Locally-accurate advection over steep terrain on a new type of Cartesian mesh

TODO: (working title)

James Shaw
13th April 2016

1 Introduction

Increasing spatial resolution means that numerical weather prediction models are able to resolve smaller-scale, steep slopes in terrain. A large majority of operational models use terrain-following coordinates to represent orography, but such models can suffer from increased numerical errors near steep slopes where the coordinate transformation becomes almost singular TODO: citations. Such singularities can be avoided by using the cut-cell method, which has been proposed as an alternative to terrain-following coordinates. The cut-cell method represents terrain using piecewise polynomial functions that intersect with an orthogonal, Cartesian mesh. Several studies of idealised flows have found that cut-cell models produce results with an accuracy that is comparable to, or better than, terrain-following models (Yamazaki and Satomura, 2008; Good et al., 2014; Shaw and Weller, 2016).

TODO: however, cut cells bring their own problems: the small cell problem, and loss of accuracy near the lower boundary. this paper is going to address these two issues...hopefully!

TODO: first describe the cut cell method, which typically describes the terrain by a piecewise bilinear function (although higher-order functions have been tried, e.g. Kirkpatrick et al. (2003).

Explicit, finite volume advection schemes must satisfy the Courant–Friedrichs–Lewy (CFL) constraint in order to be stable. The CFL constraint insists that the maximum timestep is proportional to the volume of the smallest cell. The cut cell method can create arbitrarily small cells in the vicinity of the terrain that impose severe constraints on the timestep. TODO: I need to talk about the CFL constraint w.r.t. flow direction, so maybe I should expand this discussion of CFL constraint. Adcroft et al. (1997) and Kirkpatrick et al. (2003) both talk about this.

There are a variety of techniques that alleviate the timestep constraint for cut cell meshes. One technique is to combine small cells with neighbouring cells, so that the smallest cell volume and, hence, the maximum timestep, is increased. Ye et al. (1999) identified cells with cell centres below ground, and combined each of them with the cell above. They applied the technique to a two-dimensional model

This is not the CFL const

Figure 1: TODO: an example diagram of a 3D cell with a bilinear terrain surface, highlighting face areas open to the air

of viscous incompressible flow. The technique ensures that the smallest cell volume is at least half the volume of an uncut cell, hence the maximum timestep is also constrained to be at least half the maximum timestep for the equivalent mesh with no cut cells. Yamazaki et al. (2016) extended this cell-combining technique to a three-dimensional, fully-compressible, non-hydrostatic atmospheric model, in which small cells are combined vertically or horizontally depending on the steepness of the terrain slope in the small cell. TODO: and? so what?

TODO: cell combining has disadvantages: velocity points may not have pressure points on both sides (Kirkpatrick et al., 2003), so it is no longer possible to separate horizontal and vertical pressure gradient calculations (Walko and Avissar, 2008). Kirkpatrick et al. (2003) also says that it is difficult to extend cell merging techniques to three dimensions, but Yamazaki et al. (2016) shows this can be done reasonably straightforwardly.

Another technique that alleviates the timestep constraint is the thin-wall approximation, in which the computational volume of a cell unaltered when it is cut. In other words, a cut cell is assigned a computational volume equal to its original, uncut, physical volume. The area of a cell face is calculated as the area unoccupied by solid terrain. In the thin-wall approximation, a cut cell can be conceptualised as a cardboard box without a lid and with side walls that are infinitesimally thin. Straight lines are cut along the side walls so that the box's upper edges lie along the bilinear terrain surface. TODO: *An example of the thin-wall approximation is shown in Fig. 1*.

By using computational volumes that are equally large for cut and uncut cells, the thin-wall approximation imposes no additional timestep constraints compared to an equivalent Cartesian mesh with no cut cells. The cell-combination technique still constrains the timestep because smaller cell volumes still remain where cells are not combined. Hence, the thin-wall technique should permit timesteps up to twice as large as those permitted by the cell-combination technique.

TODO: but thin-wall approximation also has difficulties: Yamazaki and Satomura (2010) talk about "internal inconsistency" (presumably they mean that cell volumes are inconsistent with face areas, but I'll email Hiroe and check this). Walko and Avissar (2008) provide a nice example of a thin-wall problem, possibly adapted from Calhoun and LeVeque (2000), describing the retardation of a cold front in uniform horizontal flow along a flat surface that includes long, thin, rectangular cut cells.

TODO: as a slight aside, Calhoun and LeVeque (2000) talk about using "capacity functions" and talk about flow through porous media, but this technique seems to be somewhat (if not entirely) equivalent to the thin-wall approximation

TODO: I should also discuss the partially implicit method of Jebens et al. (2011). And perhaps other methods that I have yet to satisfactorily understand: a volume-of-fluid approach by Almgren et al. (1997), and the master–slave cell-linking approach by Kirkpatrick et al. (2003).

TODO: what about existing work on unstructured/boundary fitted meshes? Almgren et al. (1997) has masses of citations for loads of different mesh techniques.

TODO: The next topics to discuss are: loss of accuracy at the lower boundary (2nd order schemes often become only 1st-order accurate locally), then how our slanted cell mesh technique and cubicUpwindCPCFit advection scheme might be able to increase timesteps and increase local accuracy...maybe!

