Computational Microelectronics L23

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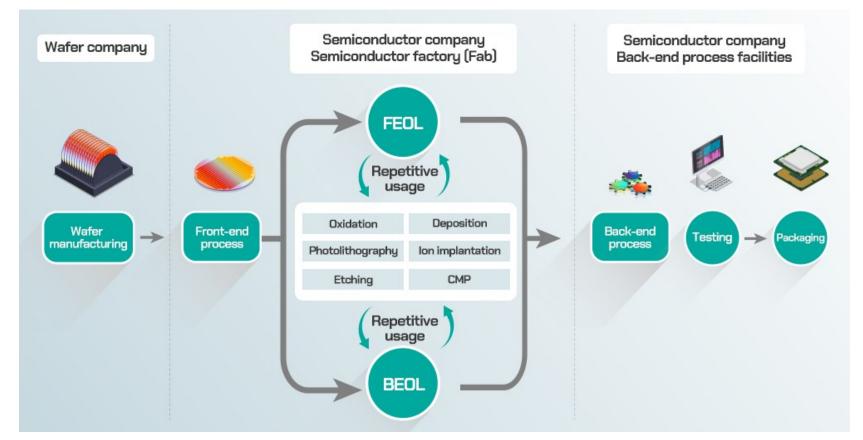
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Thermal expansion

Scope of TCAD

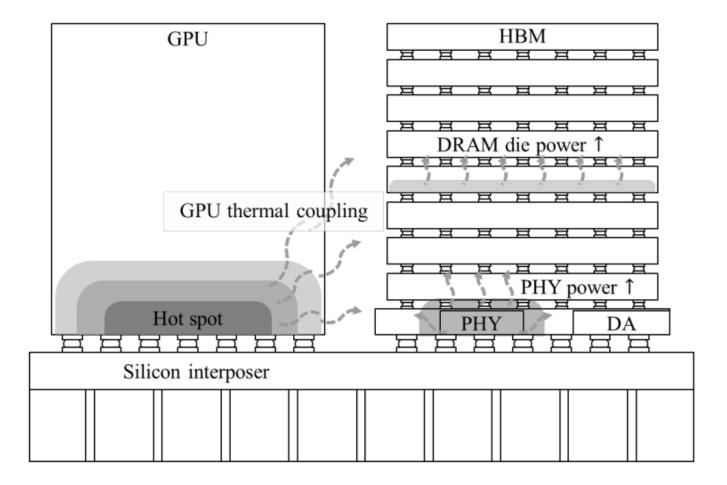
- TCAD serves to support the development process of semiconductor device technology.
 - Front-ent/back-end



Semiconductor manufacturing process (SK hynix)

Temperature as a key quantity

- GPU-HBM
 - Is this really in the scope of TCAD?



Thermal issues of HBM-GPU module on silicon interposer process (K. Son et al., EDAPS, 2023)

Thermal expansion

- Linear expansion
 - Coefficient of linear thermal expansion,

$$\alpha_L = \frac{1}{L} \frac{dL}{dT}$$

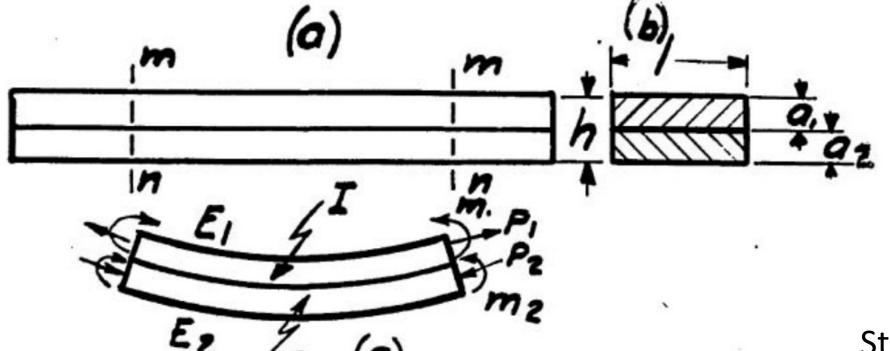
(For silicon, 2.6 X 10⁻⁶ K⁻¹)

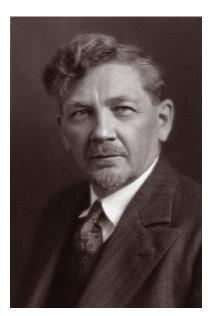
-Then, the thermal strain becomes

$$\varepsilon_{thermal} = \frac{\Delta L}{L} = \alpha_L \Delta T$$

Bimetal strip

- S. Timoshenko, "Analysis of bi-metal thermostats," Journal of the Optical Society of America, vol. 11, pp. 233-255 (1925)
 - Let us follow the paper. (Some figures are taken from that paper.)





