

EEE-2103: Electronic Devices and Circuits

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Emitter Bias Configuration

Emitter bias configuration and its dc equivalent circuit →

Base-Emitter loop →

$$+V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0$$

$$I_E = (\beta + 1)I_B$$

$$V_{CC} - I_B R_B - V_{BE} - (\beta + 1)I_B R_E = 0$$

$$-I_B(R_B + (\beta + 1)R_E) + V_{CC} - V_{BE} = 0$$

$$I_B(R_B + (\beta + 1)R_E) = V_{CC} - V_{BE}$$

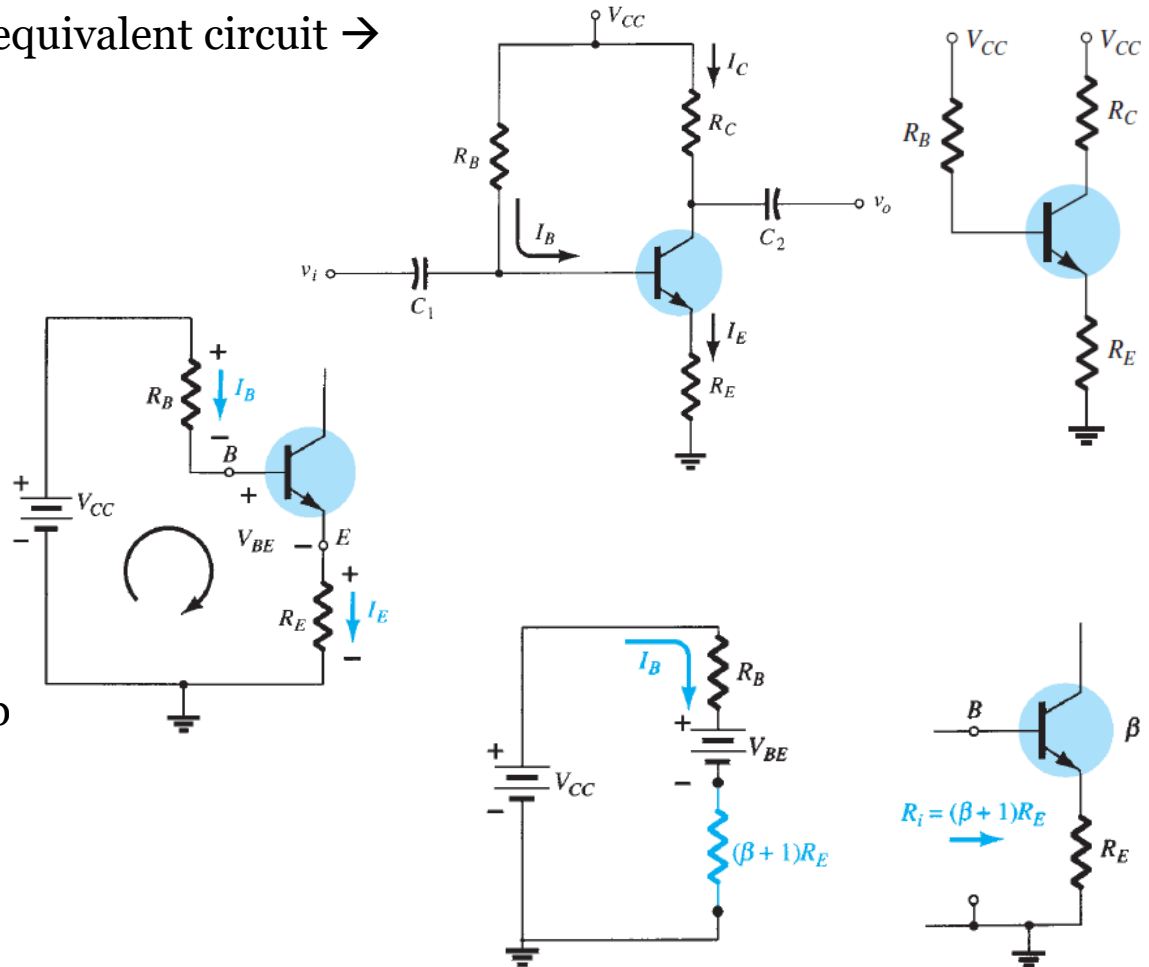
$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E}$$

