$\ensuremath{\mathsf{TTK4190}}$ - Assignment 3

Group 27

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1 Part 3: Speed Control

1.1 Problem 1: Propeller Revolution and Speed Control

1.1.1 Problem 1a

After using the wageningen-function, the updated values are $K_T = 0.6367$ and $K_Q = 0.1390$

1.1.2 Problem 1b

The code is updated to include the dynamics of the prime mover system with the following equations.

$$\frac{Q_m}{Y}(s) = \frac{K}{Ts+1} \tag{1}$$

$$\dot{Q_m} = -\frac{Q_m}{T} + \frac{K}{t}(m_c - n) \tag{2}$$

The shaft speed dynamics \dot{n} is also updated, and the code is shown below.

$$\dot{n} = \frac{Q_m - Q - Q_f}{I_m} \tag{3}$$

1.1.3 **Problem 1c**

```
256
    % propeller dynamics
    Im = 100000; Tm = 10; Km = 0.6;
257
                                                     % propulsion parameters
258
259
    % added feedforward
    Td = U_d * Xu / (t_thr - 1); % desired thrust (N)
260
261
262
    n_{term} = Td/(rho * Dia^{4} * KT);
    n_d = sign(n_term) * sgrt(abs(n_term));
                                                   % desired propeller speed (rps)
263
264
                                                     % friction torque (Nm)
265
    Qd = rho * Dia^4 * KQ * abs(n_d) * n_d;
                                                    % desired propeller moment (Nm)
266
267
    Y = Qd/Km;
                                                     % control input to main motor
268
    Qm_{-}dot = -Qm/Tm + Km/Tm * Y;
269
    n_{dot} = (Qm_{QQ})/Im;
271
    % store simulation data in a table (for testing)
272
    simdata(i,:) = [t n_d \Delta_c n \Delta eta' nu' u_d psi_d r_d z];
273
274
275
    % Euler integration
   xd = euler2(xd_dot,xd,h);
                                                 % reference model
276
                                                 % integral state
277
   z = euler2(e_psi, z, h);
    Qm = euler2(Qm_dot,Qm,h);
   eta = euler2(eta_dot,eta,h);
279
   nu = euler2(nu_dot, nu, h);
    \Delta = \text{euler2}(\Delta_{-}\text{dot}, \Delta, h);
   n = euler2(n_dot,n_h)
```

Listing 1: Full code propeller dynamics

1.1.4 Problem 1d

Assuming $u_r = u$, $\dot{u} = \dot{u}_r = 0$, u = U, $x_{\delta\delta}\delta^2 = 0$, U is given by

$$U = \frac{(t-1)T}{x_u} \tag{4}$$

1.2 Problem 1e

With the equation from the last problem we get

$$T_d = \frac{U_d x_u}{t - 1} \tag{5}$$

and

$$n_{term} = \frac{T_d}{\rho * d^4 * K_T} \tag{6}$$

$$n_d = sign(n_{term})\sqrt{abs(n_{term})} \tag{7}$$

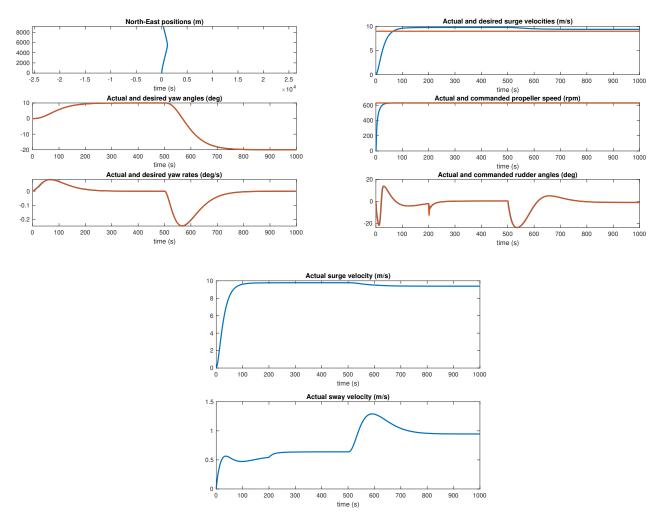


Figure 1: Ship behaviour with Propeller Revolution and Speed Control

No, we do not achieve the desired speed with constant heading angle. The surge velocity has a stationary error and does not reach the reference speed of $U_d = 9[m/s]$. This is because of the assumptions in the equation in problem 1d. To fix this we can add a feed-forward controller:

```
1 %Problem le: added feedforward
2 Td = (U_d-nu_c(1))*Xu/(t_thr-1);
```

Listing 2: Feed-forward

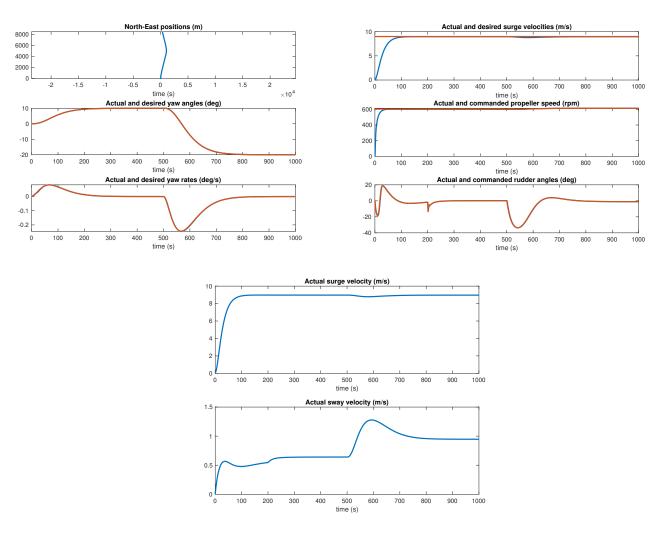


Figure 2: Ship behaviour with feed-forward

1.3 Problem 1f

Yes, with a 20[deg] setpoint change in heading, the speed will drop for a small period. This can be seen in figure 2. This is because of the sway velocity during the turn, so it need to be decomposed to be corrected to reference again.