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Tot boldions	
<pre>function Abbas_HW_10_Wire_MoM() % Hasan Tahir Abbas</pre>	
% ECEN 637	
% Homework 10: Computation of Input Adm	nittance and Radiation Pattern
of a	
% Wire Antenna	
% 11/27/2015	
8	
%	
<pre>% Pocklington Integral Equation is use % Radiation Pattern as explained in:</pre>	ed to compute the Admittance and
% Gibson, Walton C. "The Method of Mom Taylor	ments in Electromagnetics,"
%	and Francis/CRC,
2008.	
8	
8	
<pre>% Gauss_Quadrature based Numerical Inte</pre>	gration (Built-in Function)
% Input Admittance	
% Far-field pattern calculation	
% Utilization of Toeplitz nature of the	e impedance matrix (Only one row
% needs to be computed)	
% DADAMEMEDO AND MADIADIES LIST	
<pre>% PARAMETERS AND VARIABLES LIST o.</pre>	
% % M = Total Wire Segments	

```
% f = Frequency
% c = Speed of light
% xmu = Permeability of free space
% eps0 = Permittivity of free space
% omega = Angular Frequency
% K = Propagation Constant
% lambda = Wavelength
% a = Wire Radius;
% L = Wire Length
% E rad = Radiated Far-field
% I = Current on the wire
% Y = Input Admittance of the wire
% num theta = number of angle values for polar plot
% num_length = number of lengths of wire
% FUNCTIONS LIST
% -----
% Pocklington() = Calculates the Pocklington EFIE solution
% Pocklington Pattern() = Calculates the Pocklington EFIE Far-field
pattern
% Pocklington_Current() = Calculates the Current on the wire
close all
```

Parameters

Global variables are used to span across all the functions in this code According to MATLAB's documentation, a better and safer option will be persistent type variables

```
global c xmu eps0
global f omega lambda K
global Lengths M a
global num_theta num_length
global Yin
global E_rad_4by5 E_rad
global I_wire
e **********
§ ***************
e *********
f = 300e6;
c = 2.99792458e8; % Speed of light
xmu = 4*pi*1e-7; % Permeability of free space
eps0 = 8.854187817e-12; % Permittivity of free space
omega = 2.0*pi*f;
K = omega*sqrt(xmu*eps0);
lambda = c/f;
a = 7.022e - 3*lambda;
% a = 1.588e - 3*lambda;
num_length = 101;
```

Main Program

```
initialize();
```

Input Admittance

Far-fields

```
First h = 4/5*lambda

E_rad_4by5 = Pocklington_pattern(4*lambda/5);

% Second h = lambda

E_rad = Pocklington_pattern(lambda);
```

Currents

```
I_wire = Pocklington_Current(.7*lambda, 1.588e-3*lambda); % to match
the given figure
```

Plot Solutions

End Main Program

Initialize

```
*******************
```

```
function initialize()
% Set all the variables to zero
```

Pocklington Equation Solver

```
function Yin = Pocklington(L)
global eps0
global omega K
global M a
deltaz = L / M;
z = linspace(-0.5*L, 0.5*L - deltaz, M);
Z = zeros(M);
for j = 1 : 1 % Only one iteration is needed as impedance matrix can
 be constructed through its Toeplitz property
    for k = 1 : M
        fun = @(zp) \exp(-1i*K*sqrt((z(j) - zp).^2 + a^2))...
            ./sqrt((z(j) - zp).^2 + a^2); % Make a symbolic Function
 of z_prime
        % This calculation is based on the reference cited in the code
        % introduction.
        % Mathematical Modeling of Eq. 4.63
        zp_upper = z(k) + deltaz/2; % Upper limit of integration
        dz\_upper = z(j) - zp\_upper; % Represents (z(m) - z(n)) for the
 upper limit
        zp_lower = z(k) - deltaz/2; % Lower limit of integration
        dz_lower = z(j) - zp_lower; % Represents (z(m) - z(n)) for the
 limit limit
```

