

# ELL100: INTRODUCTION TO ELECTRICAL ENGG.

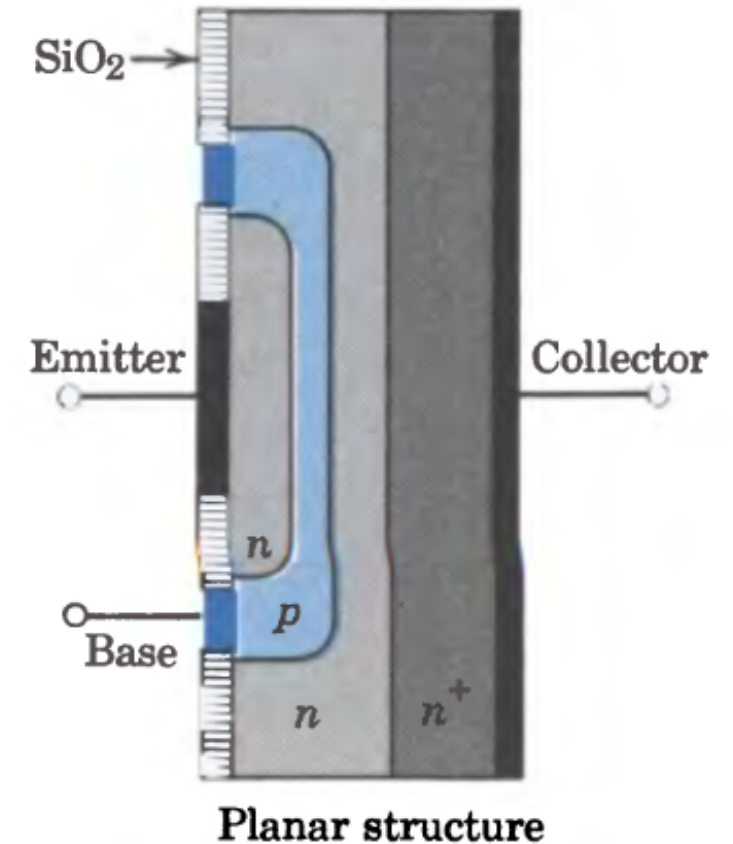
## **Bipolar Junction Transistors (BJT) - Basics**

Instructor: Debanjan Bhowmik

Reference: Donald Neamen's 'Electronic Circuit Analysis'  
Chapter 3 (BJT)

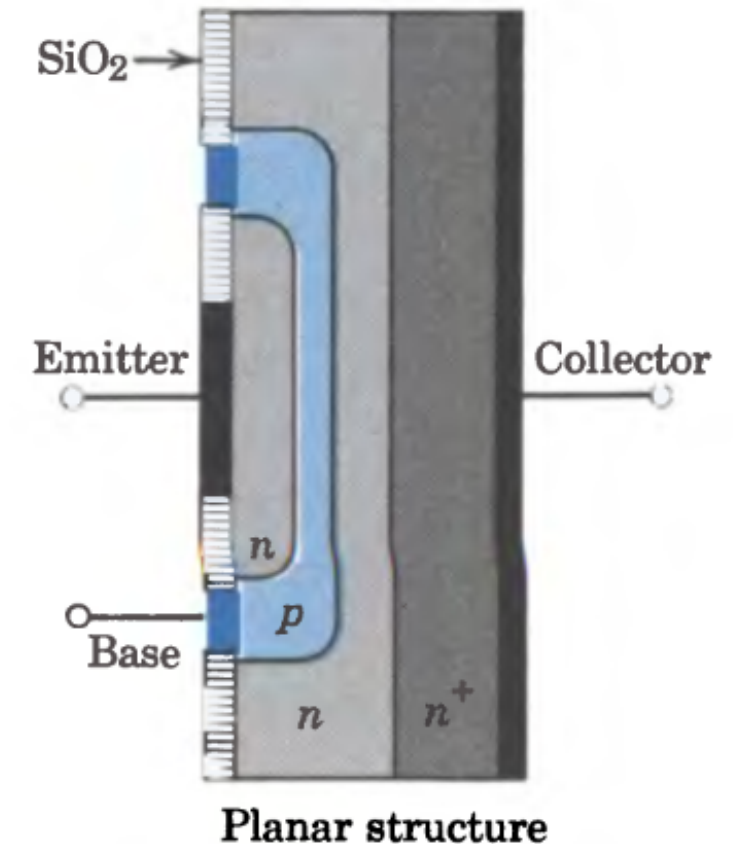
# Bipolar Junction Transistor

- Three terminal device
- Transistor: Transfer of resistance
- Two pn junctions in close proximity
- Achieved by sandwiching a narrow n(p) type material between two p(n)-type material sections.
- Bipolar: Both electrons and holes contribute in current
- Type: npn or pnp



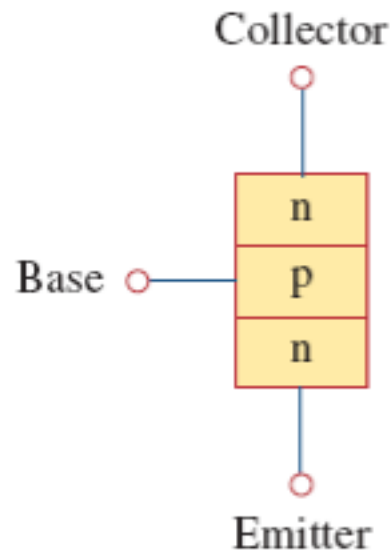
# Bipolar Junction Transistor

- Three terminal device
- Transistor: Transfer of resistance.
- Two pn junctions in close proximity.
- Achieved by sandwiching a narrow n(p) type material between two p(n)-type material sections.
- Bipolar: Both electrons and holes contribute in current
- Type: npn or pnp

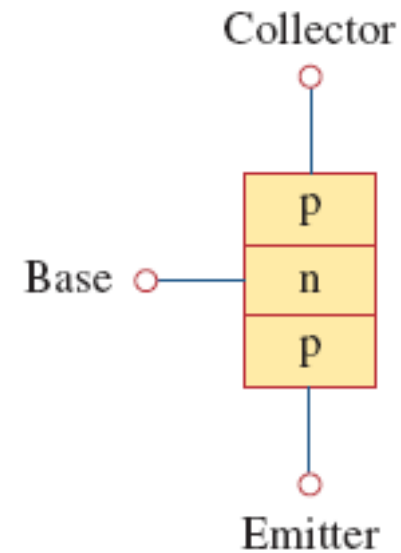
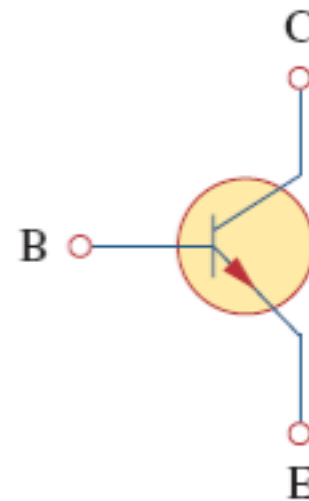


- **Doping order**  
 $N_{\text{emitter}} > N_{\text{collector}} > N_{\text{base}}$
- **Thickness order**  
 $T_{\text{collector}} > T_{\text{emitter}} > T_{\text{base}}$

