

# Special Topics on Basic EECS I

## VLSI Devices

### Lecture 25

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# A simpler form of $I_d$

- By taking the difference, we can find a simpler form:

$$I_d = \mu_{eff} \frac{W}{L} \left\{ C_{ox} \left( V_{gs} - V_{fb} - 2\phi_B - \frac{1}{2} V_{ds} \right) V_{ds} - \frac{2}{3} \sqrt{2\epsilon_{si} q N_a} [(2\phi_B + V_{ds})^{1.5} - (2\phi_B)^{1.5}] \right\} \quad \text{Taur, Eq. (3.22)}$$

- For a given  $V_{gs}$ ,  $I_d$  first increases linearly with  $V_{ds}$ , then gradually levels off to a saturated value.

# Linear (triode) region

- When  $V_{ds}$  is small, we may keep only up to the first order.

$$\begin{aligned} I_d &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} (V_{gs} - V_{fb} - 2\phi_B) V_{ds} - \frac{2}{3} \sqrt{2\epsilon_{si} q N_a} \left[ \frac{3}{2} (2\phi_B)^{0.5} V_{ds} \right] \right\} \\ &= \mu_{eff} \frac{W}{L} C_{ox} \left( V_{gs} - V_{fb} - 2\phi_B - \frac{\sqrt{4\epsilon_{si} q N_a \phi_B}}{C_{ox}} \right) V_{ds} \\ &= \mu_{eff} \frac{W}{L} C_{ox} (V_{gs} - V_t) V_{ds} \end{aligned} \quad \text{Taur, Eq. (3.23)}$$

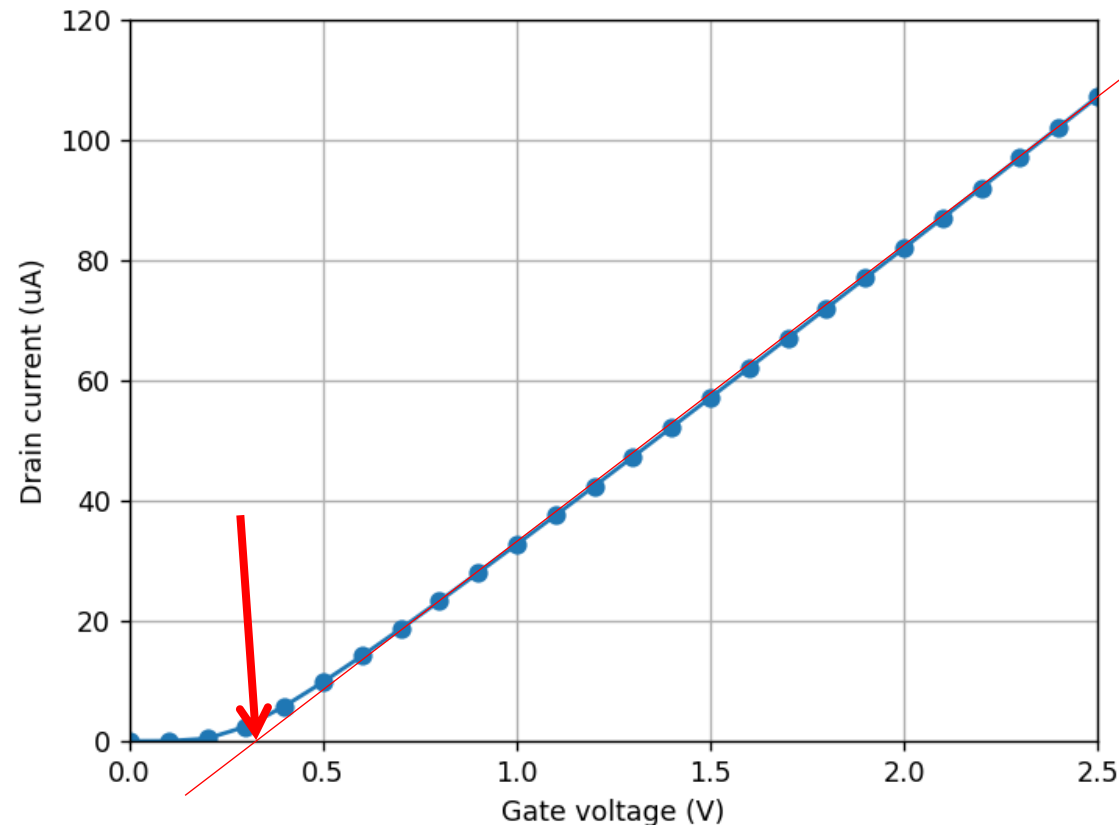
– The threshold voltage,  $V_t$ , is given by

$$V_t = V_{fb} + 2\phi_B + \frac{\sqrt{4\epsilon_{si} q N_a \phi_B}}{C_{ox}} \quad \text{Taur, Eq. (3.24)}$$

– It is the gate voltage when the surface potential reaches at  $2\phi_B$ .

