

# Numerical simulation of dynamic processes in a nuclear reactor by state change modal method

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Multiscale Methods and Large-scale Scientific Computing  
August 2, 2017, Yakutsk

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# Introduction

- Neutron transport
- Multigroup diffusion equation
- Spectral problems
- Quasistatic method
- Modal method



In this paper, we formulate a general strategy for the approximate solution of nonstationary problems of neutron transport in nuclear reactors, which is oriented to fast real-time calculations using the State Change Modal (SCM) method.

# Problem statement

## Multigroup diffusion approximation

$$\begin{aligned} \frac{1}{v_g} \frac{\partial \phi_g}{\partial t} - \nabla \cdot D_g \nabla \phi_g + \Sigma_{rg} \phi_g - \sum_{g' \neq g}^G \Sigma_{s, g' \rightarrow g} \phi_{g'} &= \\ = (1 - \beta) \chi_g \sum_{g'=1}^G \nu \Sigma_{fg'} \phi_{g'} + \tilde{\chi}_g \sum_{m=1}^M \lambda_m c_m, \quad g = 1, 2, \dots, G. \end{aligned}$$

The density of sources of delayed neutrons is described as follows:

$$\frac{\partial c_m}{\partial t} + \lambda_m c_m = \beta_m \sum_{g=1}^G \nu \Sigma_{fg} \phi_g, \quad m = 1, 2, \dots, M,$$

where  $\beta_m$  is a fraction of delayed neutrons of  $m$  type, and

$$\beta = \sum_{m=1}^M \beta_m.$$

# Initial and boundary conditions

The albedo-type conditions are set at the boundary  $\partial\Omega$  of the area  $\Omega$ :

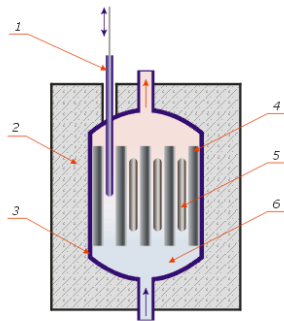
$$D_g \frac{\partial \phi_g}{\partial n} + \gamma_g \phi_g = 0, \quad g = 1, 2, \dots, G,$$

where  $n$  is outer normal to the boundary  $\partial\Omega$ .

We consider boundary problem with the initial condition:

$$\phi_g(\mathbf{x}, 0) = \phi_g^0(\mathbf{x}), \quad g = 1, 2, \dots, G,$$

$$c_m(\mathbf{x}, 0) = c_m^0(\mathbf{x}), \quad m = 1, 2, \dots, M.$$



# Operator formulation

Let's write the boundary problem in operator form. Define vectors

$\phi = \{\phi_1, \phi_2, \dots, \phi_G\}$ ,  $\mathbf{c} = \{c_1, c_2, \dots, c_M\}$  and matrix:

$$\begin{aligned} V &= (v_{gg'}), & v_{gg'} &= \delta_{gg'} v_g^{-1}, & D &= (d_{gg'}), & d_{gg'} &= -\delta_{gg'} \nabla \cdot D_g \nabla, \\ S &= (s_{gg'}), & s_{gg'} &= \delta_{gg'} \Sigma_g - \Sigma_{s,g' \rightarrow g}, & R &= (r_{gg'}), & r_{gg'} &= (1 - \beta) \chi_g \nu \Sigma_{fg'}, \\ B &= (b_{gm}), & b_{gm} &= \tilde{\chi}_g \lambda_m, & \Lambda &= (\lambda_{mm'}), & \lambda_{mm'} &= \lambda_m \delta_{mm'}, \\ Q &= (q_{mg}), & q_{mg} &= \beta_m \nu \Sigma_{fg}, & g, g' &= 1, 2, \dots, G, & m, m' &= 1, 2, \dots, M. \end{aligned}$$

Using the set definitions, we get boundary problem in operator formulation:

$$\begin{aligned} V \frac{d\phi}{dt} + (D + S)\phi &= R\phi + B\mathbf{c}, \\ \frac{d\mathbf{c}}{dt} + \Lambda\mathbf{c} &= Q\phi. \end{aligned}$$

The Cauchy problem is solved under the following initial conditions:

$$\phi(0) = \phi^0, \quad \mathbf{c}(0) = \mathbf{c}^0,$$

where  $\phi^0 = \{\phi_1^0, \phi_2^0, \dots, \phi_G^0\}$ ,  $\mathbf{c}^0 = \{c_1^0, c_2^0, \dots, c_M^0\}$ .