$R_E \rightarrow$ part of CE loop
appears as $(\beta + 1)R_E$ in BE loop

$$R_i = (\beta + 1)R_E$$

$$\text{Net voltage} = V_{CC} - V_{BE}$$

$$\text{Resistance} = R_B + (\beta + 1)R_E$$



Emitter Bias Configuration

Collector-Emitter loop \rightarrow

$$+I_E R_E + V_{CE} + I_C R_C - V_{CC} = 0$$

$$I_E \approx I_C$$

$$V_{CE} - V_{CC} + I_C(R_C + R_E) = 0$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$V_E = I_E R_E$$

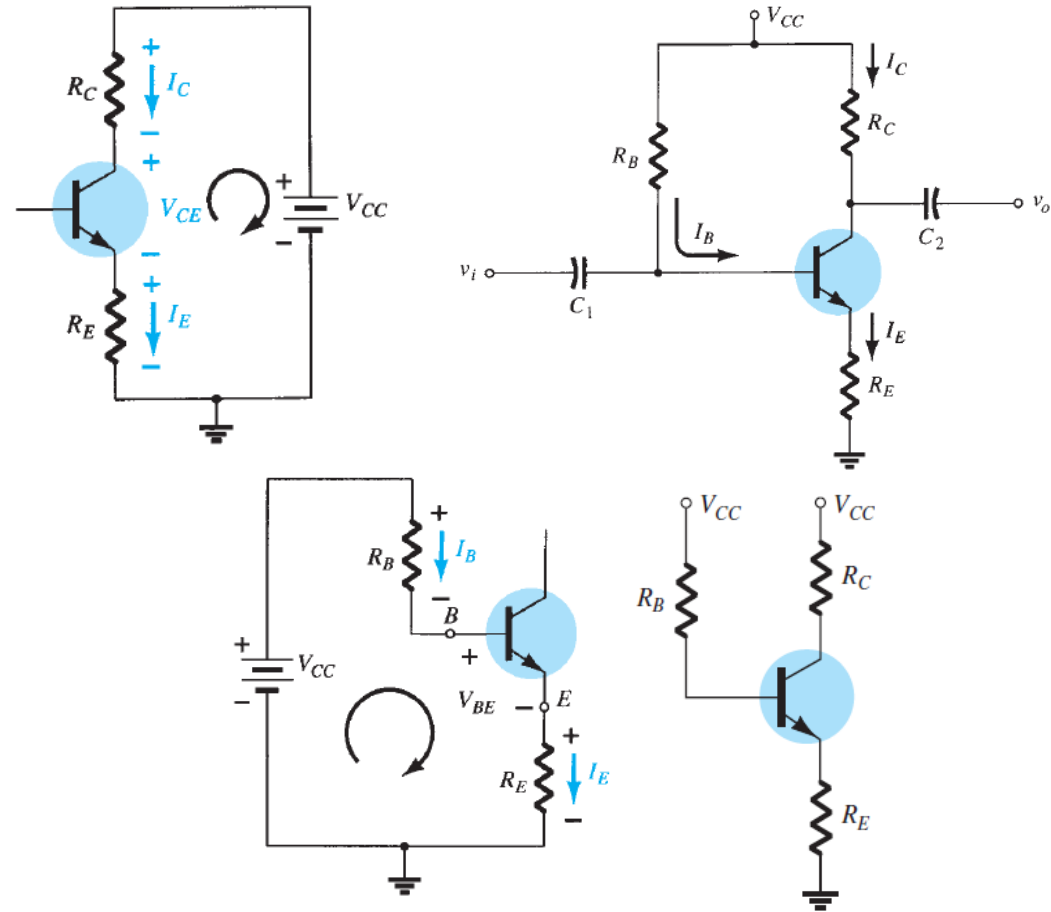
$$V_{CE} = V_C - V_E$$

$$V_C = V_{CE} + V_E$$

$$V_C = V_{CC} - I_C R_C$$

$$V_B = V_{CC} - I_B R_B$$

$$V_B = V_{BE} + V_E$$



Emitter Bias Configuration

Problem-24:

For the emitter-bias network of Fig. 24, determine

a) I_B . b) I_C . c) V_{CE} . d) V_C . e) V_E . f) V_B . g) V_{BC} .

