UCL Mechanical Engineering 2020/2021

MECH0011 Final Coursework

NCWT3

May 19, 2021

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1 Question 1

1.1 a

The data was imported into MATLAB and the shape of the hydrofoil, the chord line and the mean camber line were plotted for all four hydrofoils.

```
clc
   clear
   close all
  %define vars
  i = ["EPPLER 818 Hydrofoil", "NACA 63-412 Aifoil", "RG 8 Airfoil", "YS
      930 Hydrofoil"]; %index hydrofoil names from sheets for ease
  data = zeros (122,2,4); %initialise matrix
   counter = 0; %initialise counter
  x = linspace(0,1,100); %interpolation range initialisation
9
10
  %import data
11
   for j = 1:4 %index all data for plots
12
       counter = counter + 1; %increment counter
13
       data(:,:,counter) = readmatrix('suppFiles.xlsx','Sheet',i(j),'Range',
14
           'A3:B124'); %loop through sheets and pull data
  end
15
16
  %camber line calculation
17
  %pull positive and negative coordinate points
18
  %eppler
19
  dataPos1 = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'A3:B37');
20
   dataNeg1 = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'A38:B70');
21
  %naca
23
   dataPos2 = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'A3:B28');
24
   dataNeg2 = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'A29:B54');
25
26
27
  dataPos3 = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'A3:B34');
   dataNeg3 = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'A35:B64');
29
30
  %ys
31
  dataPos4 = readmatrix('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'A3:B65');
32
   dataNeg4 = readmatrix ('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'A66:B124');
33
34
  %interpolate hydrofoil shape with 100 data points from 0 to 1
  %eppler
36
  dataIntPos1 = interp1(dataPos1(:,1), dataPos1(:,2), x);
37
   dataIntNeg1 = interp1(dataNeg1(:,1), dataNeg1(:,2), x);
38
39
  %naca
```

```
dataIntPos2 = interp1(dataPos2(:,1), dataPos2(:,2), x);
   dataIntNeg2 = interp1(dataNeg2(:,1), dataNeg2(:,2), x);
42
43
   %rg
44
   dataIntPos3 = interp1(dataPos3(:,1), dataPos3(:,2), x);
45
   dataIntNeg3 = interp1(dataNeg3(:,1), dataNeg3(:,2), x);
46
47
   %vs
48
   dataIntPos4 = interp1(dataPos4(:,1), dataPos4(:,2), x);
49
   dataIntNeg4 = interp1(dataNeg4(:,1), dataNeg4(:,2), x);
51
   %calculate camber line
52
   %eppler
53
   camber1 = (dataIntPos1 + dataIntNeg1)./2;
54
55
   camber2 = (dataIntPos2 + dataIntNeg2)./2;
57
58
59
   camber3 = (dataIntPos3 + dataIntNeg3)./2;
60
   %vs
62
   camber 4 = (dataIntPos 4 + dataIntNeg 4)./2;
63
64
   %plot data
65
   subplot (4,1,1)
66
   \operatorname{plot}\left(\operatorname{dataPos1}\left(:,1\right), \operatorname{dataPos1}\left(:,2\right), \operatorname{b}\right), \operatorname{dataNeg1}\left(:,1\right), \operatorname{dataNeg1}\left(:,2\right), \operatorname{b}\right), x
       , camber1, 'r')
   axis image
68
   grid on
69
   xlabel('Chord')
70
   ylabel('Z(x)')
71
   title ('Plot of ' + i(1))
72
   x \lim ([-0.05 \ 1.05])
73
   ylim ([-0.05 \ 0.1])
74
   legend('Hydrofoil profile', 'Mean camber line')
75
76
   subplot (4,1,2)
77
   plot (dataPos2(:,1), dataPos2(:,2), 'b', dataNeg2(:,1), dataNeg2(:,2), 'b', x
       , camber 2 , 'r')
   axis image
79
   grid on
80
   xlabel('Chord')
81
   ylabel('Z(x)')
   title ('Plot of ' + i(2))
   x \lim ([-0.05 \ 1.05])
84
   ylim ([-0.05 \ 0.1])
85
   legend ('Hydrofoil profile', 'Mean camber line')
86
87
   subplot (4,1,3)
   \operatorname{plot}\left(\operatorname{dataPos3}\left(:,1\right),\ \operatorname{dataPos3}\left(:,2\right),'b',\operatorname{dataNeg3}\left(:,1\right),\ \operatorname{dataNeg3}\left(:,2\right),'b',\ x
       , camber 3, 'r')
   axis image
90
```

```
grid on
91
     xlabel('Chord')
92
     ylabel('Z(x)')
93
     title ('Plot of ' + i(3))
    x \lim ([-0.05 \ 1.05])
95
    ylim ([-0.05 \ 0.1])
96
     legend('Hydrofoil profile','Mean camber line')
97
98
     subplot (4,1,4)
99
     \operatorname{plot}\left(\operatorname{dataPos4}\left(:,1\right), \operatorname{dataPos4}\left(:,2\right), \operatorname{b}, \operatorname{dataNeg4}\left(:,1\right), \operatorname{dataNeg4}\left(:,2\right), \operatorname{b}, x\right)
100
          , camber4, 'r')
     axis image
101
     grid on
102
     xlabel('Chord')
103
     ylabel('Z(x)')
104
     title ('Plot of ' + i(4))
105
    x \lim ([-0.05 \ 1.05])
106
    ylim ([-0.05 \ 0.1])
107
    legend('Hydrofoil profile', 'Mean camber line')
108
```

