- **4.4.3.3** In frames with V bracings, the non-dimensional slenderness $\overline{\lambda}$ should be less than or equal to 2.0.
- **4.4.3.4** In structures of up to two storeys, no limitation applies to $\overline{\lambda}$.
- **4.4.3.5** Yield resistance $N_{\rm pl,Rd}$ of the gross cross-section of the diagonals should be such that $N_{\rm pl,Rd} \ge N_{\rm Ed}$.
- **4.4.3.6** In frames with V bracings, the compression diagonals should be designed for the compression resistance in accordance with EN 1993.
- **4.4.3.7** The connections of the diagonals to any member should satisfy the design rules of **4.2.3**.
- **4.4.3.8** In order to satisfy a homogeneous dissipative behaviour of the diagonals, it should be checked that the maximum overstrength Ω_i defined in **4.4.4.1** does not differ from the minimum value Ω by more than 25%.
- **4.4.3.9** Energy dissipating semi-rigid and/or partial strength connections are permitted, provided that all of the following conditions are satisfied:
- (a) Connections have an elongation capacity consistent with global deformations;
- **(b)** Effect of connections deformation on global drift is taken into account using nonlinear static (pushover) global analysis or non-linear time history analysis.

4.4.4 Beams and columns

4.4.4.1 – Beams and columns with axial forces should meet the following minimum resistance requirement:

$$N_{\rm pl,Rd}(M_{\rm Ed}) \ge N_{\rm Ed,G} + 1.1 \,\gamma_{\rm ov} \,\Omega \,N_{\rm Ed,E}$$
 (4.11)

where $N_{\rm pl,Rd}(M_{\rm Ed})$ is the design buckling resistance of the beam or the column in accordance with EN 1993, taking into account the interaction of the buckling resistance with the bending moment $M_{\rm Ed}$, defined as its design value in the seismic design situation; $N_{\rm Ed,G}$ is the axial force in the beam or in the column due to the non-seismic actions included in the combination of actions for the seismic design situation; $N_{\rm Ed,E}$ is the axial force in the beam or in the column due to the design seismic action; $\gamma_{\rm ov}$ is the overstrength factor, Ω is the minimum value of $\Omega_{\rm i} = N_{\rm pl,Rd,i} / N_{\rm Ed,i}$ over all the diagonals of the braced frame system; where $N_{\rm pl,Rd,i}$ is the design resistance of diagonal i; $N_{\rm Ed,i}$ is the design value of the axial force in the same diagonal i in the seismic design situation.

- **4.4.4.2** In frames with V bracings, the beams should be designed to resist:
- (a) all non-seismic actions without considering the intermediate support given by the diagonals;
- (b) unbalanced vertical seismic action effect applied to the beam by the braces after buckling of the compression diagonal. This action effect is calculated using $N_{\rm pl,Rd}$ for the brace in tension and $\gamma_{\rm pb}$ $N_{\rm pl,Rd}$ for the brace in compression (The factor $\gamma_{\rm pb}$ is used for the estimation of the post buckling resistance of diagonals in compression, which may be taken as 0.3).