

# PHYS 241 Final Exam

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## Preliminary

*My signature below certifies that I have not, nor will I, consult with any other person about the exam, or any other subject related to it*

## Question 1

(a)

We first and foremost write the KVL equations

$$\begin{array}{ll} \text{(KCL)} & I_1 + I_3 = I_2 \\ \text{(KVL1)} & V_1 - R_1 I_1 - R_2 I_2 = 0 \\ \text{(KVL2)} & V_2 - I_2(R_2 + R_3) + I_1(R_3) = 0 \end{array} \implies \begin{cases} R_1 I_1 + R_2 I_2 & = V_1 \\ -R_3 I_1 + (R_2 + R_3) I_2 & = V_2 \end{cases}$$

This leads to the linear equation system

$$\begin{pmatrix} R_1 & R_2 \\ -R_3 & R_2 + R_3 \end{pmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix} = \begin{pmatrix} V_1 \\ V_2 \end{pmatrix} \rightarrow \begin{pmatrix} 5 \text{ k}\Omega & 1 \text{ k}\Omega \\ -1 \text{ k}\Omega & 2 \text{ k}\Omega \end{pmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix} = \begin{pmatrix} 12 \text{ V} \\ 3 \text{ V} \end{pmatrix}.$$

This system is trivially solved using *Cramer's Rule*

$$\begin{pmatrix} 5 \text{ k}\Omega & 1 \text{ k}\Omega \\ -1 \text{ k}\Omega & 2 \text{ k}\Omega \end{pmatrix}^{-1} \begin{pmatrix} 12 \text{ V} \\ 3 \text{ V} \end{pmatrix} = \frac{1}{11} \begin{pmatrix} 2 \text{ k}\Omega & -1 \text{ k}\Omega \\ 1 \text{ k}\Omega & 5 \text{ k}\Omega \end{pmatrix} \begin{pmatrix} 12 \text{ V} \\ 3 \text{ V} \end{pmatrix} = \begin{pmatrix} 21/11 \\ 27/11 \end{pmatrix}.$$

Therefore, the values for  $I_1$  and  $I_2$  are respectively 1.909 mA and 2.455 mA.

To find the values of  $V_A$  and  $V_B$  the nodal method is applied

$$I_1 = \frac{V_1 - V_A}{R_2} \implies V_A = V_1 - I_1 R_1 = 12 \text{ V} - 1.909 \times 10^{-3} \text{ A} \times 5000 \Omega = 2.455 \text{ V}.$$

The voltage at the point  $V_B$  is simply 0 V since that point is a ground.

(b)

Since voltage is conserved along a loop and since there is a ground placed right after the positive polarity of the f.e.m source, then  $V_B$  must necessarily be  $-12$  V. Moreover, the direction of the currents is not altered by changing the ground's place in the present configuration so we may apply the nodal method for  $I_2$  that was found in (a)

$$I_2 = \frac{V_A - V_B}{R_2} \implies V_A = I_2 R_2 + V_B = 2.455 \text{ mA} \times 1000 \Omega - 12 \text{ V} = -9.455 \text{ V}.$$

**Question 2**

(a)

At  $t = 0$  the capacitor is fully discharged, hence  $Q(0) = 0 \text{ C} \implies \Delta V_C(0) = 0 \text{ V}$ . Since  $R_2$  is in parallel with  $C$ , then it follows that  $\Delta V_{R_2}(0) = 0 \text{ V}$  as well. Applying Kirchhoff's law along the first loop and isolating  $I$  yields

$$I(0) = \frac{V_0}{R_1}.$$

(b)

After a long time, the capacitor is "fully" charged such that no voltage is dropped across it. So we may effectively remove this component from the circuit, compute the equivalent resistance from the resistors in series and apply Kirchhoff's law along the circuit to obtain

$$I(t)_{t \rightarrow \infty} = \frac{V_0}{R_1 + R_2}.$$

(c)

Three equations are needed

$$\textcircled{1}. I = I_1 + I_2 \qquad \textcircled{2}. V_0 = I_1 R_1 + I_2 R_2 \qquad \textcircled{3}. R_2 I_2 = \frac{Q}{C}.$$