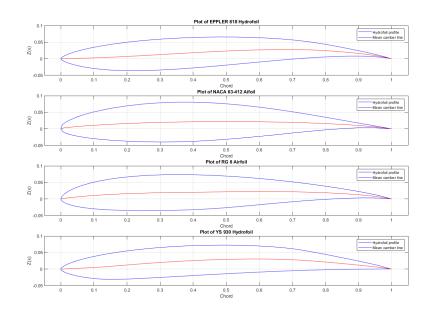


Figure 1: Graphs to show hydrofoil shape, chord line and mean camber line for four different hydrofoils.

1.2 b

MATLAB was used to calculate the lift-to-drag ratio for each hydrofoil.

```
clc
clear
close all
define vars
i = ["EPPLER 818 Hydrofoil", "NACA 63-412 Aifoil", "RG 8 Airfoil", "YS
930 Hydrofoil"]; %index hydrofoil names from sheets for ease
```

```
7
  %pull cl and cd from data
8
  %eppler
  epplerCL = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'E2:E79');
10
  epplerCD = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'F2:F79');
11
12
  %naca
13
  nacaCL = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'E2:E107');
14
  nacaCD = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'F2:F107');
15
16
17
  rgCL = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'E2:E101');
18
  rgCD = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'F2:F101');
19
20
  \% ys
21
  ysCL = readmatrix('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'E2:E78');
  ysCD = readmatrix('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'F2:F78');
23
24
  %plot data
25
   plot (epplerCL, epplerCD, 'r', nacaCL, nacaCD, 'g', rgCL, rgCD, 'b', ysCL, ysCD, '
      magenta')
  legend(i(1), i(2), i(3), i(4))
27
   axis square
28
   grid on
29
  xlabel('C_L')
30
   ylabel ('C_D')
  title ('Plot of lift-to-drag ratio for '+ i(4))
```

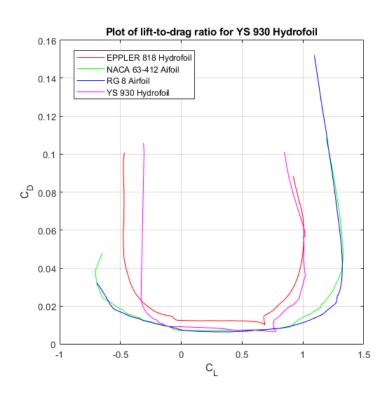


Figure 2: Graph to show lift-to-drag ratio for four different hydrofoils.