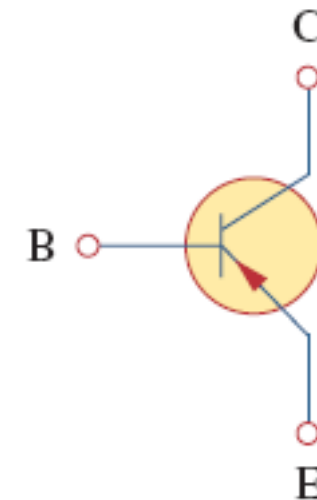
# Bipolar Junction Transistor: Symbol



n-p-n transistor symbol



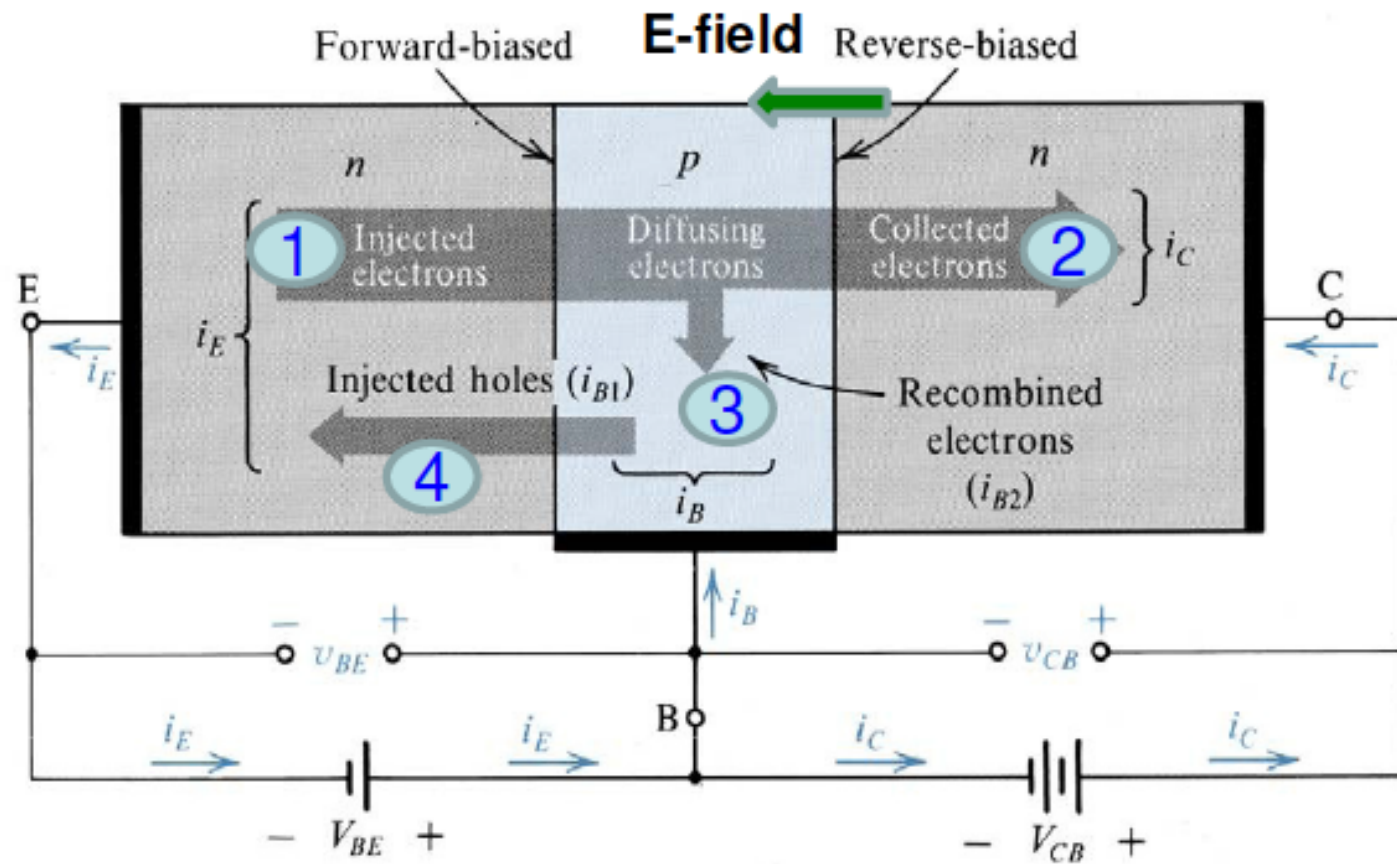
p-n-p transistor symbol



Emitter lead is identified by an arrow pointing in the direction of 'positive' charge flow in normal operation.