# Finite element method

Let  $H^1(\Omega)$  – sobolev space,  $v \in H^1$ :  $v^2$  and  $|\nabla v|^2$  have a finite integral in  $\Omega$ . For  $\mathbf{v} = \{v_1, v_2, \dots, v_d\}$  define  $V^d = [H^1(\Omega)]^d$ . For test functions use notations  $\xi = \{\xi_1, \xi_2, \dots, \xi_G\}$ ,  $\zeta = \{\zeta_1, \zeta_2, \dots, \zeta_M\}$ .

In variation formulation we are looking for  $\phi \in V^D$ ,  $\mathbf{c} \in V^M$  such that:

$$\begin{aligned} \int_{\Omega} \left( v \frac{\phi^{n+1} - \phi^n}{\tau} + S \phi^{n+1} \right) \xi dx + \int_{\Omega} \sum_{g=1}^G D_g \nabla \phi_g^{n+1} \nabla \xi_g dx + \\ + \int_{\partial\Omega} \sum_{g=1}^G \gamma_g \phi_g^{n+1} \xi_g dx = \int_{\Omega} R \phi^{n+1} \xi dx + \int_{\Omega} B \mathbf{c}^{n+1} \xi dx, \\ \int_{\Omega} \mathbf{c}^{n+1} \zeta dx = \int_{\Omega} \tilde{\Lambda} \mathbf{c}^n \zeta dx + \int_{\Omega} \tau Q \phi^{n+1} \zeta dx \end{aligned}$$

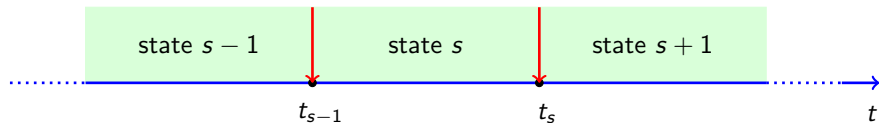
for all  $\xi \in V^D$ ,  $\zeta \in V^M$ .

Let introduce a discrete function spaces  $V_h^D \subset V^D$ ,  $V_h^M \subset V^M$  and define discrete variational problem.

The standard Lagrangian finite elements of degree  $p = 1, 2$  and  $3$  are used.

# State change scheme

The state of the reactor is characterized by the constant coefficients of the system of multigroup diffusion equations.



Dynamic processes in a nuclear reactor can be considered as a change of states. At a certain time  $t = t_s$ ,  $s = 1, 2, \dots$  an instantaneous change of state occurs. The state  $s$  is defined by the parameters in equations:

$$V(t) = V(t_s), \quad D(t) = D(t_s), \quad S(t) = S(t_s), \quad R(t) = R(t_s), \quad B(t) = B(t_s)$$

$$\Lambda(t) = \Lambda(t_s), \quad Q(t) = Q(t_s), \quad t_{s-1} < t \leq t_s, \quad s = 1, 2, \dots$$



# Modal approximation

An approximate description of the non-stationary process at a separate stage is based on modal approximation. An approximate solution is sought in the form of decomposition in eigenfunctions of time and  $\alpha$ -eigenvalue problem.

Let's  $\mathbf{u} = \{\phi, \mathbf{c}\}$ ,  $\phi(t_{s-1}) = \phi^s$ ,  $\mathbf{c}(t_{s-1}) = \mathbf{c}^s$ . In a separate stage  $s$  the following system is considered

$$\mathbf{B} \frac{d\mathbf{u}}{dt} + \mathbf{A}\mathbf{u} = 0, \quad t_{s-1} < t \leq t_s,$$

with constants

$$\mathbf{A} = \begin{pmatrix} D(t_s) + S(t_s) - R(t_s) & -B(t_s) \\ -Q(t_s) & \Lambda(t_s) \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} V(t_s) & 0 \\ 0 & I \end{pmatrix}.$$

Supplemented by the corresponding initial condition

$$\mathbf{u}(t_{s-1}) = \mathbf{u}^s.$$

The main feature of the problems we are considering is that the matrices  $\mathbf{A}_h$  and  $\mathbf{B}_h$  are real and asymmetric.

# Modal approximation

The modal approximation corresponds to the representation of the approximate solution ( $\mathbf{u}_h \approx \mathbf{u}_N$ ) of problem in the following form

$$\mathbf{u}_N(\mathbf{x}, t) = \sum_{n=1}^N a_n(t) \mathbf{w}_n(\mathbf{x}),$$

where  $N$  is the number of dominant eigenvalues of the spectral problem,  $\mathbf{w}_n(\mathbf{x})$  — corresponding eigenfunctions.