2 Mesh generation

TODO: describe how we construct a slanted cell mesh. at some point in the paper we must justify the choice of 'tolerance', which was set to $2\Delta z/5$ in Shaw and Weller (2016) without much justification.

TODO: although we are only considering 2D idealised tests in this paper, it would be nice to show that our method extends to 3D – why don't we try it out with some real digital surface model data?

great idea. And with a hexagonal mesh

3 Multidimensional advection scheme

TODO: describe the advection scheme

4 Results

TODO: use the thermal advection test from Shaw and Weller (2016), but with steeper slopes. compare with BTF meshes and cut cell meshes created using the ASAM mesh generator. use Co close to 1 and report on the timesteps for each type of mesh.

TODO: report \(\ell_2 \) error norms, min/max values for BTF. slantedCell and cutCell meshes

TODO: I haven't thought much about this yet, but there's a lot of literature that says

"2nd-order schemes become 1st-order at the lower boundary", and talk about global accuracy versus local accuracy. I'm not sure how to measure local order of accuracy, but I think I should examine order-of-accuracy for cubicUpwindCPCFit. The work by Ye et al. (1999) is quite similar to ours: they use polynomial stencils to interpolate onto boundaries, and test an explicit advection scheme which they show is 2nd order globally and locally.

TODO: should we compare cubicUpwindCPCFit with a more standard scheme? such as QUICK, maybe? because it's well-known, fairly high-order, implemented in OpenFOAM, Kirkpatrick et al. (2003) uses it...lower order schemes are more likely to be too diffusive or just unstable, especially on BTF meshes

TODO: I don't think I want to go beyond advection scheme/advection tests in this paper because I think it will lose its focus. that said, I have had some very good results of resting atmosphere on the slanted cell mesh compared to cut cell and BTF meshes, and

You would have to check

it might be interesting to see how steep we can go, and what happens to the spurious circulations...

5 Conclusions

6 Acknowledgements

TODO: Supervisors, funding bodies. ASAM group for the mesh generator—I should ask permission to use cut cell meshes in this paper

References

- Adcroft, A., C. Hill, and J. Marshall, 1997: Representation of topography by shaved cells in a height coordinate ocean model. *Mon. Wea. Rev.*, **125**, 2293–2315, doi:10.1175/1520-0493(1997)125<2293:ROTBSC>2.0.CO;2.
- Almgren, A. S., J. B. Bell, P. Colella, and T. Marthaler, 1997: A Cartesian grid projection method for the incompressible Euler equations in complex geometries. *SIAM J. Sci. Comput.*, **18**, 1289–1309, doi:10.1137/S1064827594273730.
- Calhoun, D., and R. J. LeVeque, 2000: A Cartesian grid finite-volume method for the advection-diffusion equation in irregular geometries. *J. Comp. Phys.*, **157**, 143–180, doi:10.1006/jcph.1999.6369.
- Good, B., A. Gadian, S.-J. Lock, and A. Ross, 2014: Performance of the cut-cell method of representing orography in idealized simulations. *Atmos. Sci. Lett.*, **15**, 44–49, doi:10.1002/asl2.465.
- Jebens, S., O. Knoth, and R. Weiner, 2011: Partially implicit peer methods for the compressible Euler equations. *J. Comp. Phys.*, **230**, 4955–4974, doi:10.1016/j.jcp.2011.03.015.
- Kirkpatrick, M., S. Armfield, and J. Kent, 2003: A representation of curved boundaries for the solution of the Navier–Stokes equations on a staggered three-dimensional Cartesian grid. *J. Comp. Phys.*, **184**, 1–36, doi:10.1016/S0021-9991(02)00013-X.
- Shaw, J., and H. Weller, 2016: Comparison of terrain following and cut cell grids using a non-hydrostatic model. *Mon. Wea. Rev.*, doi:10.1175/MWR-D-15-0226.1.
- Walko, R. L., and R. Avissar, 2008: The Ocean-Land-Atmosphere Model (OLAM). Part II: Formulation and tests of the nonhydrostatic dynamic core. *Mon. Wea. Rev.*, **136**, 4045–4062, doi:10.1175/2008MWR2523.1.
- Yamazaki, H., and T. Satomura, 2008: Vertically combined shaved cell method in a z-coordinate nonhydrostatic atmospheric model. *Atmos. Sci. Lett.*, **9**, 171–175, doi:10.1002/asl.187.

- Yamazaki, H., and T. Satomura, 2010: Nonhydrostatic atmospheric modeling using a combined Cartesian grid. *Mon. Wea. Rev.*, **138**, 3932–3945, doi:10.1175/2010MWR3252.1.
- Yamazaki, H., T. Satomura, and N. Nikiforakis, 2016: 3D cut-cell modelling for high-resolution atmospheric simulations. *Quart. J. Roy. Meteor. Soc.*, doi:10.1002/qj.2736.
- Ye, T., R. Mittal, H. Udaykumar, and W. Shyy, 1999: An accurate Cartesian grid method for viscous incompressible flows with complex immersed boundaries. *J. Comp. Phys.*, **156**, 209–240, doi:10.1006/jcph.1999.6356.