$$a) I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E} = \frac{20 - 0.7}{430 \times 10^3 + (50 + 1)1 \times 10^3} = 40.1 \mu A$$

$$b) I_C = \beta I_B = (50)(40.1 \times 10^{-6}) = 2.01 \text{ mA}$$

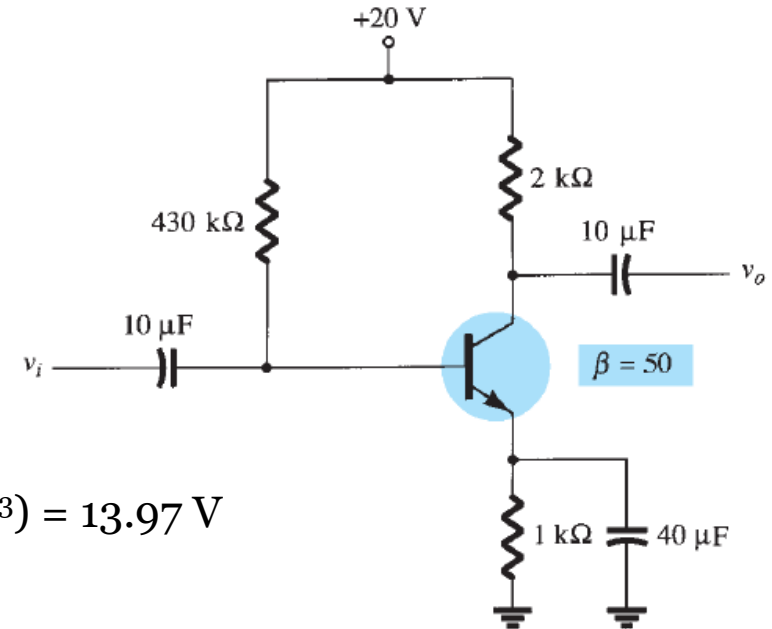
$$c) V_{CE} = V_{CC} - I_C(R_C + R_E) = 20 - (2.01 \times 10^{-3})(2 \times 10^3 + 1 \times 10^3) = 13.97 \text{ V}$$

$$d) V_C = V_{CC} - I_C R_C = 20 - (2.01 \times 10^{-3})(2 \times 10^3) = 15.98 \text{ V}$$

$$e) V_E = V_C - V_{CE} = 15.98 - 13.97 = 2.01 \text{ V}$$

$$f) V_B = V_{BE} + V_E = 0.7 + 2.01 = 2.71 \text{ V}$$

$$g) V_{BC} = V_B - V_C = 2.71 - 15.98 = -13.27 \text{ V}$$

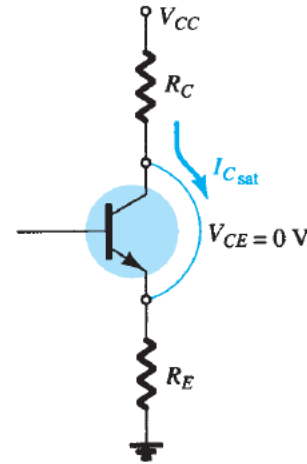


Emitter Bias Configuration

Saturation level →

Collector saturation level = max I_C

$$I_{Csat} = \frac{V_{CC}}{R_C + R_E}$$



Load line analysis →

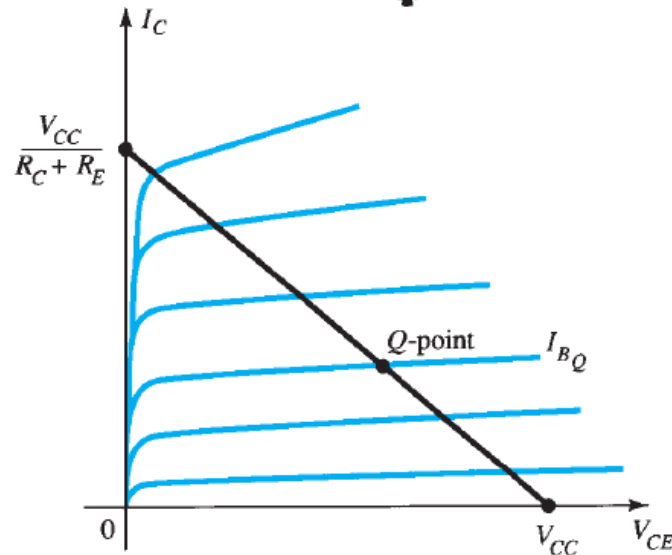
$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$I_C = 0 \rightarrow$$