Let us define eigenfunctions and eigenvalues as the solution of the  $\alpha$ -eigenvalue problem:

$$\mathbf{A}_h \mathbf{v} = \lambda \mathbf{B}_h \mathbf{v}.$$

Then we obtain

$$\begin{aligned} a_n(t) \mathbf{w}_n(\mathbf{x}) &= b_n \operatorname{Re}(\exp(-\lambda_n(t - t_{s-1})) \mathbf{v}_n(\mathbf{x})), \\ a_{n+1}(t) \mathbf{w}_{n+1}(\mathbf{x}) &= b_{n+1} \operatorname{Im}(\exp(-\lambda_n(t - t_{s-1})) \mathbf{v}_n(\mathbf{x})). \end{aligned}$$

A special attention should be paid to define the coefficients  $a_n(t_{s-1}) = b_n$ ,  $n = 1, 2, \dots, N$ . For this, the initial condition is involved. For example, in the case of real eigenvalues, we have

$$\mathbf{u}_h^s(\mathbf{x}) = \sum_{n=1}^{N_h} b_n \mathbf{v}_n(\mathbf{x}).$$

# Time scale processes

The initial condition includes two components

$$\mathbf{u}_h^s(\mathbf{x}) = (\phi_h^s(\mathbf{x}), \mathbf{c}_h^s(\mathbf{x})).$$

Dynamic behaviour of these components is due to different time-scale processes.

Delayed neutrons source determines **slow processes**, when  $\mathbf{c}(\mathbf{x}, t)$  changes slightly with the reactor state change. In contrast, neutron flux  $\phi(\mathbf{x}, t)$  determines **fast processes** when the reactor state changes.

By virtue of this separation of dynamic processes, we model the slow phase of the dynamics of the reactor with modal approximation and orientate ourselves on the approximate prediction of the initial state for delayed neutrons, only the function  $\mathbf{c}_h^s(\mathbf{x})$  is approximated. The approximation  $\phi_h^s(\mathbf{x})$  is not of interest to us, we do not model a fast phase of the state change.

# Adjoint spectral problem

Consider the adjoint spectral problem

$$\mathbf{A}_h^T \tilde{\mathbf{v}} = \lambda \mathbf{B}_h^T \tilde{\mathbf{v}}.$$

The eigenfunctions of problems are orthogonal in the sense of the equality

$$(\mathbf{B}_h \mathbf{v}_n, \tilde{\mathbf{v}}_m) = 0, \quad m \neq n, \quad m, n = 1, 2, \dots, N_h.$$

In view of this, one can obtain

$$b_n = \frac{1}{(\mathbf{B}_h \mathbf{v}_n, \tilde{\mathbf{v}}_n)} (\mathbf{u}_h^s, \mathbf{B}_h \tilde{\mathbf{v}}_n), \quad n = 1, 2, \dots, N_h.$$

In the approximate solution of problem only the first  $N$  coefficients  $b_n$  are used:

$$\mathbf{c}_h^s(\mathbf{x}) \approx \sum_{n=1}^N b_n \mathbf{c}_n(\mathbf{x}),$$

where  $\mathbf{v}_n(\mathbf{x}) = (\phi_n(\mathbf{x}), \mathbf{c}_n(\mathbf{x}))$ . In this case, the spectral problems are solved for  $N$  dominant eigenvalues.

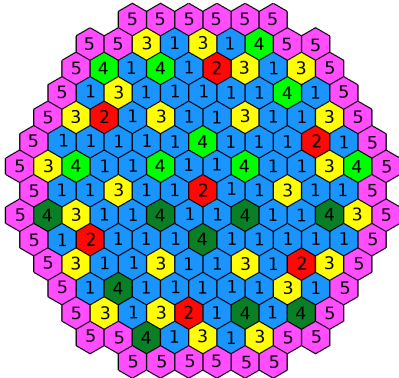
# Computation scheme

**Off-line calculation.** Calculation of the coefficients of the mathematical model of the multigroup diffusion approximation for the isolated reactor states, which is performed in advance. The status passport also includes calculated dominant eigenvalues and eigenfunctions of the  $\alpha$ -eigenvalue problem. These data can be supplemented by dominant eigenvalues and eigenvalues of the conjugate eigenvalue problem.

**On-line calculation.** Real-time modeling is carried out on the basis of the modal solution of the problem. The coefficients in the representation are calculated from the initial condition. The solution for other time intervals is determined according to modal approximation.