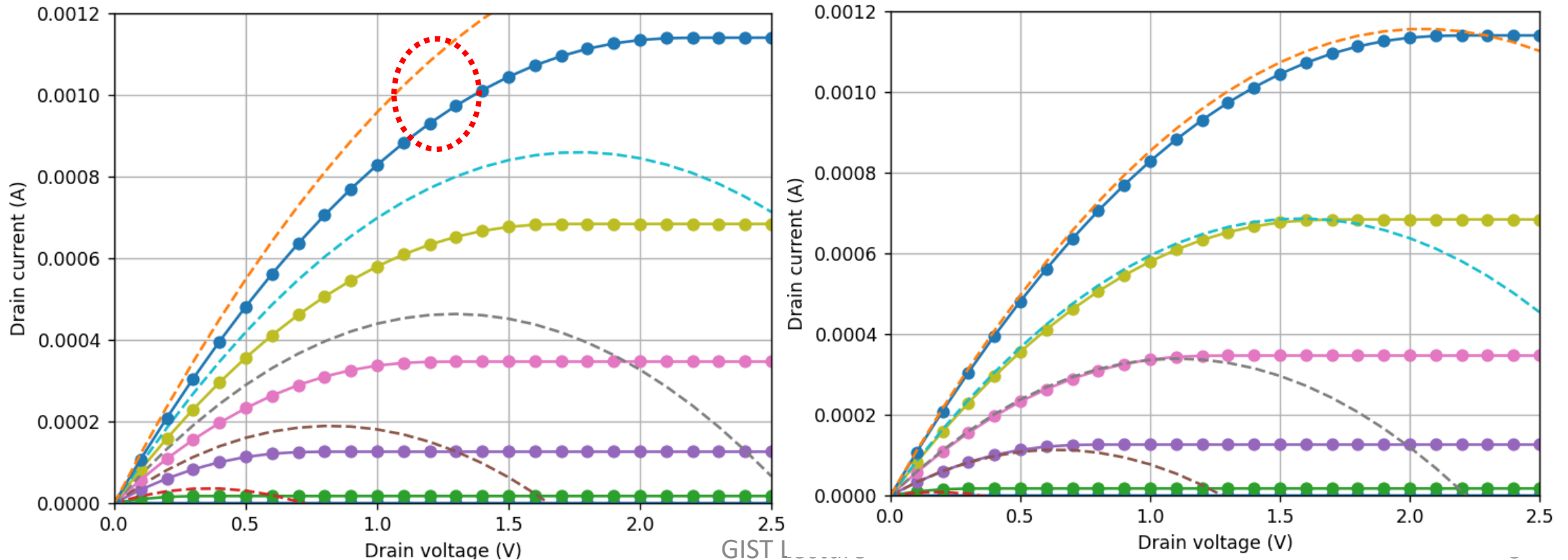
# In our previous example,

- The threshold voltage is about 0.11 V.
  - In reality, a *linearly extrapolated threshold voltage* is slightly higher than the “ $2\phi_B$ ”  $V_t$ .



# Comparison

- Output characteristics by Taur, Eq. (3.22) & Taur, Eq. (3.23)
  - Difference in  $V_t$  ( $\sim 0.2$  V)



# Parabolic region

- We must keep up to the second order.

$$\begin{aligned} I_d &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} \left( V_{gs} - V_{fb} - 2\phi_B - \frac{1}{2} V_{ds} \right) V_{ds} \right. \\ &\quad \left. - \frac{2}{3} \sqrt{2\epsilon_{si} q N_a} \left[ \frac{3}{2} (2\phi_B)^{0.5} V_{ds} + \frac{3}{8} (2\phi_B)^{-0.5} V_{ds}^2 \right] \right\} \\ &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} \left( V_{gs} - V_t - \frac{1}{2} V_{ds} \right) V_{ds} - \frac{1}{4} \sqrt{2\epsilon_{si} q N_a} [(2\phi_B)^{-0.5} V_{ds}^2] \right\} \\ &= \mu_{eff} \frac{W}{L} \left\{ C_{ox} (V_{gs} - V_t) V_{ds} - \frac{1}{2} C_{ox} \left[ 1 + \frac{\sqrt{\epsilon_{si} q N_a / (4\phi_B)}}{C_{ox}} \right] V_{ds}^2 \right\} \end{aligned}$$

Taur, Eq. (3.25)

# Let's introduce a factor, $m$ .

- It is given as

$$m = 1 + \frac{\sqrt{\epsilon_{si} q N_a / (4 \phi_B)}}{C_{ox}} \quad \text{Taur, Eq. (3.26)}$$

- From the maximum depletion width,

$$W_{dm} = \sqrt{\frac{4 \epsilon_{si} \phi_B}{q N_a}} \quad \text{Taur, Eq. (2.190)}$$

- An alternative form is available,

$$m = 1 + \frac{C_{dm}}{C_{ox}} = 1 + \frac{3 t_{ox}}{W_{dm}} \quad \text{Taur, Eq. (3.27)}$$