Numerical Integration Using Gauss_Quadratures

```
int part =
 quadgk(fun,zp_lower,zp_upper,'RelTol',1e-8,'AbsTol',1e-12);
        R_upper = sqrt(dz_upper^2 + a^2); % Represents R for the upper
 limit
        R_lower = sqrt(dz_lower^2 + a^2); % Represents R for the lower
 limit
        sum_part_upper = (dz_upper)*(1 + 1i*K*R_upper)...
            ./R_upper^3*exp(-1i*K*R_upper); % Exact Evalation of the
 second term (upper limit) in Eq. 4.63 of the reference
        sum_part_lower = (dz_lower)*(1 + 1i*K*R_lower)...
            ./R_lower^3*exp(-1i*K*R_lower); % Exact Evalation of the
 second term (lower limit) in Eq. 4.63 of the reference
        Z(j,k) = K^2*int_part + sum_part_upper - sum_part_lower; %
 Pocklington Integral for j not equal to k
        if j == k
        % This is done to avoid very small numbers in the denominator
            % For all the diagonal elements of Z, terms only need to
 be calculated once
            R_{upper} = sqrt( (-deltaz/2)^2 + a^2); % Here z(m) = z(n)
            R_{lower} = sqrt((deltaz/2)^2 + a^2);
            sum_part_upper = (-deltaz/2)*(1 + 1i*K*R_upper)...
                ./R_upper^3*exp(-1i*K*R_upper);
            sum_part_lower = (deltaz/2)*(1 + 1i*K*R_lower)...
                ./R_lower^3*exp(-li*K*R_lower);
            num = sqrt(1 + 4*a^2/deltaz^2) + 1;
            denom = sqrt(1 + 4*a^2/deltaz^2) - 1;
            self = (log(num/denom) - 1i*K*deltaz); % Approximation of
 the integral term as described in reference
            Z(j,k) = K^2*self + sum_part_upper - sum_part_lower; %
 Diagonal Elements of the impedance matrix
         end
    end
end
Z = toeplitz(real(Z(1,:))) + 1i*toeplitz(imag(Z(1,:))); % Make a
Toeplitz matrix out of a row vector
V = zeros(M,1); % Initialize Source (RHS)
V(floor(M/2)+1) = -1i*4*pi*omega*eps0*(1.0/deltaz); % Delta Source
```

Calculate the current

```
I = Z \setminus V;
```

Input impedance and admittance

Pocklington Equation Solver only for Far-fields

```
function ERad = Pocklington_pattern(L)
global eps0 xmu
global omega K
global M a num_theta theta
deltaz = L / M;
ERad = zeros(1,num_theta);
z = linspace(-0.5*L , 0.5*L - deltaz, M);
Z = zeros(M);
for j = 1 : 1
    for k = 1 : M
        fun = @(zp) \exp(-1i*K*sqrt((z(j) - zp).^2 + a^2))...
            ./sqrt(( z(j) - zp).^2 + a^2); % Make a symbolic Function
 of z_prime
        % This calculation is based on the reference cited in the code
        % introduction.
        % Mathematical Modeling of Eq. 4.63
        zp\_upper = z(k) + deltaz/2; % Upper limit of integration
        dz_{upper} = z(j) - zp_{upper}; % Represents (z(m) - z(n)) for the
 upper limit
        zp_lower = z(k) - deltaz/2; % Lower limit of integration
        dz_lower = z(j) - zp_lower; % Represents (z(m) - z(n)) for the
 limit limit
```

Numerical Integration Using Gauss_Quadratures

```
int_part =
quadgk(fun,zp_lower,zp_upper,'RelTol',1e-8,'AbsTol',1e-12);
    R_upper = sqrt(dz_upper^2 + a^2); % Represents R for the upper
limit
```

```
R_lower = sqrt(dz_lower^2 + a^2); % Represents R for the lower
 limit
        sum_part_upper = (dz_upper)*(1 + 1i*K*R_upper)...
            ./R upper^3*exp(-li*K*R upper); % Exact Evalation of the
 second term (upper limit) in Eq. 4.63 of the reference
        sum_part_lower = (dz_lower)*(1 + li*K*R_lower)...
            ./R_lower^3*exp(-1i*K*R_lower); % Exact Evalation of the
 second term (lower limit) in Eq. 4.63 of the reference
        Z(j,k) = K^2*int_part + sum_part_upper - sum_part_lower; %
 Pocklington Integral for j not equal to k
        if j == k
        % This is done to avoid very small numbers in the denominator
            % For all the diagonal elements of Z, terms only need to
 be calculated once
            R_{upper} = sqrt( (-deltaz/2)^2 + a^2); % Here z(m) = z(n)
            R_{lower} = sqrt((deltaz/2)^2 + a^2);
            sum_part_upper = (-deltaz/2)*(1 + 1i*K*R_upper)...
                ./R upper^3*exp(-1i*K*R upper);
            sum_part_lower = (deltaz/2)*(1 + 1i*K*R_lower)...
                ./R_lower^3*exp(-li*K*R_lower);
            num = sqrt(1 + 4*a^2/deltaz^2) + 1;
            denom = sqrt(1 + 4*a^2/deltaz^2) - 1;
            self = (log(num/denom) - 1i*K*deltaz); % Approximation of
 the integral term as described in reference
            Z(j,k) = K^2*self + sum_part_upper - sum_part_lower; %
 Diagonal Elements of the impedance matrix
         end
    end
end
Z = toeplitz(real(Z(1,:))) + 1i*toeplitz(imag(Z(1,:))); % Make a
Toeplitz matrix out of a row vector
V = zeros(M-2,1); % Initialize Source (RHS)
V(floor((M-2)/2)+1) = -1i*4*pi*omega*eps0*(1.0/deltaz); % Delta
 Source
I = zeros(M,1);
```