# VVER-1000 benchmark

The dynamics of the VVER-1000 reactor during the transition from the supercritical mode to the subcritical mode



- two-dimensional
- two group instantaneous and one group of delayed neutrons
- triangles per cassette  $\kappa$  varies from 6 to 96
- order of finite elements  $p$  varies from 1 to 3
- two types of perturbation

# Supercritical state: $\alpha$ -eigenvalue problem

Table: Eigenvalues  $\alpha_n = \lambda_n^{(\alpha)}$ ,  $n = 1, 2, \dots, 5$

$p$	$\kappa$	$\alpha_1$	$\alpha_2, \alpha_3$	$\alpha_4, \alpha_5$
1	6	-0.22557	$0.04241 \mp 3.08808\text{e-}06i$	$0.06588 \mp 4.80449\text{e-}07i$
	24	-0.82690	$0.03777 \mp 5.37884\text{e-}06i$	$0.06489 \mp 1.37315\text{e-}06i$
	96	-1.74998	$0.03619 \mp 5.69002\text{e-}06i$	$0.06456 \mp 1.40299\text{e-}06i$
2	6	-2.10154	$0.03592 \mp 4.96474\text{e-}06i$	$0.06452 \mp 1.21320\text{e-}06i$
	24	-2.46601	$0.03562 \mp 5.78277\text{e-}06i$	$0.06445 \mp 1.40897\text{e-}06i$
	96	-2.50375	$0.03559 \mp 5.80693\text{e-}06i$	$0.06444 \mp 1.41324\text{e-}06i$
3	6	-2.47975	$0.03561 \mp 5.83718\text{e-}06i$	$0.06445 \mp 1.41869\text{e-}06i$
	24	-2.50294	$0.03559 \mp 5.80783\text{e-}06i$	$0.06444 \mp 1.41341\text{e-}06i$
	96	-2.51280	$0.03558 \mp 5.80954\text{e-}06i$	$0.06444 \mp 1.41362\text{e-}06i$

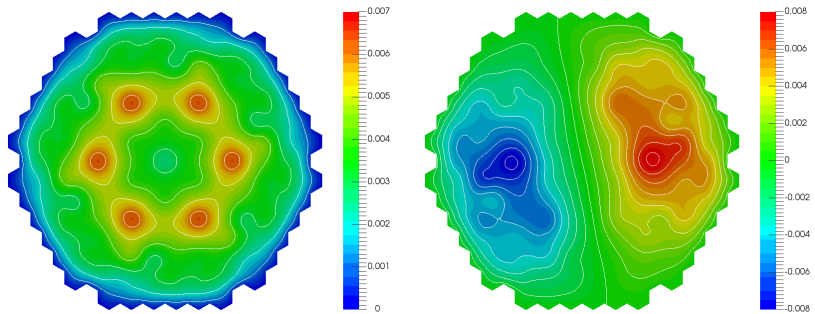
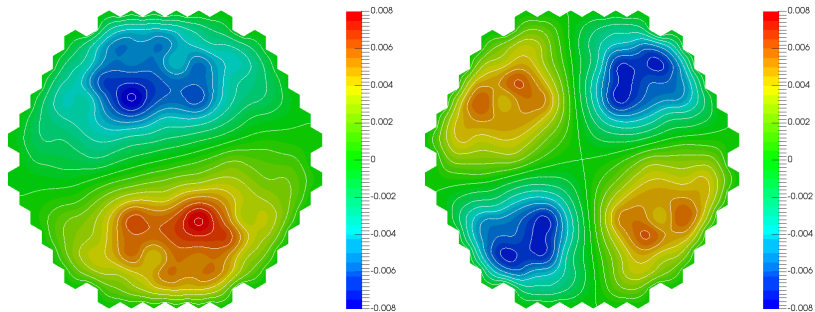


Figure: The eigenfunction  $\varphi_1^{(1)}$  (left) and real part of eigenfunctions  $\varphi_1^{(2)}$ ,  $\varphi_1^{(3)}$  (right).





**Figure:** Imaginary part of eigenfunctions  $\varphi_1^{(2)}$ ,  $-\varphi_1^{(3)}$  (left) and real part of eigenfunctions  $\varphi_1^{(4)}$ ,  $\varphi_1^{(5)}$  (right).

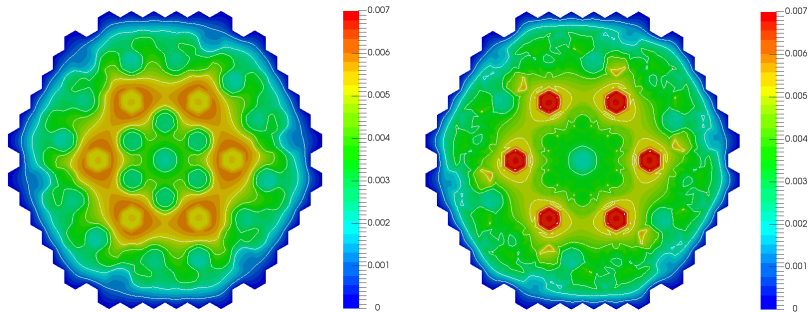


Figure: The eigenfunction  $\varphi_2^{(1)}$  (left) and the eigenfunctions  $s^{(1)}$  (right).

