

# Electromagnetic Waves in Linear (Dielectric) Media

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- Introduction to Electrodynamics, David J. Griffiths (3rd ed.)
  - Chapter 9, 9.3 Electromagnetic Waves in Linear Media

# Linear Dielectric Media

## When is a dielectric medium called linear?

- A dielectric medium is called linear if its polarization is linearly proportional to the (weak) electric field

$$\mathbf{P} = \epsilon_0 \chi_e \mathbf{E}$$

- In the nonlinear regime, higher order terms become important and are useful for several optical applications.

$$P = \epsilon_0 \chi_e^{(1)} E + \epsilon_0 \chi_e^{(2)} E^2 + \epsilon_0 \chi_e^{(3)} E^3 + \dots$$

- The second order term ( $\chi_e^{(2)} E^2$ ) is responsible for second harmonic generation etc.
- The third order term ( $\chi_e^{(3)} E^3$ ) is responsible for third harmonic generation, intensity dependent refractive index etc.

# Linear Dielectric Media

## When is a dielectric medium called linear?

- Optical fibers are well known examples where third order nonlinearity is at play.
- For linear dielectrics the electric displacement is also a linear function of electric field.

$$\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P} = \epsilon_0(1 + \chi_e) \mathbf{E} = \epsilon_0 \epsilon_r \mathbf{E} = \epsilon \mathbf{E}$$

where  $\epsilon_r = 1 + \chi_e = \epsilon/\epsilon_0$  is called the relative permittivity or dielectric constant of the material.

- Glass is a very common example of a linear dielectric material, other examples are dilute gases.

# Maxwell's Equations in Matter: Recap

- Maxwell's equations in a non-conducting medium read,

$$\nabla \cdot \mathbf{D} = 0$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = - \frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t}$$

# Maxwell's Equations in Matter: Recap

- For a linear medium  $\mathbf{D} = \epsilon \mathbf{E}$  and  $\mathbf{H} = \mathbf{B}/\mu$ , so the Maxwell's equations can be written as

$$\nabla \cdot \mathbf{E} = 0$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = - \frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{B} = \mu \epsilon \frac{\partial \mathbf{E}}{\partial t}$$

# Electromagnetic Wave Equation

- Now if we take curl of the curl equation of  $\mathbf{E}$  (Faraday's law), and use the Gauss's law

$$\nabla \times (\nabla \times \mathbf{E}) = \nabla \times \left( -\frac{\partial \mathbf{B}}{\partial t} \right)$$

$$\nabla (\nabla \cdot \mathbf{E}) - \nabla^2 \mathbf{E} = -\frac{\partial}{\partial t} (\nabla \times \mathbf{B})$$

$$\nabla^2 \mathbf{E} = \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) \mathbf{E} = \mu\epsilon \frac{\partial^2 \mathbf{E}}{\partial t^2}$$

- Similarly, one can derive the wave equation for magnetic field  $\mathbf{B}$  (HW).

# Electromagnetic Wave Equation

- On comparison with the standard form of wave equation, we can identify the speed of the propagation of an electromagnetic wave in a linear medium as

$$v = \frac{1}{\sqrt{\mu\epsilon}} = \frac{c}{\sqrt{\mu\epsilon/\mu_0\epsilon_0}} = \frac{c}{n}$$

where  $n = \sqrt{\epsilon\mu/\epsilon_0\mu_0}$  is called the refractive index of the medium.



# Electromagnetic Wave Equation

- For most materials  $\mu \cong \mu_0$  so

$$n \cong \sqrt{\epsilon/\epsilon_0} = \sqrt{\epsilon_r} \Rightarrow v = \frac{c}{\sqrt{\epsilon_r}}$$

- $\epsilon_r$  is called the dielectric constant of the medium and is mostly greater than one.
- Therefore EM waves have a speed less than 'c' while traveling in a medium.

# Plane Wave Solutions

- The plane wave solutions in the complex notation can be written as for the vacuum case:

$$\tilde{\mathbf{E}}(z, t) = \tilde{\mathbf{E}}_0 e^{i(kz - \omega t)}$$

$$\tilde{\mathbf{B}}(z, t) = \tilde{\mathbf{B}}_0 e^{i(kz - \omega t)}$$

where  $\tilde{\mathbf{E}}_0 = \mathbf{E}_0 e^{i\delta}$  and  $\tilde{\mathbf{B}}_0 = \mathbf{B}_0 e^{i\delta}$ .