We first differentiate with respect to time  $\textcircled{3}$  and isolate  $\dot{I}_2$  yielding

$$\frac{dI_2}{dt} = \frac{I_1}{R_2 C}. \tag{1}$$

Then we substitute  $\textcircled{1}$  into  $\textcircled{2}$  giving

$$V_0 = R_1 I_1 + (R_1 + R_2) I_2. \tag{2}$$

Differentiating with respect to time Equation 2 and substitute Equation 1 inside

$$\begin{aligned} V_0 = R_1 I_1 + (R_1 + R_2) I_2 \xrightarrow{d/dt} 0 &= R_1 \frac{dI_1}{dt} + (R_1 + R_2) \frac{dI_2}{dt} \\ &= R_1 \frac{dI_1}{dt} + \frac{(R_1 + R_2)}{R_2 C} I_1 \end{aligned}$$

Diving both sides by  $R_1$  and letting  $\tau \equiv R_1 R_2 C / (R_1 + R_2)$  we have a first order linear differential equation

$$\frac{dI_1}{dt} + \frac{I_1}{\tau} = 0.$$

From ODEs, there exists an integrating factor  $\mu(t) = e^{\int p(t) dt} = e^{\int 1/\tau dt} = e^{t/\tau + C} = e^{t/\tau} e^C = C_1 e^{t/\tau}$ , where  $C_1 \equiv e^C$ . We let  $C_1 = 1$  since only one integrating factor is needed and thus  $\mu(t) = e^{t/\tau}$ . Moreover, the general solution is given by  $y(t) = \frac{1}{\mu(t)} \int \mu(t) q(t) dt$ , i.e.,

$$I_1(t) = \frac{1}{e^{t/\tau}} \int e^{t/\tau}(0) dt = C_2 e^{-t/\tau}$$

The initial condition is the initial current therefore  $C_2 \equiv I_1(0)$ , finally

$$I_1(t) = I_1(0) e^{-t/\tau}. \quad (3)$$

We now integrate Equation 1 and substitute Equation 3 to have an expression for  $I_2(t)$

$$I_2(t) = \int_0^t \frac{I_1}{C R_2} dt = \frac{I_1(0)}{C R_2} \int_0^t e^{-t/\tau} dt = \frac{I_1(0)}{C R_2} \tau (1 - e^{-t/\tau}).$$

Combining the previous result with Equation 3 provides a value for the current  $I(t)$

$$\begin{aligned} I(t) = I_1(t) + I_2(t) &= I_1(0) e^{-t/\tau} + \frac{I_1(0)}{C R_2} \tau (1 - e^{-t/\tau}) \\ &= I_1(0) \left[ e^{-t/\tau} + \frac{\tau (1 - e^{-t/\tau})}{c R_2} \right] \end{aligned}$$

Using the result from (a),  $I_1(0)$  is the initial current in the circuit therefore

$$I(t) = \frac{V_0}{R_1} \left[ e^{-t/\tau} + \frac{\tau (1 - e^{-t/\tau})}{c R_2} \right], \text{ with } \tau = \frac{R_1 R_2 C}{R_1 + R_2}.$$

### Question 3

(a)

$$\frac{V'}{V} = \frac{Z_{R_2}}{Z_{R_1} + Z_{R_2}} = \frac{R_2}{R_1 + R_2}.$$

The amplitude is simply  $R_2/(R_1 + R_2)$  since this is not a complex number. The phase is 0 since there is no imaginary part and  $\tan^{-1}(0) = 0$ . Having found the essential terms, we write

$$V_{\text{out}} = \frac{V_0 \cos(\omega t) R_2}{(R_1 + R_2)}.$$

(b)

Let  $R_T \equiv R_1 + R_2$  since the resistors are in series. Then

$$\frac{V'}{V} = \frac{Z_C}{Z_C + Z_{R_T}} = \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R_T} = \frac{1}{1 + j\omega C R_T} = \frac{1}{1 + j\omega\tau} \quad , \text{ with } \tau = R_T C.$$