# Adjoint spectral problem

**Table:** Eigenvalues  $\alpha_n = \lambda_n^{(\alpha)}$ ,  $n = 1, 2, \dots, 10$  for direct and adjoint problems

$n$	$\alpha_n$ for direct	$\alpha_n$ for adjoint
1	-2.51280117966	-2.51280117972
2,3	0.0355815000364 $\mp$ 5.80954455861e-06	0.0355815000365 $\mp$ 5.80954421646e-06
4,5	0.0644427013767 $\mp$ 1.41362187449e-06	0.0644427013767 $\mp$ 1.41362190730e-06
6	0.0702618501639	0.0702618501639
7	0.0714652882224	0.0714652882164
8	0.0726456060606	0.0726456060606
9,10	0.0734708921578 $\mp$ 4.02332269037e-08	0.0734708921578 $\mp$ 4.02332146248e-08

Table: Scalar product  $(\phi_1^{(n)}, \phi_1^{(m)})$ ,  $n, m = 1, 2, \dots, 5$

$n \backslash m$	1	2	3	4	5
1	1.0e-00	1.3e-08	2.2e-08	-3.8e-08	9.8e-09
2	1.3e-08	1.0e-00	-1.6e-08	-1.6e-08	1.4e-08
3	2.2e-08	-1.6e-08	1.0e-00	-9.8e-09	-1.1e-08
4	-3.8e-08	-1.6e-08	-9.8e-09	1.0e-00	-3.9e-10
5	9.8e-09	1.4e-08	-1.1e-08	-3.9e-10	1.0e-00
6	-1.8e-09	4.1e-08	-1.8e-08	-1.1e-08	2.9e-09
7	1.0e-02	1.2e-09	1.1e-08	1.4e-08	-1.6e-08
8	-3.2e-09	-2.0e-07	-3.3e-08	4.0e-09	-1.9e-08
9	-2.2e-08	-3.1e-03	-7.5e-03	3.0e-09	6.3e-09
10	1.6e-09	7.5e-03	-3.1e-03	-1.1e-08	6.3e-09

Within the modal method, we can not rely on high accuracy when considering a relatively small number of dominant eigenvalues. Therefore, in the example under consideration, we can assume that the eigenvalues are real, and the corresponding eigenfunctions are orthogonal. Instead of

$$b_n = \frac{1}{(\mathbf{B}_h \mathbf{v}_n, \tilde{\mathbf{v}}_n)} (\mathbf{u}_h^s, \mathbf{B}_h \tilde{\mathbf{v}}_n), \quad n = 1, 2, \dots, N_h$$

coefficients are used

$$b_n \approx \frac{1}{(\mathbf{c}_n, \mathbf{c}_n)} (\mathbf{c}_h^s, \mathbf{c}_n), \quad n = 1, 2, \dots, N,$$

to approximate the initial condition.

# The symmetric perturbation

In the supercritical mode, due to the sufficiently large magnitude of the main eigenvalue, the regular regime of the reactor is rapidly developing, where

$$\mathbf{u}(\mathbf{x}, t) \approx a_1 \exp(-\alpha_1 t) \mathbf{v}_1^0(\mathbf{x}).$$

Here  $\mathbf{v}_1^0(\mathbf{x})$  is the first mode of the supercritical state. We consider the problem with the transition from this supercritical state at  $t_0 = 0$  to the subcritical state.

The subcritical stage is characterized by a 15% increase in the coefficient  $\Sigma_2$  for material 4 in the VVER-1000 test diffusion constants. Thus, the dynamics of the reactor is as follows:

$$\Sigma_2 \longrightarrow 1.15\Sigma_2 \quad (\text{material 4}).$$

The initial state is characterized by specifying the initial conditions at  $t_0 = 0$  as