# Plane Wave Solutions

- The solutions must satisfy  $\nabla \cdot \mathbf{E} = 0$  and  $\nabla \cdot \mathbf{B} = 0$ .
- This condition leads to the following

$$\hat{\mathbf{k}} \cdot \mathbf{E} = 0; \hat{\mathbf{k}} \cdot \mathbf{B} = 0$$

- Electromagnetic waves are transverse waves.
- Now from Faraday's law

$$\nabla \times \tilde{\mathbf{E}} = -\frac{\partial \tilde{\mathbf{B}}}{\partial t}$$

one obtains  $\tilde{\mathbf{B}}_0 = \frac{k}{\omega} (\hat{\mathbf{k}} \times \tilde{\mathbf{E}}_0) = \frac{1}{v} (\hat{\mathbf{k}} \times \tilde{\mathbf{E}}_0)$

- Fields  $\mathbf{E}$  and  $\mathbf{B}$  are mutually perpendicular to each other.

# Electromagnetic Plane Waves in Linear Media

To summarize the characteristics of EM plane waves in linear media

- They travel in the medium with a speed less than the speed of light.
- They are transverse waves as  $\hat{k} \cdot \mathbf{E} = \hat{k} \cdot \mathbf{B} = 0$  for a plane EM wave propagating in arbitrary direction.
- Electric and magnetic fields associated with an EM wave in a linear media are perpendicular to each other.

# Energy, Momentum and Intensity of EM Waves

- One can obtain the energy density, momentum density as well as intensity of EM wave in a linear media, by making following substitutions in the vacuum case expressions.

$$\epsilon_0 \Rightarrow \epsilon; \mu_0 \Rightarrow \mu; c \Rightarrow v \quad (1)$$

- The averaged energy density for an EM wave in a linear medium

$$\langle u \rangle = \frac{1}{2} \epsilon E_0^2$$

- Similarly, the Poynting vector will be

$$\begin{aligned} \mathbf{S} &= \frac{1}{\mu} (\mathbf{E} \times \mathbf{B}) \\ &= v \epsilon E_0^2 \cos^2(kz - \omega t + \delta) \hat{z} \end{aligned}$$

# Energy, Momentum and Intensity of EM Waves

- The averaged momentum density

$$\langle p \rangle = \frac{1}{2v} \epsilon E_0^2 \hat{k}$$

- And the intensity of the EM wave

$$I = \langle S \rangle = \frac{1}{2} \epsilon v E_0^2$$

# Reflection and Transmission of EM Waves: Boundary Conditions

- The boundary conditions at the interface between two non-conducting linear dielectric media having permittivities  $\epsilon_1$  and  $\epsilon_2$ , and permeabilities  $\mu_1$  and  $\mu_2$ , respectively.

$$(i) \epsilon_1 E_1^\perp = \epsilon_2 E_2^\perp$$

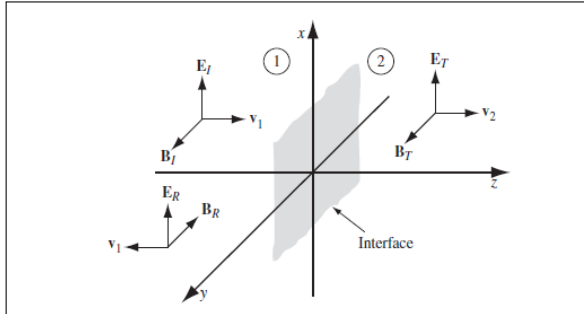
$$(ii) B_1^\perp = B_2^\perp$$

$$(iii) \mathbf{E}_1^\parallel = \mathbf{E}_2^\parallel$$

$$(iv) \frac{1}{\mu_1} \mathbf{B}_1^\parallel = \frac{1}{\mu_2} \mathbf{B}_2^\parallel$$

# Reflection+Transmission of EM Waves: Normal Incidence

- Consider a plane wave of frequency  $\omega$ , having polarization in x-direction, is traveling in z-direction in a linear medium '1'. It encounters an interface (in xy-plane) between medium '1' and another linear medium '2'.
- Depending on the refractive indices of two media, a part of the incident wave energy gets reflected while the remaining part gets transmitted.