1.3 c

At a low angle of attack, the flow is attached to the hydrofoil and separates close to the trailing edge, leaving a small wake. The streamlined shape of the hydrofoil exerts a large shear force on the flow passing over it, leading to a large skin drag but low form drag. As we increase the angle of attack, the flow separation moves along the top of the hydrofoil. This decreases the shear force acting on the hydrofoil and the skin drag starts to reduce, with form drag increasing. At the stall angle, the pressure distribution along the top of the hydrofoil dramatically changes due to flow separation, suction pressure is mostly/all lost and a large wake with turbulent effects is present. The primary drag effect here is now form drag, as the flow is not attached along the length of the hydrofoil surface.

1.4 d

MATLAB was used to calculate each of the variables for each hydrofoil.

```
clc
  clear
2
  close all
3
  %define vars
  i = ["EPPLER 818 Hydrofoil", "NACA 63-412 Aifoil", "RG 8 Airfoil", "YS
      930 Hydrofoil"]; %index hydrofoil names from sheets for ease
  x = linspace(0,1,100); %interpolation range initialisation
  %max percentage camber line calculation
  %camber line calculation
  %pull positive and negative coordinate points
11
  %eppler
12
  dataPos1 = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'A3:B37');
13
  dataNeg1 = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'A38:B70');
14
15
  %naca
16
  dataPos2 = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'A3:B28');
17
  dataNeg2 = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'A29:B54');
18
19
  %rg
20
  dataPos3 = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'A3:B34');
21
  dataNeg3 = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'A35:B64');
22
23
  %ys
24
  dataPos4 = readmatrix('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'A3:B65');
25
  dataNeg4 = readmatrix ('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'A66:B124');
26
  %interpolate hydrofoil shape with 100 data points from 0 to 1
28
  %eppler
29
  dataIntPos1 = interp1(dataPos1(:,1), dataPos1(:,2), x);
30
  dataIntNeg1 = interp1(dataNeg1(:,1), dataNeg1(:,2), x);
31
32
  %naca
33
  dataIntPos2 = interp1(dataPos2(:,1), dataPos2(:,2), x);
34
  dataIntNeg2 = interp1(dataNeg2(:,1), dataNeg2(:,2), x);
35
36
```

```
%rg
37
  dataIntPos3 = interp1(dataPos3(:,1), dataPos3(:,2), x);
38
   dataIntNeg3 = interp1(dataNeg3(:,1), dataNeg3(:,2), x);
39
  \%ys
41
  dataIntPos4 = interp1(dataPos4(:,1), dataPos4(:,2), x);
42
   dataIntNeg4 = interp1(dataNeg4(:,1), dataNeg4(:,2), x);
43
44
  %calculate camber line
  %eppler
46
  camber1 = (dataIntPos1 + dataIntNeg1)./2;
47
48
  %naca
49
  camber2 = (dataIntPos2 + dataIntNeg2)./2;
50
51
52
  camber3 = (dataIntPos3 + dataIntNeg3)./2;
53
54
55
  camber4 = (dataIntPos4 + dataIntNeg4)./2;
56
57
  %maximum camber per hydrofoil
58
  %eppler
59
  percCamber1 = max(camber1);
60
61
  %naca
  percCamber2 = max(camber2);
63
64
65
  percCamber3 = max(camber3);
66
67
  %ys
68
  percCamber4 = max(camber4);
69
70
  %clean-up output
71
  percCamber = 100.*[percCamber1 percCamber2 percCamber3 percCamber4];
72
73
  %maximum percentage thickness calculation
75
   thickness1 = (abs(dataIntPos1) + abs(dataIntNeg1));
76