$$V_{CE} = V_{CC}$$

$$V_{CE} = 0 \rightarrow$$

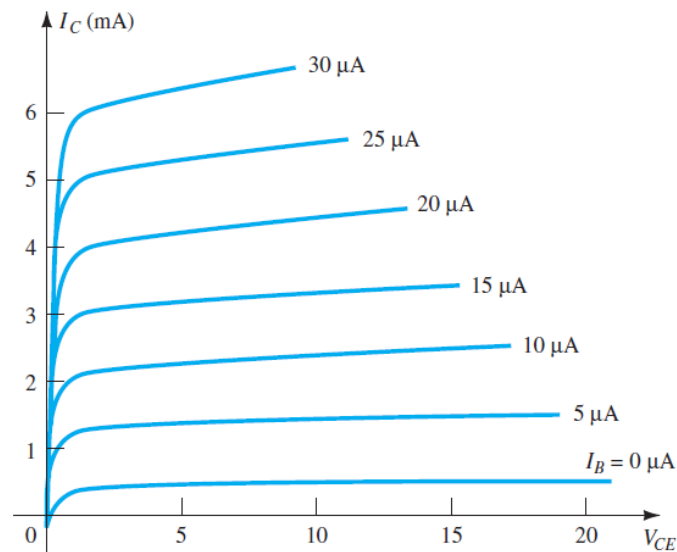
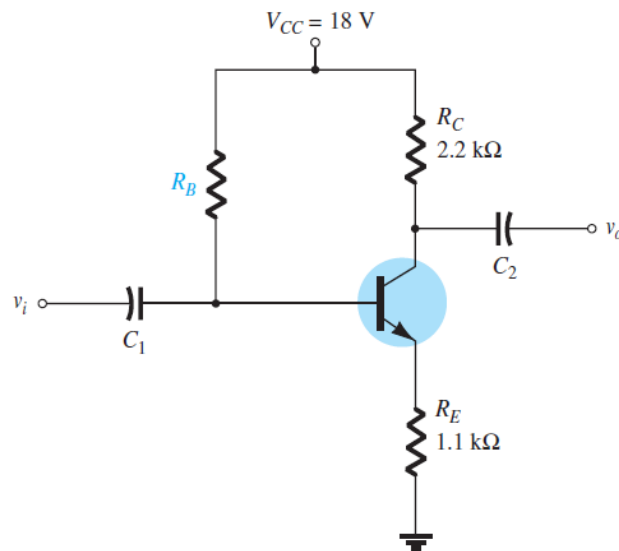
$$I_C = \frac{V_{CC}}{R_C + R_E}$$



Emitter Bias Configuration

Problem-25:

- Draw the load line for the network of Fig. 25(a) on the characteristics for the transistor appearing in Fig. 25(b).
- For a Q -point at the intersection of the load line with a base current of $15\ \mu\text{A}$, find the values of I_{CQ} and V_{CEQ} .
- Determine the dc beta at the Q -point.
- Using the beta for the network determined in part c, calculate the required value of R_B and suggest a possible standard value.



Emitter Bias Configuration

Problem-25:

a) At $V_{CE} = 0 \text{ V}$: $I_C = \frac{V_{CC}}{R_C + R_E} = \frac{18}{2.2 \times 10^3 + 1.1 \times 10^3} = 5.45 \text{ mA}$

At $I_C = 0 \text{ mA}$: $V_{CE} = V_{CC} = 18 \text{ V}$

Resulting load line appears in Fig. 25(c).