# Reflection+Transmission of EM Waves: Normal Incidence

- The electric and magnetic fields for incident, reflected and transmitted waves:

*Incident Wave*

$$\tilde{\mathbf{E}}_I(z, t) = \tilde{E}_{0I} e^{i(k_1 z - \omega t)} \hat{x}; \quad \tilde{\mathbf{B}}_I(z, t) = \frac{\tilde{E}_{0I}}{v_1} e^{i(k_1 z - \omega t)} \hat{y}$$

*Reflected Wave*

$$\tilde{\mathbf{E}}_R(z, t) = \tilde{E}_{0R} e^{i(-k_1 z - \omega t)} \hat{x}; \quad \tilde{\mathbf{B}}_R(z, t) = -\frac{\tilde{E}_{0R}}{v_1} e^{i(-k_1 z - \omega t)} \hat{y}$$

*Transmitted Wave*

$$\tilde{\mathbf{E}}_T(z, t) = \tilde{E}_{0T} e^{i(k_2 z - \omega t)} \hat{x}; \quad \tilde{\mathbf{B}}_T(z, t) = \frac{\tilde{E}_{0T}}{v_2} e^{i(k_2 z - \omega t)} \hat{y}$$

# Reflection+Transmission of EM Waves: Normal Incidence

- At the interface electric and magnetic fields will satisfy following boundary conditions:

$$E_1^{\parallel} = E_2^{\parallel}$$
$$\frac{B_1^{\parallel}}{\mu_1} = \frac{B_2^{\parallel}}{\mu_2}$$

- The field components normal to the interface plane are zero in case of normal incidence.
- In terms of incident, reflected and transverse components, the above conditions read

$$\tilde{E}_{0I} + \tilde{E}_{0R} = \tilde{E}_{0T}$$
$$\frac{1}{\mu_1}(\tilde{B}_{0I} + \tilde{B}_{0R}) = \frac{1}{\mu_2}\tilde{B}_{0T}$$

# Reflection+Transmission of EM Waves: Normal Incidence

- Writing B in terms of E

$$\frac{1}{\mu_1} \left( \frac{\tilde{E}_{0I}}{v_1} - \frac{\tilde{E}_{0R}}{v_1} \right) = \frac{1}{\mu_2 v_2} \tilde{E}_{0T}$$
$$\Rightarrow \tilde{E}_{0I} - \tilde{E}_{0R} = \frac{\mu_1 v_1}{\mu_2 v_2} \tilde{E}_{0T} = \beta \tilde{E}_{0T}$$

where

$$\beta = \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{\mu_1 n_2}{\mu_2 n_1}$$

- Solving for electric field components one obtains

$$\tilde{E}_{0R} = \left( \frac{1 - \beta}{1 + \beta} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2}{1 + \beta} \right) \tilde{E}_{0I}$$

# Reflection+Transmission of EM Waves: Normal Incidence

- As for most of the linear media  $\mu \approx \mu_0$ , therefore

$$\beta = \frac{\mu_1 v_1}{\mu_2 v_2} \approx \frac{\mu_0 v_1}{\mu_0 v_2} = \frac{v_1}{v_2} = \frac{n_2}{n_1}$$

- Therefore, we can also write the reflected and transmitted field components in terms of  $v_1$  and  $v_2$  as follows

$$\tilde{E}_{0R} = \left( \frac{v_2 - v_1}{v_2 + v_1} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2v_2}{v_2 + v_1} \right) \tilde{E}_{0I}$$

- Also in terms of refractive indices of the two media,  $n_1$  and  $n_2$

$$\tilde{E}_{0R} = \left( \frac{n_1 - n_2}{n_1 + n_2} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2n_1}{n_1 + n_2} \right) \tilde{E}_{0I}$$

# Reflection+Transmission of EM Waves: Normal Incidence

$$\tilde{E}_{0R} = \left( \frac{v_2 - v_1}{v_2 + v_1} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2v_2}{v_2 + v_1} \right) \tilde{E}_{0I}$$