We compute the amplitude

$$\left| \frac{V'}{V} \right| = \left( \left( \frac{1}{1 + j\omega\tau} \right) \left( \frac{1}{1 - j\omega\tau} \right) \right)^{1/2} = \frac{1}{\sqrt{1 + (\omega\tau)^2}}.$$

It follows that for the phase

$$\begin{aligned} \because \left( \frac{1}{1 + j\omega\tau} \right) \left( \frac{1 - j\omega\tau}{1 - j\omega\tau} \right) &= \frac{1}{1 + (\omega\tau)^2} - j \frac{\omega\tau}{1 + (\omega\tau)^2} \\ \varphi(\omega) = \tan^{-1} \left( \frac{\text{Im}[V'/V]}{\text{Re}[V'/V]} \right) &= -\tan^{-1} \omega\tau. \end{aligned}$$

Having found all the essential terms it follows that

$$V'(t) = V_{\text{out}} = \frac{V_0}{\sqrt{1 + (\omega\tau)^2}} \cos(\omega t - \tan^{-1} \omega\tau).$$

(c)

As  $\omega \rightarrow 0$  the impedance of the capacitor is very high compared to the equivalent resistance, therefore little voltage is dropped across the resistors such that  $V'_0 \approx 0$ . The current leads by  $\pi/2$  meaning that the phase shift is  $\pi/2$ .

As  $\omega \rightarrow \infty$  the capacitor's impedance vanishes and all voltage is dropped across the equivalent resistors such that  $V'_0 \approx V_0$  and thus the phase shift is  $\approx 0$ .

Given these limits and the circuit's configuration, we can regard this circuit as a low-pass RC filter.

#### Question 4

(a)

Let us first compute  $a_0$

$$\frac{a_0}{2} = \frac{1}{T} \left( \int_{-T/2}^0 -V_0 dt + \int_0^{T/2} V_0 dt \right) = \frac{1}{T} \left( -\frac{T}{2} + \frac{T}{2} \right) = 0 \implies a_0 = 0.$$

The given square wave is an odd function therefore  $a_n = 0 \forall n \in \mathbb{N}_+$ .

$$\begin{aligned}
 b_{n>0} &= \frac{1}{T} \left[ \int_{-T/2}^0 -V_0 \sin(\omega_n t) dt + \int_0^{T/2} V_0 \sin(\omega_n t) dt \right] \\
 &= \frac{1}{T} \left[ -\frac{V_0}{\omega_n} \left( -\cos(\omega_n t) \right) \Big|_{-T/2}^0 + \frac{V_0}{\omega_n} \left( -\cos(\omega_n t) \right) \Big|_0^{T/2} \right] \\
 &= \frac{1}{T} \left[ \frac{-V_0}{\omega_n} \left( -1 + \cos \left( \frac{-2n\pi T}{2T} \right) \right) + \frac{V_0}{\omega_n} \left( -\cos \left( \frac{2n\pi T}{2T} \right) + 1 \right) \right] \\
 &= \frac{-V_0}{2n\pi} \cos(-\pi n) + \frac{V_0}{n\pi} - \frac{V_0}{2n\pi} \cos(n\pi)
 \end{aligned}$$

Using the identity  $\cos(-x) = \cos(x)$  and rearranging yields

$$\begin{aligned}
 &= \frac{V_0}{n\pi} (1 - \cos(n\pi)) \\
 &= \frac{2V_0}{n\pi} \left( \frac{1 - \cos(n\pi)}{2} \right) = \frac{2V_0}{n\pi} \sin^2 \left( \frac{n\pi}{2} \right).
 \end{aligned}$$

We note that

$$\frac{2V_0}{n\pi} \sin^2 \left( \frac{n\pi}{2} \right) \begin{cases} 1 & , \text{for } n \text{ odd} \\ 0 & , \text{for } n \text{ even} \end{cases}$$

Finally, we write the Fourier series for the given square wave

$$f(t) = \frac{2V_0}{\pi} \sum_{n=1}^{\infty} \frac{1}{(2n-1)} \sin \left( \frac{2\pi(2n-1)t}{T} \right).$$

(b)

