

## UNIT-4

### OP-AMP Applications-2

#### Comparator:

To obtain for better performance, we shall also look at integrated designed specifically as comparators and converters. A comparator as its name implies, compares a signal voltage on one input of an op-amp with a known voltage called a reference voltage on the other input. Comparators are used in circuits such as,

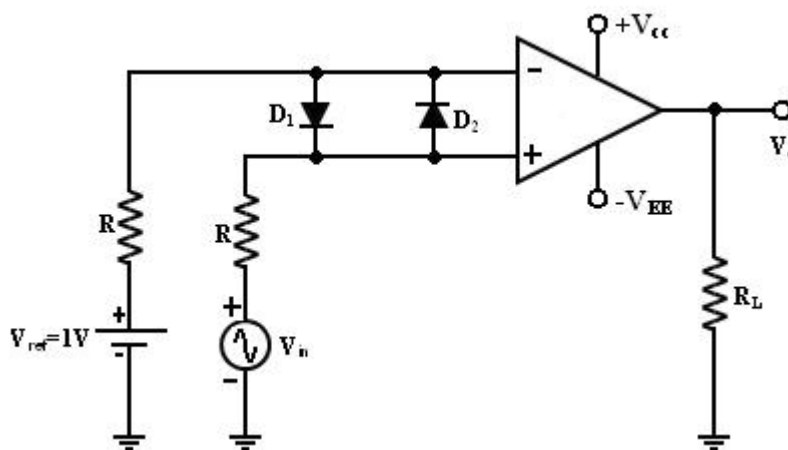
Digital Interfacing

Schmitt Trigger

Discriminator

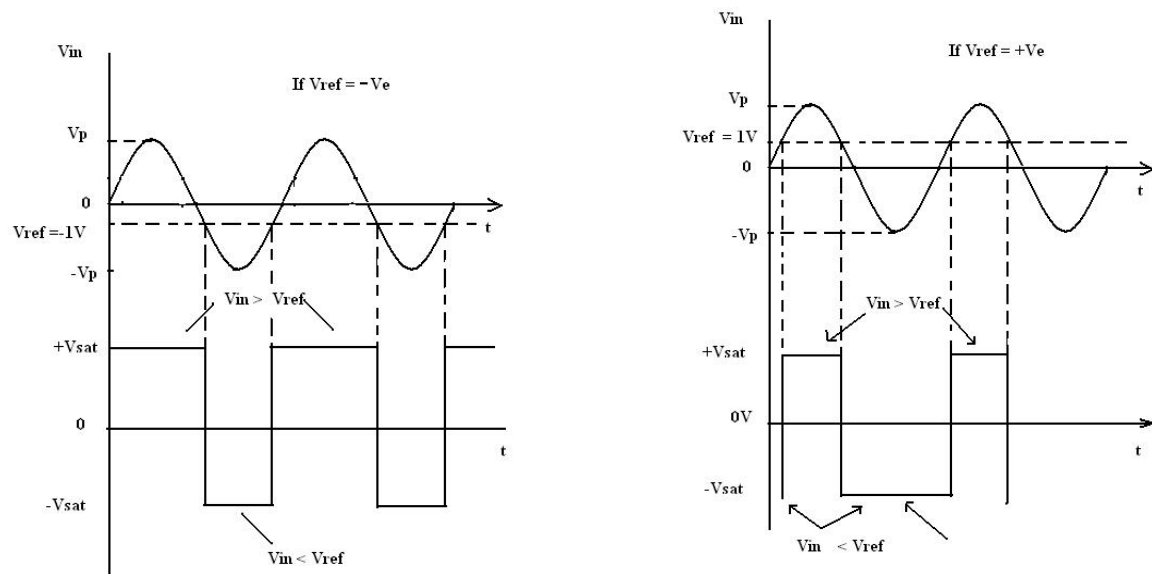
Voltage level detector and oscillators

#### 1. Non-inverting Comparator:

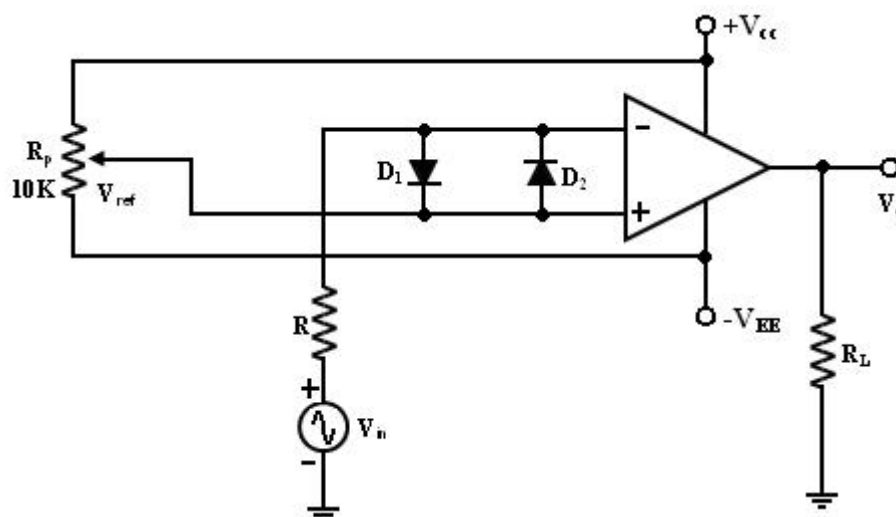


A fixed reference voltage  $V_{ref}$  of 1 V is applied to the negative terminal and time varying signal voltage  $V_{in}$  is applied to the positive terminal. When  $V_{in}$  is less than  $V_{ref}$  the output becomes  $V_0$  at  $-V_{sat}$  [ $V_{in} < V_{ref} \Rightarrow V_0 (-V_{sat})$ ]. When  $V_{in}$  is greater than  $V_{ref}$ , the (+) input becomes positive, the  $V_0$  goes to  $+V_{sat}$ . [ $V_{in} > V_{ref} \Rightarrow V_0 (+V_{sat})$ ]. Thus the  $V_0$  changes from one saturation level to another. The diodes  $D_1$  and  $D_2$  protect the op-amp from damage due to the excessive input voltage  $V_{in}$ . Because of these diodes, the difference input voltage  $V_{id}$  of the op-amp diodes are called clamp diodes. The resistance  $R$  in series with  $V_{in}$  is used to limit the current through  $D_1$  and  $D_2$ . To reduce offset problems, a resistance  $R_{comp} = R$  is connected between the (-ve) input and  $V_{ref}$ .

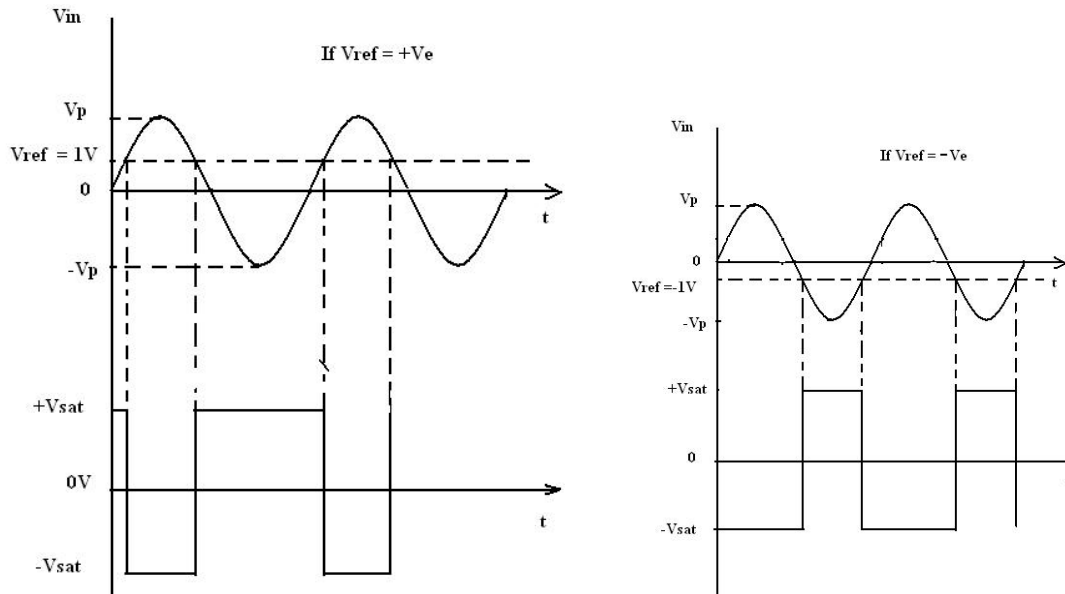
## Input and Output Waveforms:



## 2. Inverting Comparator:

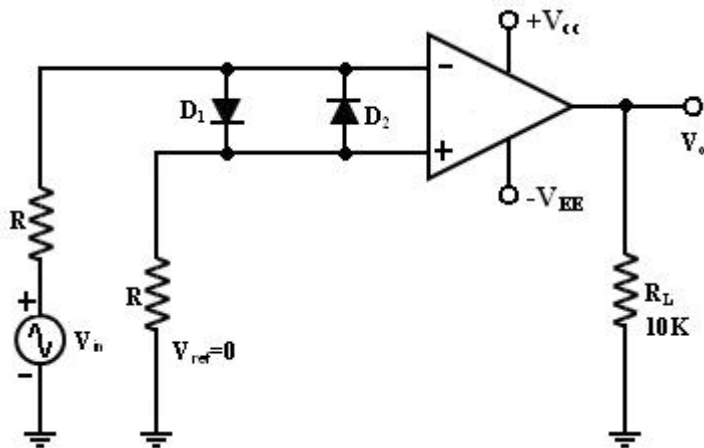


This figure shows an inverting comparator in which the reference voltage  $V_{ref}$  is applied to the (+) input terminal and  $V_{in}$  is applied to the (-) input terminal. In this circuit  $V_{ref}$  is obtained by using a  $10K$  potentiometer that forms a voltage divider with dc supply voltages  $+V_{cc}$  and  $-V_{ee}$  and the wiper connected to the input. As the wiper is moved towards  $+V_{cc}$ ,  $V_{ref}$  becomes more positive. Thus a  $V_{ref}$  of a desired amplitude and polarity can be obtained by simply adjusting the  $10k$  potentiometer.

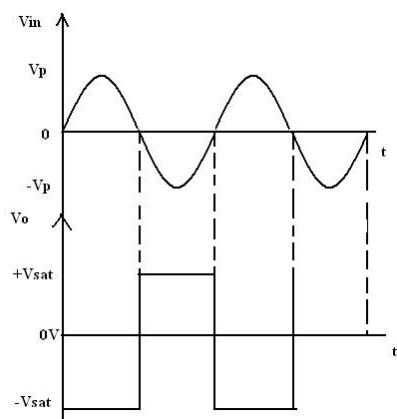


## APPLICATIONS OF COMPARATORS:

### Zero Crossing Detector: [ Sine wave to Square wave converter]



One of the application of comparator is the zero crossing detector or —sine wave to Square wave Converter. The basic comparator can be used as a zero crossing detector by setting  $V_{ref}$  is set to Zero. ( $V_{ref} = 0V$ ). This Fig shows when in what direction an input signal  $V_{in}$  crosses zero volts. (i.e) the o/p  $V_o$  is driven into negative saturation when the input the signal  $V_{in}$  passes through zero in positive direction. Similarly, when  $V_{in}$  passes through Zero in negative direction the output  $V_o$  switches and saturates positively.

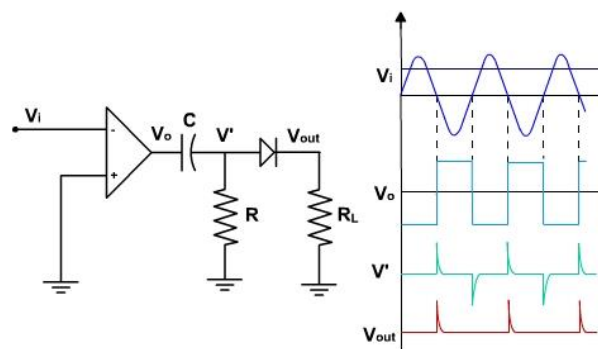


## Drawbacks of Zero- crossing detector:

In some applications, the input  $V_{in}$  may be a slowly changing waveform, (i.e) a low frequency signal. It will take  $V_{in}$  more time to cross 0V, therefore  $V_o$  may not switch quickly from one saturation voltage to the other. Because of the noise at the op-amp's input terminals the output  $V_o$  may fluctuate between 2 saturations voltages  $+V_{sat}$  and  $-V_{sat}$ . Both of these problems can be cured with the use of regenerative or positive feedback that cause the output  $V_o$  to change faster and eliminate any false output transitions due to noise signals at the input. Inverting comparator with positive feedback. This is known as —Schmitt Triggerl.

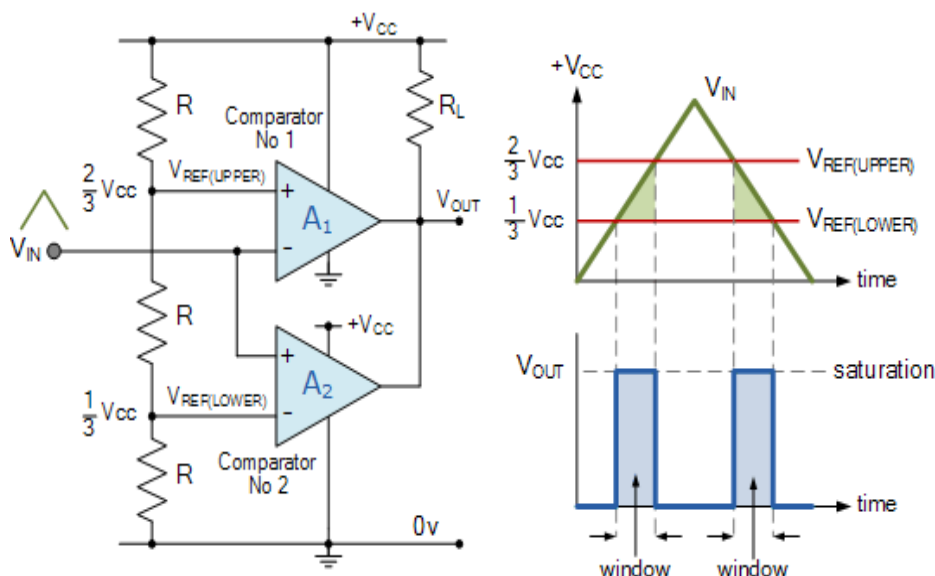
## TIME MARKER GENERATOR:

The resistance is chosen so that the zener operates in zener region. When  $V_R = 0$  then the output changes rapidly from one state to other very rapidly every time that the input passes through zero as shown in fig.



Such a configuration is called zero crossing detector. If we want pulses at zero crossing then a differentiator and a series diode is connected at the output. It produces single pulses at the zero crossing point in every cycle.