## Phases of Reflected and Transmitted Components

- *Transmitted wave always remains in phase with the incident wave.*
- *Reflected wave is in phase with the incident wave if  $v_2 > v_1$  (or  $n_1 > n_2$ , wave traveling from denser to rarer medium).*
- *Reflected wave is  $180^\circ$  out of phase with the incident wave if  $v_1 > v_2$  (or  $n_2 > n_1$ , wave traveling from rarer to denser medium).*

# Reflection+Transmission of EM Waves: Normal Incidence

## Reflection and Transmission Coefficients

- Reflection coefficient is the ratio of the reflected intensity to the incident intensity, i.e.

$$R = \frac{I_R}{I_I} = \left( \frac{E_{0R}}{E_{0I}} \right)^2 = \left( \frac{n_1 - n_2}{n_1 + n_2} \right)^2$$

- Similarly, transmission coefficient is the ratio of the transmitted intensity to the incident intensity, i.e.

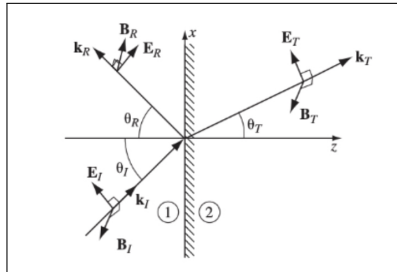
$$T = \frac{I_T}{I_I} = \left( \frac{\epsilon_2 v_2}{\epsilon_1 v_1} \right) \left( \frac{E_{0T}}{E_{0I}} \right)^2 = \frac{4n_1 n_2}{(n_1 + n_2)^2}$$

- It can be easily verified that as required by conservation of energy

$$R + T = 1$$

# Reflection+Transmission of EM Waves: Oblique Incidence

- Consider a plane wave of frequency  $\omega$ , incident at angle  $\theta_I$  to the normal of the interface between media '1' and '2'.
- x-z plane is the *plane of incidence* as it contains  $\mathbf{k}_I$ ,  $\mathbf{k}_R$ , and the normal to the interface ( $\hat{z}$ ).
- A part of the incident wave gets reflected and the remaining part gets refracted (transmitted at an angle different from the angle of incidence).



# Reflection+Transmission of EM Waves: Oblique Incidence

- The electric and magnetic fields for incident, reflected and transmitted waves:

*Incident Wave*

$$\tilde{\mathbf{E}}_I(\mathbf{r}, t) = \tilde{\mathbf{E}}_{0I} e^{i(\mathbf{k}_I \cdot \mathbf{r} - \omega t)}; \quad \tilde{\mathbf{B}}_I(\mathbf{r}, t) = \frac{1}{v_1} (\hat{\mathbf{k}}_I \times \tilde{\mathbf{E}}_I)$$

*Reflected Wave*

$$\tilde{\mathbf{E}}_R(\mathbf{r}, t) = \tilde{\mathbf{E}}_{0R} e^{i(\mathbf{k}_R \cdot \mathbf{r} - \omega t)}; \quad \tilde{\mathbf{B}}_R(\mathbf{r}, t) = \frac{1}{v_1} (\hat{\mathbf{k}}_R \times \tilde{\mathbf{E}}_R)$$

*Transmitted Wave*

$$\tilde{\mathbf{E}}_T(\mathbf{r}, t) = \tilde{\mathbf{E}}_{0T} e^{i(\mathbf{k}_T \cdot \mathbf{r} - \omega t)}; \quad \tilde{\mathbf{B}}_T(\mathbf{r}, t) = \frac{1}{v_2} (\hat{\mathbf{k}}_T \times \tilde{\mathbf{E}}_T)$$



# Reflection+Transmission of EM Waves: Oblique Incidence

- Now invariance of the frequency  $\omega$  leads to,

$$\omega = k_I v_1 = k_R v_1 = k_T v_2$$
$$\Rightarrow k_I = k_R = \frac{v_2}{v_1} k_T = \frac{n_1}{n_2} k_T$$

- And the electric field and magnetic field must satisfy appropriate boundary conditions at the interface between two media.