# BJT- Basic Working

Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias

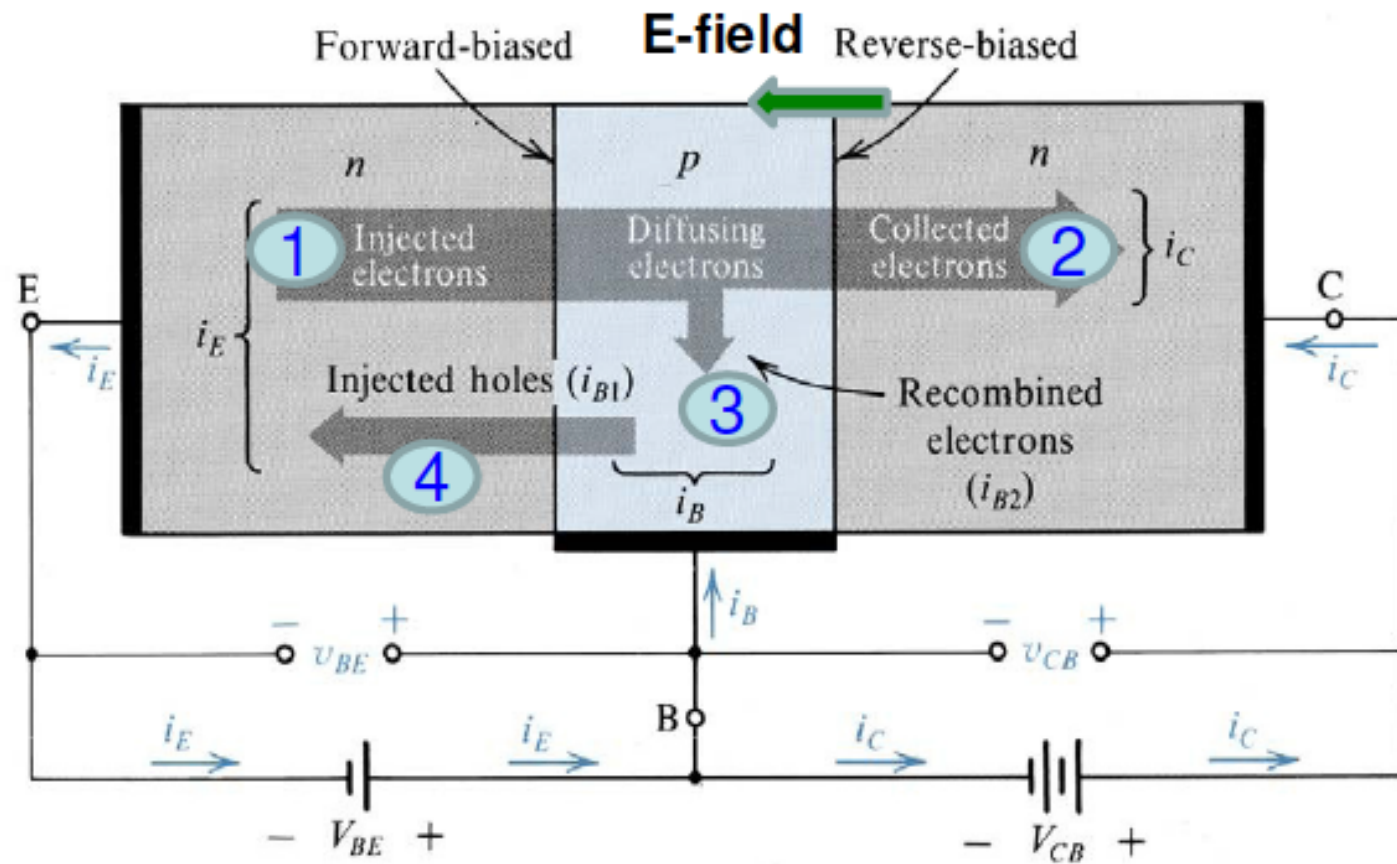


# BJT- Basic Working

Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias

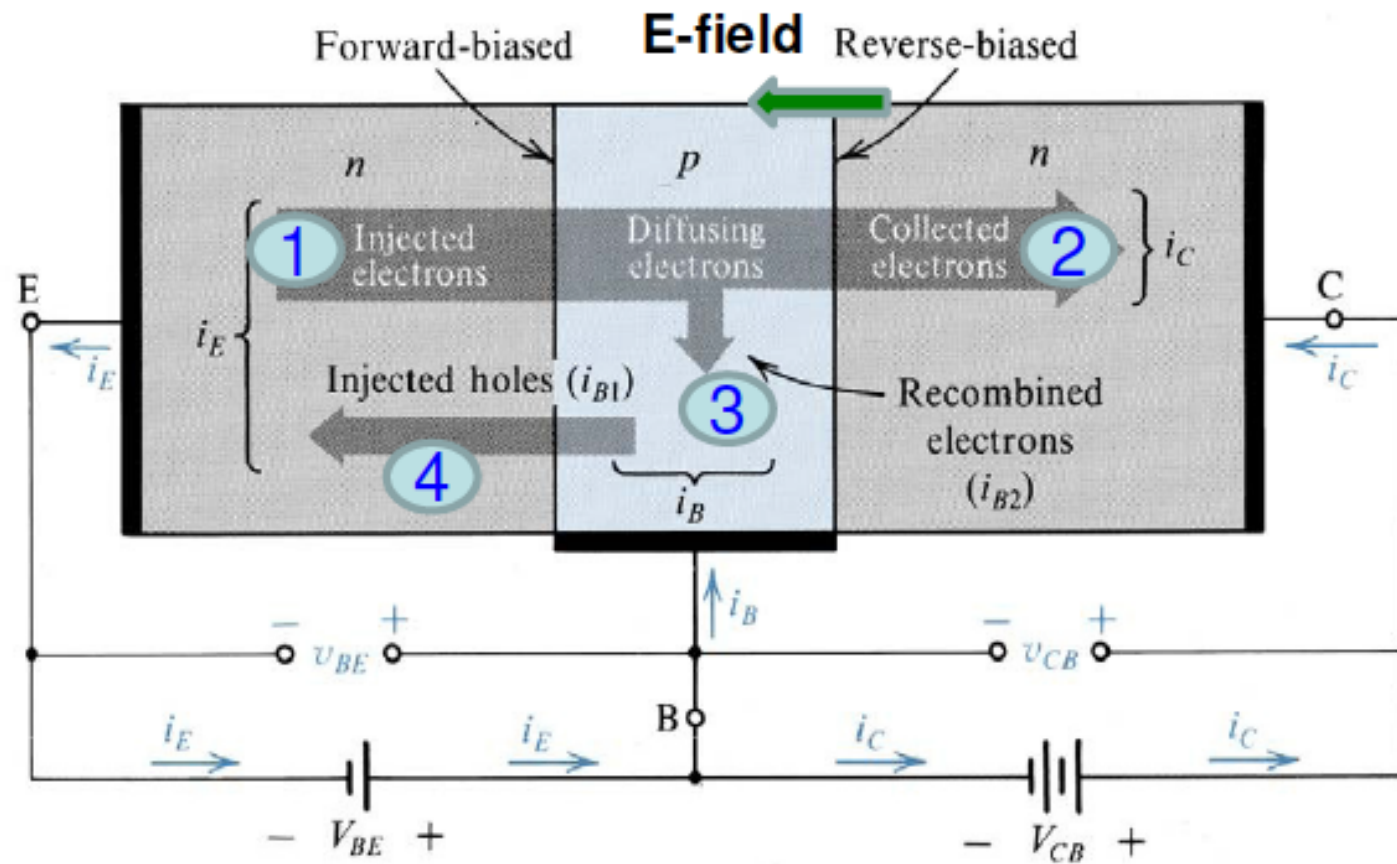
1. Forward bias of EB Jn causes electrons to diffuse from emitter into base.

2. As base region is very thin, the majority of electrons diffuse to the edge of the depletion region of CB Jn, and then are swept to the collector by the electric field of the reverse-biased CB Jn. **(Collected electrons recombine with 'holes' provided by VCB supply.)**  $i_C = \alpha I_E$



# BJT- Basic Working

Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias



1. Forward bias of EB Jn causes electrons to diffuse from emitter into base.

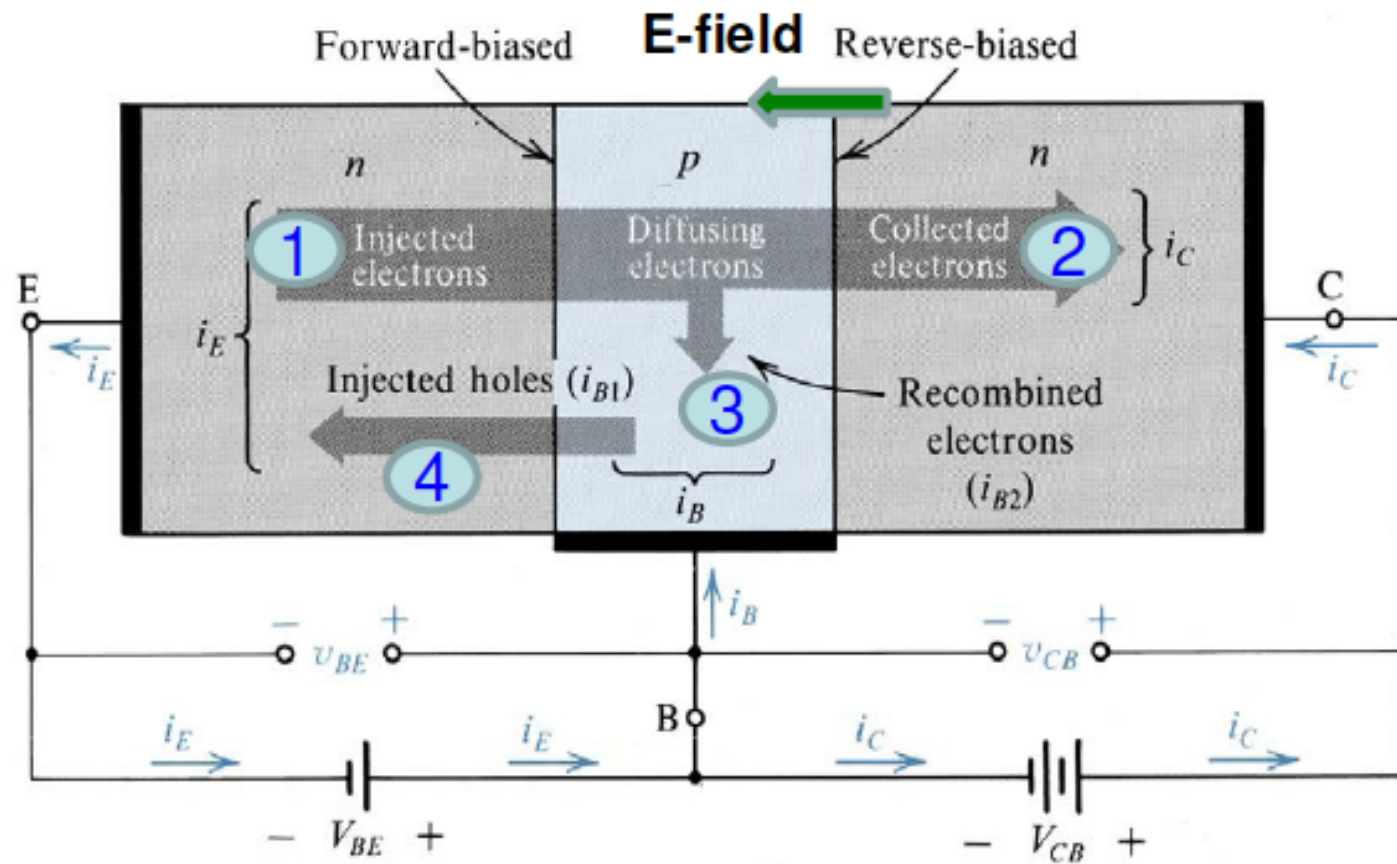
2. As base region is very thin, the majority of electrons diffuse to the edge of the depletion region of CB Jn, and then are swept to the collector by the electric field of the reverse-biased CB Jn. (Collected electrons recombine with 'holes' provided by VCB supply.)  $i_C = \alpha I_E$

3. Small fraction of the electrons recombine with holes in base region.



# BJT- Basic Working

Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias



1 . Forward bias of EB Jn causes electrons to diffuse from emitter into base.

2. As base region is very thin, the majority of electrons diffuse to the edge of the depletion region of CB Jn, and then are swept to the collector by the electric field of the reverse-biased CB Jn. (Collected electrons recombine with 'holes' provided by VCB supply.)  $i_C = \alpha I_E$