b) $V_{CEQ} \approx 7.5 \text{ V}$, $I_{CQ} \approx 3.3 \text{ mA}$

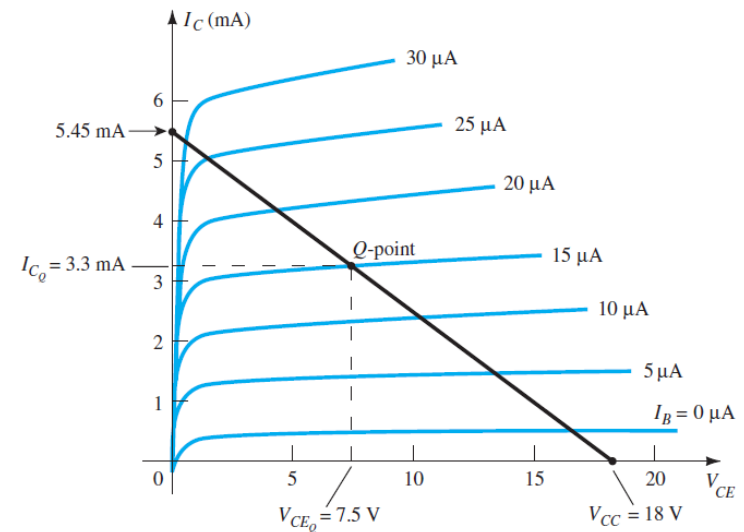
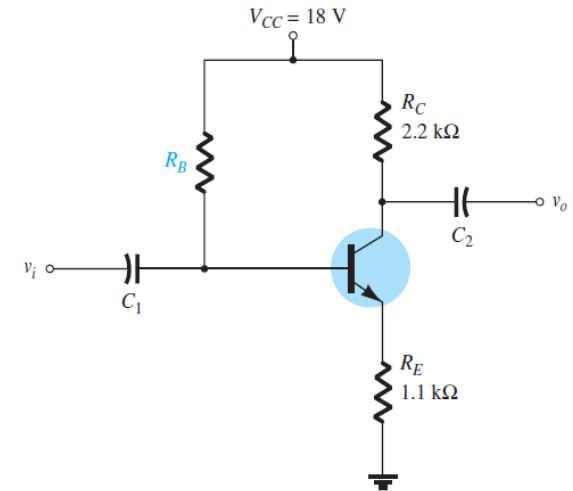
c) $\beta = I_{CQ}/I_{BQ} = 3.3 \times 10^{-3} / 15 \times 10^{-6} = 220$

d) $I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E} = \frac{18 - 0.7}{R_B + (220 + 1)1.1 \times 10^3} = 15 \times 10^{-6}$

$15 \times 10^{-6} R_B + (15 \times 10^{-6})(243.1 \times 10^3) = 17.3$

$15 \times 10^{-6} R_B = 13.65$

$R_B = 13.65 / 15 \times 10^{-6} = 910 \text{ k}\Omega$

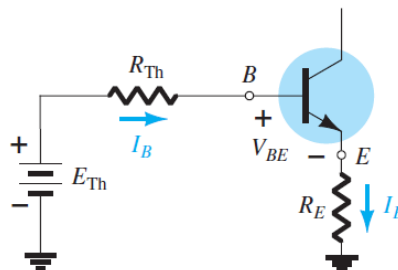
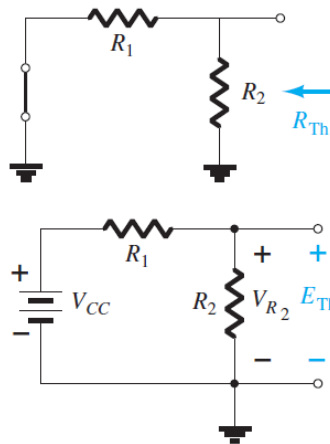


Voltage Divider Bias Configuration

Exact analysis:

$$R_{Th} = R_1 || R_2$$

$$E_{Th} = V_{R2} = \frac{R_2 V_{CC}}{R_1 + R_2}$$

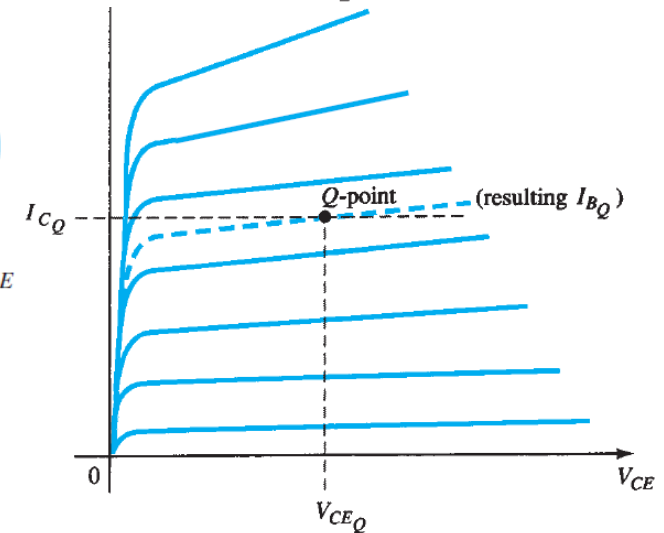
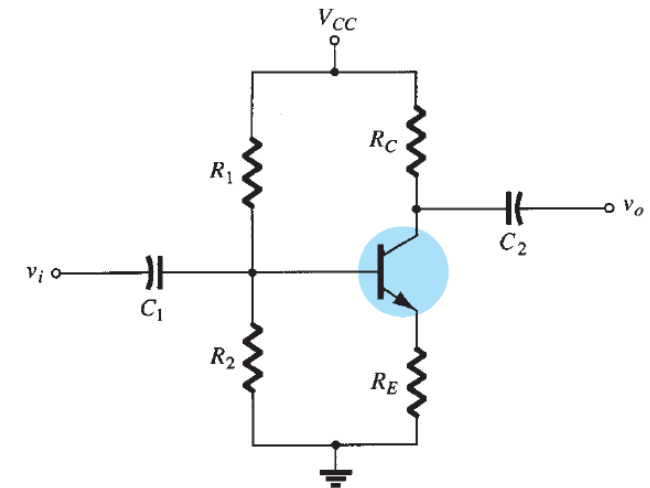
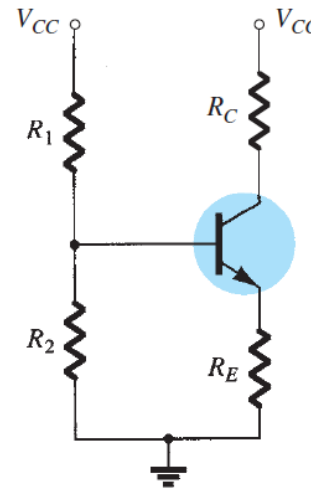
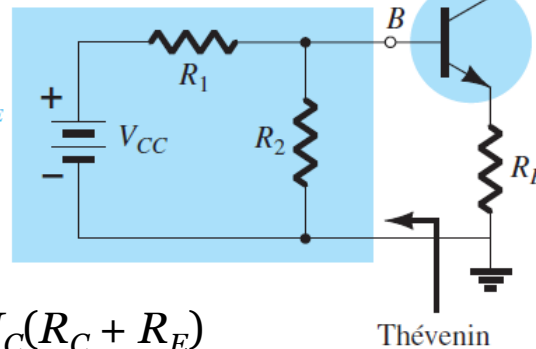


$$E_{Th} - I_B R_{Th} - V_{BE} - I_E R_E = 0$$

$$I_E = (\beta + 1) I_B$$

$$I_B = \frac{E_{Th} - V_{BE}}{R_{Th} + (\beta + 1) R_E}$$

$$V_{CE} = V_{CC} - I_C (R_C + R_E)$$



Voltage Divider Bias Configuration

Problem-26:

Determine the dc bias voltage V_{CE} and the current I_C for the voltage divider configuration of Fig. 26.

$$R_{Th} = R_1 \parallel R_2 = \frac{(39 \times 10^3)(3.9 \times 10^3)}{39 \times 10^3 + 3.9 \times 10^3} = 3.55 \text{ k}\Omega$$

$$E_{Th} = V_{R2} = \frac{R_2 V_{CC}}{R_1 + R_2} = \frac{(3.9 \times 10^3)(22)}{39 \times 10^3 + 3.9 \times 10^3} = 2 \text{ V}$$

$$I_B = \frac{E_{Th} - V_{BE}}{R_{Th} + (\beta + 1)R_E} = \frac{2 - 0.7}{3.55 \times 10^3 + (101)(1.5 \times 10^3)} = 8.38 \text{ }\mu\text{A}$$

$$I_{CQ} = \beta I_B = (100)(8.38 \times 10^{-6}) = 0.84 \text{ mA}$$

$$\begin{aligned} V_{CEQ} &= V_{CC} - I_C(R_C + R_E) \\ &= 22 - (0.84 \times 10^{-3})(10 \times 10^3 + 1.5 \times 10^3) \\ &= 12.34 \text{ V} \end{aligned}$$