## Window Detector:



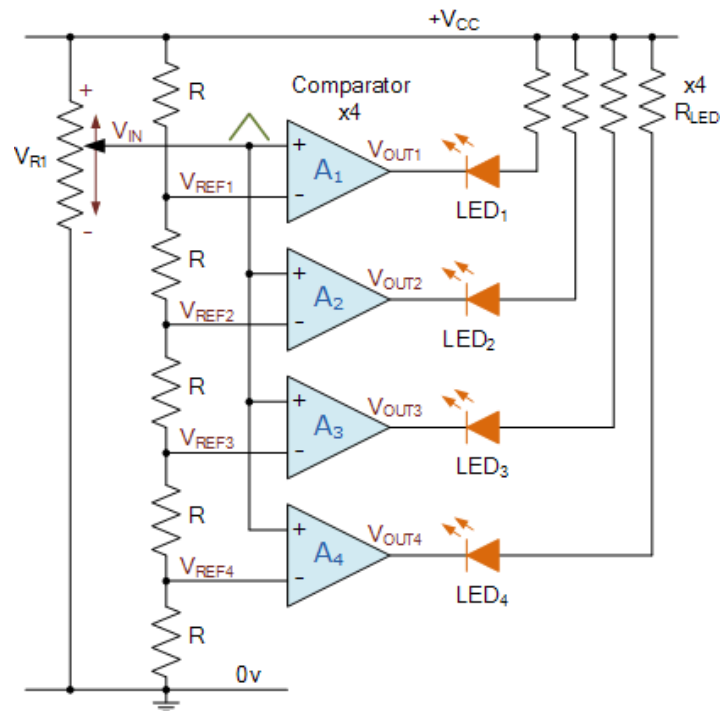
- The window detector circuit detects when an unknown voltage falls within a specified voltage band or window.
- It is also called window comparator.

- The initial switching condition of the circuit is the open-collector output of op-amp A<sub>1</sub> “OFF” with the open-collector output of op-amp A<sub>2</sub>, “ON” (sinking current) so V<sub>OUT</sub> is equal to 0V.
- When V<sub>IN</sub> is below the lower voltage level, V<sub>REF(LOWER)</sub> which equates to 1/3V<sub>cc</sub>, V<sub>OUT</sub> will be LOW.
- When V<sub>IN</sub> exceeds this 1/3V<sub>cc</sub> lower voltage level, the first op-amp comparator detects this and switches its open-collector output HIGH. This means that both op-amps have their outputs HIGH at the same time. No current flows through the pull-up resistor R<sub>L</sub> so V<sub>OUT</sub> is equal to V<sub>cc</sub>.
- As V<sub>IN</sub> continues to increase it passes the upper voltage level, V<sub>REF(UPPER)</sub> at 2/3V<sub>cc</sub>. At this point the second op-amp comparator detects this and switches its output LOW and V<sub>OUT</sub> becomes equal to 0V.
- Then the difference between V<sub>REF(UPPER)</sub> and V<sub>REF(LOWER)</sub> (which is 2/3V<sub>cc</sub> – 1/3V<sub>cc</sub> in this example) creates the switching window for the positive going signal.
- Lets now assume that V<sub>IN</sub> is at its maximum value and equal to V<sub>cc</sub>. As V<sub>IN</sub> decreases it passes the upper voltage level V<sub>REF(UPPER)</sub> of the second op-amp comparator which switches the output HIGH. As V<sub>IN</sub> continues to decrease it passes the lower voltage level, V<sub>REF(LOWER)</sub> of the first op-amp comparator once again switching the output LOW.
- Then the difference between V<sub>REF(UPPER)</sub> and V<sub>REF(LOWER)</sub> creates the window for the negative going signal. So we can see that as V<sub>IN</sub> passes above or passes below the upper and lower reference levels set by the two op-amp comparators, the output signal V<sub>OUT</sub> will be HIGH or LOW.
- In this simple example we have set the upper trip level at 2/3V<sub>cc</sub> and the lower trip level at 1/3V<sub>cc</sub> (because we used three equal value resistors), but can be any values we choose by adjusting the input thresholds. As a result, the window width can be customized for a given application.
- If we used a dual power supply and set the upper and lower trip levels to say ±10 volts and V<sub>IN</sub> was a sinusoidal waveform, then we could use this window comparator circuit as a zero crossing detector of the sine wave which would produce an output, HIGH or LOW every time the sine wave crossed the zero volts line from positive to negative or negative to positive.

## Level Detector:

- Level detector circuit is used to detect the input voltage level when it crosses certain voltage level (ref level). A LED or some indicator is used as a output level indicator.
- As above, the voltage divider network provides a set of reference voltages for the individual op-amp comparator circuits. To produce the four reference voltages will require five resistors.
- The junction at the bottom pair of resistors will produce a reference voltage that is one-fifth the supply voltage, 1/5V<sub>cc</sub> using equal value resistors. The second pair 2/5V<sub>cc</sub>, a third pair 3/5V<sub>cc</sub> and so on, with these reference voltages increasing by a fixed amount of one-fifth (1/5) towards 5/5V<sub>cc</sub> which is actually V<sub>cc</sub>.
- As the common input voltage increases, the output of each op-amp comparator circuit switches in turn thereby turning OFF the connected LED starting with the lower comparator, A<sub>4</sub> and upwards towards A<sub>1</sub> as the input voltage increases. So by setting the

values of the resistors in the voltage divider network, the comparators can be configured to detect any voltage level. One good example of the use of voltage level detection and indication would be for a battery condition monitor by reversing the LED's and connecting them to 0V (ground) instead of  $V_{CC}$ .



- Also by increasing the number of op-amp comparators in the set, more trigger points can be created. So for example, if we had eight op-amp comparators in the chain and fed the output of each comparator to an 8-to-3 line Digital Encoder, we could make a very simple analogue-to-digital converter, (ADC) that would convert the analogue input signal into a 3-bit binary code (0-to-7).

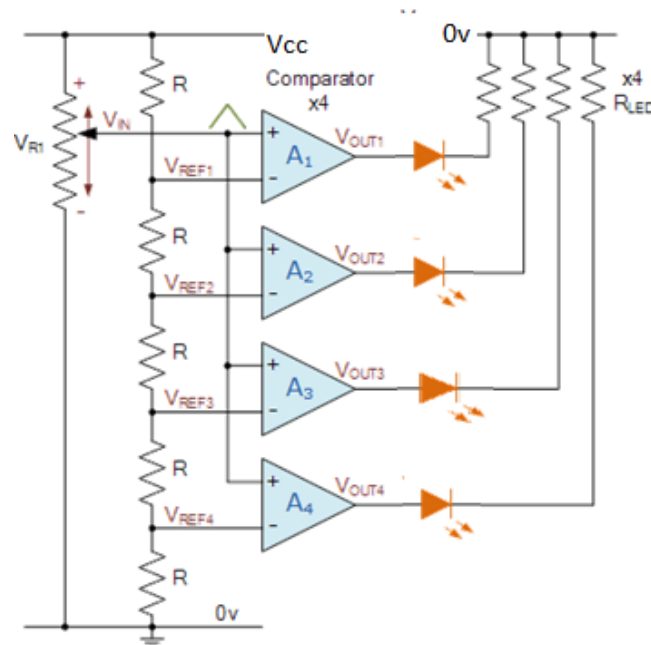


Fig: Battery level Indicator using level detector circuit.

## Rectifiers:

**AC** and **DC** are two frequent terms that you encounter while studying the flow of electrical charge. **Alternating Current (AC)** has the property to change its state continuously. For example, if we consider a sine wave, the current flows in one direction for positive half cycle and in the opposite direction for negative half cycle. On the other hand, **Direct Current (DC)** flows only in one direction.

An electronic circuit, which produces either DC signal or a pulsated DC signal, when an AC signal is applied to it is called as a **rectifier**. This chapter discusses about op-amp based rectifiers in detail.