# Reflection+Transmission of EM Waves: Oblique Incidence

- Writing field components parallel and perpendicular to the interface,

$$(i) \quad \epsilon_1 \left( \tilde{E}_I^\perp + \tilde{E}_R^\perp \right) = \epsilon_2 \tilde{E}_T^\perp$$

$$(ii) \quad \tilde{B}_I^\perp + \tilde{B}_R^\perp = \tilde{B}_T^\perp$$

$$(iii) \quad \tilde{\mathbf{E}}_I^\parallel + \tilde{\mathbf{E}}_R^\parallel = \tilde{\mathbf{E}}_T^\parallel$$

$$(iv) \quad \frac{1}{\mu_1} \left( \tilde{\mathbf{B}}_I^\parallel + \tilde{\mathbf{B}}_R^\parallel \right) = \frac{1}{\mu_2} \tilde{\mathbf{B}}_T^\parallel$$

# Reflection+Transmission of EM Waves: Oblique Incidence

- Using the traveling wave form for incident, reflected, as well as transmitted components

$$\begin{aligned}\epsilon_1 \left( \tilde{E}_{I0}^{\perp} e^{i(\mathbf{k}_I \cdot \mathbf{r} - \omega t)} + \tilde{E}_{R0}^{\perp} e^{i(\mathbf{k}_R \cdot \mathbf{r} - \omega t)} \right) &= \epsilon_2 \tilde{E}_{T0}^{\perp} e^{i(\mathbf{k}_T \cdot \mathbf{r} - \omega t)} \\ \tilde{B}_{I0}^{\perp} e^{i(\mathbf{k}_I \cdot \mathbf{r} - \omega t)} + \tilde{B}_{R0}^{\perp} e^{i(\mathbf{k}_R \cdot \mathbf{r} - \omega t)} &= \tilde{B}_{T0}^{\perp} e^{i(\mathbf{k}_T \cdot \mathbf{r} - \omega t)} \\ \tilde{\mathbf{E}}_{I0}^{\parallel} e^{i(\mathbf{k}_I \cdot \mathbf{r} - \omega t)} + \tilde{\mathbf{E}}_{R0}^{\parallel} e^{i(\mathbf{k}_R \cdot \mathbf{r} - \omega t)} &= \tilde{\mathbf{E}}_{T0}^{\parallel} e^{i(\mathbf{k}_T \cdot \mathbf{r} - \omega t)} \\ \frac{1}{\mu_1} \left( \tilde{\mathbf{B}}_{I0}^{\parallel} e^{i(\mathbf{k}_I \cdot \mathbf{r} - \omega t)} + \tilde{\mathbf{B}}_{R0}^{\parallel} e^{i(\mathbf{k}_R \cdot \mathbf{r} - \omega t)} \right) &= \frac{1}{\mu_2} \tilde{\mathbf{B}}_{T0}^{\parallel} e^{i(\mathbf{k}_T \cdot \mathbf{r} - \omega t)}\end{aligned}$$

- They all seem to have a generic form, at  $z = 0$

$$() e^{i(\mathbf{k}_I \cdot \mathbf{r} - \omega t)} + () e^{i(\mathbf{k}_R \cdot \mathbf{r} - \omega t)} = () e^{i(\mathbf{k}_T \cdot \mathbf{r} - \omega t)}$$

# Reflection+Transmission of EM Waves: Oblique Incidence

- As boundary conditions must hold for all times at each point on the interface ( $z = 0$ ), the exponents must be equal, i.e.,

$$\begin{aligned}(\mathbf{k}_I \cdot \mathbf{r} - \omega t) &= (\mathbf{k}_R \cdot \mathbf{r} - \omega t) = (\mathbf{k}_T \cdot \mathbf{r} - \omega t) \\ \Rightarrow \mathbf{k}_I \cdot \mathbf{r} &= \mathbf{k}_R \cdot \mathbf{r} = \mathbf{k}_T \cdot \mathbf{r}\end{aligned}$$

- Incident, reflected and transmitted wave vectors lie in the same plane called the '*plane of incidence*'.

