

Lecture 9

Note Title

01-04-2021

Impulse-momentum relations

Impulse \underline{I} of a force \underline{F} & its angular impulse $\underline{I}_{\text{ang } A}$ about a point A for time interval (t_1, t_2) are defined by

$$\underline{I}(t_1, t_2) = \int_{t_1}^{t_2} \underline{F}(t) dt$$

$$\underline{I}_{\text{ang } A}(t_1, t_2) = \int_{t_1}^{t_2} \underline{M}_A(t) dt$$

Instantaneous impulse at t_1 if

$$\underline{I}(t_1) = \lim_{t_1 \rightarrow t_2} \int_{t_1}^{t_2} \underline{F}(t) dt \neq 0$$

$$\underline{I}_{\text{ang } A}(t_1) = \lim_{t_1 \rightarrow t_2} \int_{t_1}^{t_2} \underline{M}_A(t) dt \neq 0$$

Euler's 1st axiom \Rightarrow

$$I(t_1, t_2) = \int_{t_1}^{t_2} \underline{F} dt = \int_{t_1}^{t_2} \dot{\underline{p}} dt = \int_{\underline{p}(t_1)}^{\underline{p}(t_2)} d\underline{p}$$

$$\Rightarrow I(t_1, t_2) = \underline{p}(t_2) - \underline{p}(t_1) = \Delta \underline{p} = m \Delta \underline{v}_c = \sum_i m_i \Delta \underline{v}_{ci}$$

Impulse of external force \underline{F} equals the change in momentum

Inst. Impulse \Rightarrow

$$\underline{I}(t_1) = \Delta \underline{p} = \underline{p}(t_1^+) - \underline{p}(t_1^-) = m \Delta \underline{v}_c = \sum m_i \Delta \underline{v}_{c_i}$$

\rightarrow all changes are instantaneous (there is no change in position)

if $I(t_1, t_2) = 0 \Rightarrow$ conservation of momentum

$$\underline{p}(t_2) = \underline{p}(t_1) ; \underline{v}_c(t_2) = \underline{v}_c(t_1) ; \sum m_i \underline{v}_{c_i}(t_2) = \sum m_i \underline{v}_{c_i}(t_1)$$

If a particular component δ_i impulse is zero, then the corresponding component of momentum is conserved

Angular impulse - moment of momentum relations

All wrt Inertial frame I $\underline{a}_A \equiv \underline{a}_A|_I$ etc

If A is a point such that $\underline{a}_A = 0$ or $A \equiv C$ or $\underline{a}_A \parallel \underline{AC}$

$$\Rightarrow \underline{M}_A = \dot{\underline{H}}_A$$

$$\underline{I}_{ang A}(t_1, t_2) = \int_{t_1}^{t_2} \underline{M}_A dt = \int_{\underline{H}_A(t_1)}^{\underline{H}_A(t_2)} d\underline{H}_A$$

$$= \underline{H}_A(t_2) - \underline{H}_A(t_1) = \Delta \underline{H}_A$$

External angular impulse about A equals the change in moment of momentum about A

— If $\underline{I}_{ang A}(t_1, t_2) = 0 \Rightarrow$ conservation of moment of momentum about A $\underline{H}_A(t_2) = \underline{H}_A(t_1)$

— If $\underline{M}_A \equiv 0$ then $\underline{H}_A(t) = \underline{H}_A^0$

If A is fixed in I; If components of $\underline{I}_{ang A}(t_1, t_2)$

along a fixed direction is zero then H_A along that direction is conserved

— If inst ang impulse is considered, no change in configuration; but a change in \underline{H}_A or \underline{H}_C or \underline{H}_O
A! such that $\underline{a}_A = 0$, $a_A \parallel \underline{CA}$ or $\underline{CA} = 0$