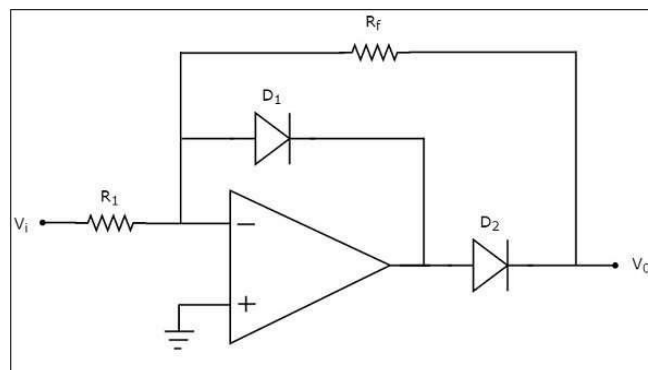
## Types of Rectifiers

Rectifiers are classified into two types: **Half wave rectifier** and **Full wave rectifier**. This section discusses about these two types in detail.

### Precision Half wave Rectifier

A **half wave rectifier** is a rectifier that produces positive half cycles at the output for one half cycle of the input and zero output for the other half cycle of the input.

The **circuit diagram** of a half wave rectifier is shown in the following figure.



Observe that the circuit diagram of a half wave rectifier shown above looks like an inverting amplifier, with two diodes  $D_1$  and  $D_2$  in addition.

The **working** of the half wave rectifier circuit shown above is explained below

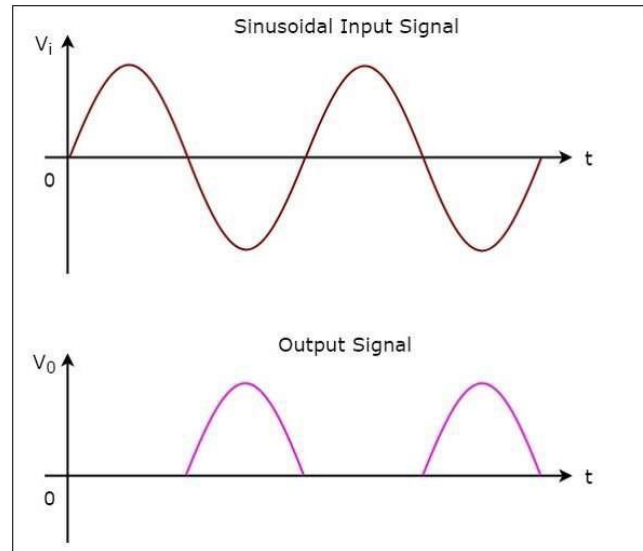
- For the **positive half cycle** of the sinusoidal input, the output of the op-amp will be negative. Hence, diode  $D_1$  will be forward biased.
- When diode  $D_1$  is in forward bias, output voltage of the op-amp will be  $-0.7\text{ V}$ . So, diode  $D_2$  will be reverse biased. Hence, the **output voltage** of the above circuit is **zero** volts.
- Therefore, there is **no (zero) output** of half wave rectifier for the positive half cycle of a sinusoidal input.
- For the **negative half cycle** of sinusoidal input, the output of the op-amp will be positive. Hence, the diodes  $D_1$  and  $D_2$  will be reverse biased and forward biased respectively. So, the output voltage of above circuit will be –

$$V_0 = - \left( \frac{R_f}{R_1} \right) V_1$$

- Therefore, the output of a half wave rectifier will be a **positive half cycle** for a negative half cycle of the sinusoidal input.

## Wave forms

The **input** and **output waveforms** of a half wave rectifier are shown in the following figure

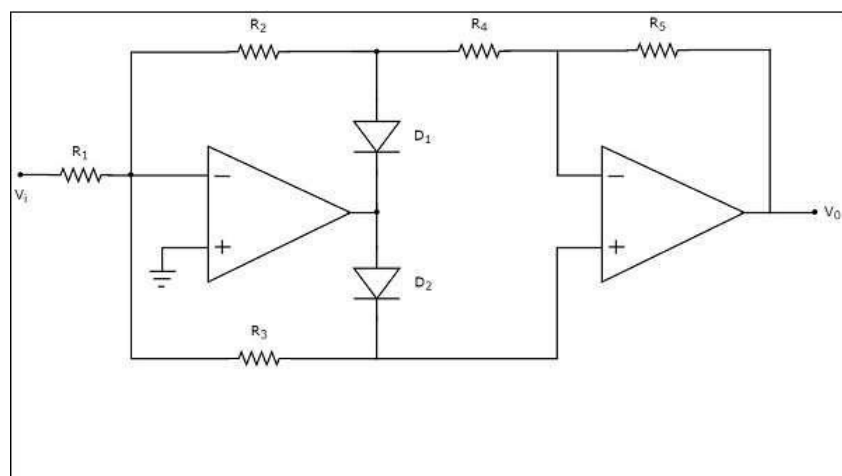


As you can see from the above graph, the half wave rectifier circuit diagram that we discussed will produce **positive half cycles** for negative half cycles of sinusoidal input and zero output for positive half cycles of sinusoidal input.

## Precision Full wave Rectifier:

A **full wave rectifier** produces positive half cycles at the output for both half cycles of the input.

The **circuit diagram** of a full wave rectifier is shown in the following figure –



The above circuit diagram consists of two op-amps, two diodes,  $D_1$  &  $D_2$  and five resistors,  $R_1$  to  $R_5$ . The **working** of the full wave rectifier circuit shown above is explained below –

- For the **positive half cycle** of a sinusoidal input, the output of the first op-amp will be negative. Hence, diodes  $D_1$  and  $D_2$  will be forward biased and reverse biased respectively.



- Then, the output voltage of the first op-amp will be –

$$V_{01} = - \left( \frac{R_2}{R_1} \right) V_i$$

- Observe that the output of the first op-amp is connected to a resistor  $R_4$ , which is connected to the inverting terminal of the second op-amp. The voltage present at the non-inverting terminal of second op-amp is 0 V. So, the second op-amp with resistors,  $R_4$  and  $R_5$  acts as an **inverting amplifier**.
- The output voltage of the second op-amp will be

$$V_0 = - \left( \frac{R_5}{R_4} \right) V_{01}$$

**Substituting** the value of  $V_{01}$  in the above equation, we get –

$$\Rightarrow V_0 = - \left( \frac{R_5}{R_4} \right) \left\{ - \left( \frac{R_2}{R_1} \right) V_i \right\}$$

$$\Rightarrow V_0 = \left( \frac{R_2 R_5}{R_1 R_4} \right) V_i$$

- Therefore, the output of a full wave rectifier will be a positive half cycle for the **positive half cycle** of a sinusoidal input. In this case, the gain of the output is  $\frac{R_2 R_5}{R_1 R_4}$ .
- If we consider  $R_1 = R_2 = R_4 = R_5 = R$ , then the gain of the output will be one.
- For the **negative half cycle** of a sinusoidal input, the output of the first op-amp will be positive. Hence, diodes  $D_1$  and  $D_2$  will be reverse biased and forward biased respectively.
- The output voltage of the first op-amp will be –

$$V_{01} = - \left( \frac{R_3}{R_1} \right) V_i$$

The output of the first op-amp is directly connected to the non-inverting terminal of the second op-amp. Now, the second op-amp with resistors,  $R_4$  and  $R_5$  acts as a **non-inverting amplifier**.

