

$$h_c/h_b = 8.6/1.4 = 6.1$$

(in SI: $h_c/h_b = 2.62/0.43 = 6.1$)

Because $h_c/h_b \geq 0.2$ drift loads must be considered (see Section 7.7.1).

$$h_d \text{ (leeward step)} = 3.8 \text{ ft (1.16 m)}$$

(Fig. 7-9 with $p_g = 40 \text{ lb/ft}^2 \text{ (1.92 kN/m}^2\text{)}$
and $l_u = 100 \text{ ft [30.5 m]}$)

$$h_d \text{ (windward step)} = 3/4 \times 4.8 \text{ ft (1.5 m)}$$

$$= 3.6 \text{ ft (1.1 m) (4.8 ft [1.5 m])}$$

from Fig. 7-9 with $p_g = 40 \text{ lb/ft}^2 \text{ [1.92 kN/m}^2\text{]}$
and $l_u = \text{length of lower roof} = 170 \text{ ft [52 m]}$)

Leeward drift governs, use $h_d = 3.8 \text{ ft (1.16 m)}$
Because $h_d < h_c$,

$$h_d = 3.8 \text{ ft (1.16 m)}$$

$$w = 4h_d = 15.2 \text{ ft (4.64 m), say } 15 \text{ ft (4.6 m)}$$

$$p_d = h_d \gamma = 3.8(19) = 72 \text{ lb/ft}^2$$

(in SI: $p_d = 1.16(3.02) = 3.50 \text{ kN/m}^2$)

Rain on Snow Surcharge: A rain-on-snow surcharge load need not be considered because p_g is greater than $20 \text{ lb/ft}^2 \text{ (0.96 kN/m}^2\text{)}$. See Fig. C7-7 for snow loads on both roofs.

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