

**Table 19.2-1 Values of  $G/G_o$  and  $v_s/v_{so}$** 

Site Class	Value of $v_s/v_{so}$			Value of $G/G_o$		
	$S_{DS}/2.5$			$S_{DS}/2.5$		
	$\leq 0.1$	0.4	$\geq 0.8$	$\leq 0.1$	0.4	$\geq 0.8$
A	1.00	1.00	1.00	1.00	1.00	1.00
B	1.00	0.97	0.95	1.00	0.95	0.90
C	0.97	0.87	0.77	0.95	0.75	0.60
D	0.95	0.71	0.32	0.90	0.50	0.10
E	0.77	0.22	<sup>a</sup>	0.60	0.05	<sup>a</sup>
F	<sup>a</sup>	<sup>a</sup>	<sup>a</sup>	<sup>a</sup>	<sup>a</sup>	<sup>a</sup>

Note: Use straight-line interpolation for intermediate values of  $S_{DS}/2.5$ .

<sup>a</sup>Should be evaluated from site specific analysis

with the soil strain levels associated with the design earthquake motion. The average shear modulus ( $G$ ) for the soils beneath the foundation at large strain levels and the associated shear wave velocity ( $v_s$ ) needed in these computations shall be determined from Table 19.2-1 where

$v_{so}$  = the average shear wave velocity for the soils beneath the foundation at small strain levels ( $10^{-3}$  percent or less)

$G_o = \gamma v_{so}^2/g$  = the average shear modulus for the soils beneath the foundation at small strain levels

$\gamma$  = the average unit weight of the soils

Alternatively, for structures supported on mat foundations that rest at or near the ground surface or are embedded in such a way that the side wall contact with the soil is not considered to remain effective during the design ground motion, the effective period of the structure is permitted to be determined from

$$\tilde{T} = T \sqrt{1 + \frac{25\alpha r_a \bar{h}}{v_s^2 T^2} \left( 1 + \frac{1.12 r_a \bar{h}^2}{\alpha_\theta r_m^3} \right)} \quad (19.2-5)$$

where

$\alpha$  = the relative weight density of the structure and the soil defined by

$$\alpha = \frac{\bar{W}}{\gamma A_o \bar{h}} \quad (19.2-6)$$

$r_a$  and  $r_m$  = characteristic foundation lengths defined by

$$r_a = \sqrt{\frac{A_o}{\pi}} \quad (19.2-7)$$

**Table 19.2-2 Values of  $\alpha_\theta$** 

$r_m/v_s T$	$\alpha_\theta$
$< 0.05$	1.0
0.15	0.85
0.35	0.7
0.5	0.6

and

$$r_m = 4 \sqrt{\frac{4I_o}{\pi}} \quad (19.2-8)$$

where

$A_o$  = the area of the load-carrying foundation

$I_o$  = the static moment of inertia of the load-carrying foundation about a horizontal centroidal axis normal to the direction in which the structure is analyzed

$\alpha_\theta$  = dynamic foundation stiffness modifier for rocking as determined from Table 19.2-2

$v_s$  = shear wave velocity

$T$  = fundamental period as determined in Section 12.8.2

### 19.2.1.2 Effective Damping

The effective damping factor for the structure-foundation system ( $\tilde{\beta}$ ) shall be computed as follows:

$$\tilde{\beta} = \beta_o \frac{0.05}{\left( \frac{\tilde{T}}{T} \right)^3} \quad (19.2-9)$$

where

$\beta_o$  = the foundation damping factor as specified in Fig. 19.2-1

For values of  $\frac{S_{DS}}{2.5}$  between 0.10 and 0.20 the values of  $\beta_o$  shall be determined by linear interpolation vetween the solid lines and the dashed lines of Fig. 19.2-1.

The quantity  $r$  in Fig. 19.2-1 is a characteristic foundation length that shall be determined as follows:

$$\text{For } \frac{\bar{h}}{L_o} \leq 0.5, r = r_a \quad (19.2-10)$$

$$\text{For } \frac{\bar{h}}{L_o} \geq 1, r = r_m \quad (19.2-11)$$