The output voltage of the second op-amp will be –

$$V_0 = \left( 1 + \frac{R_5}{R_4} \right) V_{01}$$

**Substituting** the value of  $V_{01}$  in the above equation, we get

$$\Rightarrow V_0 = \left(1 + \frac{R_5}{R_4}\right) \left\{ - \left(\frac{R_3}{R_1}\right) V_i \right\}$$

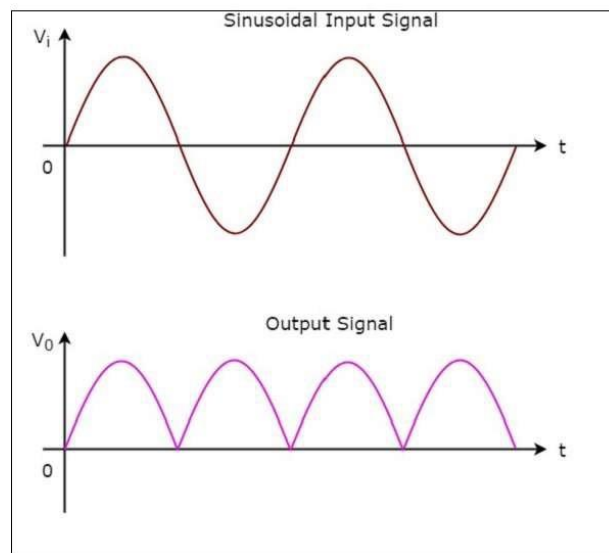
$$\Rightarrow V_0 = - \left(\frac{R_3}{R_1}\right) \left(1 + \frac{R_5}{R_4}\right) V_i$$

Therefore, the output of a full wave rectifier will be a **positive half cycle** for the negative half cycle of sinusoidal input also. In this case, the magnitude of the gain of the output is

$$\left(\frac{R_3}{R_1}\right) \left(1 + \frac{R_5}{R_4}\right)$$

- If we consider  $R_1 = R_2 = R_3 = R_4 = R_5 = R$  then the gain of the output will be **one**.

The **input** and **output waveforms** of a full wave rectifier are shown in the following figure



As you can see in the above figure, the full wave rectifier circuit diagram that we considered will produce only **positive half cycles** for both positive and negative half cycles of a sinusoidal input.

## Log And Anti Log Amplifiers:

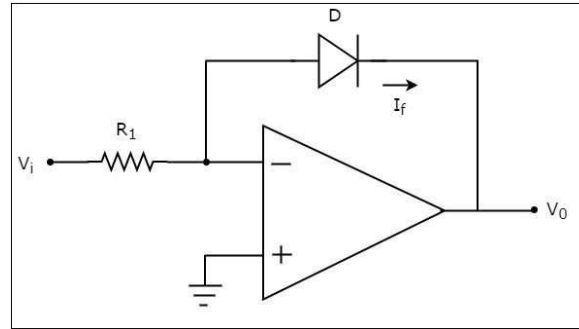
The electronic circuits which perform the mathematical operations such as logarithm and anti-logarithm (exponential) with an amplification are called as **Logarithmic amplifier** and **Anti-Logarithmic amplifier** respectively.

This chapter discusses about the **Logarithmic amplifier** and **Anti-Logarithmic amplifier** in detail. Please note that these amplifiers fall under non-linear applications.

### Logarithmic Amplifier

A **logarithmic amplifier**, or a **log amplifier**, is an electronic circuit that produces an output that is proportional to the logarithm of the applied input. This section discusses about the op-amp based logarithmic amplifier in detail.

An op-amp based logarithmic amplifier produces a voltage at the output, which is proportional to the logarithm of the voltage applied to the resistor connected to its inverting terminal. The **circuit diagram** of an op-amp based logarithmic amplifier is shown in the following figure –



In the above circuit, the non-inverting input terminal of the op-amp is connected to ground. That means zero volts is applied at the non-inverting input terminal of the op-amp.

According to the **virtual short concept**, the voltage at the inverting input terminal of an op-amp will be equal to the voltage at its non-inverting input terminal. So, the voltage at the inverting input terminal will be zero volts.

The **nodal equation** at the inverting input terminal's node is –

$$\frac{0 - V_i}{R_1} + I_f = 0$$

$$\Rightarrow I_f = \frac{V_i}{R_1} \dots \dots \text{Equation 1}$$

The following is the **equation for current** flowing through a diode, when it is in forward bias

$$I_f = I_s e^{\left(\frac{V_f}{nV_T}\right)} \dots \dots \text{Equation 2}$$

where,

$I_s$  is the saturation current of the diode,

$V_f$  is the voltage drop across diode, when it is in forward bias,

$V_T$  is the diode's thermal equivalent voltage.

The **KVL equation** around the feedback loop of the op amp will be –

$$0 - V_f - V_o = 0$$

$$\Rightarrow V_f = -V_o$$

Substituting the value of  $V_f$  in Equation 2, we get –

$$I_f = I_s e^{\left(\frac{-V_0}{nV_T}\right)} \dots\dots \text{Equation 3}$$

Observe that the left hand side terms of both equation 1 and equation 3 are same. Hence, equate the right hand side term of those two equations as shown below –

$$\frac{V_i}{R_1} = I_s e^{\left(\frac{-V_0}{nV_T}\right)}$$

$$\frac{V_i}{R_1 I_s} = e^{\left(\frac{-V_0}{nV_T}\right)}$$

Applying **natural logarithm** on both sides, we get –

$$\ln\left(\frac{V_i}{R_1 I_s}\right) = \frac{-V_0}{nV_T}$$

$$V_0 = -nV_T \ln\left(\frac{V_i}{R_1 I_s}\right)$$

Note that in the above equation, the parameters  $n$ ,  $V_T$  and  $I_s$  are constants. So, the output voltage  $V_0$  will be proportional to the **natural logarithm** of the input voltage  $V_i$  for a fixed value of resistance  $R_1$ .

Therefore, the op-amp based logarithmic amplifier circuit discussed above will produce an output, which is proportional to the natural logarithm of the input voltage

$V_i$ , when  $R_1 I_s = 1V$ .

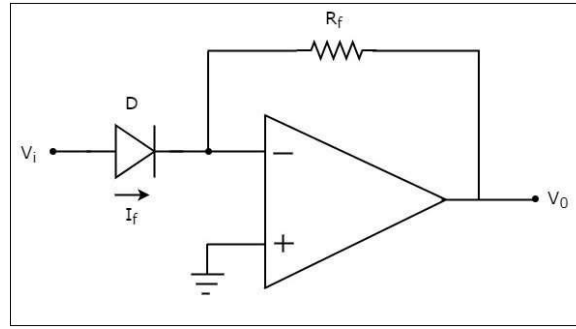
Observe that the output voltage  $V_0$  has a **negative sign**, which indicates that there exists a  $180^\circ$  phase difference between the input and the output.

## Anti-Logarithmic Amplifier

An **anti-logarithmic amplifier**, or an **anti-log amplifier**, is an electronic circuit that produces an output that is proportional to the anti-logarithm of the applied input. This section discusses about the op-amp based anti-logarithmic amplifier in detail.

An op-amp based anti-logarithmic amplifier produces a voltage at the output, which is proportional to the anti-logarithm of the voltage that is applied to the diode connected to its inverting terminal.

The **circuit diagram** of an op-amp based anti-logarithmic amplifier is shown in the following figure –



In the circuit shown above, the non-inverting input terminal of the op-amp is connected to ground. It means zero volts is applied to its non-inverting input terminal.

According to the **virtual short concept**, the voltage at the inverting input terminal of op-amp will be equal to the voltage present at its non-inverting input terminal. So, the voltage at its inverting input terminal will be zero volts.