77
  %naca
78
   thickness2 = (abs(dataIntPos2) + abs(dataIntNeg2));
79
80
81
   thickness3 = (abs(dataIntPos3) + abs(dataIntNeg3));
82
83
  %ys
84
   thickness4 = (abs(dataIntPos4) + abs(dataIntNeg4));
85
  %max thickness per hydrofoil
87
  %eppler
88
  \max Thick1 = \max(thickness1);
```

```
90
   %naca
91
   \max Thick2 = \max(thickness2);
92
   %rg
94
   \max Thick3 = \max(thickness3);
95
96
97
   \max Thick4 = \max(thickness4);
98
99
   %clean-up output
100
   maxThick = 100.*[maxThick1 maxThick2 maxThick3 maxThick4];
101
102
   %maximum lift coefficient
103
   %pull angle of attack, cl and cd from data
   %eppler
105
   epplerData = readmatrix('suppFiles.xlsx', 'Sheet', i(1), 'Range', 'D2:F79');
106
107
   %naca
108
   nacaData = readmatrix('suppFiles.xlsx', 'Sheet', i(2), 'Range', 'D2:F107');
109
110
   %rg
111
   rgData = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'D2:F101');
112
113
   \%ys
114
   ysData = readmatrix('suppFiles.xlsx', 'Sheet', i(4), 'Range', 'D2:F78');
115
116
   %find max cl
117
   %eppler
118
   maxEpplerCL = max(epplerData(:,2));
119
120
   %naca
121
   \max NacaCL = \max(nacaData(:,2));
122
123
124
   \max RgCL = \max(rgData(:,2));
125
126
   %vs
127
   maxYsCL = max(vsData(:,2));
128
129
   %clean-up output
130
   maxCL = [maxEpplerCL maxNacaCL maxRgCL maxYsCL];
131
132
   %find angle of attack at max cl
133
   %eppler
134
   critEppler = epplerData(epplerData(:,2) == maxEpplerCL,1);
135
136
   %naca
137
   critNaca = nacaData(nacaData(:,2) == maxNacaCL,1);
138
   %rg
140
   critRg = rgData(rgData(:,2) = maxRgCL,1);
141
142
```

```
%ys SPECIAL CASE VALUE ASCERTAINED EMPIRICALLY
   critYs = 9;
144
145
   %clean-up output
146
   crit = [critEppler critNaca critRg critYs];
147
148
   \%lift coefficient for alpha = 0
149
   %eppler
150
   liftAlpha0Eppler = epplerData(epplerData(:,1) == 0,2);
151
152
153
   liftAlpha0Naca = nacaData(nacaData(:,1) == 0,2);
154
155
   %rg
156
   liftAlpha0Rg = rgData(rgData(:,1) == 0,2);
157
158
   %vs
159
   liftAlpha0Ys = ysData(ysData(:,1) == 0,2);
160
161
   %clean-up output
162
   liftAlpha0 = [liftAlpha0Eppler liftAlpha0Naca liftAlpha0Rg liftAlpha0Ys];
163
164
   %angle of attack corresponding to cl = 0
165
   %find min cl
166
   %eppler
167
   minEpplerCL = min(abs(epplerData(:,2)));
168
169
   %naca
170
   minNacaCL = min(abs(nacaData(:,2)));
171
172
173
   minRgCL = min(abs(rgData(:,2)));
174
176
   minYsCL = min(abs(ysData(:,2)));
177
178
   %find angle of attack at min cl
179
   %eppler
   AOAMinEppler = epplerData(epplerData(:,2) == minEpplerCL,1);
181
182
183
   AOAMinNaca = nacaData(nacaData(:,2) == -minNacaCL,1);
184
185
186
   AOAMinRg = rgData(rgData(:,2) = -minRgCL,1);
187
188
189
   AOAMinYs = ysData(ysData(:,2) = -minYsCL,1);
190
191
   %clean-up output
192
   AOAMin = [AOAMinEppler AOAMinNaca AOAMinRg AOAMinYs];
193
194
   %generate table
```

T = table(i', percCamber', maxThick', maxCL', crit', liftAlpha0', AOAMin');

| Maximum | | |
|----------------------------------|--|--|
| ber % thickness lift coefficient | | |
| 9.362 1.008 | | |
| 11.992 1.330 | | |
| 10.795 1.323 | | |
| 9.088 1.018 | | |
| | | |

Table 1: Table to show maximum percentage camber and thickness and the maximum lift coefficient for four hydrofoils.