We first and foremost find an expression for the transfer function

$$H(\omega) = \frac{\left( \frac{1}{Z_L} + \frac{1}{Z_C} \right)^{-1}}{\left( \frac{1}{Z_L} + \frac{1}{Z_C} \right)^{-1} + Z_R} = \frac{\left( \frac{1}{j\omega L} + j\omega C \right)^{-1}}{\left( \frac{1}{j\omega L} + j\omega C \right)^{-1} + R} = \frac{1}{1 + R \left( \frac{1}{j\omega L} + j\omega C \right)}$$

Multiplying by  $j\omega L$  and diving by  $R$  whilst defining  $\tau \equiv L/R$  with  $LC = 1/\omega_0^2$  yields

$$H(\omega) = \frac{j\omega L}{j\omega L + R(1 - (\omega/\omega_0)^2)} = \frac{j\omega\tau}{j\omega\tau + 1 - (\omega/\omega_0)^2}.$$

We carry on by finding the amplitude of  $H(\omega)$

$$|H(\omega)| = \left( \left( \frac{j\omega\tau}{j\omega\tau + 1 - (\omega/\omega_0)^2} \right) \left( \frac{-j\omega\tau}{-j\omega\tau + 1 - (\omega/\omega_0)^2} \right) \right)^{1/2} = \frac{\omega\tau}{\sqrt{(1 - (\omega/\omega_0)^2)^2 + (\omega\tau)^2}}.$$

Finally, we look for the phase

$$\left( \frac{j\omega\tau}{j\omega\tau + 1 - (\omega/\omega_0)^2} \right) \left( \frac{1 - (\omega/\omega_0)^2 - j\omega\tau}{1 - (\omega/\omega_0)^2 - j\omega\tau} \right) = \frac{(\omega\tau)^2}{(1 - (\omega/\omega_0)^2)^2 + (\omega\tau)^2} + j \frac{(\omega\tau)(1 - (\omega/\omega_0)^2)}{(1 - (\omega/\omega_0)^2)^2 + (\omega\tau)^2}$$

$$\therefore \varphi_n(\omega_n) = \tan^{-1} \left( \frac{(\omega\tau)(1 - (\omega/\omega_0)^2)}{(\omega\tau)^2} \right) = \tan^{-1} \left( \frac{1 - (\omega/\omega_0)^2}{\omega\tau} \right).$$

Using the result from (a) we write the  $V_{\text{out}}$  function

$$V_{\text{out}} = \sum_{n=1}^{\infty} \frac{2V_0}{\pi(2n-1)} \frac{\omega_n\tau}{\sqrt{(1 - (\omega_n/\omega_0)^2)^2 + (\omega_n\tau)^2}} \sin \left( \omega_n t + \tan^{-1} \left( \frac{1 - (\omega_n/\omega_0)^2}{\omega_n\tau} \right) \right). \quad (4)$$

To see which frequencies go through, we look for  $\omega_0 \pm \Delta\omega$

$$\omega_0 = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{(1 \text{ mH})(2.8 \text{ }\mu\text{F})}} = 18898 \text{ s}^{-1}.$$

$$\tau = \frac{L}{R} = \frac{1 \text{ mH}}{3 \text{ k}\Omega} = 3.33 \times 10^{-7} \text{ s}.$$

$$Q = \frac{1}{\tau\omega_0} = \frac{1}{(3.33 \times 10^{-7} \text{ s})(18898 \text{ s}^{-1})} = 158.74$$

$$\Delta\omega = \frac{\omega_0}{Q} = \frac{18898 \text{ s}^{-1}}{158.74} = 119.05 \text{ s}^{-1}.$$

$$\therefore \omega_0 \pm \Delta\omega = (18898 \pm 119) \text{ s}^{-1}.$$

We now look for the frequency components which lie within this range

$$\omega_1 = \frac{2\pi(1)}{T} = \cancel{6283.2 \text{ s}^{-1}} \quad \omega_2 = \frac{2\pi(2)}{T} = \cancel{12566.4 \text{ s}^{-1}} \quad \omega_3 = \frac{2\pi(3)}{T} = 18849.6 \text{ s}^{-1} \checkmark.$$