The **nodal equation** at the inverting input terminal's node is –

$$-I_f + \frac{0 - V_0}{R_f} = 0$$

$$\Rightarrow -\frac{V_0}{R_f} = I_f$$

$$\Rightarrow V_0 = -R_f I_f \dots \dots \dots \text{Equation 4}$$

We know that the equation for the current flowing through a diode, when it is in forward bias, is as given below –

$$I_f = I_s e^{\left(\frac{V_f}{nV_T}\right)}$$

Substituting the value of If in Equation 4, we get

$$V_0 = -R_f \left\{ I_s e^{\left(\frac{V_f}{nV_T}\right)} \right\}$$

$$V_0 = -R_f I_s e^{\left(\frac{V_f}{nV_T}\right)} \dots \dots \dots \text{Equation 5}$$

The KVL equation at the input side of the inverting terminal of the op amp will be

$$V_i - V_f = 0$$

$$V_f = V_i$$

Substituting, the value of Vf in the Equation 5, we get –

$$V_0 = -R_f I_s e^{\left(\frac{V_i}{nV_T}\right)}$$

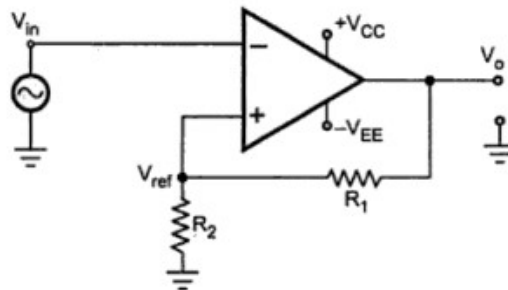
Note that, in the above equation the parameters  $n$ ,  $V_T$  and  $I_s$  are constants. So, the output voltage  $V_0$  will be proportional to the **anti-natural logarithm** (exponential) of the input voltage  $V_i$ , for a fixed value of feedback resistance  $R_f$ .

Therefore, the op-amp based anti-logarithmic amplifier circuit discussed above will produce an output, which is proportional to the anti-natural logarithm (exponential) of the input voltage  $V_i$  when,  $R_f I_s = 1V$ . Observe that the output voltage  $V_0$  is having a **negative sign**, which indicates that there exists a  $180^\circ$  phase difference between the input and the output.

## Schmitt Trigger:

- A **Schmitt trigger** is a special type of comparator circuit with hysteresis implemented , used to avoid unwanted triggering.
- It is also called **Regenerative Comparator**.
- The op-amp Schmitt Triggers are two types
  - Inverting Schmitt Trigger
  - Non-inverting Schmitt Trigger.

## Inverting Schmitt Trigger:



- $V_{in} > V_{ref} \rightarrow V_o = -V_{sat}$
- $V_{in} < V_{ref} \rightarrow V_o = +V_{sat}$
- Ref . Voltage Controlled by the  $R_1$  &  $R_2$  Resistors.

**Contd..**

$$+V_{\text{ref}} = \frac{V_0}{R_1 + R_2} \times R_2 = \frac{+V_{\text{sat}}}{R_1 + R_2} \times R_2 \dots \text{positive saturation}$$

$$-V_{\text{ref}} = \frac{V_0}{R_1 + R_2} \times R_2 = \frac{-V_{\text{sat}}}{R_1 + R_2} \times R_2 \dots \text{negative saturation}$$

- $+V_{\text{ref}}$  is for positive saturation when  $V_0 = +V_{\text{sat}}$  and is called **Upper Threshold Voltage ( $V_{\text{UT}}$ )**
- $-V_{\text{ref}}$  is negative saturation when  $V_0 = -V_{\text{sat}}$  and is called **Lower Threshold Voltage ( $V_{\text{LT}}$ )**

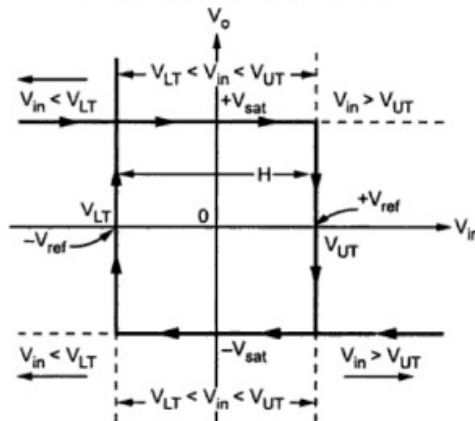
**Contd..**

- $V_{\text{in}} > V_{\text{UT}} \rightarrow V = -V_{\text{sat}}$
- $V_{\text{in}} < V_{\text{LT}} \rightarrow V_0 = +V_{\text{sat}}$
- $V_{\text{LT}} < V_{\text{in}} < V_{\text{UT}} \rightarrow V_0 = \text{Previous state}$
- The difference between  $V_{\text{UT}}$  &  $V_{\text{LT}}$  is called width of hysteresis. Denoted as **H**
- Hysteresis is also called **dead band** or **dead zone**.



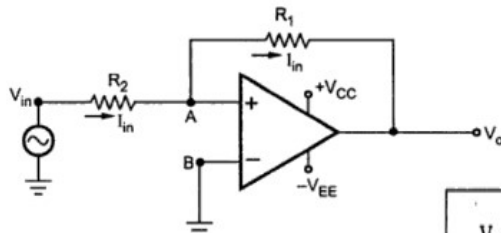
Contd..

$$H = \frac{2 V_{sat} R_2}{R_1 + R_2}$$



- Hysteresis Transfer characteristics.

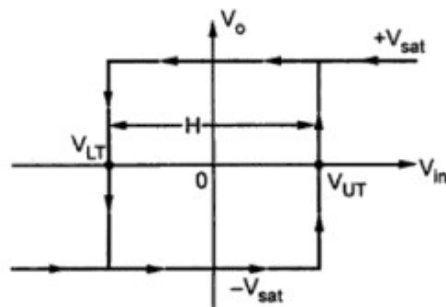
## Non-Inverting Schmitt Trigger



$$V_{UT} = I_{in} R_2 = \frac{R_2}{R_1} (+V_{sat}) = V_{sat} \frac{R_2}{R_1}$$

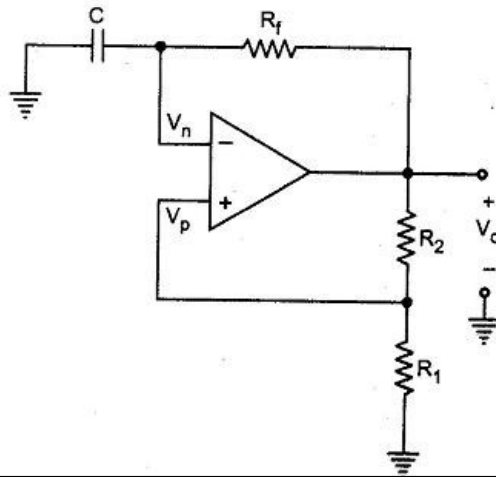
$$V_{LT} = \frac{R_2}{R_1} (-V_{sat}) = -V_{sat} \frac{R_2}{R_1}$$

$$H = V_{UT} - V_{LT} = 2 V_{sat} \frac{R_2}{R_1}$$



### SQUAREWAVE GENERATOR:

- The square wave generator using op amp means the astable multivibrator circuit using op-amp.