| | | Lift coefficient | Angle of attack α_0 |
|----------------------|-----------------|--------------------------|----------------------------|
| Hydrofoil | Stall angle | for $\alpha = 0^{\circ}$ | corresponding to $C_L = 0$ |
| EPPLER 818 Hydrofoil | 7.75° | 0.361 | -3° |
| NACA 63-412 Aifoil | 13° | 0.338 | -3° |
| RG 8 Airfoil | 12.75° | 0.382 | -3° |
| YS 930 Hydrofoil | 9° | 0.391 | -3.75° |
| | | | |

Table 2: Table to show the stall angle, lift coefficient for $\alpha = 0^{\circ}$ and the angle of attack α_0 corresponding to $C_L = 0$ for four hydrofoils.

The hydrofoils both have a higher percentage camber than the airfoils. They also have a lower percentage thickness than the airfoils. We can see that this leads to a reduction in the stall angle and subsequently their maximum lift coefficients are lower. However, we can see that they perform better at $\alpha = 0^{\circ}$. This can be attributed to the fact that at small α , larger camber generates more lift, at the expense of a smaller stall angle, as the boundary layer is more prone to separation at higher α . However, increasing either percentage camber or thickness will increase C_D .

1.5 e

The RG 8 Airfoil was selected as it has a high stall angle, with a subsequently large maximum lift coefficient, the lift coefficient at $\alpha = 0^{\circ}$ is also the second highest. We can calculate the lift on the hydrofoil using 1.1:

$$L = \frac{1}{2}\rho C_L V_w^2 A \tag{1.1}$$

where ρ is the density of seawater, C_L is the lift coefficient for a given angle of attack, V_w is the velocity of the fluid relative to the wing and A is the projected surface area of the wing. The surface area A can be found by integration:

$$A = \int_{x_0}^{b+x_0} (-0.07x + c_0) \, \mathrm{d}x \tag{1.2}$$

$$A = \left[-0.035x^2 + c_0 x \right]_{x_0}^{b+x_0} \tag{1.3}$$

 $x_0 = 0.1$ as given in the material. I have also selected $b = 2 \,\mathrm{m}$, hence:

$$A = -0.035(2.1)^{2} + c_{0}(2.1) + 0.035(0.1)^{2} - c_{0}(0.1)$$
(1.4)

$$A = 2c_0 - 0.154 \tag{1.5}$$

Substituting 1.5 into 1.1:

$$L = \frac{1}{2}\rho C_L V_w^2 \left(2c_0 - 0.154\right) \tag{1.6}$$

Rearranging for c_0 :

$$(2c_0 - 0.154) = \frac{L}{\frac{1}{2}\rho C_L V_w^2} \tag{1.7}$$

$$c_0 = \frac{L}{\rho C_L V_w^2} + 0.077 \tag{1.8}$$

The following values were used: $\rho = 1036 \,\mathrm{kg}\,\mathrm{m}^{-3}$ [1], $V_w = 11 \,\mathrm{m}\,\mathrm{s}^{-1}$ (39.6 km h⁻¹), $L = 2000 \times 9.81 \approx 20\,000 \,\mathrm{N}$. MATLAB was used to plot the chord length against the angle of attack. As V_w represents the upper speed limit of the boat, we want to select a low angle of attack, to reduce the amount of drag on the foil. Hence, the value for C_L at $\alpha = 0$ will be used.

```
clc
  clear
2
  close all
  %define vars
  i = ["EPPLER 818 Hydrofoil", "NACA 63-412 Aifoil", "RG 8 Airfoil", "YS
      930 Hydrofoil"; %index hydrofoil names from sheets for ease
  Vw = 11; \%39.6 \text{km/h}
  VwLower = 6; \%21.6 km/h
  %pull angle of attack, cl and cd from data
10
11
  rgData = readmatrix('suppFiles.xlsx', 'Sheet', i(3), 'Range', 'D2:F101');
12
13
  %chord length equation
14
  RGChord = ((20000)./(1036.*(Vw^2).*(rgData(rgData(:,1) == 0,2)))) +
      0.077; finds CL at alpha = 0 and inputs into equation and solves
  L = 0.5.*1036.*(Vw^2).*(rgData(rgData(:,1) == 0,2)).*((2.*RGChord) - 0.154)
16
      ; %check
  LLower = 0.5.*1036.*(VwLower^2).*(rgData(rgData(:,1) == 11,2)).*((2.*)
     RGChord) -0.154); %alpha = 11 degrees
```

