Chapter 1

Finite Element Method

1.1 Introduction to the method

- Discretisation of the model to elements
- Governing equations for each element
- Assembled to give system equations
- $\bullet \ [k]\{U\} = \{F\}$
- [k] is a square matrix, stiffness matrix $\{U\}$ is the vector of unknown nodal displacements or temperatures and $\{F\}$ is the vector of applied nodal forces

1.2 1D element - the pin jointed bar

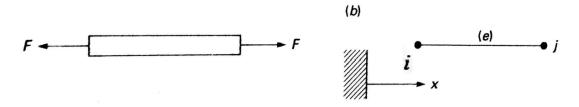


Figure 1.1: Pin jointed bar.

$$u = a + bx \tag{1.1}$$

$$u_i = a + bx_i \tag{1.2}$$

$$u_j = a + bx_j (1.3)$$

where $u_{i,j}$ are unknown nodal displacements and $x_{i,j}$ are known nodal coordinates.

This leads to:

$$a = \frac{\left(u_i x_j - u_j x_i\right)}{L} \tag{1.4}$$

$$b = \frac{\left(u_j - u_i\right)}{L} \tag{1.5}$$

$$u = \frac{x_j - x}{L} u_i + \frac{x - x_i}{L} u_j \tag{1.6}$$

$$u = N_i u_i + N_j u_j (1.7)$$

where $L = x_j - x_i$. N_i and N_j are called shape functions. When a structure is loaded and reaches an equilibrium its potential energy must be minimum.

$$\Pi = \Lambda - W \tag{1.8}$$

where Λ is strain energy and W is work done by external loads (pressure load, body force, nodal forces).

$$W = u_i F_i + u_j F_j = \{U\}^T \{F\}$$
(1.9)

where:

$$\{U\}^T = \begin{bmatrix} u_i & u_j \end{bmatrix} \tag{1.10}$$

$$\{F\} = \begin{Bmatrix} F_i \\ F_j \end{Bmatrix} \tag{1.11}$$

$$\Lambda = \int_{x_i}^{x_j} \left(\frac{1}{2}\sigma\varepsilon A\right) dx \Lambda = \frac{AE}{2} \int_{x_i}^{x_j} \left(\varepsilon^2\right) dx \tag{1.12}$$

where $\sigma = E\varepsilon$ and is the stress, Λ is strain energy density, A is surface area and x is length. Using the definition of strain:

$$\varepsilon = \frac{\mathrm{d}u}{\mathrm{d}x} \tag{1.13}$$

We can differentiate our shape function:

$$\varepsilon = \frac{\left(-u_i + u_j\right)}{I_i} \tag{1.14}$$

Leading to:

$$\Lambda = \frac{AE}{2L} \left(-u_i + u_j \right)^2 \tag{1.15}$$

$$\Lambda = \frac{AE}{2L} \begin{bmatrix} u_i & u_j \end{bmatrix} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_i \\ u_j \end{Bmatrix}$$
 (1.16)

$$= \frac{1}{2} \{U\}^T [k] \{U\} \tag{1.17}$$

where the stiffness matrix is:

$$[k] = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \tag{1.18}$$

Potential energy must be minimised

$$\Pi = \frac{1}{2} \{U\}^T [k] \{U\} - \{U\}^T \{F\}$$
(1.19)

$$\frac{\partial \Pi}{\partial u_i} = \frac{\partial \Pi}{\partial u_j} = 0 \text{ or } \frac{\partial \Pi}{\partial \{U\}} = 0$$
 (1.20)

$$\frac{\partial\Pi}{\partial\{U\}} = [k]\{U\} - \{F\} = 0$$
 (1.21)

$$\Pi = \sum_{e=1}^{E} \left(\Lambda^{(e)} - W \right) \tag{1.23}$$

Leading to:

$$\frac{\partial\Pi}{\partial\{U\}} = \left(\sum_{e=1}^{E} \left[k^{(e)}\right]\right) \{U\} - \{F\} = 0 \tag{1.24}$$

1.2.1 Exercise

Calculate the displacement and stress using the stiffness matrix.

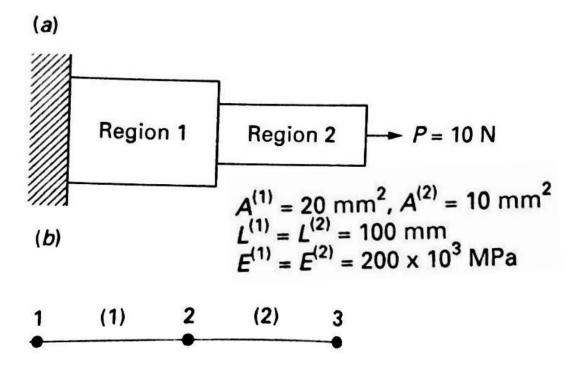


Figure 1.2: Exercise, 3 node 1D problem.

$$[k_1] = \frac{A_1 E_1}{L_1} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 4 & -4 \\ -4 & 4 \end{bmatrix} \times 10^4 \,\mathrm{N}\,\mathrm{mm}^{-1}$$
 (1.25)

$$[k_2] = \frac{A_2 E_2}{L_2} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 2 & -2 \\ -2 & 2 \end{bmatrix} \times 10^4 \,\mathrm{N}\,\mathrm{mm}^{-1}$$
 (1.26)

$$[k] = \begin{bmatrix} 4 & -4 & 0 \\ -4 & 6 & -2 \\ 0 & -2 & 2 \end{bmatrix} \times 10^4 \,\mathrm{N}\,\mathrm{mm}^{-1}$$
 (1.27)

$$\{F\}^{T} = \begin{bmatrix} 0 & 0 & 10 \end{bmatrix} 10^{4} \times \begin{bmatrix} 4 & -4 & 0 \\ -4 & 6 & -2 \\ 0 & -2 & 2 \end{bmatrix} \begin{Bmatrix} u_{1} \\ u_{2} \\ u_{3} \end{Bmatrix} = \begin{Bmatrix} 0 + R1 \\ 0 \\ 10 \end{Bmatrix}$$
 (1.28)

Leading to (commented in Latex):