### SQUAREWAVE GENERATOR:

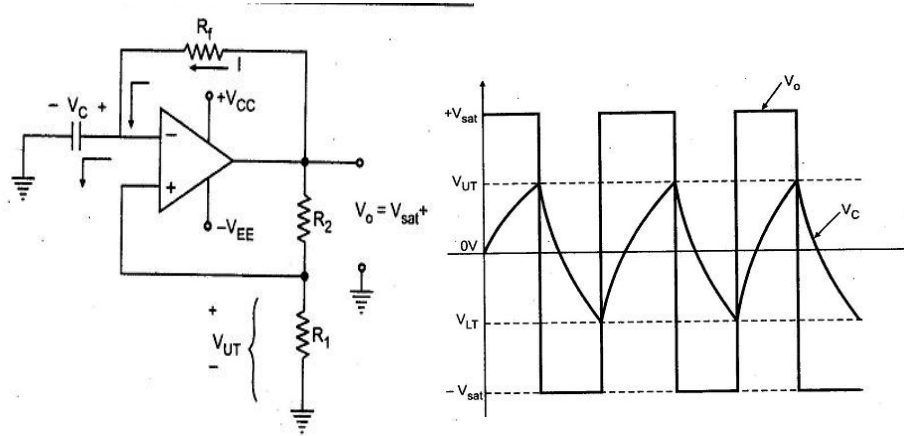
When  $V_o$  is at  $+V_{sat}$ , the feedback voltage is called the upper threshold voltage  $V_{UT}$  and is given as

$$V_{UT} = \frac{R_1 \cdot +V_{sat}}{R_1 + R_2} \quad \dots (1)$$

When  $V_o$  is at  $-V_{sat}$ , the feedback voltage is called the lower-threshold voltage  $V_{LT}$  and is given as

$$V_{LT} = \frac{R_1 \cdot -V_{sat}}{R_1 + R_2} \quad \dots (2)$$

**Contd..**



### **Frequency of Oscillation:**

- The voltage across the capacitor as a function of time is given as

$$V_c(t) = V_{max} + (V_{initial} - V_{max})e^{(-t/T)} \quad \dots (3)$$

Where,

$V_c(t)$  is the instantaneous voltage across the capacitor.

$V_{initial}$  is the initial voltage

$V_{max}$  is the voltage toward which the capacitor is charging.

**Contd..**

- Let us consider the charging of capacitor from  $V_{LT}$  to  $V_{UT}$ , where  $V_{LT}$  is the initial voltage,  $V_{UT}$  is the instantaneous voltage and  $+V_{sat}$  is the maximum voltage.
- At  $t = T_1$ , voltage across capacitor reaches  $V_{UT}$  and therefore equation (3) becomes

$$V_{UT} = +V_{sat} + (V_{LT} - +V_{sat})e^{(-T_1/R_f C)} \quad \dots (4)$$

$$\therefore -(V_{LT} - +V_{sat})e^{(-T_1/R_f C)} = +V_{sat} - V_{UT}$$

**Contd..**

$$e^{(-T_1/R_f C)} = \frac{(+V_{sat} - V_{UT})}{(+V_{sat} - V_{LT})}$$

$$\frac{-T_1}{R_f C} = \ln \left( \frac{+V_{sat} - V_{UT}}{+V_{sat} - V_{LT}} \right)$$

$$T_1 = -R_f C \ln \left( \frac{+V_{sat} - V_{UT}}{+V_{sat} - V_{LT}} \right)$$

$$= R_f C \ln \left( \frac{+V_{sat} - V_{LT}}{+V_{sat} - V_{UT}} \right) \quad \dots (5)$$

- The time taken by capacitor to charge from  $V_{UT}$  to  $V_{LT}$  is same as time required for charging capacitor from  $V_{LT}$  to  $V_{UT}$ . Therefore, total time required for one oscillation is given as

**Contd..**

$$T = 2T_1 \quad \dots (6)$$

$$= 2R_f C \ln \left( \frac{+V_{sat} - V_{LT}}{+V_{sat} - V_{UT}} \right) \quad \dots (7)$$

- The frequency of oscillation can be determined as  $f_o = 1/T$ , where T represents the time required for one oscillation.
- Substituting the value of T we get,

$$f_o = \frac{1}{2 R_f C \ln \left( \frac{+V_{sat} - V_{LT}}{+V_{sat} - V_{UT}} \right)} \quad \dots (8)$$

**Contd..**

Substituting the values of  $V_{UT}$  and  $V_{LT}$  we get,

$$T = 2 R_f C \ln \left[ \frac{+V_{sat} - (R_1 \times -V_{sat}) / (R_1 + R_2)}{+V_{sat} - (R_1 \times +V_{sat}) / (R_1 + R_2)} \right]$$

If magnitudes of  $+V_{sat}$  and  $-V_{sat}$  are equal,

$$T = 2 R_f C \ln \left[ \frac{+V_{sat} \left( 1 + \frac{R_1}{R_1 + R_2} \right)}{+V_{sat} \left( 1 - \frac{R_1}{R_1 + R_2} \right)} \right]$$

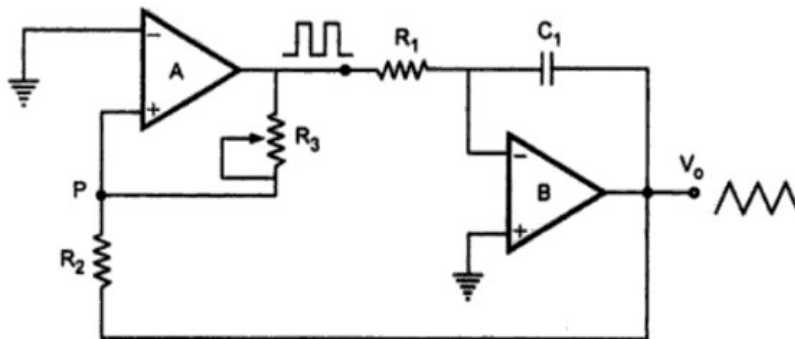
$$T = 2 R_f C \ln \left( \frac{2R_1 + R_2}{R_2} \right)$$

# IC Applications

## UNIT-III

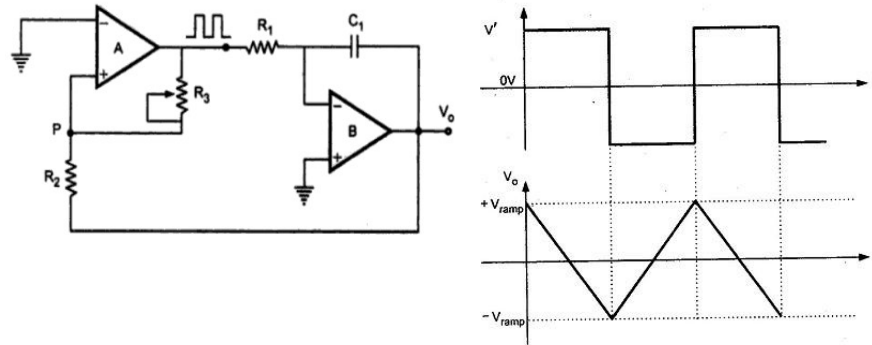
### TOPIC: Triangular & Sawtooth wave Generator

#### Triangular wave Generator



- It is the combination of Schmitt Trigger and integrator.
- A  $\rightarrow$  Square wave (Schmitt Trigger)
- B  $\rightarrow$  Triangular wave (Integrator)

Contd..



- Output wave forms of triangular wave generator

#### Amplitude & Frequency Calculation:

- When comparator output is at  $+V_{sat}$ , the effective voltage at point P is given by

$$-V_{ramp} + \frac{R_2}{R_2 + R_3} [ +V_{sat} - (-V_{ramp}) ] \quad \dots (1)$$

When effective voltage at P becomes equal to zero, we can write above equation

$$-V_{ramp} + \frac{R_2}{R_2 + R_3} [ +V_{sat} - (-V_{ramp}) ] = 0$$

$$-V_{ramp} + \frac{R_2}{R_2 + R_3} (V_{ramp}) + \frac{R_2}{R_2 + R_3} (+V_{sat}) = 0$$

Contd..

$$\frac{-R_3}{R_2 + R_3} (V_{\text{ramp}}) = -\frac{R_2}{R_2 + R_3} (+V_{\text{sat}})$$

$$-V_{\text{ramp}} = \frac{-R_2}{R_3} (+V_{\text{sat}}) \quad \dots (2)$$

Similarly, when comparator output is at  $-V_{\text{sat}}$ , we can write,

$$V_{\text{ramp}} = \frac{-R_2}{R_3} (-V_{\text{sat}}) \quad \dots (3)$$

The peak to peak amplitude of the triangular wave can be given as

$$\begin{aligned} V_{o(pp)} &= +V_{\text{ramp}} - (-V_{\text{ramp}}) \\ &= \frac{-R_2}{R_3} (-V_{\text{sat}}) - \left( \frac{-R_2}{R_3} \right) (+V_{\text{sat}}) \end{aligned} \quad \dots (4)$$

Contd..

