural Engineering 147 (6) (2021) 04021058.
1040 doi:10.1061/(ASCE)ST.1943-541X.0003004.
- 1041 [77] V. V. Degtyarev, Neural networks for predicting shear strength of CFS
1042 channels with slotted webs, Journal of Constructional Steel Research 177
1043 (2021) 106443. doi:10.1016/j.jcsr.2020.106443.

- 1044 [78] V. V. Degtyarev, M. Z. Naser, Boosting machines for predicting shear
1045 strength of CFS channels with staggered web perforations, *Structures* 34
1046 (2021) 3391–3403. doi:[10.1016/j.istruc.2021.09.060](https://doi.org/10.1016/j.istruc.2021.09.060).
- 1047 [79] M. Z. Naser, V. Kodur, H.-T. Thai, R. Hawileh, J. Abdalla, V. V. Degt-
1048 yarev, Structuresnet and firenet: Benchmarking databases and machine
1049 learning algorithms in structural and fire engineering domains, *Journal of
1050 Building Engineering* 44 (2021) 102977. doi:[10.1016/j.jobe.2021.10.297](https://doi.org/10.1016/j.jobe.2021.10.297).
- 1051 [80] V. V. Degtyarev, Predicting shear strength of cfs channels with slotted
1052 webs by machine learning models, *Architecture, Structures and Construc-
1053 tion* doi:[10.1007/s44150-021-00001-0](https://doi.org/10.1007/s44150-021-00001-0).
- 1054 [81] Y. Sharifi, A. Moghboli, M. Hosseinpour, H. Sharifi, Neural networks for
1055 lateral torsional buckling strength assessment of cellular steel I-beams,
1056 *Advances in Structural Engineering* 22 (9) (2019) 2192–2202. doi:[10.177/1369433219836176](https://doi.org/10.177/1369433219836176).
- 1057 [82] AS 4100:1990. Steel structures, Standards Association of Australia, Syd-
1058 ney, Australia, 1990.
- 1059 [83] M. Abambres, K. Rajana, K. D. Tsavdaridis, T. P. Ribeiro, Neural
1060 network-based formula for the buckling load prediction of I-section cellular
1061 steel beams, *Computers* 8 (1) (2019) 2. doi:[10.3390/computers8010002](https://doi.org/10.3390/computers8010002).
- 1062 [84] F. P. V. Ferreira, R. Shamass, V. Limbachiya, K. D. Tsavdaridis, C. H.
1063 Martins, Lateral–torsional buckling resistance prediction model for steel
1064 cellular beams generated by Artificial Neural Networks (ANN), *Thin-
1065 Walled Structures* 170 (2022) 108592. doi:[10.1016/j.tws.2021.108592](https://doi.org/10.1016/j.tws.2021.108592).
- 1066 [85] V. Limbachiya, R. Shamass, Application of artificial neural networks for
1067

- 1069 web-post shear resistance of cellular steel beams, *Thin-Walled Structures*
1070 161 (2021) 107414. doi:doi.org/10.1016/j.tws.2020.107414.
- 1071 [86] S. Lundberg, S.-I. Lee, A unified approach to interpreting model predic-
1072 tions, arXiv preprint arXiv:1705.07874.
- 1073 [87] S. Fares, J. Coulson, D. Dinehart, Design Guide 31: Castellated and Cel-
1074 lular Beam Design, American Institute of Steel Construction, Chicago, IL,
1075 USA, 2016.
- 1076 [88] T. Hastie, R. Tibshirani, J. Friedman, The elements of statistical learn-
1077 ing: data mining, inference, and prediction, Springer Science & Business
1078 Media, 2009.
- 1079 [89] A. Géron, Hands-on machine learning with Scikit-Learn, Keras, and Ten-
1080 sorFlow: Concepts, tools, and techniques to build intelligent systems,
1081 O'Reilly Media, 2019.
- 1082 [90] L. Breiman, Random forests, *Machine learning* 45 (1) (2001) 5–32. doi:
1083 [10.1023/A:1010933404324](https://doi.org/10.1023/A:1010933404324).
- 1084 [91] T. K. Ho, Random decision forests, in: Proceedings of 3rd international
1085 conference on document analysis and recognition, Vol. 1, IEEE, 1995, pp.
1086 278–282. doi:[10.1109/ICDAR.1995.598994](https://doi.org/10.1109/ICDAR.1995.598994).
- 1087 [92] J. H. Friedman, Greedy function approximation: a gradient boosting ma-
1088 chine, *Annals of Statistics* (2001) 1189–1232.
- 1089 [93] F. Pedregosa, G. Varoquaux, A. Gramfort, V. Michel, B. Thirion,
1090 O. Grisel, M. Blondel, P. Prettenhofer, R. Weiss, V. Dubourg, et al.,
1091 Scikit-learn: Machine learning in Python, *the Journal of Machine Learn-
1092 ing Research* 12 (2011) 2825–2830.

- 1093 [94] T. Chen, C. Guestrin, XGBoost: A scalable tree boosting system, in:
1094 Proceedings of the 22nd ACM SIGKDD international conference on knowledge
1095 discovery and data mining, 2016, pp. 785–794. doi:10.1145/2939672.
1096 2939785.
- 1097 [95] G. Ke, Q. Meng, T. Finley, T. Wang, W. Chen, W. Ma, Q. Ye, T.-Y. Liu,
1098 LightGBM: A highly efficient gradient boosting decision tree, Advances
1099 in Neural Information Processing Systems 30 (2017) 3146–3154.
- 1100 [96] A. V. Dorogush, V. Ershov, A. Gulin, CatBoost: gradient boosting with
1101 categorical features support, arXiv preprint arXiv:1810.11363.
- 1102 [97] M. Naser, A. Alavi, Insights into performance fitness and error metrics for
1103 machine learning, arXiv preprint arXiv:2006.00887.
- 1104 [98] M. Z. Naser, An engineer’s guide to eXplainable Artificial Intelligence and
1105 Interpretable Machine Learning: Navigating causality, forced goodness,
1106 and the false perception of inference, Automation in Construction 129
1107 (2021) 103821. doi:10.1016/j.autcon.2021.103821.
- 1108 [99] B. Peleg, P. Sudhölter, Introduction to the theory of cooperative games,
1109 Vol. 34, Springer Science & Business Media, 2007.
- 1110 [100] BS EN 1993-1-5: 2006. Design of steel structures—Part 1-5 Plated struc-
1111 tural elements, British Standards Institution, London, UK, 2006.
- 1112 [101] ANSI/AISC 360-16. Specification for structural steel buildings, American
1113 Institute of Steel Construction, Chicago, Illinois, USA, 2016.
- 1114 [102] C. Topkaya, S. Şahin, A comparative study of AISC-360 and EC3 strength
1115 limit states, International Journal of Steel Structures 11 (1) (2011) 13–27.
1116 doi:10.1007/S13296-011-1002-x.

₁₁₁₇ [103] S. J. Hicks, R. M. Lawson, J. W. Rackham, P. Fordham, Comparative
₁₁₁₈ structure cost of modern commercial buildings, Steel Construction Insti-
₁₁₁₉ tute, 2004.