$$\mathbf{u}(\mathbf{x}, 0) = \mathbf{v}_1^0(\mathbf{x}).$$

**Table:** Subcritical state:  $\alpha_n = \lambda_n^{(\alpha)}$ ,  $n = 1, 2, \dots, 5$

$p$	$\kappa$	$\alpha_1$	$\alpha_2, \alpha_3$	$\alpha_4, \alpha_5$
1	6	0.03602	$0.05760 \mp 1.49652\text{e-}06i$	$0.06890 \mp 4.92606\text{e-}07i$
	24	0.02656	$0.05502 \mp 2.06007\text{e-}06i$	$0.06804 \mp 1.01253\text{e-}06i$
	96	0.02276	$0.05411 \mp 2.16813\text{e-}06i$	$0.06774 \mp 1.03843\text{e-}06i$
2	6	0.02250	$0.05404 \mp 1.81823\text{e-}06i$	$0.06772 \mp 8.73562\text{e-}07i$
	24	0.02144	$0.05380 \mp 2.19400\text{e-}06i$	$0.06765 \mp 1.04253\text{e-}06i$
	96	0.02125	$0.05376 \mp 2.20812\text{e-}06i$	$0.06763 \mp 1.04715\text{e-}06i$
3	6	0.02139	$0.05379 \mp 2.22579\text{e-}06i$	$0.06764 \mp 1.05369\text{e-}06i$
	24	0.02124	$0.05376 \mp 2.20883\text{e-}06i$	$0.06763 \mp 1.04736\text{e-}06i$
	96	0.02122	$0.05376 \mp 2.20951\text{e-}06i$	$0.06763 \mp 1.04756\text{e-}06i$

For an approximate solution, we use the following formulation:

$$\mathbf{u}_N(\mathbf{x}, t) = \sum_{n=1}^N b_n \exp(-\operatorname{Re} \alpha_n t) \mathbf{v}_n(\mathbf{x}),$$

where the coefficients  $b_n$ ,  $n = 1, 2, \dots, N$  are calculated according to the given initial condition.

We distinguish two phases of the dynamic process: fast and slow. In the fast phase, the initial condition: from the function  $\mathbf{u}(\mathbf{x}, 0)$  to the function  $\mathbf{u}_N(\mathbf{x}, 0)$ . The slow phase is associated with the evolution of the solution according to above equation. Within the state change modal technology, the fast phase is not modeled at all.



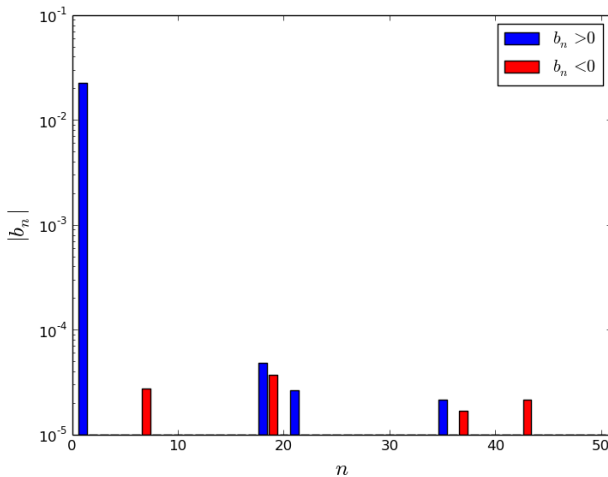
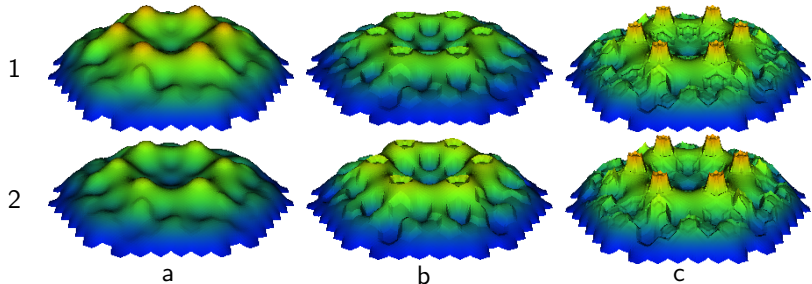


Figure: Approximate solution coefficients



**Figure:** Function  $u(x, 0)$  (string 1) and function  $u_N(x, 0)$  (ctstring 2): a — neutron flux of group 1, b — neutron flux of group 2, c — delayed neutrons source.

Let us pay attention to the substantial restructuring of the solution, which is illustrated by large changes in the neutron flux amplitudes for the first and second groups.

# The asymmetric perturbation

Consider a more complex transition to a subcritical state. The subcritical stage will be characterized by a different increase in the coefficient  $\Sigma_2$  for material 4 in the diffusion constants in the upper and lower half of the reactor cross-section. Now let the reactor dynamics corresponds to the following transformation

$$\Sigma_2 \longrightarrow \begin{cases} 1.1\Sigma_2, & \text{material 4 (top part),} \\ 1.2\Sigma_2, & \text{material 4 (bottom part).} \end{cases}$$

All eigenvalues for this reactor state are real.