Our chord length is calculated to be $c_0 = 0.4948 \,\mathrm{m}$. We must now check whether this chord length is sufficient to lift the boat at lower speeds. In order to do this we require a high angle of attack, to generate more lift. The value for C_L at 11° was used to test the lift at $6 \,\mathrm{m\,s^{-1}}$ (21.6 km h⁻¹) and MATLAB gives a lift value of 20 215 N, allowing the boat to be out of the water at lower speeds as well.

2 Question 2

3 Question 3

3.1 a

MATLAB was used to plot the boundary layer velocity profile.

```
clc
  {\tt clear}
  close all
  %import data
  data = readmatrix('suppFiles.xlsx', 'Sheet', 'Boundary Layer', 'Range', 'A2:
      B102;);
  %plot data
  plot(data(:,2), data(:,1))
  axis image
  grid on
  xlim ([0 1])
  ylim ([0 1])
13
  xlabel('y/\delta')
  ylabel('u/U')
15
  title ('Graph to show the boundary layer velocity profile')
```

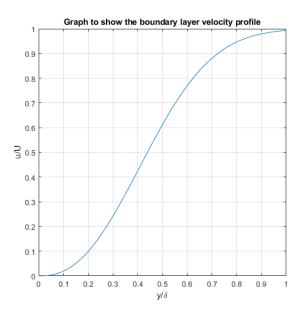


Figure 3: Graph to show boundary layer velocity profile.

4 Question 4

4.1 a

The balanced reaction equation takes the general form:

$$C_x H_v + a (O_2 + 3.76 N_2) \longrightarrow b CO_2 + c H_2 O + 3.76 d N_2$$
 (4.1)

$$CH_4 + a (O_2 + 3.76 N_2) \longrightarrow b CO_2 + c H_2O + 3.76d N_2$$
 (4.2)

where x = 1 and y = 4. Balancing atoms:

$$C: x = b \tag{4.3}$$

$$H: y = 2c \tag{4.4}$$

$$O: 2a = 2b + c \tag{4.5}$$

$$N: 2 \times 3.76a = 2 \times 3.76d \tag{4.6}$$

$$\therefore a = x + \frac{y}{4} = 2 \tag{4.7}$$

$$b = x = 1 \tag{4.8}$$

$$c = \frac{y}{2} = 2 \tag{4.9}$$

$$d = a = 2 \tag{4.10}$$

Therefore our balanced reaction equation is:

$$CH_4 + 2(O_2 + 3.76 N_2) \longrightarrow CO_2 + 2 H_2 O + 7.52 N_2$$
 (4.11)

4.2 b

The air-fuel ratio on a mass basis can be found using

$$AFR = \frac{\text{mass of air}}{\text{mass of fuel}} = \frac{x_{air}}{x_{fuel}} = \frac{n_{air}}{n_{fuel}} \frac{M_{air}}{M_{fuel}}$$
(4.12)

$$AFR = \frac{\left(x + \frac{y}{4}\right)(32 + 3.76 \times 28)}{12x + y} \tag{4.13}$$

$$AFR = \frac{\left(1 + \frac{4}{4}\right)(32 + 3.76 \times 28)}{12 + 4} \tag{4.14}$$

$$AFR = 17.167:1 \tag{4.15}$$

References

[1] Pawlowicz, R. (2013) Key Physical Variables in the Ocean: Temperature, Salinity, and Density. Nature Education Knowledge 4(4):13 https://www.nature.com/scitable/knowledge/library/key-physical-variables-in-the-ocean-temperature-102805293/ Accessed: 19/05/2021 00:00