3. Small fraction of the electrons recombine with holes in base region.

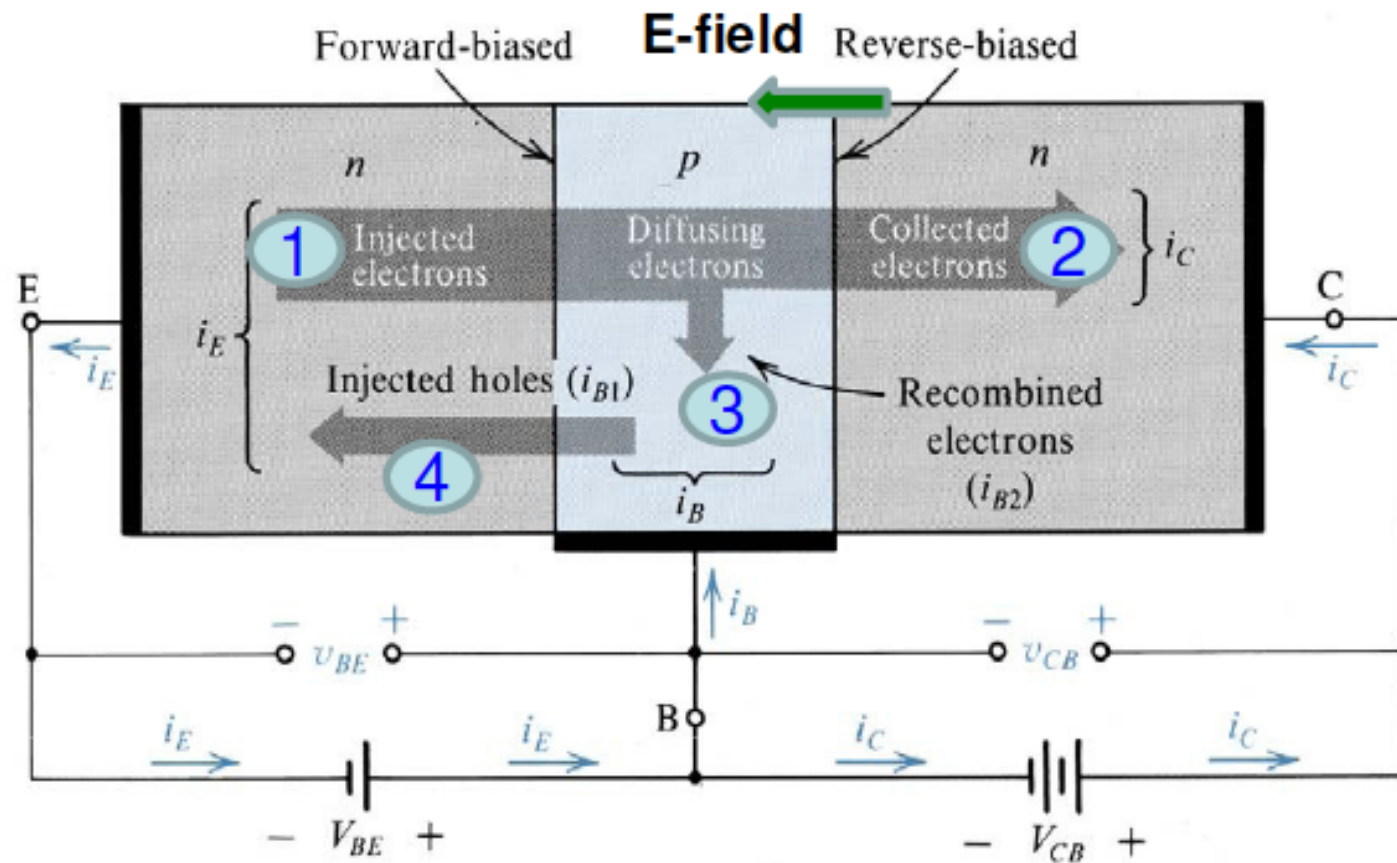
4. Holes are also injected from base to emitter region.  $(4) \ll (1)$ .

The two-carrier flow from [(1) and (4)] forms the emitter current ( $I_E$ )



# BJT- Basic Working

Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias



1 . Forward bias of EB Jn causes electrons to diffuse from emitter into base.

2. As base region is very thin, the majority of electrons diffuse to the edge of the depletion region of CB Jn, and then are swept to the collector by the electric field of the reverse-biased CB Jn. (Collected electrons recombine with 'holes' provided by VCB supply.)  $i_C = \alpha I_E$

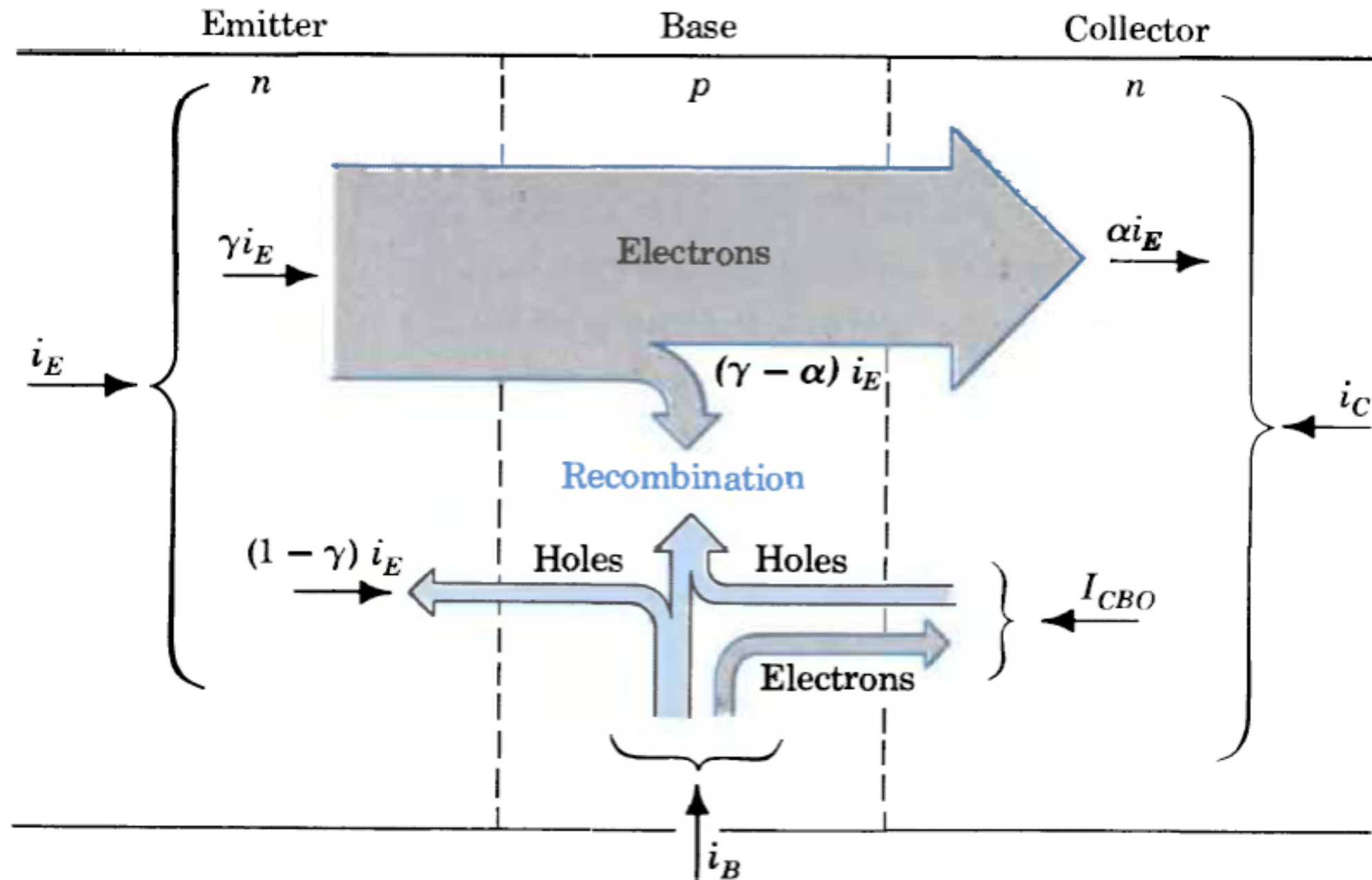
3. Small fraction of the electrons recombine with holes in base region.

4. Holes are also injected from base to emitter region.  $(4) \ll (1)$ .

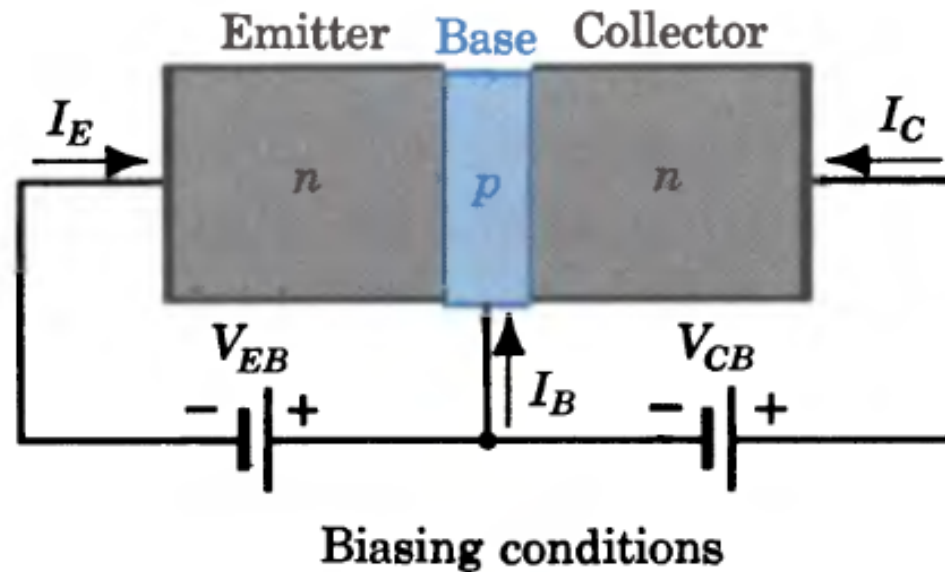
The two-carrier flow from [(1) and (4)] forms the emitter current ( $I_E$ )

