

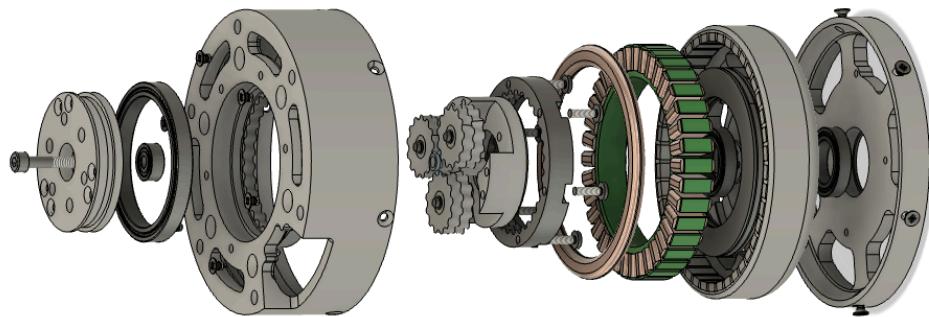
# TECHNICAL OVERVIEW: Low-Cost, Water-Cooled QDD Actuator

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**Focus:** Low-Cost, High-Torque Density Robotics & Thermal Management

## 1. Executive Summary

This project addresses the "thermal ceiling" of 3D-printed robotic actuators. While plastic actuators are incredibly cost-effective, their low thermal conductivity typically limits continuous torque. By integrating a custom water-cooling loop directly against the stator windings, this design achieved a 309% increase in continuous torque, reaching **8.6 Nm**—performance comparable to commercial metal units (\$200+) at a material cost of **\$37.30**.



## 2. Key Specifications & Performance

<b>Material Cost (USD)</b>	\$37.30
<b>Peak torque (Nm)</b>	16 Nm
<b>Peak current (A)</b>	$\geq 46.5$ A
<b>Continuous torque water-cooled (Nm)</b>	8.6 Nm
<b>Continuous current water-cooled (A)</b>	6.5 A
<b>Continuous torque no cooling (Nm)</b>	2.1 Nm
<b>Continuous current no cooling (A)</b>	0.85 A
<b>Gear Reduction</b>	7.2
<b>Weight (g)</b>	588 g

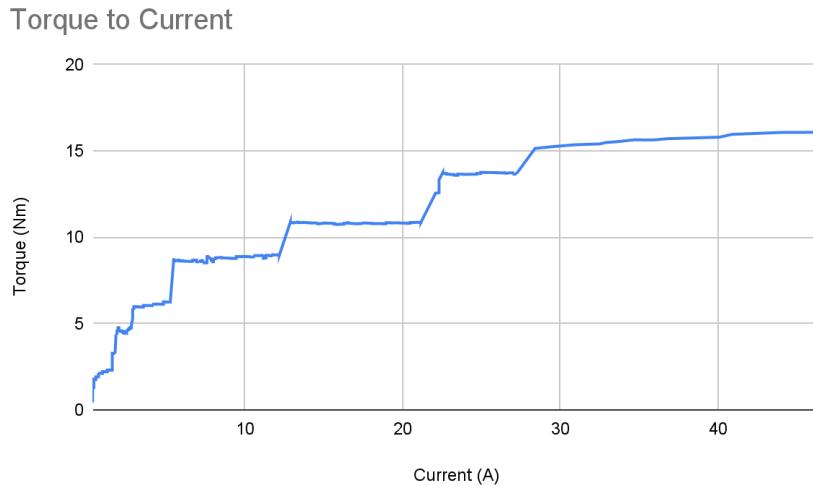


Figure 1. A torque step of the water-cooled actuator with increasing torque commands.

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### 3. Engineering Rigor & Methodology

#### A. Mechanical Design

To overcome the failure points of 3D-printed spur gears, I implemented a **7.2:1 Cycloidal Planetary Gearbox** with a herringbone profile, minimizing backlash while greatly increasing durability.

I calculated bearing moment loads using statics diagrams and dynamic load ratings, identifying failure points and iterating to achieve a final load capacity of **~25 Nm**.

#### B. Electromagnetic Customization

- **Stator:** 8110 36-slot stator, hand-wound with six parallel strands of AWG27 (6 turns/slot).
- **Rotor:** 3D-printed Polycarbonate backing with 42 N52 Neodymium magnets.
- **Simulation:** Used Simscale Electromagnetic Analysis to quantify the 13% flux loss from omitting a metal back-iron, justifying the trade-off for weight and cost.