0 - fixed in I

$$\underline{I}_{\text{ang } A}(t_1) = \Delta H_c, \quad \underline{I}_{\text{ang } 0}(t_1) = \Delta H_0$$

$$\underline{I}_{\text{ang } A}(t_1) = \Delta H_A$$

BUT $\underline{I}_{\text{ang } B}(t_1) \neq \Delta H_B$ for general B

Work energy relation for centre of mass C

$$\begin{aligned}\underline{F} \cdot \underline{v}_{C|I} &= m \underline{a}_{C|I} \cdot \underline{v}_{C|I} = \frac{d}{dt} \left[\frac{1}{2} m \underline{v}_{C|I} \cdot \underline{v}_{C|I} \right]_{|I} \\ &= \frac{d}{dt} \left[\frac{1}{2} m v_{C|I}^2 \right]_{|I}\end{aligned}$$

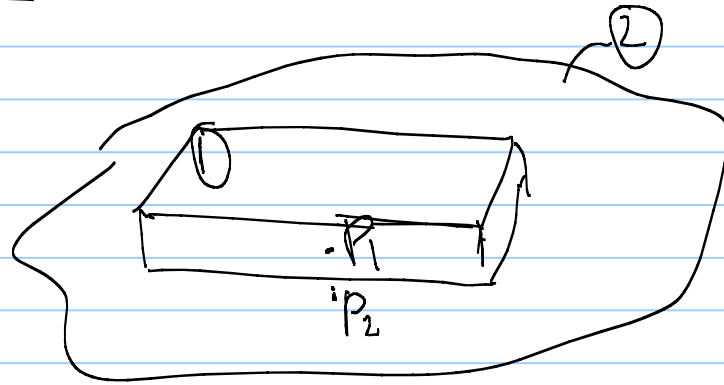
$$\Rightarrow \dot{T}_C = \dot{W}^* \quad (T_{C2} - T_{C1} = W_{1-2}^*)$$

$\dot{W}^* = \underline{F} \cdot \underline{v}_C$ = rate of work done by forces as if acting at C [≠ \dot{W} in general]

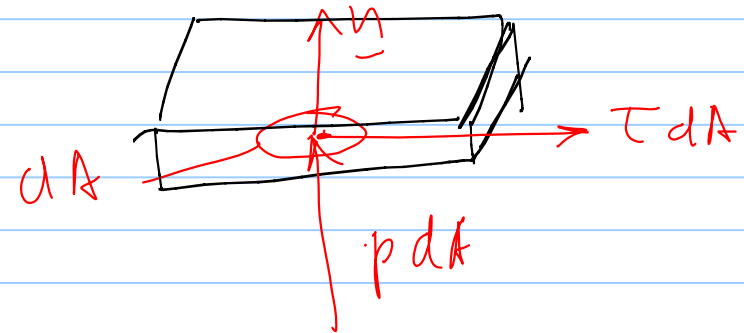
$T_C = \frac{1}{2} m v_{C|I}^2$ - kinetic energy as if all mass was

concentrated at c [$\neq T$ in general]

Axiom of Coulomb friction



$P_1 - P_2$ in contact



Normal force $\rightarrow p dA$

tangential force $\rightarrow \tau dA$

Coulomb's axiom of friction

for no slip bet'n (1) & (2) P_1 & P_2 $\tau < \mu_s p$

direction & magnitude
of τ are determined
from the eqns of motion.

for impending slip bet'n P_1 and P_2

$\tau = \mu_s p$ τ directed opposite to the
Component of $\underline{p}_{P_1 P_2}$ in the tangent plane $\perp \underline{n}$

for slip bet'n P_1 and P_2 ,

$\tau = \mu_k p$ directed
opposite to $\underline{v}_{P_1 P_2}$

μ_s — static coeff of friction

μ_k — dynamic coeff of friction.