**$I_C$  is almost independent of the magnitude of  $V_{CB}$  and ( $I_C = \alpha I_E$ ,  $\alpha=0.9\sim0.99$ )**

# BJT- Carrier Motion

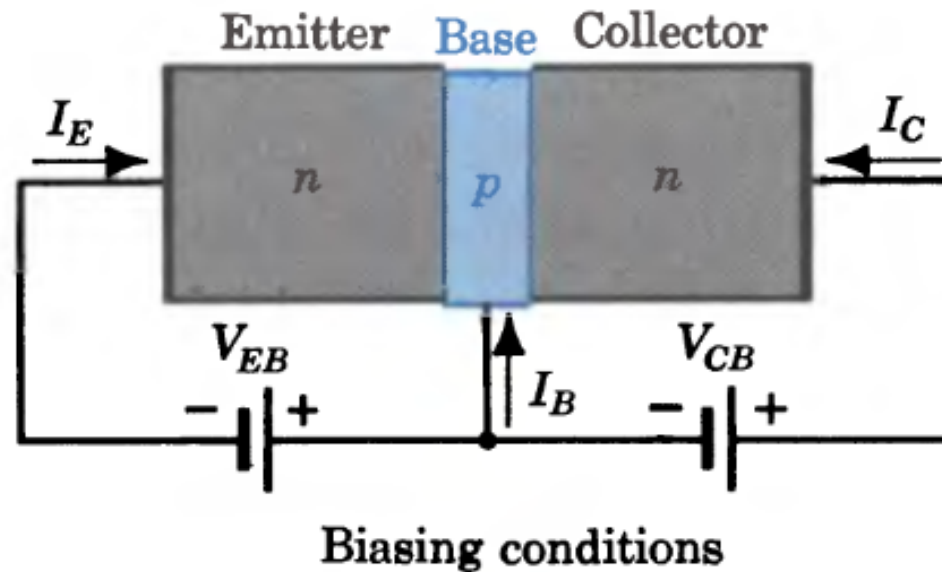


# Bipolar Junction Transistor: Modes



Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias
Reverse active	Reverse Bias	Forward Bias
Saturation	Forward bias	Forward bias
Cut off	Reverse Bias	Reverse Bias

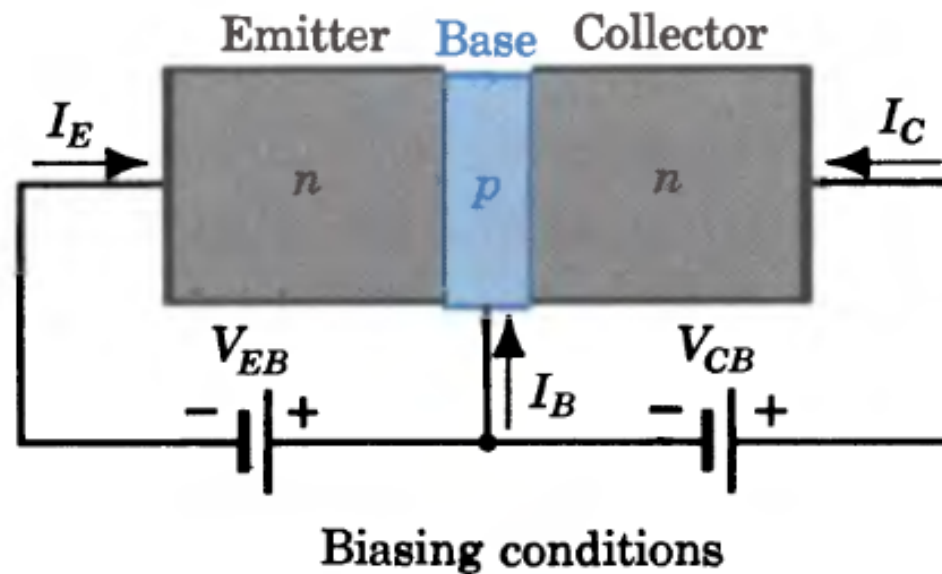
# Bipolar Junction Transistor: Modes



Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias
Reverse active	Reverse Bias	Forward Bias
Saturation	Forward bias	Forward bias
Cut off	Reverse Bias	Reverse Bias

Amplifier  
Amplifier (less effective)

# Bipolar Junction Transistor: Modes



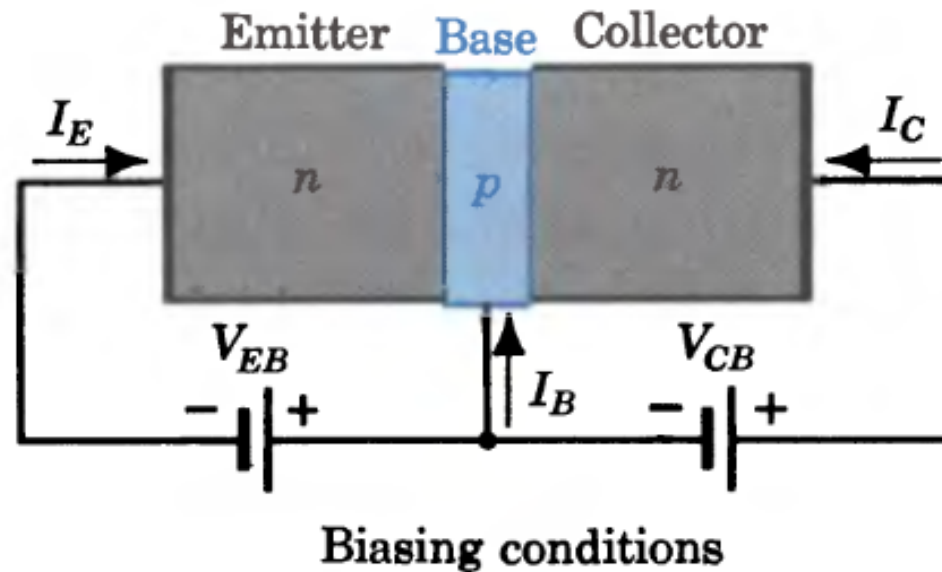
Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias
Reverse active	Reverse Bias	Forward Bias
Saturation	Forward bias	Forward bias
Cut off	Reverse Bias	Reverse Bias

Amplifier

Amplifier (less effective)

Small drop between E-B and  $I_C$   
independent of  $I_B$  (Switch ON)

# Bipolar Junction Transistor: Modes



Mode	$V_{BE}$	$V_{BC}$
Forward active	Forward bias	Reverse Bias
Reverse active	Reverse Bias	Forward Bias
Saturation	Forward bias	Forward bias
Cut off	Reverse Bias	Reverse Bias

Amplifier

Amplifier (less effective)

Switch ON

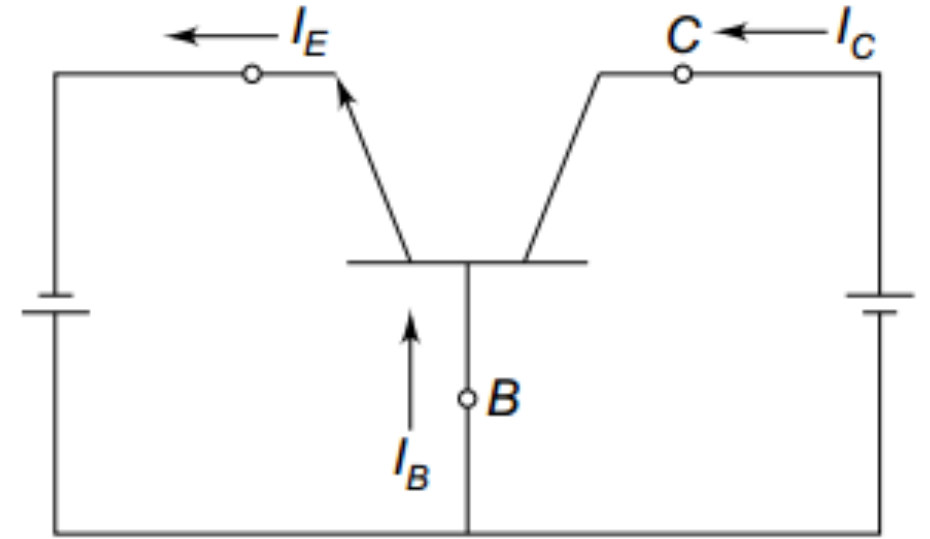
Only  $I_{CBO}$  flows in collector  
(SWITCH OFF)



## BJT currents:

$I_E$ ,  $I_B$ ,  $I_C$  are the currents flowing through emitter, base and collector terminal

$$I_E = I_B + I_C$$



## BJT currents:

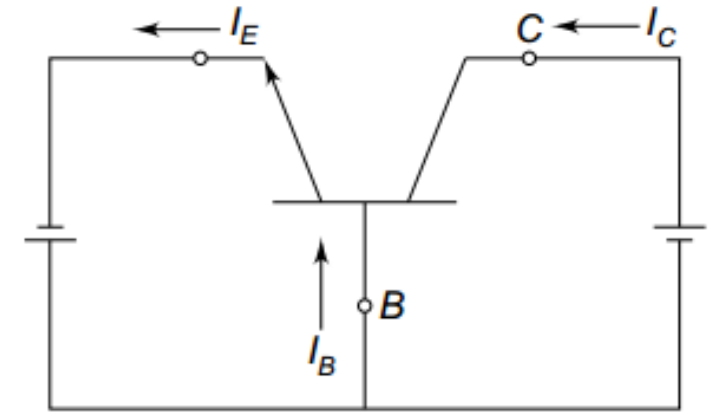
$I_E$ ,  $I_B$ ,  $I_C$  are the currents flowing through emitter, base and collector terminal.

$$I_E = I_B + I_C$$

$I_C$  is around 96% - 99.5% of  $I_E$ .

$$I_C = \alpha I_E$$

$\alpha$  is emitter to collector gain. It lies between 0.96 to 0.995.