Calculate the current

```
I(2:M-1) = Z(2:M-1,2:M-1) \setminus V;
```

Far-field

```
for i = 1 : num_theta
   cosTheta = cos(theta(i));
   sinTheta = sin(theta(i));
   ERad(i) = 0;
   for m = 1:M
      z_m = z(m) + 0.5*deltaz;
```

Pocklington Equation Current Solver

```
***************
function I = Pocklington_Current(L,a)
global eps0
global omega K
global M
deltaz = L / M;
z = linspace(-0.5*L , 0.5*L - deltaz, M);
Z = zeros(M);
for j = 1 : 1 % Only one iteration is needed as impedance matrix can
be constructed through its Toeplitz property
    for k = 1 : M
        fun = @(zp) \exp(-1i*K*sqrt((z(j) - zp).^2 + a^2))...
            ./sqrt((z(j) - zp).^2 + a^2); % Make a symbolic Function
 of z_prime
        % This calculation is based on the reference cited in the code
        % introduction.
       % Mathematical Modeling of Eq. 4.63
        zp_upper = z(k) + deltaz/2; % Upper limit of integration
       dz\_upper = z(j) - zp\_upper; % Represents (z(m) - z(n)) for the
upper limit
       zp_lower = z(k) - deltaz/2; % Lower limit of integration
        dz_lower = z(j) - zp_lower; % Represents (z(m) - z(n)) for the
 limit limit
```

Numerical Integration Using Gauss_Quadratures

```
int_part =
quadgk(fun,zp_lower,zp_upper,'RelTol',le-8,'AbsTol',le-12);

R_upper = sqrt(dz_upper^2 + a^2); % Represents R for the upper limit
```

```
R_lower = sqrt(dz_lower^2 + a^2); % Represents R for the lower
 limit
        sum_part_upper = (dz_upper)*(1 + 1i*K*R_upper)...
            ./R upper^3*exp(-li*K*R upper); % Exact Evalation of the
 second term (upper limit) in Eq. 4.63 of the reference
        sum_part_lower = (dz_lower)*(1 + li*K*R_lower)...
            ./R_lower^3*exp(-li*K*R_lower); % Exact Evalation of the
 second term (lower limit) in Eq. 4.63 of the reference
        Z(j,k) = K^2*int_part + sum_part_upper - sum_part_lower; %
 Pocklington Integral for j not equal to k
        if j == k
        % This is done to avoid very small numbers in the denominator
            % For all the diagonal elements of Z, terms only need to
 be calculated once
            R_{upper} = sqrt( (-deltaz/2)^2 + a^2); % Here z(m) = z(n)
            R_{lower} = sqrt((deltaz/2)^2 + a^2);
            sum_part_upper = (-deltaz/2)*(1 + 1i*K*R_upper)...
                ./R_upper^3*exp(-1i*K*R_upper);
            sum_part_lower = (deltaz/2)*(1 + 1i*K*R_lower)...
                ./R_lower^3*exp(-1i*K*R_lower);
            num = sqrt(1 + 4*a^2/deltaz^2) + 1;
            denom = sqrt(1 + 4*a^2/deltaz^2) - 1;
            self = (log(num/denom) - 1i*K*deltaz); % Approximation of
 the integral term as described in reference
            Z(j,k) = K^2*self + sum_part_upper - sum_part_lower; %
 Diagonal Elements of the impedance matrix
    end
end
Z = toeplitz(real(Z(1,:))) + 1i*toeplitz(imag(Z(1,:))); % Make a
Toeplitz matrix out of a row vector
V = zeros(M-2,1); % Initialize Source (RHS)
V(floor((M-2)/2)+1) = -1i*4*pi*omega*eps0*(1.0/deltaz); % Delta
 Source
I = zeros(M,1);
```

