CODE

**22.5.6.3** For prestressed members,  $V_c$  shall be permitted to be the lesser of  $V_{ci}$  calculated in accordance with 22.5.6.3.1 and  $V_{cw}$  calculated in accordance with 22.5.6.3.2 or 22.5.6.3.3.

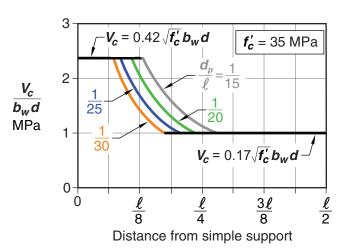
**22.5.6.3.1** The flexure-shear strength  $V_{ci}$  shall be calculated by (a) but need not be taken less than (b) or (c):

(a) 
$$V_{ci} = 0.05\lambda \sqrt{f_c'} b_w d_p + V_d + \frac{V_i M_{cre}}{M_{max}}$$
 (22.5.6.3.1a)

(b) For members with  $A_{ps}f_{se} < 0.4(A_{ps}f_{pu} + A_sf_y)$ ,

$$V_{ci} = 0.14 \lambda \sqrt{f_c'} b_w d$$
 (22.5.6.3.1b)

## COMMENTARY



**Fig. R22.5.6.2**—Application of Table 22.5.6.2 to uniformly loaded prestressed members with  $\mathbf{f_c'} = 35$  MPa.

**R22.5.6.3** Two types of inclined cracking occur in concrete beams: web-shear cracking and flexure-shear cracking. These two types of inclined cracking are illustrated in Fig. R22.5.6.3.

Web-shear cracking begins from an interior point in a member when the principal tensile stresses exceed the tensile strength of the concrete. Flexure-shear cracking is initiated by flexural cracking. When flexural cracking occurs, the shear stresses in the concrete above the crack are increased. The flexure-shear crack develops when the combined shear and flexural-tensile stress exceeds the tensile strength of the concrete.

The nominal shear strength provided by the concrete,  $V_c$ , is assumed equal to the lesser of  $V_{ci}$  and  $V_{cw}$ . The derivations of Eq. (22.5.6.3.1a) and Eq. (22.5.6.3.2) are summarized in ACI Committee 318 (1965).

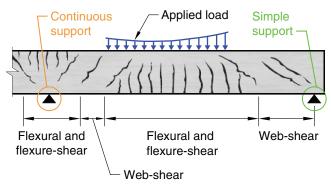


Fig. R22.5.6.3—Types of cracking in concrete beams.

**R22.5.6.3.1** In deriving Eq. (22.5.6.3.1a), it was assumed that  $V_{ci}$  is the sum of the shear required to cause a flexural crack at the section in question given by:

$$V = \frac{V_i M_{cre}}{M_{max}}$$
 (R22.5.6.3.1a)