If  $|+V_{\text{sat}}| = |-V_{\text{sat}}|$  then, we can write

$$V_{o(pp)} = \frac{R_2}{R_3} V_{\text{sat}} + \frac{R_2}{R_3} V_{\text{sat}} = \frac{2R_2}{R_3} V_{\text{sat}} \quad \dots (5)$$

• The time taken by the output to swing from  $-V_{\text{ramp}}$  to  $+V_{\text{ramp}}$  (or from  $+V_{\text{ramp}}$  to  $-V_{\text{ramp}}$ ) is equal to half the time period  $T/2$ .

• This time can be calculated from the integrator output equation as follows :

$$V_{o(pp)} = -\frac{1}{R_1 C_1} \int_0^{T/2} (-V_{\text{sat}}) dt = \left( \frac{V_{\text{sat}}}{R_1 C_1} \right) \frac{T}{2} \quad \dots (6)$$



**Contd..**

$$T = \frac{2 R_1 C_1 V_{o(pp)}}{V_{sat}} \quad \dots (7)$$

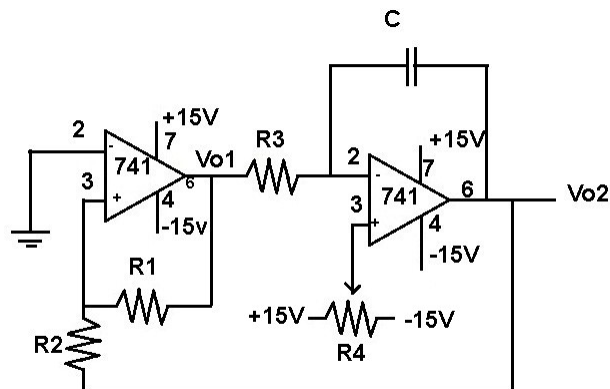
Substituting value of  $V_{o(pp)}$  we get,

$$T = \frac{2 R_1 C_1 \left( \frac{2 R_2}{R_3} V_{sat} \right)}{V_{sat}} = \frac{4 R_1 C_1 R_2}{R_3} \quad \dots (8)$$

Therefore, the frequency of oscillation can be given as,

$$f_0 = \frac{1}{T} = \frac{R_3}{4 R_1 C_1 R_2}$$

### **Sawtooth wave Generator:**

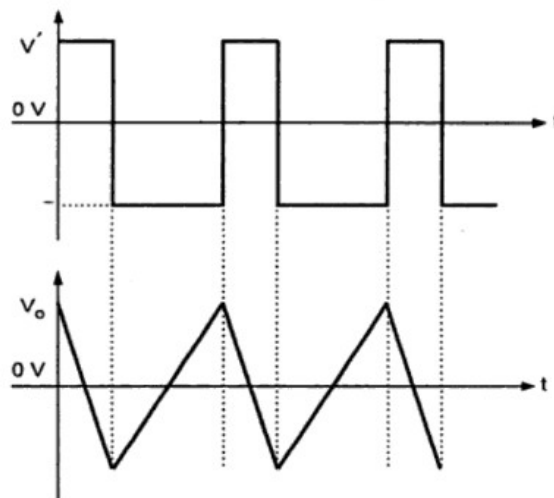


- Unlike the triangular wave, the sawtooth wave has unequal rise time & fall time.

### Contd..

- The non inverting terminal of the integrator is driven by voltage set between  $+V_{cc}$  to  $-V_{EE}$  by the potentiometer.
- Depending on R4 Setting, a certain DC level is added in the output of integrator.
- If the voltage at non-inverting terminal is
- Negative  $\rightarrow < 50\%$  (DS)  $\rightarrow$  Longer Rise time
- Positive  $\rightarrow > 50\%$  (DS)  $\rightarrow$  Longer fall time.

### Contd..



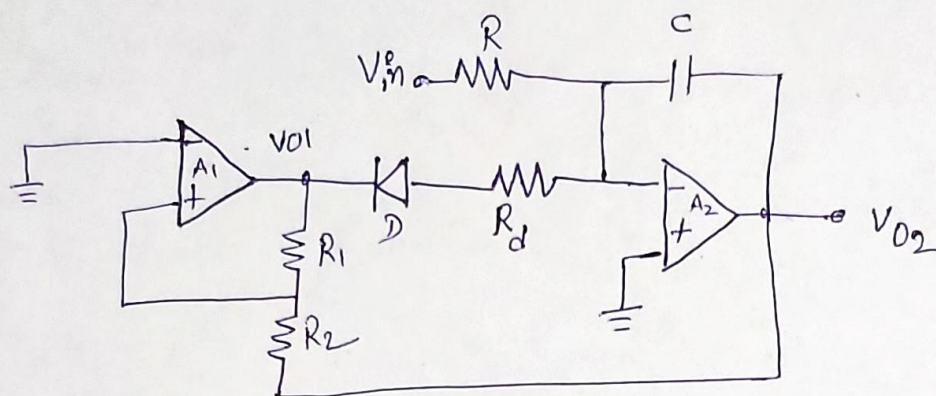
- Output waveforms of Swatooth wave generator.

# Voltage to Frequency Converter (V-F)

→ V-F converter accepts an analog input  $V_{in}$  and generates a pulse train with frequency  $f$ .

→ mathematically expressed as  $f = K \cdot V_{in}$

where  $K$  = sensitivity of V-F converter in Hz/V.



→  $A_1$  → Comparator

$A_2$  → Integrator

→ when  $V_{01}$  is negative → 'D' diode forward biased & capacitor starts charging.

→ The charging current of C is  $\frac{-V_{01}}{R_d}$

∵  $R_d \ll R$  ; capacitor charges very sharply

→  $V_{02}$  is a -ve ramp signal till it reaches to threshold value of comparator.

→ then  $V_{01}$  becomes +ve & diode (D) will be reverse biased

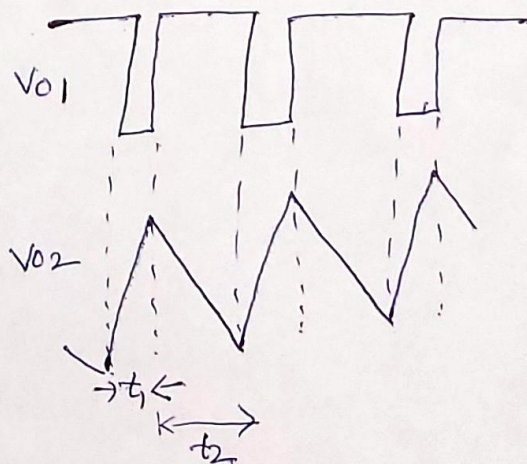
→ The voltage  $V_{in}$  produces current for integrator &  $V_{02}$  is a -ve ramp signal decided by  $V_{in}$ .

→ when that ramp reaches to Lower threshold of comparator,  $V_{01}$  becomes negative & cycle repeats

→ From the wave forms we can say,  
 $t_1 < t_2$

→ Hence o/p Frequency is decided by  $t_2$  i.e;  $V_{in}$ .

→ Here CKT acts as Voltage to frequency converter.





→ Frequency of oscillations is given by

$$f = \frac{R_1}{2R_2 RC V_{sat}} \times V_{in} = K \cdot V_{in}$$

where,  $V_{sat}$  = saturation of op-amp.