- In our previous example? It was about 1.1. (Due to a low  $N_a$ )

# Its physical meaning

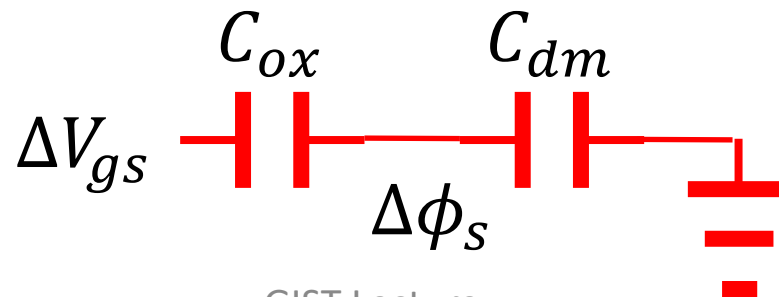
- Serial capacitors give  $\frac{C_{ox}C_{dm}}{C_{ox}+C_{dm}}$ .
  - Charge across the oxide capacitor:

$$\frac{C_{ox}C_{dm}}{C_{ox} + C_{dm}} \Delta V_{gs} = C_{dm} \Delta \phi_s$$

- Therefore,

$$m = \frac{C_{ox} + C_{dm}}{C_{ox}} = \frac{\Delta V_{gs}}{\Delta \phi_s}$$

- $m$  should be kept close to one.





# Saturation current

- Maximum value of  $I_d$  at a given  $V_{gs}$

– Recall that

$$I_d = \mu_{eff} \frac{W}{L} \left\{ C_{ox} (V_{gs} - V_t) V_{ds} - \frac{m}{2} C_{ox} V_{ds}^2 \right\} \quad \text{Taur, Eq. (3.25)}$$

– When  $V_{ds} = V_{dsat} = \frac{V_{gs} - V_t}{m}$ ,

$$I_d = I_{dsat} = \mu_{eff} C_{ox} \frac{W}{L} \frac{(V_{gs} - V_t)^2}{2m} \quad \text{Taur, Eq. (3.28)}$$

# Pinch-off

- For  $\phi_s = 2\phi_B + V$ , the Tylor expansion gives

$$Q_i = -C_{ox}(V_{gs} - V_{fb} - 2\phi_B - V) + \sqrt{4\epsilon_{si}qN_a\phi_B} + \sqrt{\frac{\epsilon_{si}qN_a}{4\phi_B}}V$$
$$Q_i = -C_{ox}\left(V_{gs} - V_t - V - \frac{1}{C_{ox}}\sqrt{\frac{\epsilon_{si}qN_a}{4\phi_B}}V\right) = C_{ox}(V_{gs} - V_t - mV)$$

Taur, Eq. (3.29)

- At  $V_{ds} = \frac{V_{gs}-V_t}{m}$  (on-set of saturation), the surface channel vanishes at the drain end of the channel.


# Subthreshold current (1)

- Subthreshold region where  $V_{gs} < V_t$

– Recall that

$$-Q_s = \sqrt{2\epsilon_{si}k_B T N_a} \left[ \frac{q\phi_s}{k_B T} + \frac{n_i^2}{N_a^2} \exp\left(\frac{q}{k_B T}(\phi_s - V)\right) \right]^{1/2}$$

Taur, Eq. (3.35)



Small in the subthreshold region

– Its Taylor expansion

$$-Q_s \approx \sqrt{2\epsilon_{si}k_B T N_a} \left[ \sqrt{\frac{q\phi_s}{k_B T}} + \frac{1}{2} \sqrt{\frac{k_B T}{q\phi_s}} \frac{n_i^2}{N_a^2} \exp\left(\frac{q}{k_B T}(\phi_s - V)\right) \right]$$

# Subthreshold current (2)

- The second term for the inversion charge

$$-Q_i \approx \sqrt{\frac{\epsilon_{si} q N_a}{2 \phi_s}} \frac{k_B T}{q} \frac{n_i^2}{N_a^2} \exp\left(\frac{q}{k_B T} (\phi_s - V)\right) \quad \text{Taur, Eq. (3.36)}$$

- In this case,  $\phi_s$  is a function of  $V_{gs}$  only.
- Recall

$$I_d = \mu_{eff} \frac{W}{L} \int_0^{V_{ds}} [-Q_i(V)] dV \quad \text{Taur, Eq. (3.10)}$$

- Then, we have

$$I_d = \mu_{eff} \frac{W}{L} \sqrt{\frac{\epsilon_{si} q N_a}{4 \phi_B}} \left(\frac{k_B T}{q}\right)^2 \left(\frac{n_i}{N_a}\right)^2 \exp\left(\frac{q \phi_s}{k_B T}\right) \left(1 - \exp\left(-\frac{q V_{ds}}{k_B T}\right)\right) \quad \text{Taur, Eq. (3.37)}$$

# Subthreshold current (3)

- Since  $m = \frac{\Delta V_{gs}}{\Delta \phi_s}$ ,  $V_{gs} - V_t = m(\phi_s - 2\phi_B)$ .