## BJT currents:

$I_E$ ,  $I_B$ ,  $I_C$  are the currents flowing through emitter, base and collector terminal

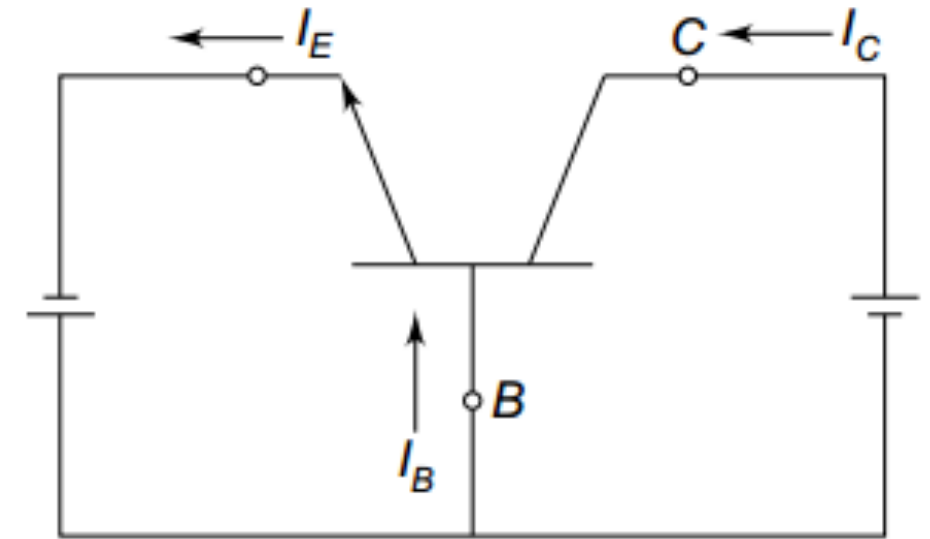
$$I_E = I_B + I_C$$

$I_C$  is around 96% - 99.5% of  $I_E$ .

$$I_C = \alpha I_E$$

$\alpha$  is emitter to collector gain. It lies between 0.96 to 0.995.

$I_C$  is approximately equal to  $I_E$ , but due to reverse biased C-B junction, a small reverse saturation current flows ( $I_{CBO}$ ).

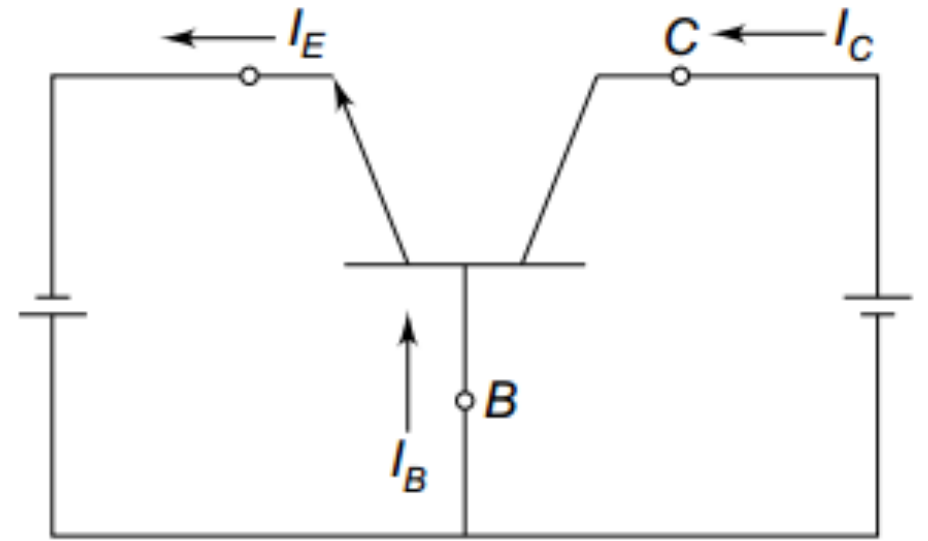


collector-to-base leakage  
current with emitter open  
circuit

# BJT currents:

$$I_E = I_B + I_C$$

$$I_C = \alpha I_E + I_{CBO}$$



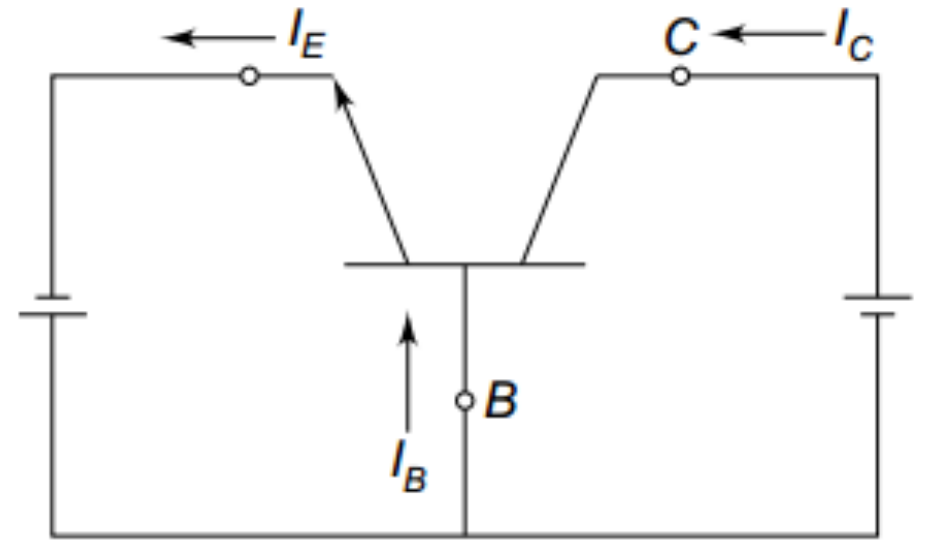
# BJT currents:

$$I_E = I_B + I_C$$

$$I_C = \alpha I_E + I_{CBO}$$

$$I_C = \alpha(I_C + I_B) + I_{CBO}$$

$$(1 - \alpha)I_C = \alpha I_B + I_{CBO}$$



# BJT currents:

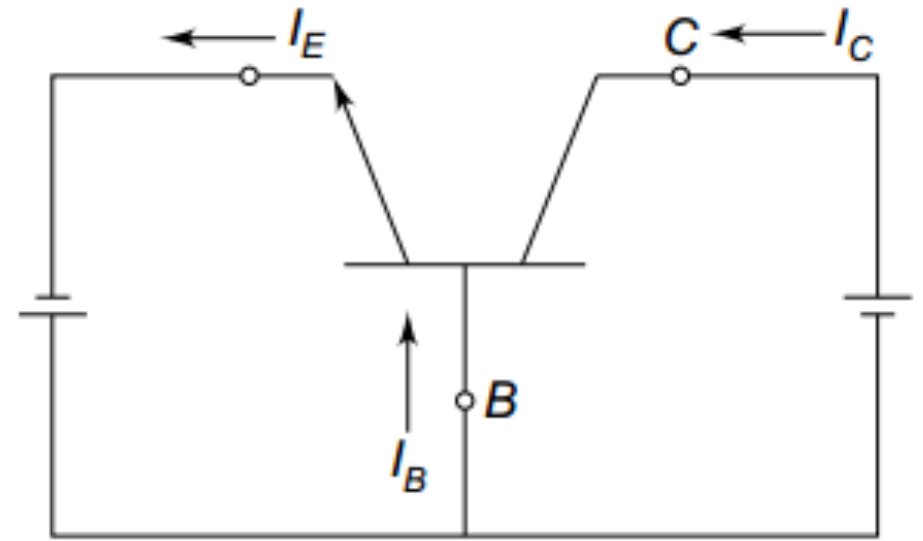
$$I_E = I_B + I_C$$

$$I_C = \alpha I_E + I_{CBO}$$

$$I_C = \alpha(I_C + I_B) + I_{CBO}$$

$$(1 - \alpha)I_C = \alpha I_B + I_{CBO}$$

$$I_C = \left( \frac{\alpha}{1 - \alpha} \right) I_B + \left( \frac{1}{1 - \alpha} \right) I_{CBO}$$