Calculate the current

Plot Solutions

```
global f lambda
global Lengths M
global theta
global Yin
global E_rad_4by5 E_rad
global I wire
% Plot Input Admittance
figure(1);
H = plot(pi*Lengths/lambda, real(Yin)*1e3, pi*Lengths/lambda,
 imaq(Yin)*1e3);
xlim([1 3.5])
H(1).Color = 'black';
H(1).LineWidth = 1.4;
H(2).Color = 'black';
H(2).LineWidth = 1.4;
H(2).LineStyle = '--';
title(['Input Admittance versus length at f = ',int2str(f/1e6), '
MHz'],'Interpreter','latex')
set(gcf,'Color','white'); % Set background color to white
set(gca, 'FontName', 'times new roman') % Set axes fonts to Times New
Roman
ax = gca;
ax.XTick = [0.5 1 2 3];
xlabel('${\beta L}/2$ ','Interpreter','latex'); % X-axis label
ylabel('G and B in mmhos ','Interpreter','latex'); % y-axis label
grid on
legend('Real Part', 'Imaginary Part');
% cleanfigure();
% matlab2tikz('filename',sprintf('ECEN637_HW10_Admittance_plot.tex'));
% First Polar Plot
figure(2)
h1 = polar(theta, abs(E_rad_4by5)./abs(E_rad_4by5(91)));
h1.Color = 'black';
h1.LineWidth = 1.4;
title(['Radiation Pattern of a Wire of length $4\times\lambda/5$ at f
    ',int2str(f/1e6), 'MHz'],'Interpreter','latex')
set(qcf,'Color','white'); % Set background color to white
set (gca, 'FontName', 'times new roman') % Set axes fonts to Times New
Roman
% cleanfigure();
matlab2tikz('filename',sprintf('ECEN637 HW10 Polar plot h 4by5lambda.tex'));
% First Polar Plot
figure(3)
P = polar(theta, 1 * ones(size(theta))); % this is done to set the
polar plot limit to 1.
set(P, 'Visible', 'off')
hold on
h3 = polar(theta, abs(E_rad)./abs(E_rad(91)));
```

```
h3.Color = 'black';
h3.LineWidth = 1.4;
title(['Radiation Pattern of a Wire of length $\lambda$ at f =
 ',int2str(f/1e6), 'MHz'],'Interpreter','latex')
set(gcf,'Color','white'); % Set background color to white
set (gca, 'FontName', 'times new roman') % Set axes fonts to Times New
Roman
% cleanfigure();
matlab2tikz('filename',sprintf('ECEN637_HW10_Polar_plot_h_lambda.tex'));
% Current Plot
figure(4)
x = linspace(-.7*lambda/2, .7*lambda/2, M);
H = plot(x, real(I wire), x, imag(I wire));
ax = gca;
H(1).Color = 'black';
H(1).LineWidth = 1.4;
H(2).Color = 'black';
H(2).LineWidth = 1.4;
H(2).LineStyle = '--';
title(['Current on the wire of half-length h = .35\lambdaa = .35\lambda
 ',int2str(f/le6), 'MHz'],'Interpreter','latex')
set(qcf,'Color','white'); % Set background color to white
set(gca, 'FontName', 'times new roman') % Set axes fonts to Times New
ax.XTick = [-.3498 -0.2625 -0.1750 -0.0875 0 0.0875 0.1750 0.2625]
 0.3498];
ax.XTickLabel = { '-h', '-.75h', '-.5h', '-.25h', '0'}
 ,'.25h', '5h', '.75h', 'h'};
ax.YTick = [-2e-3 -1e-3 \ 0 \ 1e-3 \ 2e-3];
ax.YTickLabel = { '-.002','-.001','0' , '.001', '.002'};
axis([ -.3498 .3498 -2.5e-3 2.5e-3]);
hold on
xlabel('z')
ylabel('A')
legend('Real Part', 'Imaginary Part');
grid on
% cleanfigure();
matlab2tikz('filename',sprintf('ECEN637 HW10 Current on wire plot.tex'));
end
```

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