

# Sommerfeld Integral

## Horizontally Oriented Magnetic Dipole above Silver Half-plane

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**ELECTRICAL & COMPUTER  
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# Theory

## Thin Sheet Simulation

- Volume Integral formulation

$$\mathbf{A} = \frac{\mu}{4\pi} \int_V \mathbf{J}_v(\mathbf{r}') \frac{e^{-jk_1|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} dv'$$

$$\mathbf{E}_1^{scat} = -\frac{j\omega}{k_1^2} (k_1^2 + \nabla\nabla\cdot) \mathbf{A}$$

$$\mathbf{J}_v = \frac{-jk_1}{Z_0} (\epsilon_2 - 1) \mathbf{E}_2$$

- Surface current  $J_s$   
approximated from  $J_v$

- Impedance (Leontovich)  
Boundary Conditions

$$\begin{aligned} \mathbf{E}_{tan} &= \eta Z_0 \hat{\mathbf{n}} \times \mathbf{H} \\ E^i &= \eta Z_0 J_s(x') \\ &+ \frac{\omega\mu}{4} \int_l J_s(x') H_0^{(2)}(k_2|x-x'|) dx' \end{aligned}$$

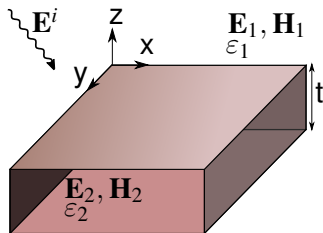


Figure: Dielectric Slab geometry

# Proposed Scheme

## Surface Integral Equation

- Surface Equivalence Theorem

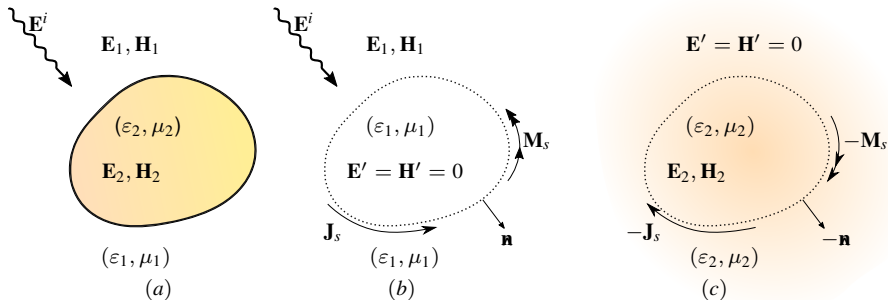


Figure: (a). Actual and its equivalent models for the (b) external and, (c) Internal region

# Proposed Scheme

## Surface Integral Equation

- Exterior Region

$$\mathbf{E}_1 = \mathbf{E}_i + \mathbf{E}_1^{scat}$$

$$= -\frac{\omega}{4k_1^2} (k_1^2 + \nabla \nabla \cdot) \int_C \mathbf{J}_s(\mathbf{p}') H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}'$$

$$- \frac{1}{4\epsilon_j} \nabla \times \int_l \mathbf{M}_s(\rho') H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}' + \mathbf{E}_i$$

$$\mathbf{H}_1 = \mathbf{H}_i + \mathbf{H}_1^{scat}$$

$$= \frac{1}{4j} \nabla \times \int_l \mathbf{J}_s(\rho') H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}'$$

$$- \frac{\omega}{4k_1^2} (k_1^2 + \nabla \nabla \cdot) \int_l \mathbf{M}_s(\rho') H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}' + \mathbf{H}_i$$

# Proposed Scheme

## Surface Integral Equation

- Interior Region

$$\begin{aligned}
 \mathbf{E}_1 &= \mathbf{E}_i + \mathbf{E}_1^{scat} \\
 &= -\frac{\omega}{4k_1^2} (k_1^2 + \nabla \nabla \cdot) \int_C (-\mathbf{J}_s(\mathbf{p}')) H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}' \\
 &\quad - \frac{1}{4j} \nabla \times \int_l (-\mathbf{M}_s(\rho')) H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}' \\
 \mathbf{H}_1 &= \mathbf{H}_i + \mathbf{H}_1^{scat} \\
 &= \frac{1}{4j} \nabla \times \int_l (-\mathbf{J}_s(\rho')) H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}' \\
 &\quad - \frac{\omega}{4k_1^2} (k_1^2 + \nabla \nabla \cdot) \int_l (-\mathbf{M}_s(\rho')) H_0^{(2)}(k_1 |\rho - \rho'|) d\mathbf{l}'
 \end{aligned}$$

# Proposed Scheme

Thin Flat Sheet  $TM_z$

$$\hat{\mathbf{n}} \times (\mathbf{E}_1 - \mathbf{E}_2) = \mathbf{0}$$

$$E_i = \frac{\omega}{4} \int_L J_z(x') \left[ H_0^{(2)}(k_1|x - x'|) + H_0^{(2)}(k_2|x - x'|) \right] dx'$$

$$\hat{\mathbf{n}} \times (\mathbf{H}_1 - \mathbf{H}_2) = \mathbf{0}$$

$$H_i^{tan} = \frac{-j\omega}{4} \int_L M_x(x') \left[ \varepsilon_1 H_0^{(2)}(k_1|x - x'|) + \varepsilon_1 H_2^{(2)}(k_1|x - x'|) \right. \\ \left. + \varepsilon_2 H_0^{(2)}(k_2|x - x'|) + \varepsilon_2 H_2^{(2)}(k_2|x - x'|) \right] dx'$$

# Proposed Scheme

## Method of moments

- Integral equations to system of linear equations

$$\begin{bmatrix} Z_{mn} & 0 \\ 0 & Y_{mn} \end{bmatrix} \begin{bmatrix} J_n \\ M_n \end{bmatrix} = \begin{bmatrix} E_m^i \\ H_m^i \end{bmatrix}$$

- Pulse basis functions and Point matching used
- Far-field

$$RCS(\phi) \simeq \int_0^L [J_z(x')\eta_1 + M_x(x') \sin(\phi_i)] e^{jk_1 x' \cos(\phi_i)} dx'$$

# Two-dimensional Electron Gas (2DEG)

## Existence of Surface Waves

$$\epsilon_1(\omega) \cdot \epsilon_2(\omega) < 0$$

- Criterion met at terahertz frequency range
- Opposite signs of dielectric constant at Semiconductor interface
- GaAs/AlGaAs semiconductor heterostructures
- Strontium Titanate/Lanthanum Aluminate (STO/LAO) oxide