

ELEC 341 – p2

Project Part 2 – Controller 100 Marks

Required Files

Available on Canvas

- **e341-p2.pdf**
- **p2Submit.p**
- **e341-APE.pdf**

Project description (this document)

*Grading script (**LATEST** version)*

Instructions for submitting graded work (for reference)

Topics

Controller Identifications

- overhead & filtering delay

Optimal Control

- phase margin

Heuristic Tuning

- performance metrics & RCGs

DESCRIPTION

- A system model is shown in **Fig 4**.
- Task-Space coordinates are defined by **Desired Pos** and **Actual Pos**.
 - **Desired Pos** (y_d) & **Actual Pos** (y_a) are the circumferential distance the gripper would travel **IF** the tine was infinitely stiff (even though it really isn't).
 - The results from Part 1 may be used to solve the system model, all except for the controller model (G_c & H_c).

- The controller parameters are shown in **Table 4**.
- The ISR runs at a control frequency **CF**.
 - The duty-cycle of the micro-controller is **DC**. This accounts for total processing time, including all filter calculations.

- The RCGs are shown in **Table 5**.
- The resolution of the Newtonian search used to optimize controller poles is specified by **MagRes** and **AngRes**.
 - The target phase margin used to determine master gain is **TargPM**.
 - After heuristic tuning, the required reduction in overshoot is **OS_u**.
 - After heuristic tuning, the required reduction in settle time is **T_s**.
 - After heuristic tuning, the response must not be over-damped ($T_r < T_s$).
 - After heuristic tuning, the steady-state error must satisfy the required **E_{ss}**.

Begin with a unity gain, 0-order controller. In other words, $G_c=1$.
Find the forward path gain: $G = x_4/x_2$ (see Fig 4)
Find the task→jnt transform: $K_{tj} = x_1/y_d$ (see Fig 4)
Find the jnt→task transform: $K_{jt} = y_a/x_4$ (see Fig 4)

11. 5 mark(s) Forward Path
- | | | |
|-----------|---------|------------|
| • Q11.G | (rad/V) | LTI Object |
| • Q11.Ktj | (rad/m) | scalar |
| • Q11.Kjt | (m/rad) | scalar |

Whether or not any filtering is done, any controller has delay associated with computations that take place during the duty-cycle, and holding the output signal for 1 control cycle.
Find the delay multiple N_{oh} that accounts for this overhead.

12. 5 mark(s) Delay Overhead
- | | | |
|-----------|--------|--------|
| • Q12.Noh | (pure) | Scalar |
|-----------|--------|--------|

Find the frequency of the most dominant pole $\mathbf{w_d}$ of \mathbf{GxHs} .
Find the maximum filter delay $\mathbf{N_f}$ for non-dominant controller FB dynamics.
For the purpose of finding $\mathbf{N_f}$, round $\mathbf{w_d}$ up to the nearest integer.
Find the corresponding **IIR** filter time constant \mathbf{tau} and weighting factor **beta**.
Find the total delay \mathbf{N} , which includes both the filter and overhead delay.

13. 10 mark(s) IIR Filter

• Q13.wd	(rad/s)	Scalar
• Q13.Nf	(pure)	Scalar
• Q13.tau	(s)	Scalar
• Q13.beta	(pure)	Scalar
• Q13.N	(pure)	Scalar

For an FIR filter with a $\mathbf{4\tau}$ window, find the number of coefficients **NC**.
Find the normalized **FIR** filter coefficients **W**.

14. 10 mark(s) FIR Filter

• Q14.NC	(pure)	Scalar
• Q14.W	(pure)	1x NC Vector

COW: A 1st order LP FIR filter is easy to verify.
If you have a $\mathbf{4\tau}$ window: $\mathbf{W(last) / W(1) \approx 2\%}$
If you have a $\mathbf{5\tau}$ window: $\mathbf{W(last) / W(1) \approx 1\%}$

Find controller feedback gain: $\mathbf{H_c = x_6/x_5}$ (see Fig 4)
Find feedback gain: $\mathbf{H = x_6/x_4}$ (see Fig 4)

15. 5 mark(s) Feedback Path

• Q15.Hc	(rad/V)	LTI Object
• Q15.H	(pure)	LTI Object

COW:
What is the DC gain of \mathbf{H} ??? What should it be ???
Do you expect \mathbf{H} to resemble a 1st or 2nd order system ??? Under or Over-damped ???

To compensate for FDD noise, use an **IIR** filter in the derivative path with a time constant $\mathbf{\frac{1}{2}}$ as large as the one used to filter sensor data in the feedback path.
Find the Partial Dynamics $\mathbf{D_p}$.
Find the initial gain for marginal stability $\mathbf{K_0}$ using the partial dynamics $\mathbf{D_p}$.
Find the cross-over frequency $\mathbf{w_{xo}}$.

16. 10 mark(s) Initial Gain

• Q16.Dp	(pure)	LTI Object
• Q16.K0	(Vs/m)	Scalar
• Q16.wxo	(rad/s)	Scalar

COW: Are GM & PM both 0 ??? Should they be ???

Find optimal ω_n & ζ values to maximize phase margin **PM** using search resolution **WnRes** & **ZetaRes** shown in **Table 5**. Only search values rounded to the search resolution.

Find the associated zero(s) **Z** from the optimal ω_n & ζ values.

Find the full dynamics **D**.

17. 15 mark(s) Controller Zeros

• Q17.Z	(rad/s)	1x2 Vector
• Q17.PM	(deg)	Scalar
• Q17.D	(V/rad)	LTI Object

Find the master gain **K** that delivers the **TargetPM** shown in **Table 5**.

18. 5 mark(s) Master Gain

• Q18.K	(V/rad)	Scalar
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Find the **Reference** gains K_p , K_i , K_d , corresponding to unity master gain **K=1**.

19. 5 mark(s) Reference Gains

• Q19.Kp	(pure)	Scalar
• Q19.Ki	(sec ⁻¹)	Scalar
• Q19.Kd	(sec)	Scalar

Find the **Reference** performance metrics, rise time T_r , peak time T_p , settle time T_s , and input overshoot **OS_u**.

20. 10 mark(s) Reference Performance Metrics

• Q20.Tr	(sec)	Scalar
• Q20.Tp	(sec)	Scalar
• Q20.Ts	(sec)	Scalar
• Q20.OSu	(%)	Scalar

Use heuristic tuning to satisfy the RCGs shown in **Table 5**. All RCGs are relative to the **Reference** performance metrics.

Find the **Tuned** gains K_p , K_i , K_d , corresponding to unity master gain **K=1**.

21. 10 mark(s) Tuned Gains

• Q21.Kp	(pure)	Scalar
• Q21.Ki	(sec ⁻¹)	Scalar
• Q21.Kd	(sec)	Scalar

Find the **Tuned** performance metrics, rise time T_r , peak time T_p , settle time T_s , and input overshoot **OS_u**.

22. 10 mark(s) Tuned Performance Metrics

• Q22.Tr	(sec)	Scalar
• Q22.Tp	(sec)	Scalar
• Q22.Ts	(sec)	Scalar
• Q22.OSu	(%)	Scalar