# BJT currents:

$$I_E = I_B + I_C$$

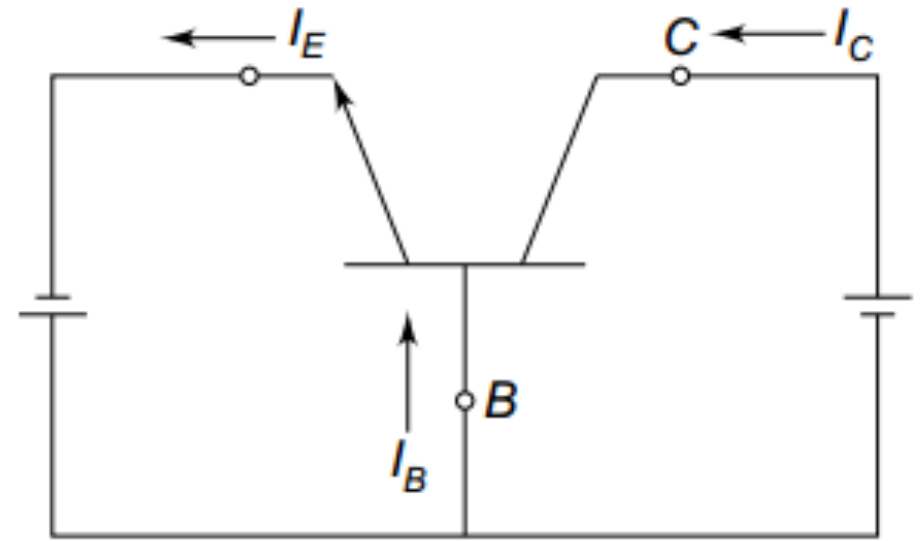
$$I_C = \alpha I_E + I_{CBO}$$

$$I_C = \alpha(I_C + I_B) + I_{CBO}$$

$$(1 - \alpha)I_C = \alpha I_B + I_{CBO}$$

$$I_C = \left( \frac{\alpha}{1 - \alpha} \right) I_B + \left( \frac{1}{1 - \alpha} \right) I_{CBO}$$

$$I_C = \beta I_B + (\beta + 1)I_{CBO} \quad \beta, \text{ base-to-collector current gain (assuming no leakage)}$$



# BJT currents:

$$I_E = I_B + I_C$$

$$I_C = \alpha I_E + I_{CBO}$$

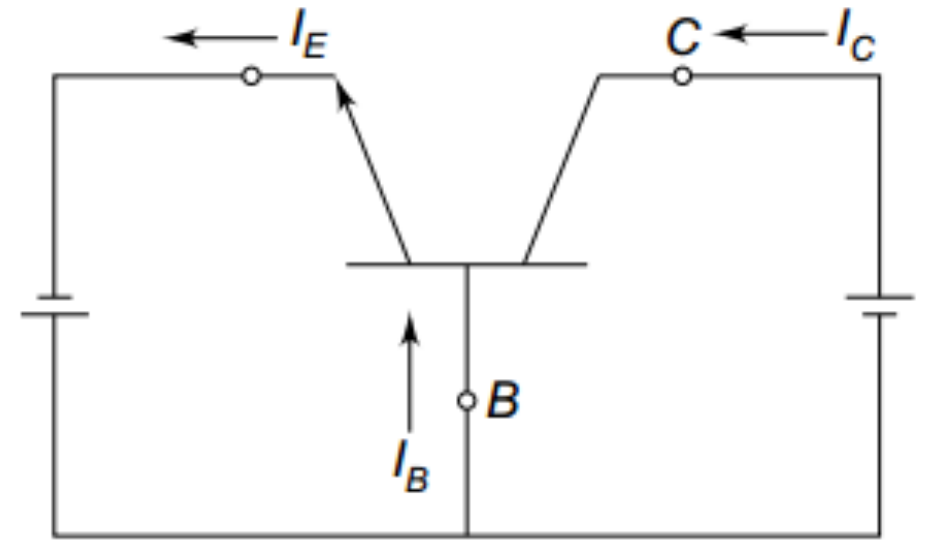
$$I_C = \alpha(I_C + I_B) + I_{CBO}$$

$$(1 - \alpha)I_C = \alpha I_B + I_{CBO}$$

$$I_C = \left( \frac{\alpha}{1 - \alpha} \right) I_B + \left( \frac{1}{1 - \alpha} \right) I_{CBO}$$

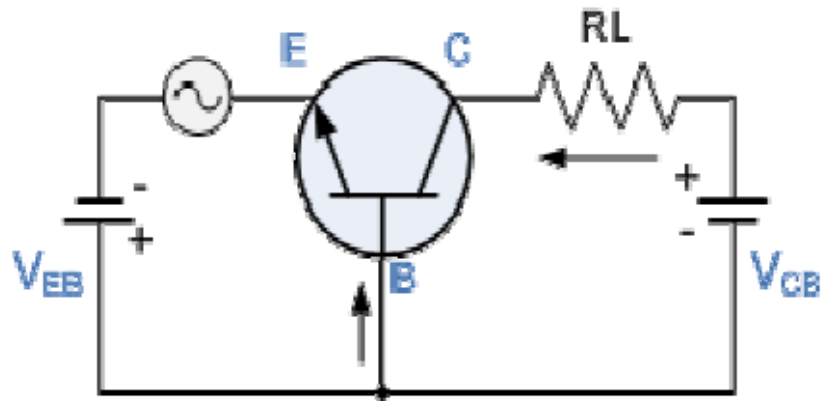
$$I_C = \beta I_B + (\beta + 1)I_{CBO}$$
  $\beta$ , base-to-collector current gain (assuming no leakage)

