

ELEC 341 – p2

# Project Part 2 – Controller 100 Marks

## Required Files

Available on Canvas

- [e341-p2.pdf](#)
- [p2Submit.p](#)
- [e341-APE.pdf](#)

*Project description (this document)*  
*Grading script (LATEST version)*  
*Instructions for submitting graded work (for reference)*

## Topics

### Controller Identifications

- overhead & filtering delay

### Optimal Control

- phase margin

### Heuristic Tuning

- performance metrics & RCGs

## DESCRIPTION

A system model is shown in **Fig 4**.

- Task-Space coordinates are defined by **Desired Pos** and **Actual Pos**.
- **Desired Pos ( $y_d$ )** & **Actual Pos ( $y_a$ )** are the circumferential distance the gripper would travel **IF** the tine was infinitely stiff (even though it really isn't).
- The results from Part 1 may be used to solve the system model, all except for the controller model ( $\mathbf{G}_c$  &  $\mathbf{H}_c$ ).

The controller parameters are shown in **Table 4**.

- The ISR runs at a control frequency **CF**.
- The duty-cycle of the micro-controller is **DC**. This accounts for total processing time, including all filter calculations.

The RCGs are shown in **Table 5**.

- The resolution of the Newtonian search used to optimize controller poles is specified by **MagRes** and **AngRes**.
- The target phase margin used to determine master gain is **TargPM**.
- After heuristic tuning, the required reduction in overshoot is **OS<sub>u</sub>**.
- After heuristic tuning, the required reduction in settle time is **T<sub>s</sub>**.
- After heuristic tuning, the response must not be over-damped ( $T_r < T_s$ ).
- After heuristic tuning, the steady-state error must satisfy the required **E<sub>ss</sub>**.

Begin with a unity gain, 0-order controller. In other words,  $\mathbf{G}_c=1$ .

Find the forward path gain:  $\mathbf{G} = \mathbf{x}_4/\mathbf{x}_2$  (see **Fig 4**)

Find the task→jnt transform:  $K_{tj} = \mathbf{x}_1/\mathbf{y}_d$  (see **Fig 4**)

Find the jnt→task transform:  $K_{jt} = \mathbf{y}_a/\mathbf{x}_4$  (see **Fig 4**)

### 11. 5 mark(s) Forward Path

- Q11.G (rad/V) LTI Object
- Q11.Ktj (rad/m) scalar
- Q11.Kjt (m/rad) scalar

Whether or not any filtering is done, any controller has delay associated with computations that take place during the duty-cycle, and holding the output signal for 1 control cycle.

Find the delay multiple **N<sub>oh</sub>** that accounts for this overhead.

### 12. 5 mark(s) Delay Overhead

- Q12.Noh (pure) Scalar

Find the frequency of the most dominant pole  $w_d$  of  $GxHs$ .

Find the maximum filter delay  $N_f$  for non-dominant controller FB dynamics.

For the purpose of finding  $N_f$ , round  $w_d$  up to the nearest integer.

Find the corresponding IIR filter time constant **tau** and weighting factor **beta**.

Find the total delay **N**, which includes both the filter and overhead delay.

#### 13. 10 mark(s) IIR Filter

- Q13.wd (rad/s) Scalar
- Q13.Nf (pure) Scalar
- Q13.tau (s) Scalar
- Q13.beta (pure) Scalar
- Q13.N (pure) Scalar

For an FIR filter with a  $4\pi$  window, find the number of coefficients **NC**.

Find the normalized FIR filter coefficients **W**.

#### 14. 10 mark(s) FIR Filter

- Q14.NC (pure) Scalar
- Q14.W (pure) 1x**NC** Vector

**COW:** A 1<sup>st</sup> order LP FIR filter is easy to verify.

If you have a  $4\pi$  window:  $W(\text{last}) / W(1) \approx 2\%$

If you have a  $5\pi$  window:  $W(\text{last}) / W(1) \approx 1\%$

Find controller feedback gain:  $H_c = x_6/x_5$  (see Fig 4)

Find feedback gain:  $H = x_6/x_4$  (see Fig 4)

#### 15. 5 mark(s) Feedback Path

- Q15.Hc (rad/V) LTI Object
- Q15.H (pure) LTI Object

**COW:**

What is the DC gain of  $H$  ??? What should it be ???

Do you expect  $H$  to resemble a 1<sup>st</sup> or 2<sup>nd</sup> order system ??? Under or Over-damped ???

To compensate for FDD noise, use an IIR filter in the derivative path with a time constant  $1/2$  as large as the one used to filter sensor data in the feedback path.

Find the Partial Dynamics  $D_p$ .

Find the initial gain for marginal stability  $K_0$  using the partial dynamics  $D_p$ .

Find the cross-over frequency  $w_{xo}$ .

#### 16. 10 mark(s) Initial Gain

- Q16.Dp (pure) LTI Object
- Q16.K0 (Vs/m) Scalar
- Q16.wxo (rad/s) Scalar

**COW:** Are GM & PM both 0 ??? Should they be ???

Find optimal  $\omega_n$  &  $\zeta$  values to maximize phase margin **PM** using search resolution **WnRes** & **ZetaRes** shown in **Table 5**. Only search values rounded to the search resolution.

Find the associated zero(s) **Z** from the optimal  $\omega_n$  &  $\zeta$  values.

Find the full dynamics **D**.

**17. 15 mark(s) Controller Zeros**

- Q17.Z (rad/s) 1x2 Vector
- Q17.PM (deg) Scalar
- Q17.D (V/rad) LTI Object

Find the master gain **K** that delivers the **TargetPM** shown in **Table 5**.

**18. 5 mark(s) Master Gain**

- Q18.K (V/rad) Scalar

Find the **Reference** gains  $K_p$ ,  $K_i$ ,  $K_d$ , corresponding to unity master gain **K=1**.

**19. 5 mark(s) Reference Gains**

- Q19.Kp (pure) Scalar
- Q19.Ki ( $\text{sec}^{-1}$ ) Scalar
- Q19.Kd (sec) Scalar

Find the **Reference** performance metrics, rise time  $T_r$ , peak time  $T_p$ , settle time  $T_s$ , and input overshoot  $OS_u$ .

**20. 10 mark(s) Reference Performance Metrics**

- Q20.Tr (sec) Scalar
- Q20.Tp (sec) Scalar
- Q20.Ts (sec) Scalar
- Q20.OSu (%) Scalar

Use heuristic tuning to satisfy the RCGs shown in **Table 5**. All RCGs are relative to the **Reference** performance metrics.

Find the **Tuned** gains  $K_p$ ,  $K_i$ ,  $K_d$ , corresponding to unity master gain **K=1**.

**21. 10 mark(s) Tuned Gains**

- Q21.Kp (pure) Scalar
- Q21.Ki ( $\text{sec}^{-1}$ ) Scalar
- Q21.Kd (sec) Scalar

Find the **Tuned** performance metrics, rise time  $T_r$ , peak time  $T_p$ , settle time  $T_s$ , and input overshoot  $OS_u$ .

**22. 10 mark(s) Tuned Performance Metrics**

- Q22.Tr (sec) Scalar
- Q22.Tp (sec) Scalar
- Q22.Ts (sec) Scalar
- Q22.OSu (%) Scalar