– Then,

$$\exp\left(\frac{q\phi_s}{k_B T}\right) = \exp\left(\frac{q(V_{gs} - V_t)}{mk_B T}\right) \exp\left(2\frac{q\phi_B}{k_B T}\right)$$

– From the above expression,

$$I_d = \mu_{eff} \frac{W}{L} \sqrt{\frac{\epsilon_{si} q N_a}{4\phi_B}} \left(\frac{k_B T}{q}\right)^2 \exp\left(\frac{q(V_{gs} - V_t)}{mk_B T}\right) \left(1 - \exp\left(-\frac{qV_{ds}}{k_B T}\right)\right)$$

Taur, Eq. (3.39)

# Subthreshold slope (1)

- $I_d$  is independent of  $V_{ds}$ , when  $V_{ds} \gg k_B T / q$ .


$$I_d = \mu_{eff} \frac{W}{L} \sqrt{\frac{\epsilon_{si} q N_a}{2\phi_s}} \left( \frac{k_B T}{q} \right)^2 \exp \left( \frac{q(V_{gs} - V_t)}{mk_B T} \right)$$

– Its gate voltage dependence is very important.

$$\log_{10} I_d = (a \text{ constant}) + \frac{q(V_{gs} - V_t)}{mk_B T} \log_{10} e$$

$$\frac{d(\log_{10} I_d)}{dV_{gs}} = \frac{q}{mk_B T} \log_{10} e$$

Subthreshold  
slope

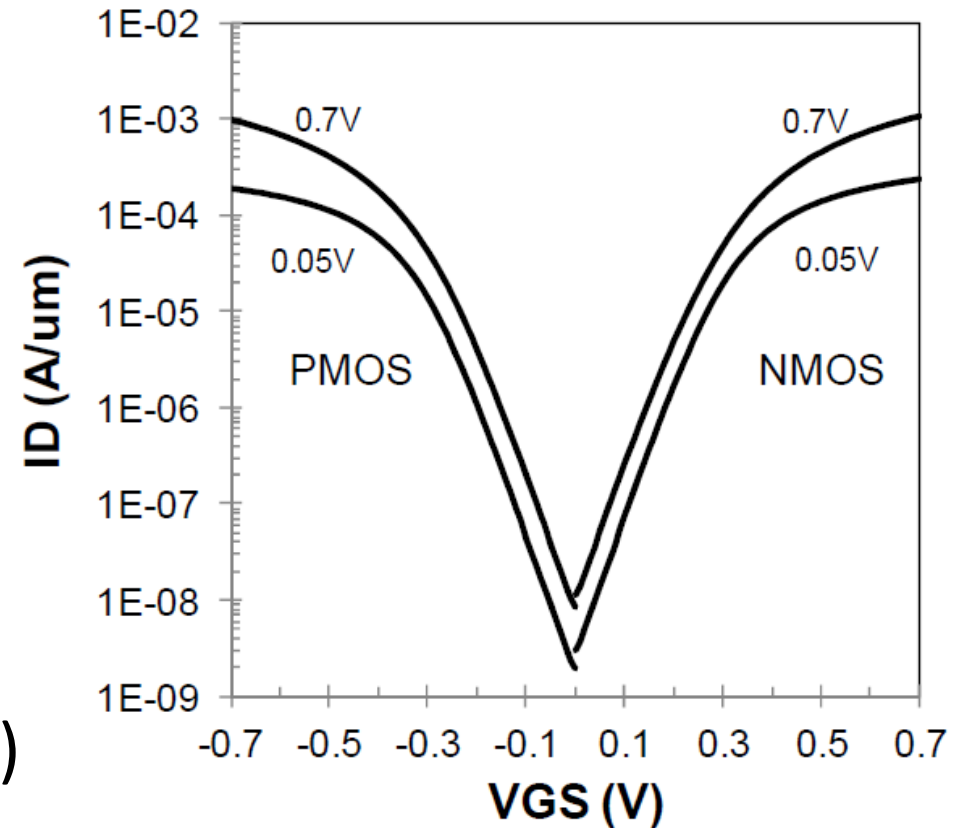

$$S = \left( \frac{d(\log_{10} I_d)}{dV_{gs}} \right)^{-1} = \frac{mk_B T}{q} \ln 10$$

Taur, Eq. (3.41)

# Subthreshold slope (2)

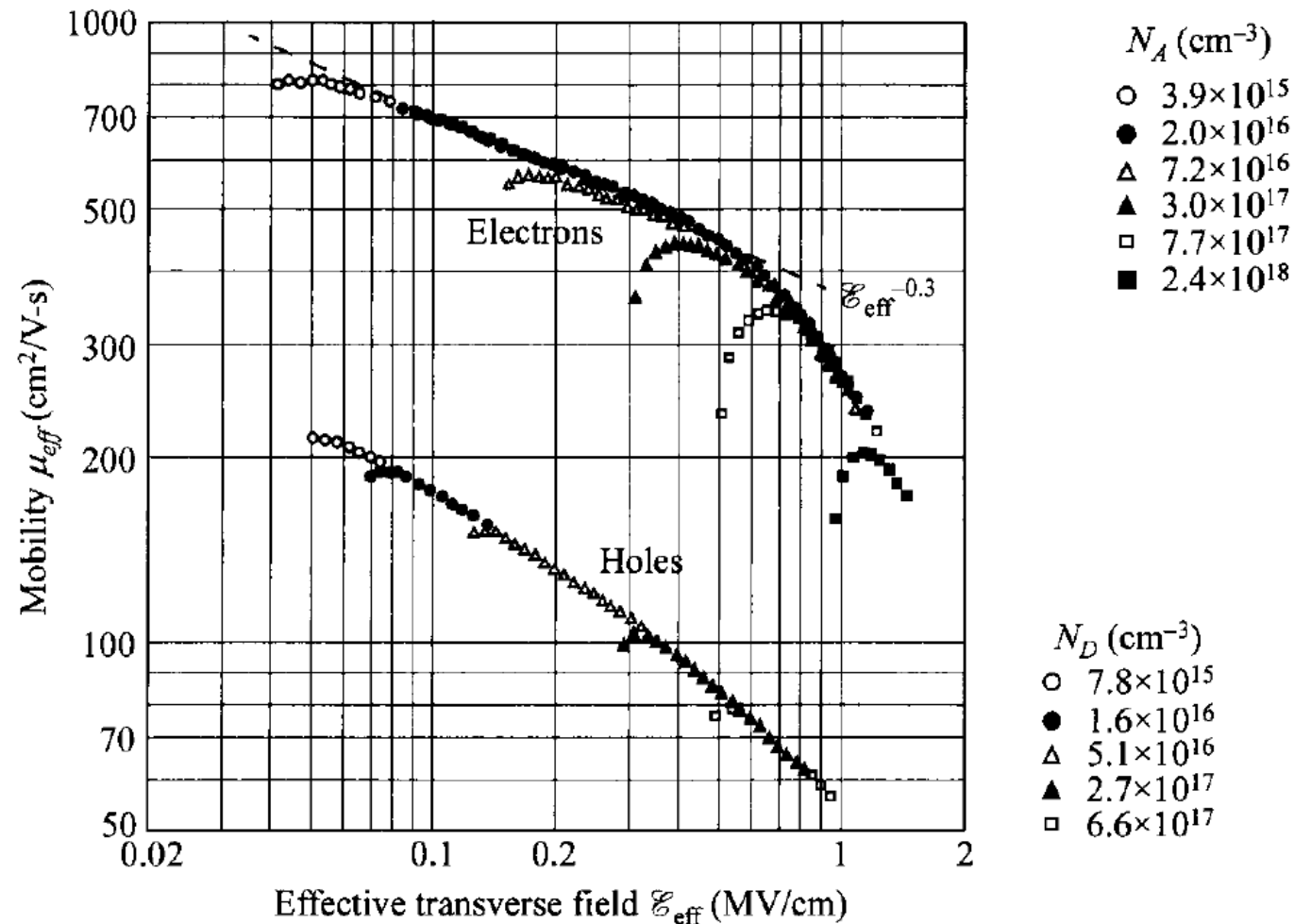
- At 300 K,  $\frac{k_B T}{q} \ln 10$  is 60 mV/dec.
  - Note that  $m$  is larger than 1.

Subthreshold behavior  
(Natarajan, IEDM 2024)



# Mobility variation

- Mobility variation (Vertical field dependence)

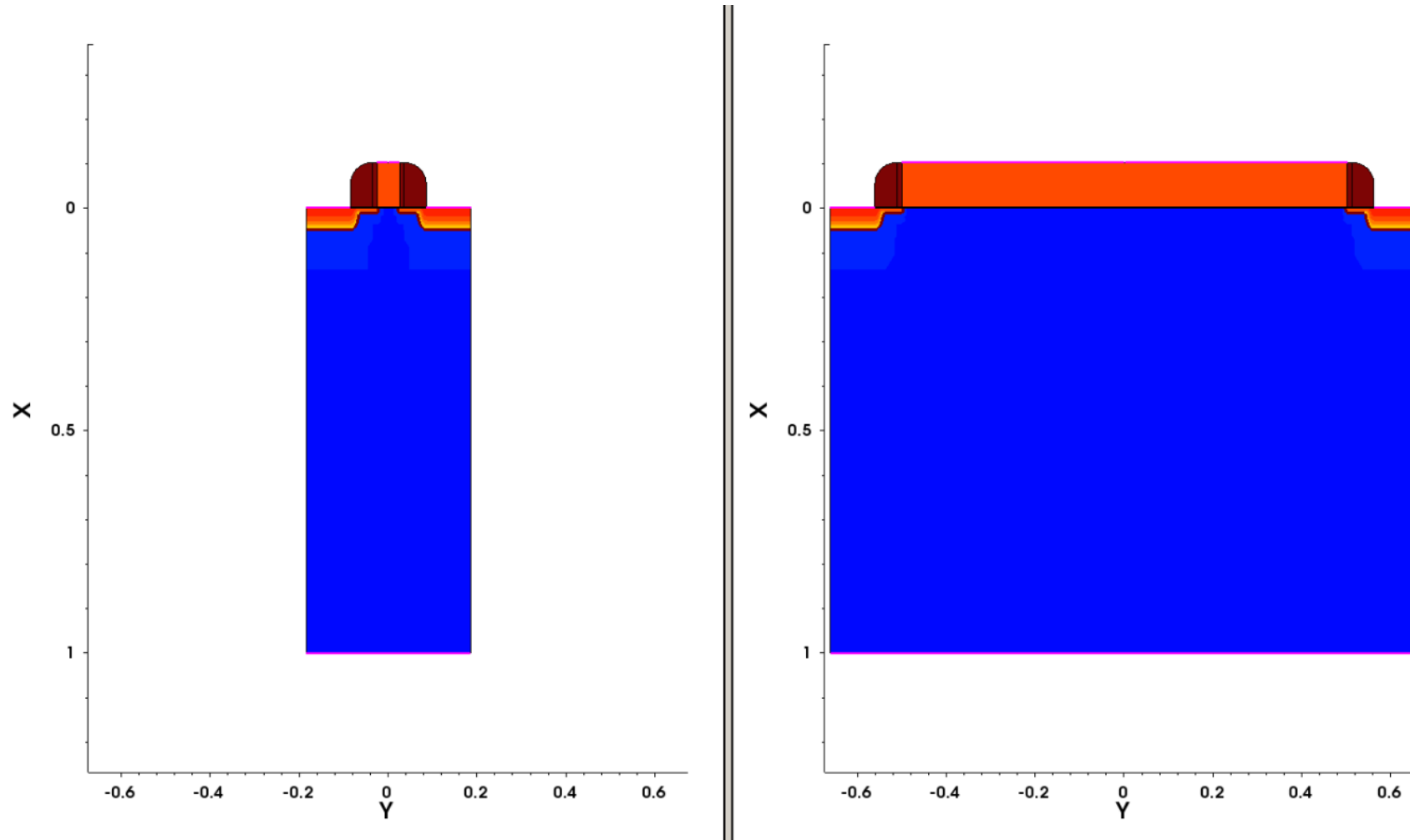


Inversion-layer  
mobility  
(Sze's book)



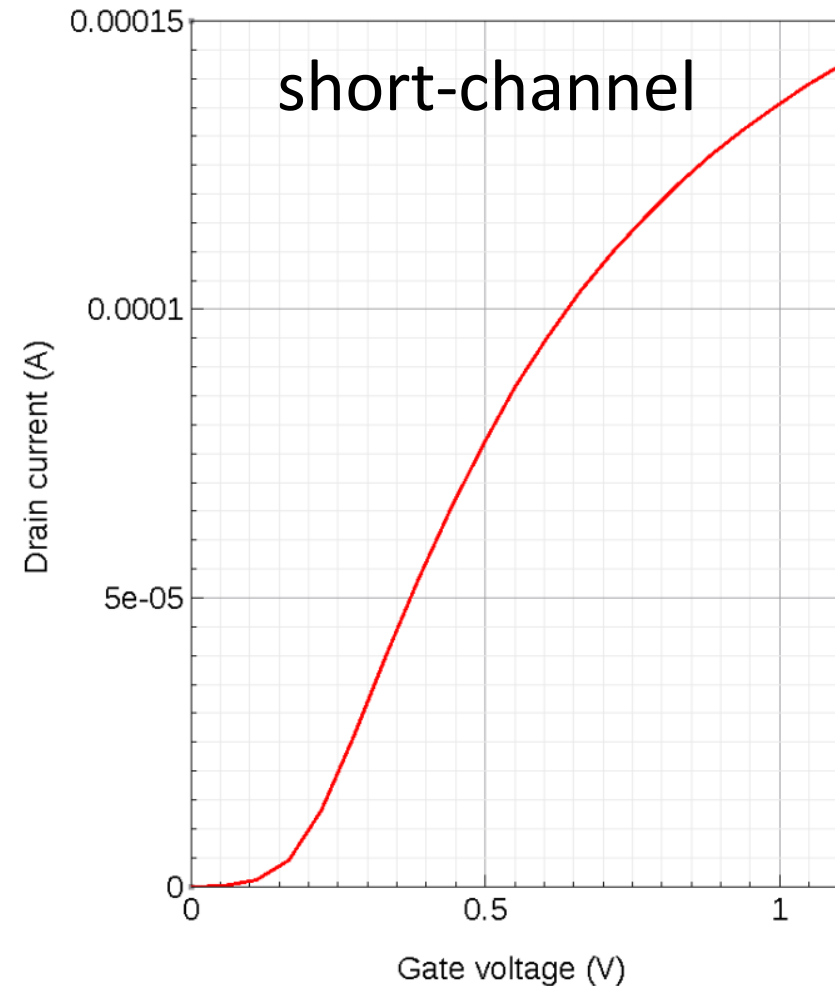
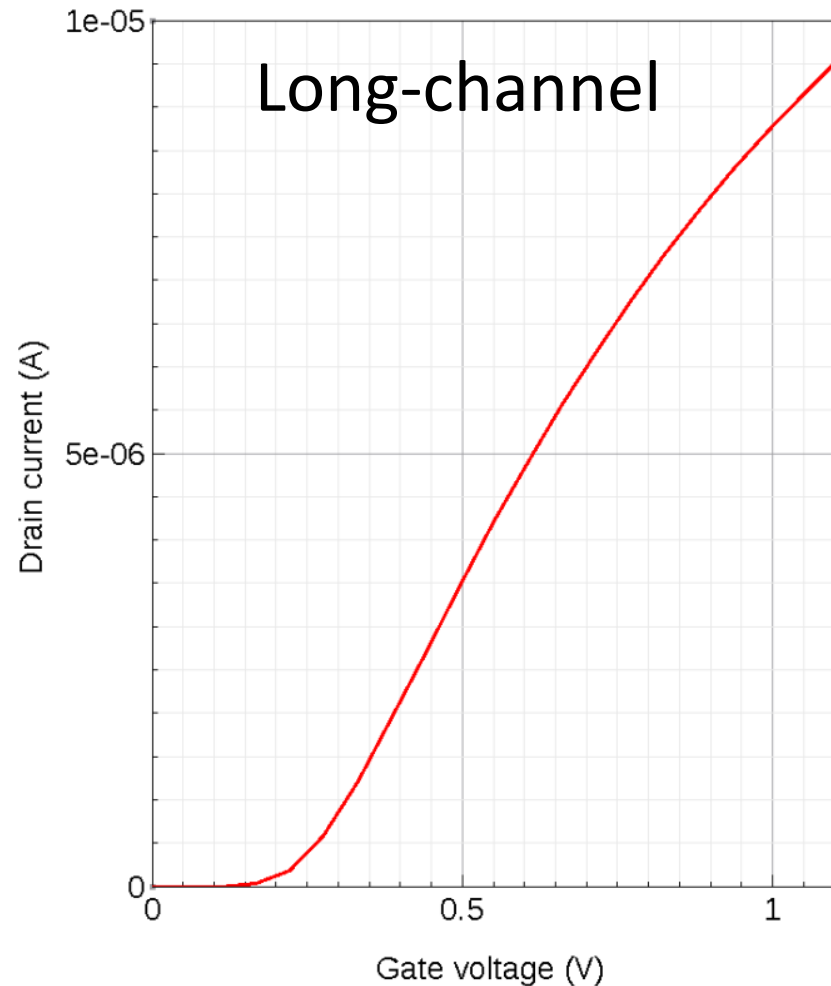
# TCAD simulation of a short-channel MOSFET

- Channel length, 50 nm



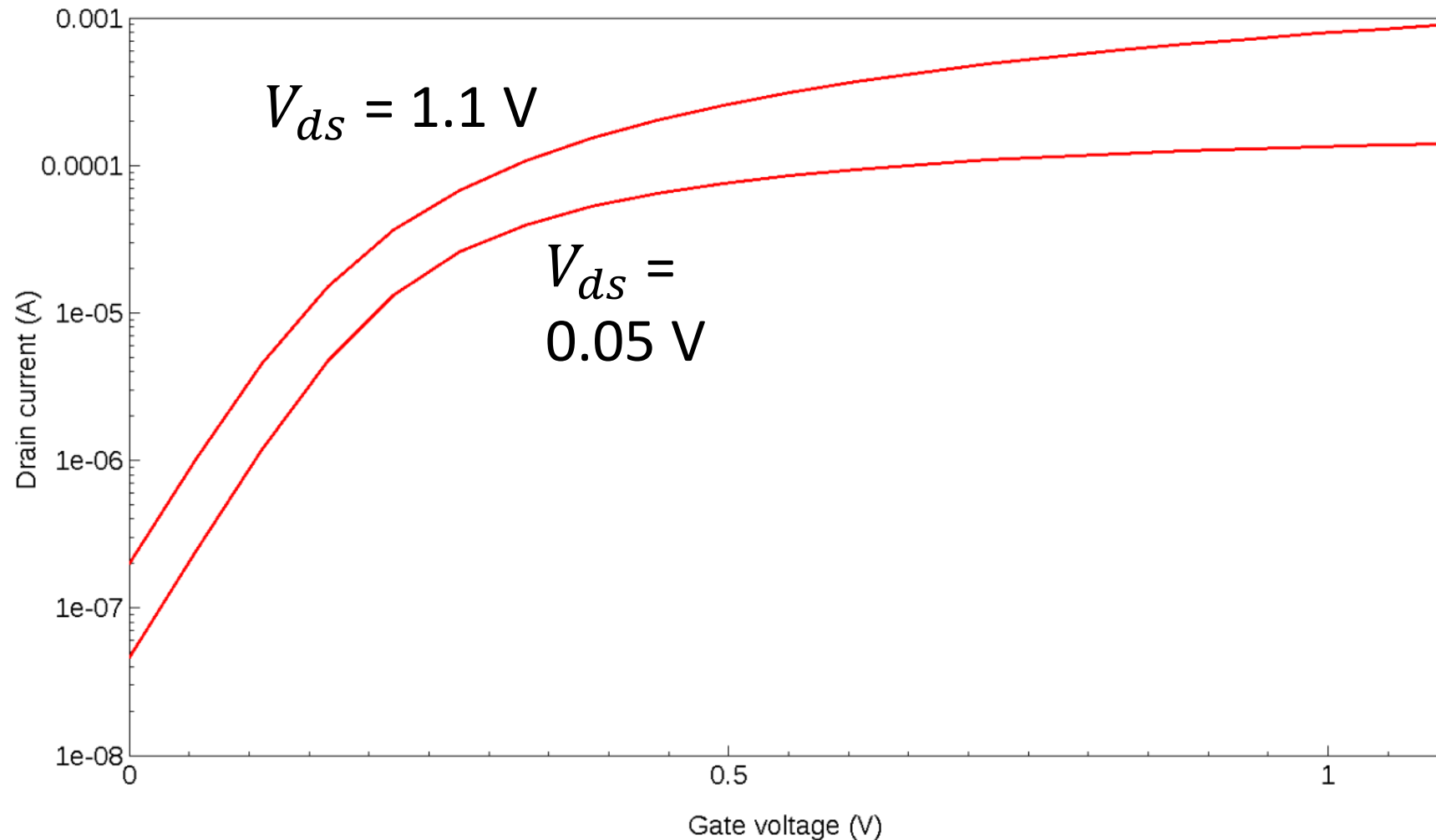
# Charge-sharing

- Compare two transistors at  $V_{ds} = 0.05$  V.



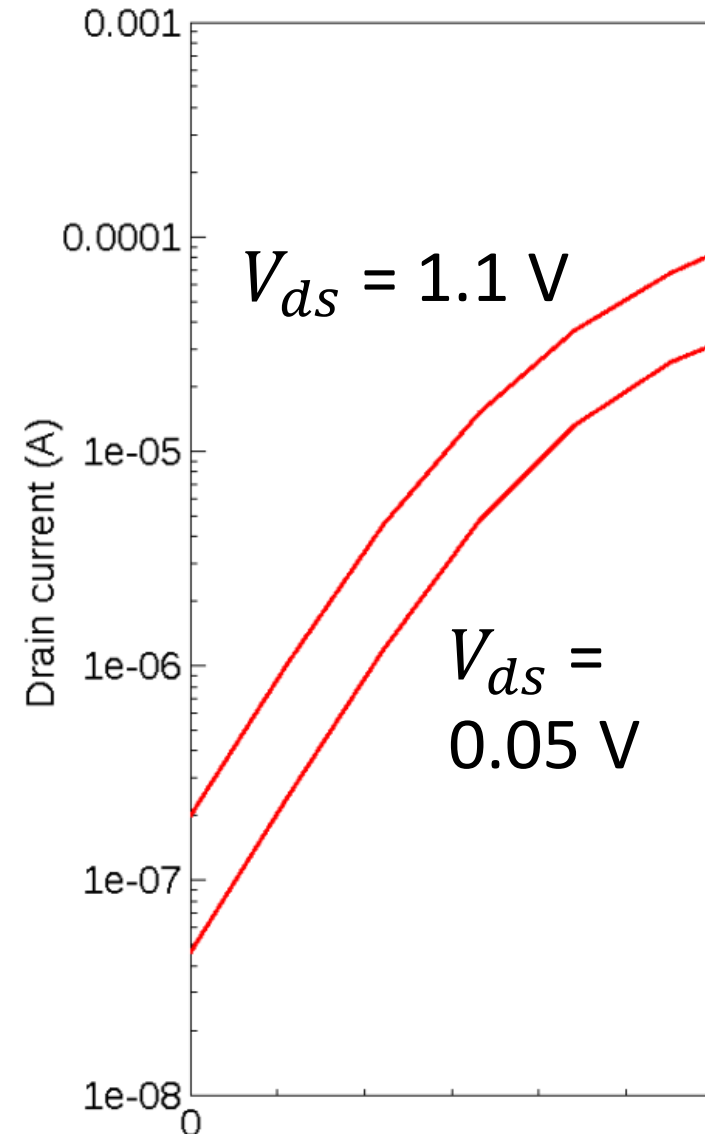
# $I_d$ versus $V_{gs}$

- Input characteristics



# DIBL (Drain-Induced Barrier Lowering)

- Difference between two curves
  - Significant increase of  $I_d$  at a high  $V_{ds}$
  - Better gate control over the channel
  - We need more(!) gates.



# Thank you!