The amplitude can then be computed with

$$A_{\text{out}} = \frac{2V_0}{\pi(2(3)-1)} \frac{\omega_3\tau}{\sqrt{(1 - (\omega_3/\omega_0)^2)^2 + (\omega_3\tau)^2}}$$

$$= \frac{2(1)}{\pi(2(3)-1)} \frac{(18849.6)(3.33 \times 10^{-7})}{\sqrt{(1 - (18849.6/18898)^2)^2 + ((18849.6)(3.33 \times 10^{-7}))^2}} = 0.09869 \text{ V}.$$

The phase is also computed with

$$\varphi = -\frac{\pi}{2} + \tan^{-1} \left( \frac{1 - \left( \frac{18849.6}{18898} \right)^2}{18849.6(3.33 \times 10^{-7})} \right) = -\frac{\pi}{2} + 39^\circ \approx -\frac{\pi}{4}.$$

**Question 5**

Since  $f(t) = t/T$  for  $|t| \leq T/2$ , let us compute  $C_k$  using the definition

$$\begin{aligned}
 C_k &= \frac{1}{T} \int_{-T/2}^{T/2} f(t) e^{-j\omega_k t} dt = \frac{1}{T^2} \int_{-T/2}^{T/2} t e^{-j\omega_k t} dt \\
 &= \frac{1}{T^2} \left[ \frac{-t e^{-j\omega_k t}}{j\omega_k} \right]_{-T/2}^{T/2} + \frac{1}{j\omega_k} \int_{-T/2}^{T/2} e^{-j\omega_k t} dt \\
 &= \frac{1}{T^2} \left[ \frac{1}{j\omega_k} \left( \frac{-T e^{-\frac{j\omega_k T}{2}}}{2} - \frac{T e^{\frac{j\omega_k T}{2}}}{2} \right) + \frac{2}{j\omega_k^2} \left( \frac{e^{\frac{j\omega_k T}{2}}}{2j} - \frac{e^{-\frac{j\omega_k T}{2}}}{2j} \right) \right] \\
 &= \frac{1}{T^2} \left[ \frac{-T \cos\left(\frac{\omega_k T}{2}\right)}{j\omega_k} + \frac{2 \sin\left(\frac{\omega_k T}{2}\right)}{j\omega_k^2} \right] \\
 &= \frac{1}{T^2} \left[ \frac{T i \cos\left(\frac{\omega_k T}{2}\right)}{\omega_k} - \frac{2 i \sin\left(\frac{\omega_k T}{2}\right)}{\omega_k^2} \right]
 \end{aligned}$$

Using  $\omega_k = 2\pi k/T$  the expression reduces to

$$C_k = \frac{\pi i k \cos(\pi k) - i \sin(\pi k)}{2\pi^2 k^2}.$$

We now compute the Fourier transform

$$\begin{aligned}
 f(t) &= \sum_{k=-\infty}^{\infty} \left( \frac{\pi i k \cos(\pi k) - i \sin(\pi k)}{2\pi^2 k^2} \right) e^{j\omega_k t} \\
 \therefore F(\omega) &= \int_{-\infty}^{\infty} \sum_{k=-\infty}^{\infty} \left( \frac{\pi i k \cos(\pi k) - i \sin(\pi k)}{2\pi^2 k^2} \right) e^{j\omega_k t} e^{-j\omega t} dt \\
 &= \sum_{k=-\infty}^{\infty} \left( \frac{\pi i k \cos(\pi k) - i \sin(\pi k)}{2\pi^2 k^2} \right) \int_{-\infty}^{\infty} e^{j(\omega_k - \omega)t} dt \\
 &= \sum_{k=-\infty}^{\infty} \left( \frac{\pi i k \cos(\pi k) - i \sin(\pi k)}{2\pi^2 k^2} \right) \underbrace{\int_{-\infty}^{\infty} e^{-j(\omega - \omega_k)t} dt}_{\equiv \delta(\omega - \omega_k)} \\
 F(\omega) &= \sum_{k=-\infty}^{\infty} \left( \frac{\pi i k \cos(\pi k) - i \sin(\pi k)}{2\pi^2 k^2} \right) \delta(\omega - \omega_k).
 \end{aligned}$$