**Table:** Subcritical asymmetric state:  $\alpha_n = \lambda_n^{(\alpha)}$ ,  $n = 1, 2, \dots, 5$

$p$	$\kappa$	$\alpha_1$	$\alpha_2$	$\alpha_3$	$\alpha_4$	$\alpha_5$
1	6	0.03347	0.05728	0.05788	0.06884	0.06889
	24	0.02333	0.05467	0.05528	0.06797	0.06802
	96	0.01925	0.05374	0.05436	0.06768	0.06772
2	6	0.01894	0.05367	0.05429	0.06765	0.06770
	24	0.01782	0.05343	0.05405	0.06758	0.06762
	96	0.01763	0.05339	0.05401	0.06757	0.06761
3	6	0.01777	0.05342	0.05404	0.06758	0.06762
	24	0.01762	0.05339	0.05400	0.06757	0.06761
	96	0.01760	0.05338	0.05400	0.06757	0.06761

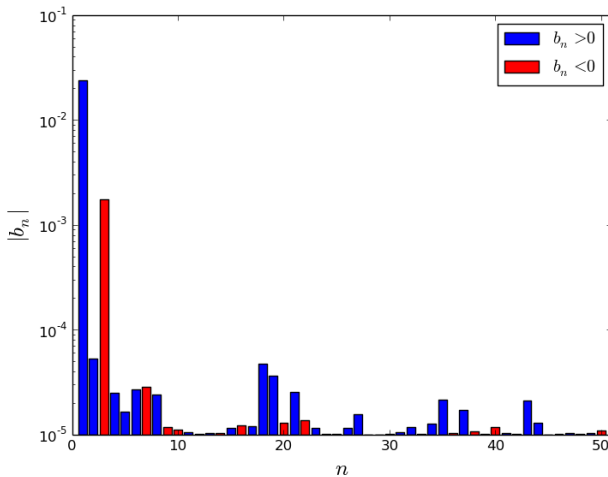
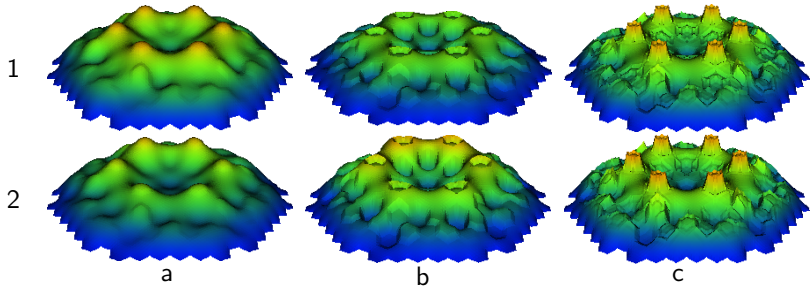


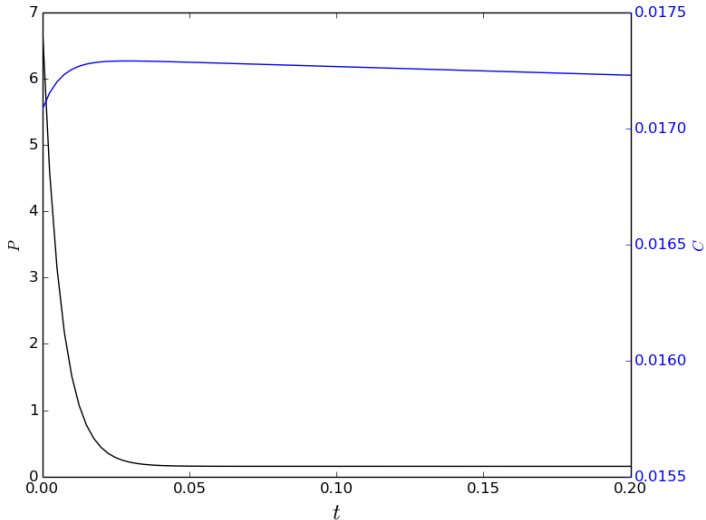
Figure: Approximate solution coefficients