Stephen Timoshenko (Wikipedia)

Fig. 1. Deflection of a bi-metal strip while uniformly heated.

Conditions

- Coefficients of expansion, α_1 and α_2 ($\alpha_2 > \alpha_1$), remain constant.
 - -Temperature from t_0 to t.
 - $-E_1$ and E_2 denote their moduli of elasticity.

Stress / strain

 $-a_1$ and a_2 are metal thicknesses. (Don't be confused with α_1 and α_2 .)

Equilibrium

At any cross-section,

$$P_1 = P_2 = P$$

$$\frac{Ph}{2} = M_1 + M_2$$

- $-P_1$ is an axial tensile force and P_2 is an axial compressive force.
- $-M_1$ and M_2 are bending moments:

$$M_1 = \frac{E_1 I_1}{\rho}$$
 Radius of curvature $M_2 = \frac{E_2 I_2}{\rho}$

Manipulation

• Now we have one equation for calculating P and ρ :

$$\frac{Ph}{2} = \frac{E_1I_1 + E_2I_2}{\rho}$$

– Another equation? Length at the interface

$$\alpha_1(t-t_0) + \frac{P_1}{E_1a_1} + \frac{a_1}{2\rho}$$

-The same quantity from metal 2

$$\alpha_2(t-t_0) - \frac{P_2}{E_2 a_2} - \frac{a_1}{2\rho}$$

-These two expressions should be identical.

Result

• Now we have one equation for calculating P and ρ :

$$\frac{1}{\rho} = \frac{(\alpha_2 - \alpha_1)(t - t_0)}{\frac{h}{2} + \frac{2(E_1I_1 + E_2I_2)}{h} \left(\frac{1}{E_1a_1} + \frac{1}{E_2a_2}\right)}$$

–A special case,
$$E_1=E_2$$
 and $a_1=a_2$, (with $I_1=\frac{a_1^3}{12}$ and $I_2=\frac{a_2^3}{12}$)

$$\frac{1}{\rho} = \frac{3}{2} \frac{(\alpha_2 - \alpha_1)(t - t_0)}{h}$$

Deformation

• Now we have one equation for calculating P and ρ :

$$\delta = \frac{l^2}{8\rho}$$

$$\alpha_1 = 12 \times 10^{-6} \,\mathrm{K}^{-1}$$

$$\alpha_2 = 19 \times 10^{-6} \,\mathrm{K}^{-1}$$

$$h = 2 \text{ mm}$$

$$t = 600 \text{ K}, t_0 = 300 \text{ K}$$

-Then,
$$\frac{1}{\rho} = 1.575 \text{ m}^{-1}$$

-When l = 20 mm, $\delta = 78.75$ μ m.

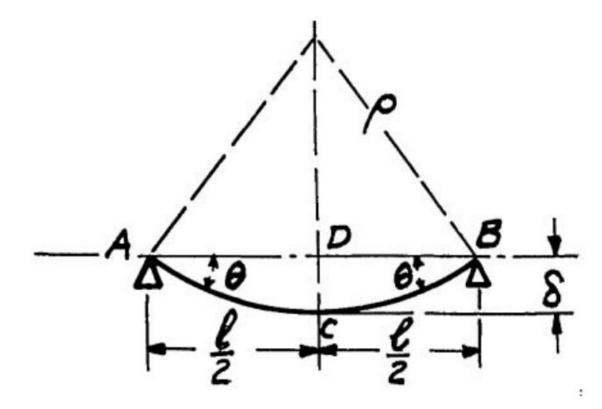


Fig. 2. Deflection of a simply supported bi-metal strip.

Thank you for your attention!