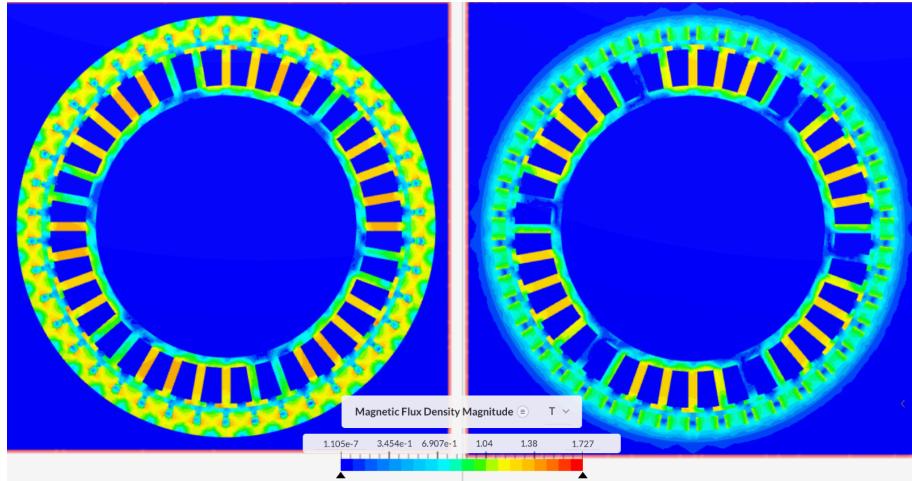


Figure 2. An electromagnetic analysis of the actuator with (left side) and without (right side) a back iron.

### C. Thermal Management (The Main Innovation)

The water-cooling channel consists of flattened 1/4" copper tubing clamped directly to the windings.

- **Simulation:** Tested various channel geometries and setups using Fusion 360 Thermal Analysis at different currents, optimizing to the final design.
- **Physical Implementation:** Used thermal paste to bridge the air gaps in hand-wound coils, achieving thermal equilibrium at **6.5A continuous current** (665% increase) while maintaining winding temperatures below **70°C**.

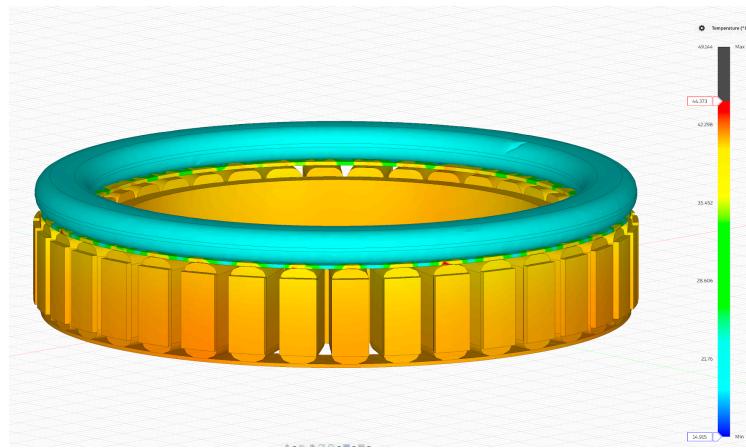


Figure 3. A Thermal analysis of the actuator with water cooling at 9A, disregarding air gaps and enamel between motor wires.

Water Cooling 6.5 A - Temperature to Time

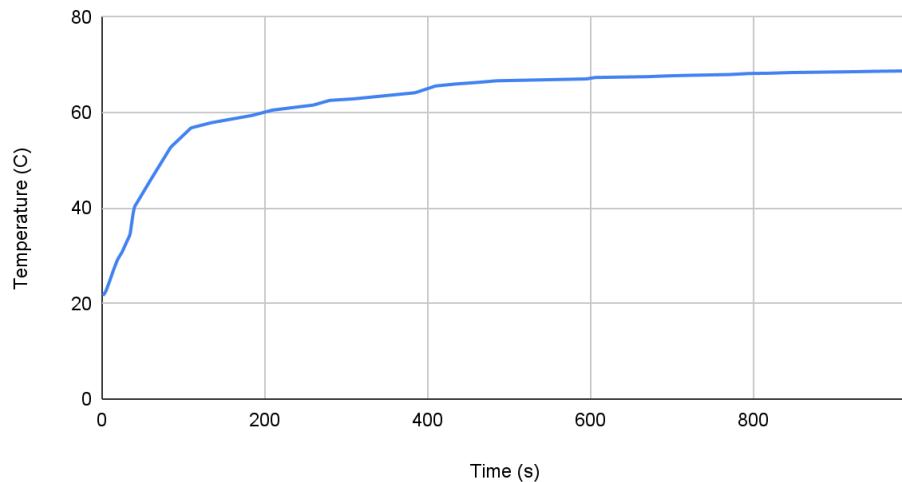


Figure 4. The maximum coil temperatures of the actuator with water cooling at 6.5A; thermal equilibrium reached at  $\sim 70^{\circ}\text{C}$ .

#### 4. Experimental Validation

- **Setup:** Custom test rig utilizing a 20kg load cell, HX711 amplifier, and a 300mm lever arm.
- **Control:** Field Oriented Control (FOC) via MKS XDrive.
- **Future Research Directions:** The torque-current relationship showed early magnetic saturation at 10A alongside unusual torque jumps, providing clear goals for Version 2.

