

## APPENDIX C—EQUIVALENCE BETWEEN SI-METRIC, MKS-METRIC, AND U.S. CUSTOMARY UNITS OF NONHOMOGENOUS EQUATIONS IN THE CODE

Provision number	SI-metric stress in MPa	mks-metric stress in kgf/cm <sup>2</sup>	U.S. Customary units stress in pounds per square inch (psi)
	1 MPa	10 kgf/cm <sup>2</sup>	145 psi
	$f'_c = 21$ MPa	$f'_c = 210$ kgf/cm <sup>2</sup>	$f'_c = 3000$ psi
	$f'_c = 28$ MPa	$f'_c = 280$ kgf/cm <sup>2</sup>	$f'_c = 4000$ psi
	$f'_c = 35$ MPa	$f'_c = 350$ kgf/cm <sup>2</sup>	$f'_c = 5000$ psi
	$f'_c = 40$ MPa	$f'_c = 420$ kgf/cm <sup>2</sup>	$f'_c = 6000$ psi
	$f_y = 280$ MPa	$f_y = 2800$ kgf/cm <sup>2</sup>	$f_y = 40,000$ psi
	$f_y = 420$ MPa	$f_y = 4200$ kgf/cm <sup>2</sup>	$f_y = 60,000$ psi
	$f_y = 550$ MPa	$f_y = 5600$ kgf/cm <sup>2</sup>	$f_y = 80,000$ psi
	$f_y = 690$ MPa	$f_y = 7000$ kgf/cm <sup>2</sup>	$f_y = 100,000$ psi
	$f_{pu} = 1725$ MPa	$f_{pu} = 17,600$ kgf/cm <sup>2</sup>	$f_{pu} = 250,000$ psi
	$f_{pu} = 1860$ MPa	$f_{pu} = 19,000$ kgf/cm <sup>2</sup>	$f_{pu} = 270,000$ psi
	$\sqrt{f'_c}$ in MPa	$3.18 \sqrt{f'_c}$ in kgf/cm <sup>2</sup>	$12 \sqrt{f'_c}$ in psi
	$0.313 \sqrt{f'_c}$ in MPa	$\sqrt{f'_c}$ in kgf/cm <sup>2</sup>	$3.77 \sqrt{f'_c}$ in psi
	$0.083 \sqrt{f'_c}$ in MPa	$0.27 \sqrt{f'_c}$ in kgf/cm <sup>2</sup>	$\sqrt{f'_c}$ in psi
	$0.17 \sqrt{f'_c}$ in MPa	$0.53 \sqrt{f'_c}$ in kgf/cm <sup>2</sup>	$2 \sqrt{f'_c}$ in psi
6.6.4.5.4	$M_{2,min} = P_u(15 + 0.03h)$	$M_{2,min} = P_u(1.5 + 0.03h)$	$M_{2,min} = P_u(0.6 + 0.03h)$
7.3.1.1.1	$\left(0.4 + \frac{f_y}{700}\right)$	$\left(0.4 + \frac{f_y}{7000}\right)$	$\left(0.4 + \frac{f_y}{100,000}\right)$
7.3.1.1.2	$(1.65 - 0.0003w_c)$	$(1.65 - 0.0003w_c)$	$(1.65 - 0.005w_c)$
7.7.3.5(c)	$0.41 \frac{b_w s}{f_{yt}}$	$4.2 \frac{b_w s}{f_{yt}}$	$60 \frac{b_w s}{f_{yt}}$
8.3.1.1	$f_r = 0.41 \sqrt{f'_c}$	$f_r = 1.33 \sqrt{f'_c}$	$f_r = 5 \sqrt{f'_c}$
8.3.1.2(b)	$h = \frac{\ell_n \left(0.8 + \frac{f_y}{1400}\right)}{36 + 5\beta(\alpha_{fm} - 0.2)} \geq 125 \text{ mm}$	$h = \frac{\ell_n \left(0.8 + \frac{f_y}{14,000}\right)}{36 + 5\beta(\alpha_{fm} - 0.2)} \geq 12.5 \text{ cm}$	$h = \frac{\ell_n \left(0.8 + \frac{f_y}{200,000}\right)}{36 + 5\beta(\alpha_{fm} - 0.2)} \geq 5 \text{ in.}$
8.3.1.2(d)	$h = \frac{\ell_n \left(0.8 + \frac{f_y}{1400}\right)}{36 + 9\beta} \geq 90 \text{ mm}$	$h = \frac{\ell_n \left(0.8 + \frac{f_y}{14,000}\right)}{36 + 9\beta} \geq 9 \text{ cm}$	$h = \frac{\ell_n \left(0.8 + \frac{f_y}{200,000}\right)}{36 + 9\beta} \geq 3.5 \text{ in.}$
8.3.4.1	$f_i \leq 0.5 \sqrt{f'_c}$	$f_i \leq 1.6 \sqrt{f'_c}$	$f_i \leq 6 \sqrt{f'_c}$
8.6.2.3	$0.17 \sqrt{f'_c}$ $0.5 \sqrt{f'_c}$	$0.53 \sqrt{f'_c}$ $1.6 \sqrt{f'_c}$	$2 \sqrt{f'_c}$ $6 \sqrt{f'_c}$