$I_{CEO}$ , reverse saturation current in CE configuration

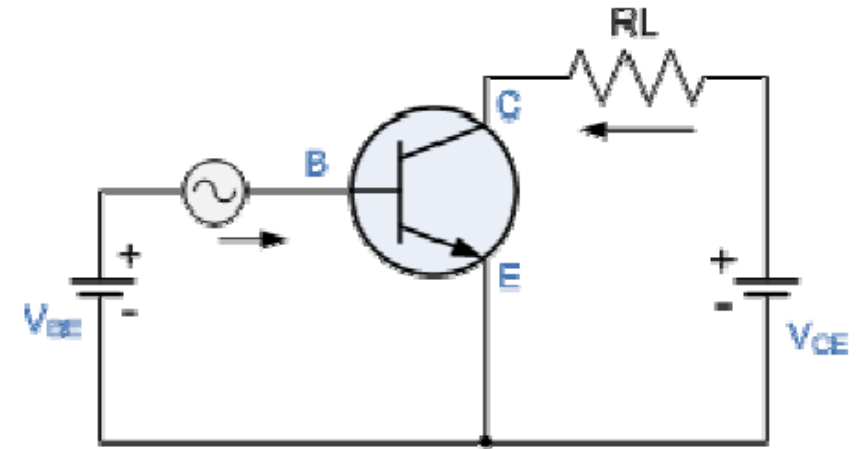


# BJT configurations

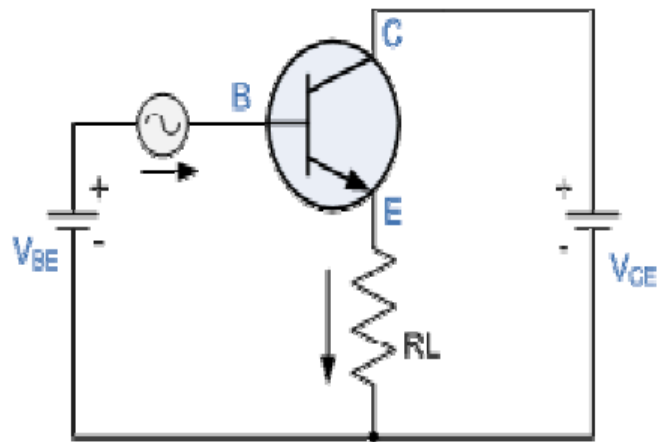
## Common base configuration



## Common emitter configuration

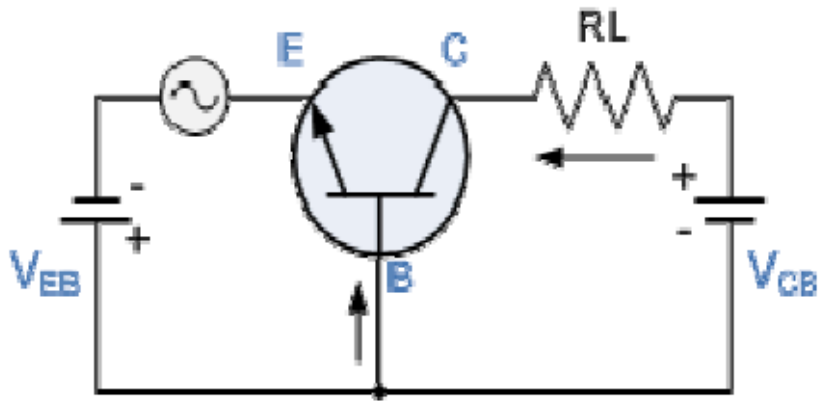


## Common collector configuration



# BJT configurations: CB

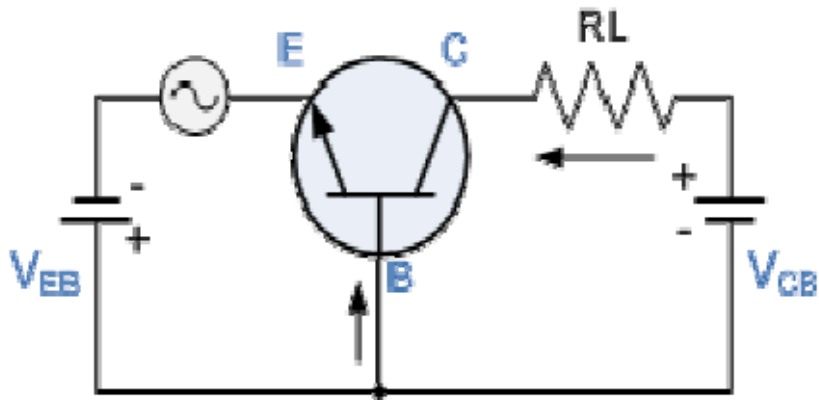
## Common base configuration



- Base is grounded/fixed.
- Base connected to both input and output side
- Input - Emitter terminal, Output - Collector terminal

# BJT configurations: CB

## Common base configuration



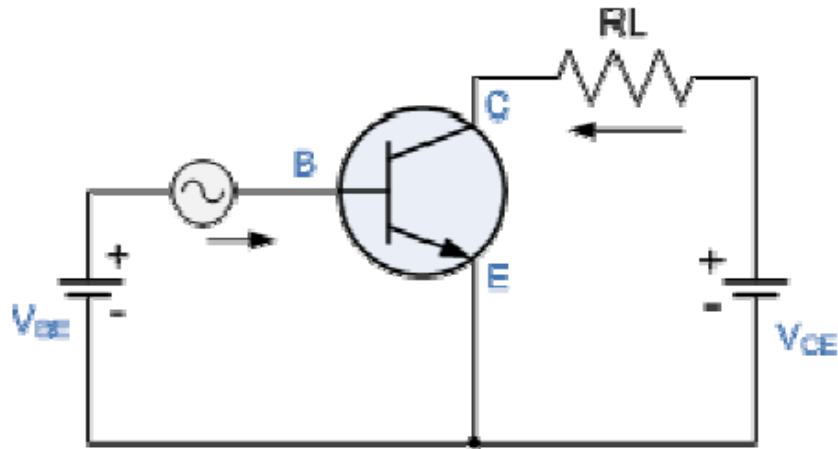
- Base is grounded/fixed.
- Base connected to both input and output side
- Input – Emitter terminal, Output – Collector terminal
- $I_e = I_c + I_b, I_c < I_e$
- CAN be used for voltage amplification.

$$A = \frac{I_c R_L}{I_e R_{IN}} \gg 1, R_L \gg R_{IN}$$

- Does not do current amplification (in fact attenuates)
- Low  $Z_{in}$ , High  $Z_{out}$ , Low power gain

# BJT configurations: CE

## Common emitter configuration

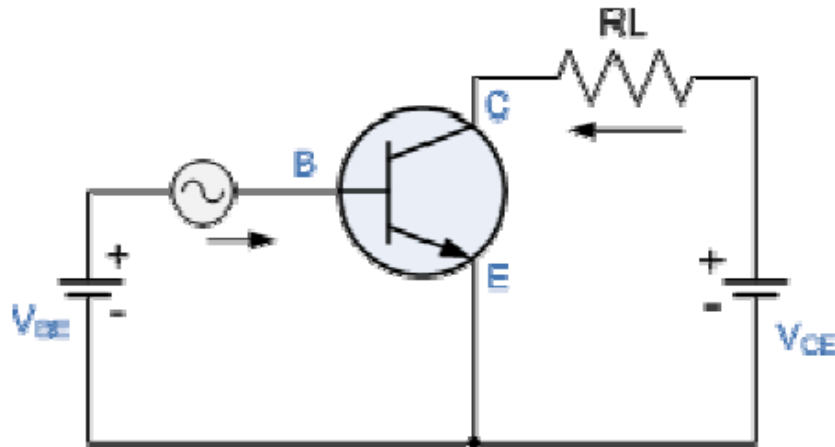


- Emitter is grounded/fixed. Collector connected to load.
- $V_C > V_E$ , (for npn)
- (Hint :  $V_{CE} - V_{BE} > 0, V_{BE} > 0$  )
- Input – Base terminal, Output – Collector terminal



# BJT configurations: CE

## Common emitter configuration



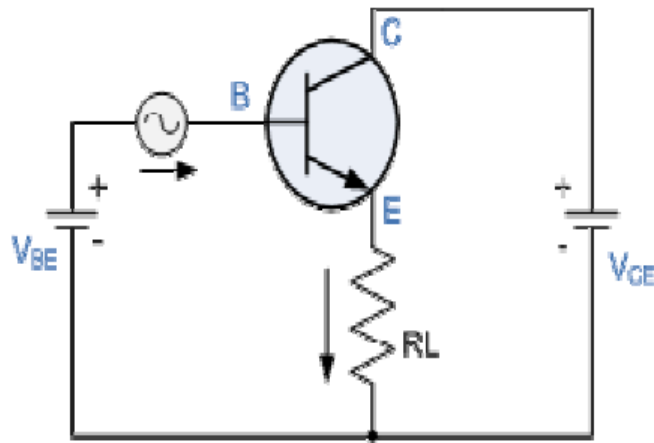
- Emitter is grounded/fixed. Collector connected to load
- $V_C > V_E$ , (for npn)
- (Hint :  $V_{CE} - V_{BE} > 0, V_{BE} > 0$  )
- Input – Base terminal, Output – Collector terminal
- $I_e = I_c + I_b, I_c \gg I_b$
- Can be used for current amplification

$$A = \frac{I_c}{I_b} \gg 1,$$

- Can also be used as voltage amplifier but amplification less than CB mode, and gives 180 degree phase shift (inversion)
- Medium  $Z_{in}$ ,  $Z_{out}$ ; High Power Gain

# BJT configurations: CC

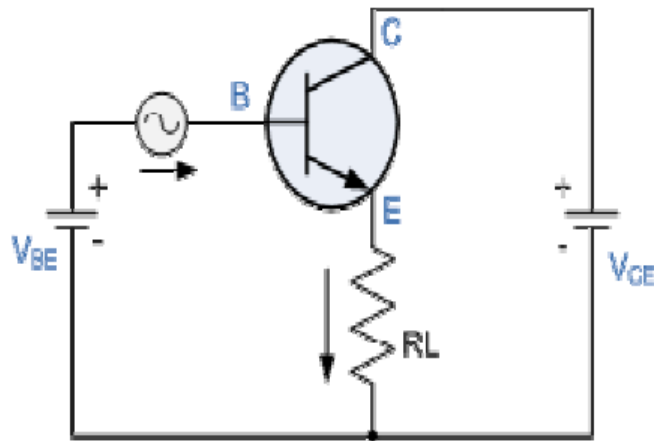
## Common collector configuration



- Collector is grounded at fixed reference. Emitter connected to load.
- Input - Base terminal, Output - Emitter terminal

# BJT configurations: CC

## Common collector configuration



- Collector is grounded at fixed reference. Emitter connected to load.
- Input – Base terminal, Output – Emitter terminal
- $I_e = I_L = I_c + I_b$ ,
- Can be used for current amplification

$$A = \frac{I_e}{I_b} \gg 1,$$

- But, voltage gain is almost unity only.
- Voltage follower or buffer (zero phase difference)
- High  $Z_{in}$ , Low  $Z_{out}$ , Medium Power Gain

# BJT configurations: Qualitative Summary

Characteristic	Common Base	Common Emitter	Common Collector
Input Impedance	Low	Medium	High
Output Impedance	Very High	High	Low
Phase Shift	0°	180°	0°
Voltage Gain	High	Medium	Low
Current Gain	Low	Medium	High
Power Gain	Medium	Very High	Medium
	Preamplifier	Most Common	Buffer