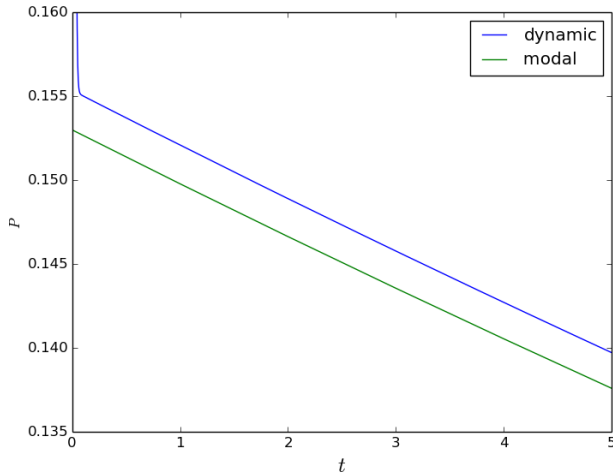
**Figure:** Function  $u(x, 0)$  (string 1) and function  $u_N(x, 0)$  (string 2) for asymmetric perturbation: a — neutron flux of group 1, b — neutron flux of group 2, c — delayed neutrons source.

In the case under consideration, the approximate solution contains several modes and can not be described only by the first mode. Calculations of the end of the fast phase are performed at  $N = 10$ .

# Fast stage of reactor state: neutronic power

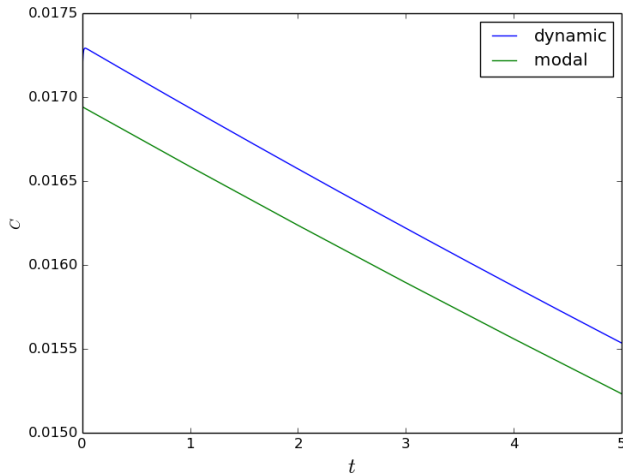


# Slow stage of reactor state: neutronic power

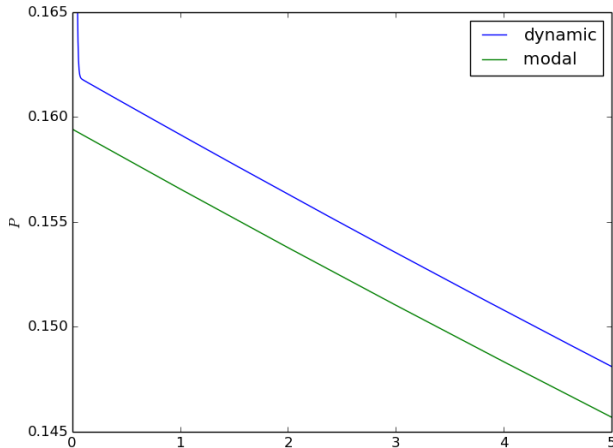




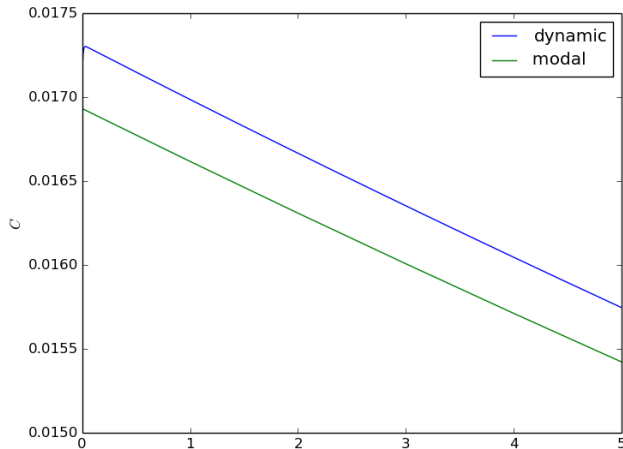
# Slow stage of reactor state: delayed neutrons source



# Slow stage of reactor state for the asymmetric perturbation: neutronic power



# Slow stage of reactor state for the asymmetric perturbation: delayed neutrons source



# Conclusion

- The problem of simulation of reactor dynamic processes is considered on the basis of multigroup neutron diffusion equations accounting for delayed neutrons. The modal approximation is used.
- In the developed SCM method a fast phase and slow phase is allocated
- Offline calculation, online calculation
- Finite Element Method, FEniCS, SLEPc
- The modeling of the reactor state change as a transfer from one state to another state, symmetric and assymetric perturbation
- Comparison of the calculational results obtained by using two methods, one based on modal approximation and another based on the full dynamics calculation

Thank you for your attention!