If the contact area is a plane then $N = \int p dA$
 $F = \int \tau dA$

For no slip

$$F < \mu_s N$$

imp slip

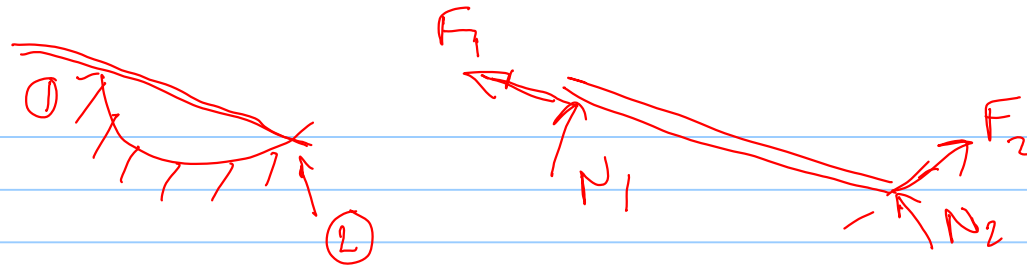
$$F = \mu_s N$$

Slip

$$F = \mu_k N$$

} (X)

Discrete point of contact? (X) are valid



$$\underline{F} \rightarrow \parallel \underline{e}_t$$

$$\underline{N} \rightarrow n_1 \underline{e}_n + n_2 \underline{e}_p$$

Free body diagrams

To apply Euler's axioms

- ① The system should be well identified and its sketch drawn in isolation from its surroundings
- ② External forces and moments exerted by the

Surroundings on the system should be drawn on the sketch

Such a diagram is called the Free body diagram (FBD)

Internal forces & internal moments should not be shown on FBD.

Equations of equilibrium

If a system is in equilibrium, then for its every part,

$$\underline{F} = 0, \quad \underline{M}_A = 0$$

Proof

If 0 is fixed point in I

$$\underline{v}_p|_I = 0, \quad \forall t$$

$$\underline{P}|_I = \int \underline{r}_{p|I} d\omega = 0$$

$$\underline{H}_0|_I = \int \underline{r}_{p0|I} \times \underline{v}_{p0|I} d\omega = 0 \quad \forall t$$

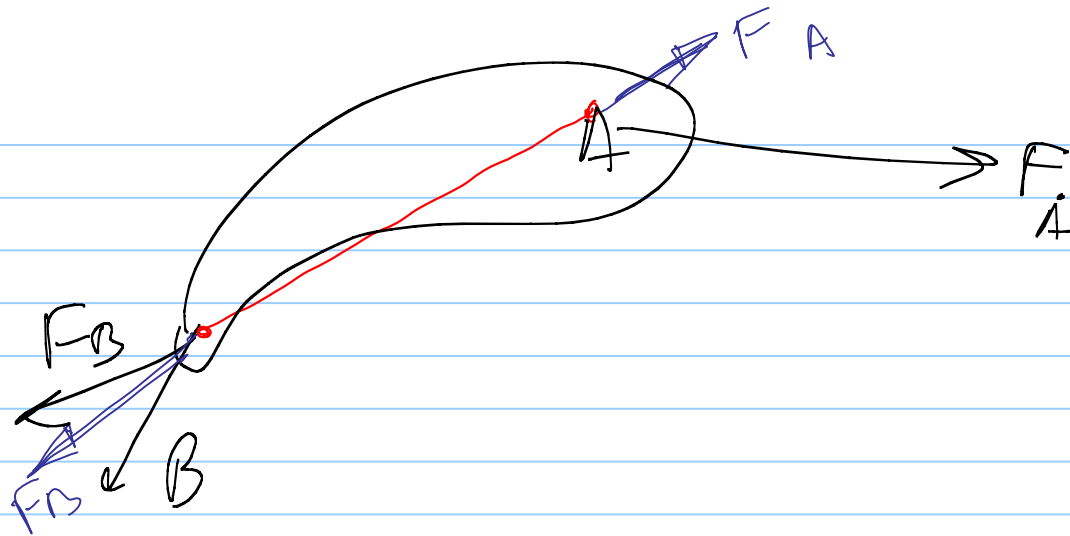
Euler's Axioms $\Rightarrow \quad \underline{F} = \dot{\underline{P}}|_I = 0$

$$\underline{M}_0 = \underline{H}_0|_I = 0 \Rightarrow \underline{M}_A = \underline{M}_0 + \underline{r}_{0A} \times \underline{F} = 0$$

Necessary but not sufficient for equilibrium.

