

## CODE

## COMMENTARY

**24.5.2.1** Prestressed flexural members shall be classified as Class U, T, or C in accordance with Table 24.5.2.1, based on the extreme fiber stress in tension  $f_t$  in the precompressed tension zone calculated at service loads assuming an uncracked section.

**Table 24.5.2.1—Classification of prestressed flexural members based on  $f_t$**

Assumed behavior	Class	Limits of $f_t$
Uncracked	U <sup>[1]</sup>	$f_t \leq 0.62 \sqrt{f'_c}$
Transition between uncracked and cracked	T	$0.62 \sqrt{f'_c} < f_t \leq 1.0 \sqrt{f'_c}$
Cracked	C	$f_t > 1.0 \sqrt{f'_c}$

<sup>[1]</sup>Prestressed two-way slabs shall be designed as Class U with  $f_t \leq 0.5 \sqrt{f'_c}$ .

**R24.5.2.1** Three classes of behavior of prestressed flexural members are defined. Class U members are assumed to behave as uncracked members. Class C members are assumed to behave as cracked members. The behavior of Class T members is assumed to be in transition between uncracked and cracked. These classes apply to both bonded and unbonded prestressed flexural members, but prestressed two-way slab systems are required to be designed as Class U with  $f_t \leq 0.5 \sqrt{f'_c}$ .

The serviceability requirements for each class are summarized in Table R24.5.2.1. For comparison, Table R24.5.2.1 also shows corresponding requirements for nonprestressed members. Due to lack of strain compatibility, it is inappropriate to include the area of unbonded prestressed reinforcement in the calculation of gross or cracked section properties, although the effective prestress force should be considered when determining the location of the neutral axis. Conversely, the calculation of section properties should account for the area of the voids created by the sheathing or duct for unbonded prestressed reinforcement. A method for evaluating stresses, deflections, and crack control in cracked prestressed members is given in Mast (1998).

The precompressed tension zone is that portion of a prestressed member where flexural tension, calculated using gross section properties, would occur under unfactored dead and live loads if the prestress force was not present. Prestressed concrete is usually designed so that the prestress force introduces compression into this zone, thus effectively reducing the magnitude of the tensile stress.

For corrosive environments, defined as an environment in which chemical attack (such as seawater, corrosive industrial atmosphere, or sewer gas) is encountered, cracking at service loads becomes more critical to long-term performance. For these conditions, cover should be increased in accordance with 20.5.1.4, and tensile stresses in the concrete reduced to minimize possible cracking at service loads.

**Table R24.5.2.1—Serviceability design requirements**

Assumed behavior	Prestressed			Nonprestressed
	Class U	Class T	Class C	
Assumed behavior	Uncracked	Transition between uncracked and cracked	Cracked	Cracked
Section properties for stress calculation at service loads	Gross section 24.5.2.2	Gross section 24.5.2.2	Cracked section 24.5.2.3	No requirement
Allowable stress at transfer	24.5.3	24.5.3	24.5.3	No requirement
Allowable compressive stress based on uncracked section properties	24.5.4	24.5.4	No requirement	No requirement
Tensile stress at service loads 24.5.2.1	$\leq 0.62 \sqrt{f'_c}$	$0.62 \sqrt{f'_c} < f_t \leq 1.0 \sqrt{f'_c}$	No requirement	No requirement
Deflection calculation basis	24.2.3.8, 24.2.4.2 Gross section	24.2.3.9, 24.2.4.2 Cracked section, bilinear	24.2.3.9, 24.2.4.2 Cracked section, bilinear	24.2.3, 24.2.4.1 Effective moment of inertia
Crack control	No requirement	No requirement	24.3	24.3
Computation of $\Delta f_{ps}$ or $f_s$ for crack control	—	—	Cracked section analysis	$M/(A_s \times \text{lever arm})$ , or $2/3 f_y$
Side skin reinforcement	No requirement	No requirement	9.7.2.3	9.7.2.3