# Reflection+Transmission of EM Waves: Oblique Incidence

## Law of Reflection

- For incident and reflected wave,

$$\begin{aligned}\mathbf{k}_I \cdot \mathbf{r} &= \mathbf{k}_R \cdot \mathbf{r} \\ k_I \sin\theta_I &= k_R \sin\theta_R \\ \sin\theta_I &= \sin\theta_R\end{aligned}$$

$$\Rightarrow \boxed{\theta_I = \theta_R}$$

## Snell's Law of Refraction

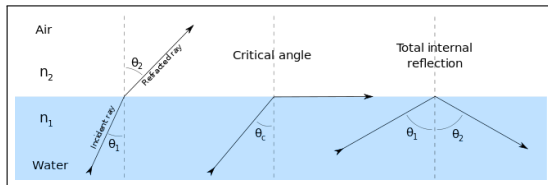
- For incident and transmitted wave,

$$\begin{aligned}\mathbf{k}_I \cdot \mathbf{r} &= \mathbf{k}_T \cdot \mathbf{r} \\ k_I \sin\theta_I &= k_T \sin\theta_T \\ n_1 \sin\theta_I &= n_2 \sin\theta_T\end{aligned}$$

$$\Rightarrow \boxed{\frac{\sin\theta_I}{\sin\theta_T} = \frac{n_2}{n_1}}$$

# Reflection+Transmission of EM Waves: Oblique Incidence

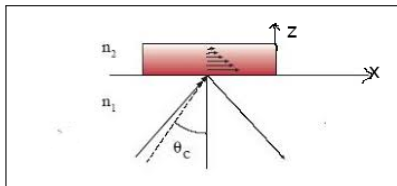
- Now from Snell's law  $\sin \theta_T = \frac{n_1}{n_2} \sin \theta_I$ .
- For  $n_1 > n_2$  if  $\theta_I = \sin^{-1}(n_2/n_1)$  then  $\sin \theta_T = 1$ , i.e.,  $\theta_T = \pi/2$ . This is called the **critical angle of incidence**,  $\theta_c$ .
- The wave incident at critical angle propagates along the interface between the two media.



# Reflection+Transmission of EM Waves: Oblique Incidence

- Also  $\cos^2\theta_T = 1 - \sin^2\theta_T = -\frac{n_1^2}{n_2^2} (\sin^2\theta_i - \sin^2\theta_c)$
- For  $\theta_i > \theta_c$ ,  $\cos \theta_T$  will become imaginary. The incident wave completely reflects into medium '1'. This is called '**Total internal reflection (TIR)**'.
- An evanescent wave is generated in the rarer medium '2', propagates along the interface and gets attenuated along z-direction <sup>1</sup>

$$\mathbf{E}_T = \mathbf{E}_{T0} e^{-\alpha z} e^{i(k_T x - \omega t)} \text{ where } \alpha = \frac{\omega}{c} \sqrt{n_1^2 \sin^2\theta_i - n_2^2}$$



<sup>1</sup>See OPTICS by Ajoy Ghatak (7<sup>th</sup> ed.), sec.23.6,23.9.

# Reflection+Transmission of EM Waves: Oblique Incidence

- Now to obtain the amplitudes of reflected and transmitted (refracted) wave for a given amplitude of the incident wave, let us consider an incident wave polarized in the plane of incidence (x-z plane).
- This means  $B^\perp = B_z = 0$ ,  $\mathbf{B}^\parallel = B_y \hat{y}$  and  $\mathbf{E}^\parallel = E_x \hat{x}$ .
- From boundary condition (i)

$$\begin{aligned}\epsilon_1 \left( \tilde{E}_{I0} + \tilde{E}_{R0} \right)_z &= \epsilon_2 \left( \tilde{E}_{T0} \right)_z \\ \epsilon_1 \left( -\tilde{E}_{I0} \sin \theta_i + \tilde{E}_{R0} \sin \theta_r \right) &= -\epsilon_2 \tilde{E}_{T0} \sin \theta_t \\ \Rightarrow \tilde{E}_{I0} - \tilde{E}_{R0} &= \beta \tilde{E}_{T0} \\ \text{where } \beta &= \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{\mu_1 n_2}{\mu_2 n_1}\end{aligned}$$



# Reflection+Transmission of EM Waves: Oblique Incidence

- Similarly from boundary condition (iii)

$$\begin{aligned}\left(\tilde{E}_{I0} + \tilde{E}_{R0}\right)_x &= \left(\tilde{E}_{T0}\right)_x \\ \left(\tilde{E}_{I0} \cos \theta_I + \tilde{E}_{R0} \cos \theta_R\right) &= \tilde{E}_{T0} \cos \theta_T \\ \Rightarrow \tilde{E}_{I0} + \tilde{E}_{R0} &= \alpha \tilde{E}_{T0} \\ \text{where } \alpha &= \frac{\cos \theta_T}{\cos \theta_I}\end{aligned}$$

# Reflection+Transmission of EM Waves: Oblique Incidence

## Fresnel's Equations

- Solving for electric field components

$$\tilde{E}_{0R} = \left( \frac{\alpha - \beta}{\alpha + \beta} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2}{\alpha + \beta} \right) \tilde{E}_{0I}$$

- These are called the Fresnel's equations<sup>a</sup> for the polarization in the plane of incidence.
- Similarly, one can obtain the following Fresnel's equations for the case of polarization perpendicular to the plane of incidence (HW).

$$\tilde{E}_{0R} = \left( \frac{1 - \alpha\beta}{1 + \alpha\beta} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2}{1 + \alpha\beta} \right) \tilde{E}_{0I}$$

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<sup>a</sup>As  $\alpha$  is a function of  $\theta_i$ , reflected and transmitted wave amplitudes also depend on  $\theta_i$ .

# Reflection+Transmission of EM Waves: Oblique Incidence

## Special Cases

- **Normal Incidence:** For  $\theta_i = 0$ ,  $\alpha = 1$

$$\tilde{E}_{0R} = \left( \frac{1 - \beta}{1 + \beta} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2}{1 + \beta} \right) \tilde{E}_{0I}$$

- **Grazing Incidence:** For  $\theta_i \approx \pi/2$ ,  $\alpha = \infty$ , leading to total reflection.

$$\tilde{E}_{0R} = \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = 0$$

- **Incidence at Brewster's Angle:** If p-polarized wave is incident at Brewster's angle, it gets completely transmitted.

$$\tilde{E}_{0T} = \tilde{E}_{0I} \text{ and } \tilde{E}_{0R} = 0$$

# Reflection+Transmission of EM Waves: Oblique Incidence

$$\tilde{E}_{0R} = \left( \frac{\alpha - \beta}{\alpha + \beta} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2}{\alpha + \beta} \right) \tilde{E}_{0I}$$

## Phases of Reflected and Transmitted Components

- *Transmitted wave always remains in phase with the incident wave.*
- *Reflected wave is in phase with the incident wave if  $\alpha > \beta$ .*
- *Reflected wave is  $180^\circ$  out of phase with the incident wave if  $\beta > \alpha$ .*

# Reflection+Transmission of EM Waves: Oblique Incidence

## Brewster's Angle

- For  $\tilde{E}_{0R} = 0$ ,  $\alpha = \beta$ , i.e.

$$\alpha = \frac{\cos \theta_T}{\cos \theta_I} = \frac{\sqrt{1 - \sin^2 \theta_T}}{\sqrt{1 - \sin^2 \theta_I}} = \frac{\sqrt{1 - \left(\frac{n_1}{n_2}\right)^2 \sin^2 \theta_I}}{\sqrt{1 - \sin^2 \theta_I}} = \beta$$
$$\Rightarrow \sin^2 \theta_B = \frac{1 - \beta^2}{(n_1/n_2)^2 - \beta^2}$$

- As usually  $\mu_1 \simeq \mu_2$ , so  $\beta \simeq n_2/n_1$ ,  $\sin^2 \theta_B \simeq \frac{\beta^2}{1+\beta^2}$  and therefore

$$\tan \theta_B \simeq \frac{n_2}{n_1}$$

# Reflection+Transmission of EM Waves: Oblique Incidence

## Brewster's Angle

- For an EM wave incident on glass from air  $\theta_B \approx 56^\circ$ .
- Also from  $\alpha = \beta$  and using Snell's law,

$$\begin{aligned}\frac{\cos \theta_I}{\cos \theta_T} &= \frac{n_1}{n_2} = \frac{\sin \theta_T}{\sin \theta_I} \\ \Rightarrow \sin 2\theta_I &= \sin 2\theta_T \\ \Rightarrow 2\theta_R &= \pi - 2\theta_T \quad \text{as } \theta_I = \theta_R \\ \Rightarrow \theta_R + \theta_T &= \pi/2\end{aligned}$$

- Therefore for an EM wave incident at Brewster's angle, reflected and transmitted waves are perpendicular to each other.

# Reflection+Transmission of EM Waves: Oblique Incidence

## Brewster's Angle

- For a s-polarized EM wave incident at Brewster's angle

$$\tilde{E}_{0R} = \left( \frac{1 - \beta^2}{1 + \beta^2} \right) \tilde{E}_{0I} \text{ and } \tilde{E}_{0T} = \left( \frac{2}{1 + \beta^2} \right) \tilde{E}_{0I}$$

- Thus for an unpolarized EM wave incident at Brewster's angle, reflected light is linearly polarized with its polarization perpendicular to the plane of incidence (s-polarized) whereas the transmitted light is partially polarized.

# Reflection+Transmission of EM Waves: Oblique Incidence

## Reflection and Transmission Coefficients

- The incident, reflected and transmitted intensities are

$$I_i = \frac{1}{2} \epsilon_1 v_1 E_{0i}^2 \cos \theta_i; \quad I_R = \frac{1}{2} \epsilon_1 v_1 E_{0R}^2 \cos \theta_R; \quad I_T = \frac{1}{2} \epsilon_2 v_2 E_{0T}^2 \cos \theta_T$$

- Therefore, reflection and transmission coefficients for a p-polarized incident wave can be written as

$$R = \frac{I_R}{I_i} = \left( \frac{E_{0R}}{E_{0i}} \right)^2 = \left( \frac{\alpha - \beta}{\alpha + \beta} \right)^2$$

$$T = \frac{I_T}{I_i} = \frac{\epsilon_2 v_2}{\epsilon_1 v_1} \left( \frac{E_{0R}}{E_{0i}} \right)^2 \frac{\cos \theta_T}{\cos \theta_i} = \alpha \beta \left( \frac{2}{\alpha + \beta} \right)^2$$

- It can be easily verified that  $R + T = 1$ , as required by conservation of energy.



# Reflection+Transmission of EM Waves: Oblique Incidence

## Reflection and Transmission Coefficients

- Similarly, reflection and transmission coefficients for a s-polarized incident wave can be written as

$$R = \frac{I_R}{I_i} = \left( \frac{E_{0R}}{E_{0i}} \right)^2 = \left( \frac{1 - \alpha\beta}{1 + \alpha\beta} \right)^2$$

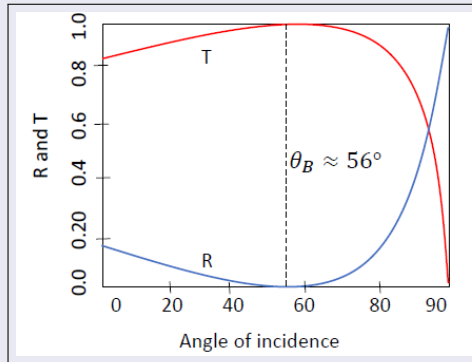
$$T = \frac{I_T}{I_i} = \frac{\epsilon_2 v_2}{\epsilon_1 v_1} \left( \frac{E_{0R}}{E_{0i}} \right)^2 \frac{\cos \theta_T}{\cos \theta_i} = \alpha\beta \left( \frac{2}{1 + \alpha\beta} \right)^2$$

- Here also  $R + T = 1$  holds good, as required by conservation of energy.

# Reflection+Transmission of EM Waves: Oblique Incidence

## Reflection and Transmission Coefficients

- As  $\alpha$  is a function of the angle of incidence, reflection and transmission coefficients also are and their dependence for p-polarization of incident light look like as shown below



# Reflection+Transmission of EM Waves: Oblique Incidence

## Reflection and Transmission Coefficients

- For s-polarization of the incident light, the complete transmission does not happen, as is evident from the following plot