Two force member

A member under the action of
two forces only (no moments)



For equilibrium

$$\underline{F_A} + \underline{F_B} = 0$$

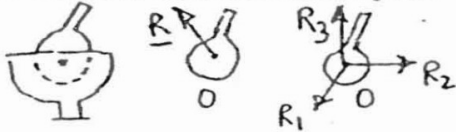
abt A $\underline{r_{BA}} \times \underline{F_B} = 0 \Rightarrow F_B$ is thru A along AB

abt B $\underline{r_{AB}} \times \underline{F_A} = 0$ F_A is thru B along AB

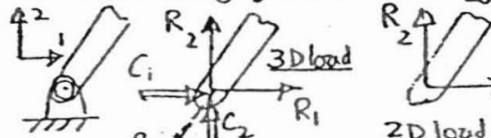
$$\underline{F_A} = -\underline{F_B}$$

Forces have equal magnitudes, opposite directions and act along the line joining their points of application

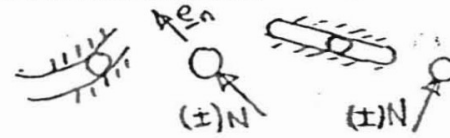
a. Smooth ball and socket joint



b. Smooth hinge joint with axis e_3



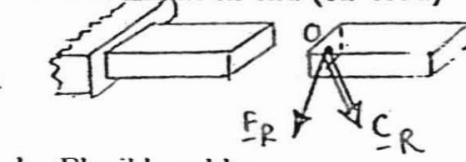
c. Pin in smooth slot



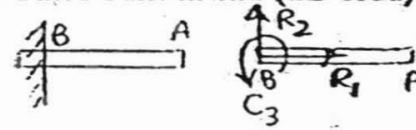
d. Smooth roller support



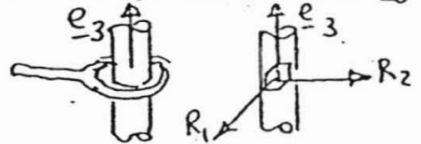
e. Fixed built-in end (3D load)



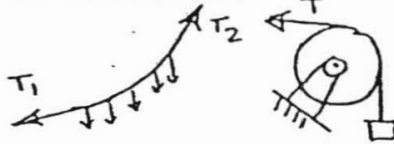
f. Fixed built-in end (2D load)



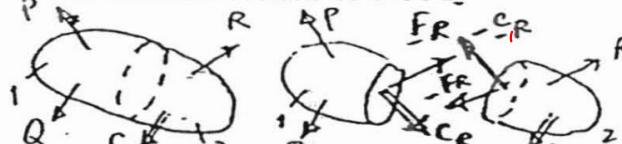
g. Smooth eye bolt with axis e_3



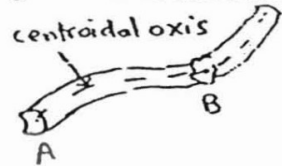
h. Flexible cable



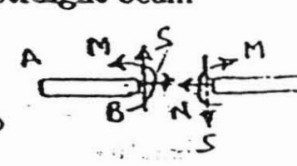
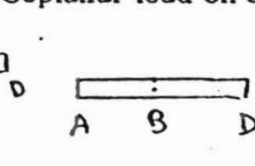
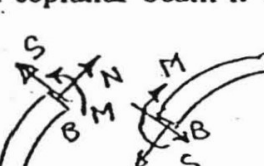
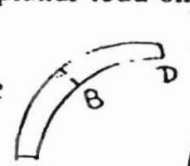
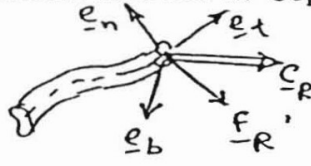
i. Internal section of a body



j. Internal force resultants in a bar



k. Coplanar load on coplanar beam l. Coplanar load on straight beam



FBD's of front wheel assembly (m_1), rear wheel assembly (m_2), chassis (m_3), and the complete road-roller with driving torque M on the rear wheels, assuming no slip, are given in Fig. 2.19:

